## Pressure Gain Combustion for Land Based Power Generation

Providing Clean Energy Technology Through Innovative Ideas

NETL – Research & Innovation Center (R&IC) and Advanced Energy Systems Program (AES)

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UTSR2018



## Outline

#### NATIONAL ENERGY TECHNOLOGY LABORATORY

#### Background

- DOE Pressure Gain Combustion
- RDE focused objectives

#### • NETL in-house research

- Experimental facilities
- A few results
- Looking Forward

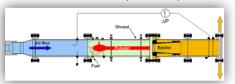




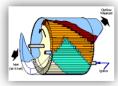
## **Current Technology Trends in PGC**

	Pulse Combustion	Wave Rotor Engine	Pulse Detonation Engine	Rotating Detonation Engine
System Analysis	- Lower pressure gain potential - Eliminates complexities of detonation waves	Large tube numbers reduce provide nearly steady flow	- Detonation offers greatest PG potential - 10% improvement in thermal efficiency	Benefits of PDE with near steady flow and hot gas ignition.
System Integration	-Few/no moving parts -Impact of ejector on unsteady flow?	- Availability as a topping cycle - Complex flow path - Start-up issues	-Cycle timing dictates hardware. -Turbine interactions need quantified -Cooling air challenges	- Small package with big impact - Start-up and wave travel issues
Components / Materials	Heat transfer/cooling concerns	- Sealing issues - Bearings	-Injectors - Thermal management -Turbomachinery	-Thermal Management -Turbomachinery
Basic Physics and Chemistry	Basic physics are understood although difficult to predict amplitudes of pulses	Basic physics of detonation or fast deflagration	- DDT challenges - Ionized flow behind shock	- Similar to physics of PDE - Complex flow field

Resonant Pulse Combustor (NASA-Glenn)



Wave Rotor Engine (IUPUI)



Multi-Tube PDE G.E. Global Research Center 2005



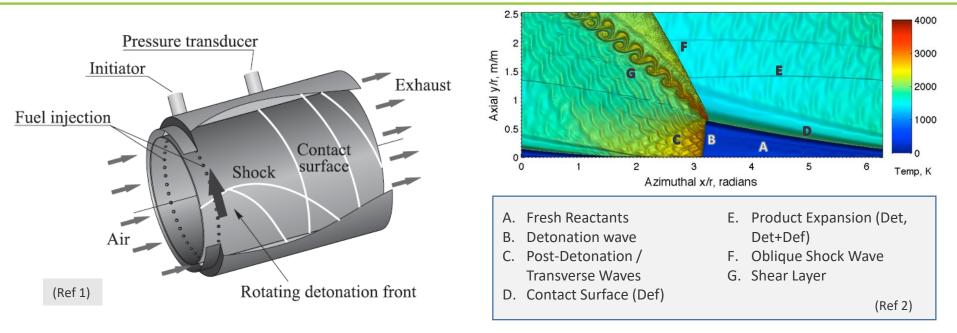
RDE Simulation NETL - 2016





## **Rotating Detonation Engines** Application and Advantages





- Fuel and air has a bulk axial flow with detonation wave traveling circumferentially, producing a "continuous wave"
- No moving parts No complex valving required at the inlet compared to PDE's
- Detonation wave, once initiated, is self-sustained.
- Unsteady periodic flow at high frequency may have minimal impact on turbine performance.
- Potential for low NOx

- 1. Wolanski, P., Proc. Comb. Institute, 2013
- 2. Nordeen et al, 49th AIAA Aerospace Sciences Meeting, Orlando, FL:, 2011.



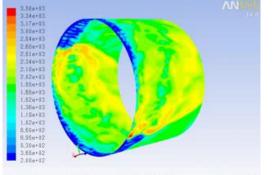
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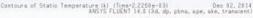
## DOE Pressure Gain Combustion Objectives

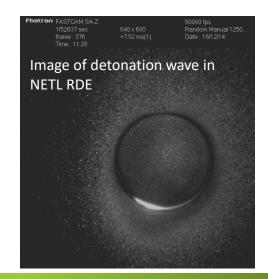
- Improve fundamental understanding of stable continuous wave detonation in a semi-enclosed channel
  - Wave directionality, bifurcation, translation speed (~CJ)
  - Det wave influence on operational parameters (i.e fuel injection/mixing)
- Develop scaling laws to better understand the parametric impacts
  - Flow, pressure temperature, fuel composition (det cell size)
  - Gap width, combustor length, diameter (number of waves)
- Maximize pressure gain / turbine work availability and reduce emissions
  - Inlet / exhaust transition configuration (including valves for PDE's)
  - Deflagration, shear layer and downstream shocks
  - CO, NOx exhaust emissions and emissions formation
- Improve modeling capabilities

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- Simultaneous detonation and deflagration
- Grid dependences, chemical kinectics
- Reduced order thermo and chemical models











## **NETL In-House Research Activities**

### • RDE Sector / Inlet Lab-Scale Test Rig

• Rapid evaluation of inlet concepts with correlation to labscale combustor.

Second

2.84e+03 2.88e+03 2.51e+03 2.34e+03

2.18e+03 2.02e+03 1.85e+03 1.88e+03

1.35e+03 1.19e+03

8.60e+02 8.95e+02 5.30e+02

65e+02

#### Computational Studies

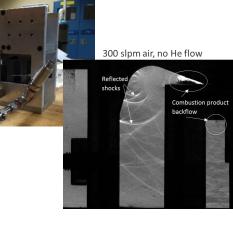
- Chemical Reactor Network (CRN)
  - Reduced order model with emissions
- CFD
  - Fundamental aspects of detonation
  - Inlet / geometry physics
  - Turbine integration

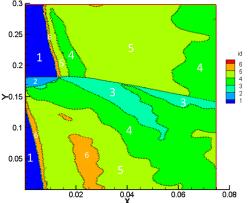
#### • Lab-Scale Full RDE Experiment

- Approximate gas turbine conditions
  - Pressure and temperature
- Increased percentage of NG (H2/Air)
- Model validation



Contours of Static Temperature (k) (Time+2.2258=03) Dec 02, : ANSYS FLUENT 14.0 13d, do, obns, spe, ske, transi



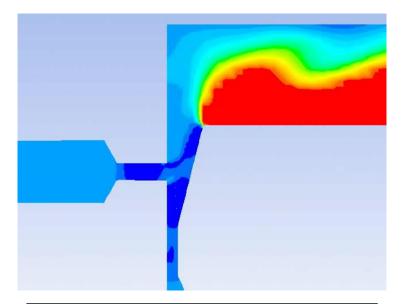




# **Understanding RDE Inlet Dynamics**



- Inlet design, reactant mixing critical to realizing PGC potential
- Mixing in an RDE is not a static process
- Injector/inlet response dictates instantaneous mixture composition
  - In particular: unequal response between fuel/air, product recirculation can result in significant deflagrative burning, unburnt fuel exiting combustor<sup>9</sup>



Understanding injector dynamic response is important to developing improved designs, achieving desired reactant mixedness

<sup>9</sup> Strakey, P., Ferguson, D., Sisler, A., Nix, A, "Computationally Quantifying Loss Mechanisms in a Rotating Detonation Engine", 54<sup>th</sup> AIAA Aerospace Sciences Meeting, San Diego, CA, 2016.



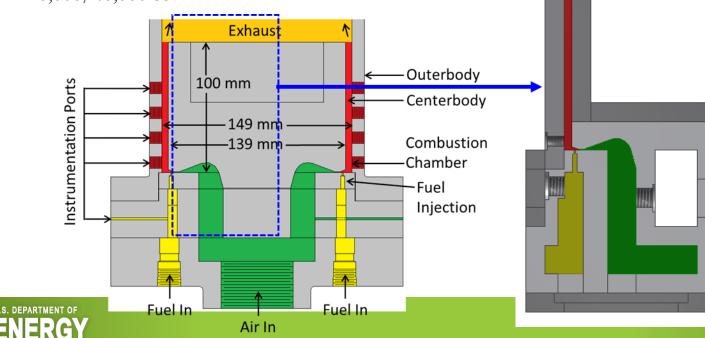


## **NETL Lab-Scale RDE Inlet Sector Rig**

#### • Small Pilot-scale 6 in diameter RDE presently operated

- Combustion annulus width 0.02 in
- Continuous air slot between fuel plate and centerbody (gap size 0.022 in)
- 80 discrete fuel injectors (ID 0.035 in)
- Nominal H<sub>2</sub>/air flow rates of 10,000/40,000 scfh

• Linear extrusion of full-scale RDE cross-section creates a representative geometry for investigating inlet designs, while simplifying diagnostics



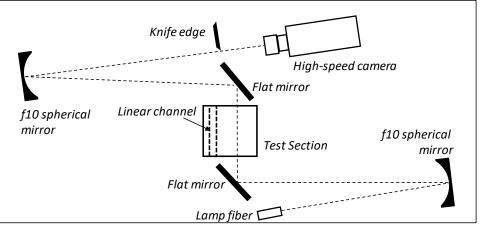


## **NETL Lab-Scale RDE Inlet Sector Rig**

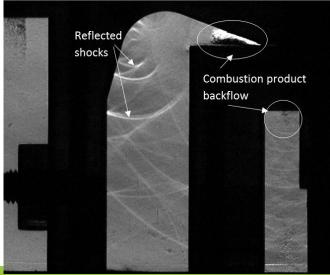
- RDE "slice" extruded 7.5cm @ 1:1 scale (full RDE with 47cm circumference)
- Semi-cold flow approach:
  - Discrete pressure pulses introduced to linear channel ("combustion annulus") via separate H<sub>2</sub>/air pre-detonator tube
  - Inert gases within inlet paths (He/air)

#### • Instrumentation:

- Optical access provided within inlet plenums on opposing sides for schlieren imaging
- Dynamic pressure measurements within linear channel and inlet plenums
- Static He/air supply pressures for inlet  $\Delta P$



#### 300 slpm air, no He flow

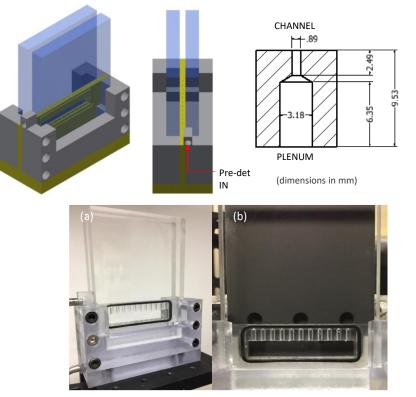




# RDE Injector Response using Acetone PLIF

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- Prior work<sup>3</sup> examined inlet response in a reduced-scale linear testing platform
- Provided qualitatively similar interruption/backflow to CFD
- Modified configuration developed to specifically investigate in-channel fuel injector response, facilitate future mixing experiments
  - 3D printed linear injector array
  - Geometry equivalent to NETL RDE
  - CDST to force interruption
  - Helium delivered to injectors
  - Amenable to schlieren and laser-based diagnostics, along with dynamic pressure measurements
- Current work presents results from highspeed acetone-PLIF experiment

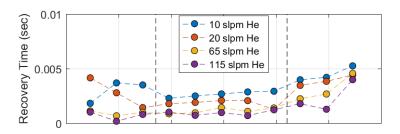


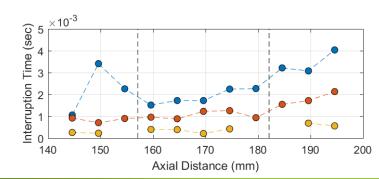
<sup>3</sup> Bedick, C., Sisler, A., Ferguson, D., Strakey, P., Nix, Andrew, Billips, D. "Development of a Lab-Scale Experimental Testing Platform for Rotating Detonation Engine Inlets", 55<sup>th</sup> AIAA Aerospace Sciences Meeting, Grapevine, TX, 2017.

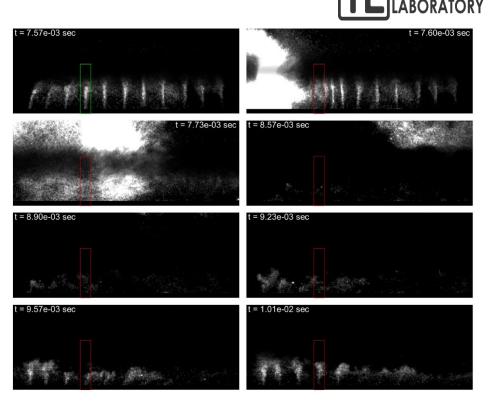


# **Dynamic Jet Analyses**

- PLIF image sequence analyzed to extract pertinent information
- Complete interruption easily observed
- Recovery occurs left-to-right
- Individual jet interruption and recovery tracked using sub-regions
- 2D correlation coefficients computed W.R.T. pre-shock reference frame







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- Run-average interruption and recovery times determined for each jet, at each condition
- Jets near channel ends inconsistent due to entrainment, possible sheet misalignment



# NETL Lab Scale RDE

#### • Rig design

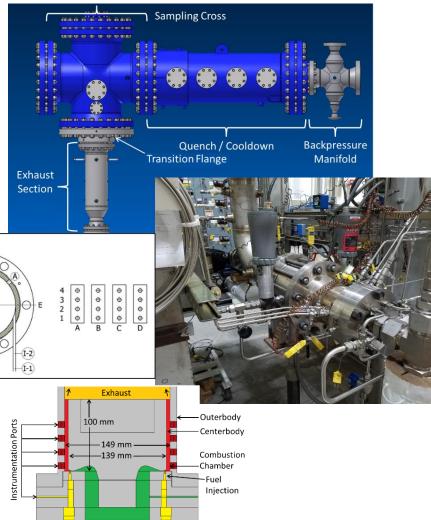
- AFRL 6 inch rig
- Enclosed flow with back pressure control valve
- Post combustor burners to control start-up flares

#### • Rig capability

- Natural gas, hydrogen, propane, ethane (0.1 kg/sec)
- Air (1.2 kg/sec)
- 20 atm, 800 K air preheat

#### • Experimental focus

- Flow rate
- Equivalence ratio
- Fuel Composition (H2 / NG)
- Air Preheat (600 K)
- Operating Pressure





Fuel In

Fuel In

Air In

N

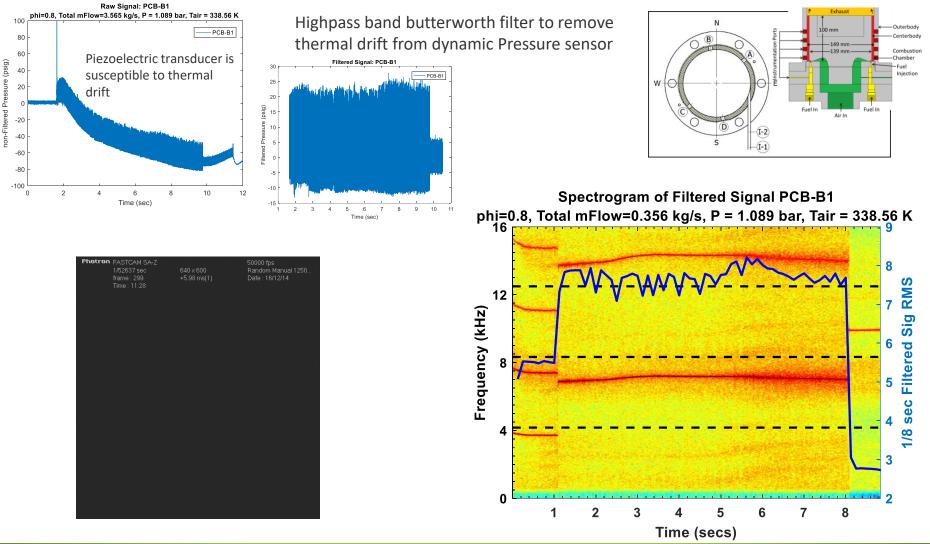
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# Example Data Analysis - H2 in Air

phi=0.8, Total mass flow ~ 0.356kg/sec P = 1.089 bar, Tair = 338 K



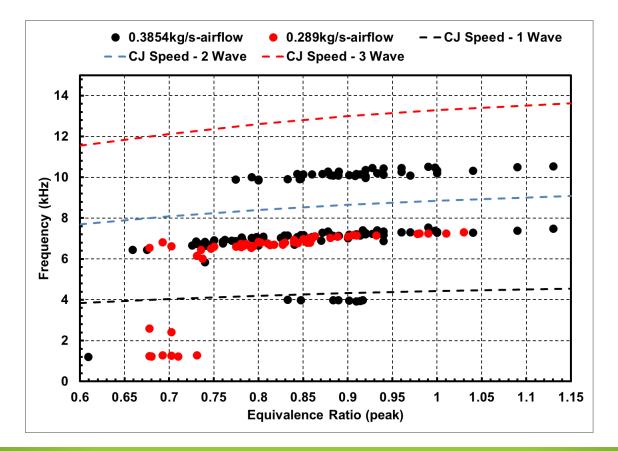


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## **Summary of Test Conditions**



Operating Conditions						
Air Flow Rates (kg/s)	Eq. Ratio	Preheat (°C)	Back Pressure (bar A)			
0.289	0.6 - 1.1	65/204	1.06			
0.3854	0.6 - 1.1	65/204	1.06 - 3.068			

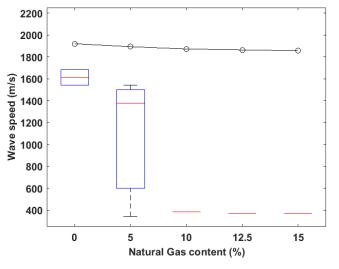




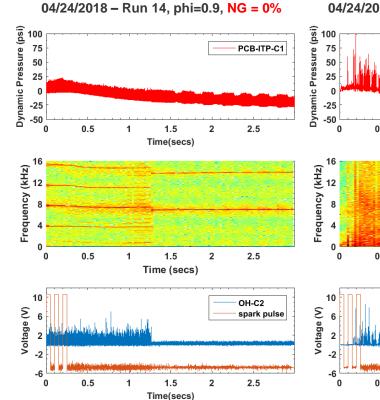
## Effect of Natural gas addition – 0.3in annulus



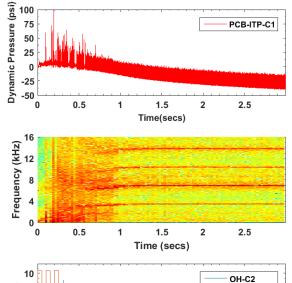
#### RDE performance at Tair – 150F, P – 1atm, phi = 0.9, total flow rate ~ 60,000scfh

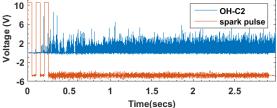


- Successful detonation achieved only at 5% NG at 1 atm op press.
- Initially unstable, may cause intermittent blow-off, but transitions to stable detonation
- Detonation achieved only with larger annulus (0.2 in vs 0.3 in)



#### 04/24/2018 – Run 21, phi=0.9, NG = 5%

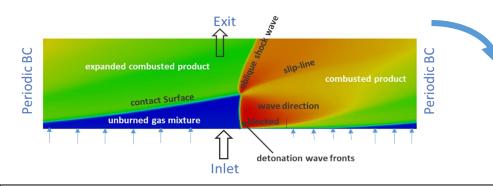




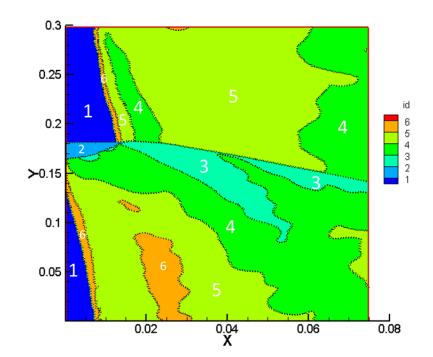


# Chemical Reacting Network for RDE application





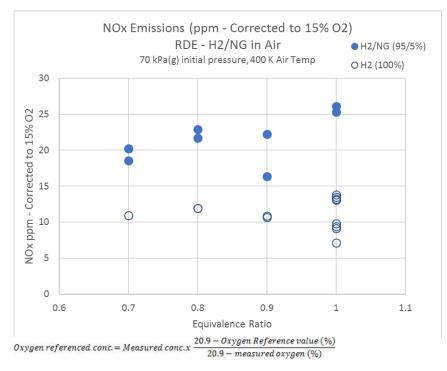
- CRN simplify the domain of combustor in "zones" that has similar conditions
- CFD with simplified global chemistry mechanism is solved From CFD data –
  - Reactors domain identified with their boundary , volume of each reactors
  - Mass flux between the reactors calculated
  - Reactor averaged T, P, density, species concentrations, velocity calculated
- In Cantera :
  - Reactor averaged properties supplied as input
  - Using detailed chemistry concentration of NOx is predicted





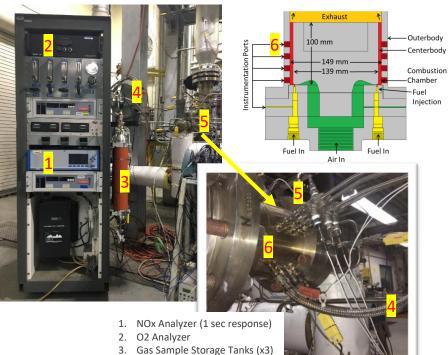
## NOx Emissions (ppm) – Corrected to 15% O2





#### Challenges

- 1. Unheated sample line permitted condensation (H2/Air) likely resulting in NO2 loss.
- 2. Some tests experiences periods of unstable and stable detonation.
- 3. Incomplete combustion (see O2 Emissions chart)

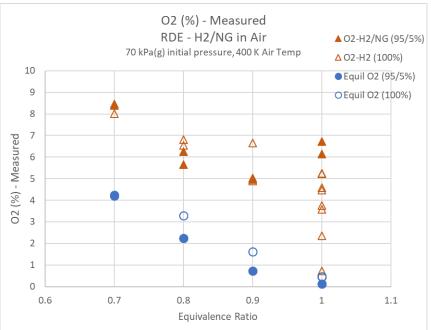


- 4. Gas sample line
- 5. RDE
- 6. Gas sample port



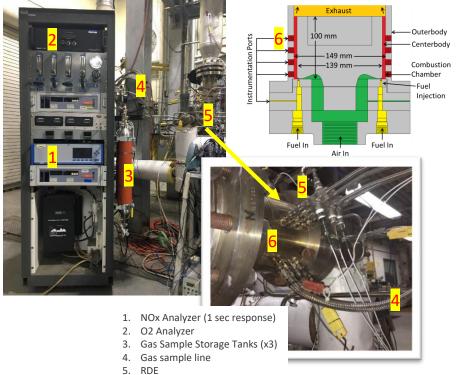
## O2 Emissions (%) – Incomplete Combustion





#### Challenges

- 1. High variability at phi = 1.0
- 2. High concentration of O2 at phi = 1.0 suggests incomplete combustion.



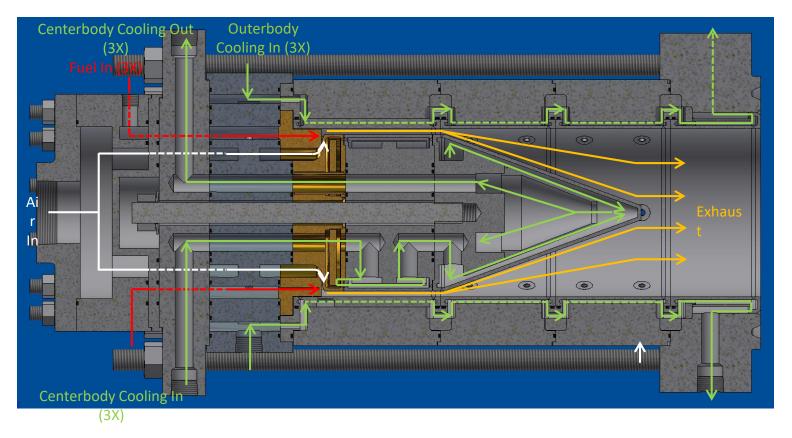
6. Gas sample port



## Installation of Cooled RDE in HPC Test Facility



Combustor Assembly – Flow Paths

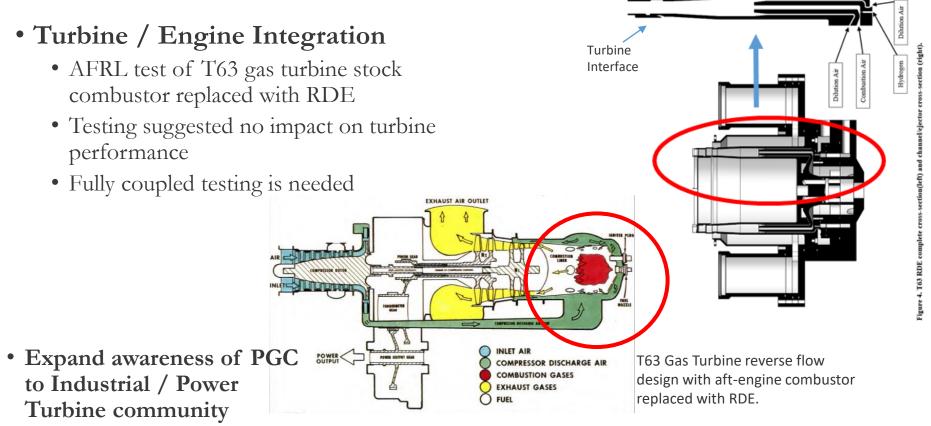


Short duration vs long duration tests (ignition and detonation wave stability, non-start)



## Maximize Pressure Gain / Turbine Work Availability





- Panel session at Turbo Expo 2018
- Technical session at Turbo Expo 2019

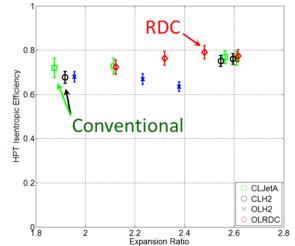
Naples et al., "Rotating Detonation Engine Implementation into an Open-Loop T63 Gas Turbine Engine", AIAA SciTech 2017



# **AFRL-DOE RDE T63 Turbine testing**



- Compare the adiabatic efficiency of a turbine driven with a conventional combustor and RDC
  - No intention of pressure gain
  - Average efficiency, not time varying
  - No study of long term structural effects on turbine
- RDC unsteadiness attenuated 65-85% in HPT
- No reduction in HPT efficiency measured with RDC setup



Andrew Naples, Ryan T. Battelle, John Hoke and Frederick R. Schauer. "T63 Turbine Response to Rotating Detonation Combustor Exhaust Flow", GT2018-75534, 2018 ASME Turbo Expo, Oslo, Norway, 11-15 June 2018.



#### RDE coupled to T63 Turbine at AFRL

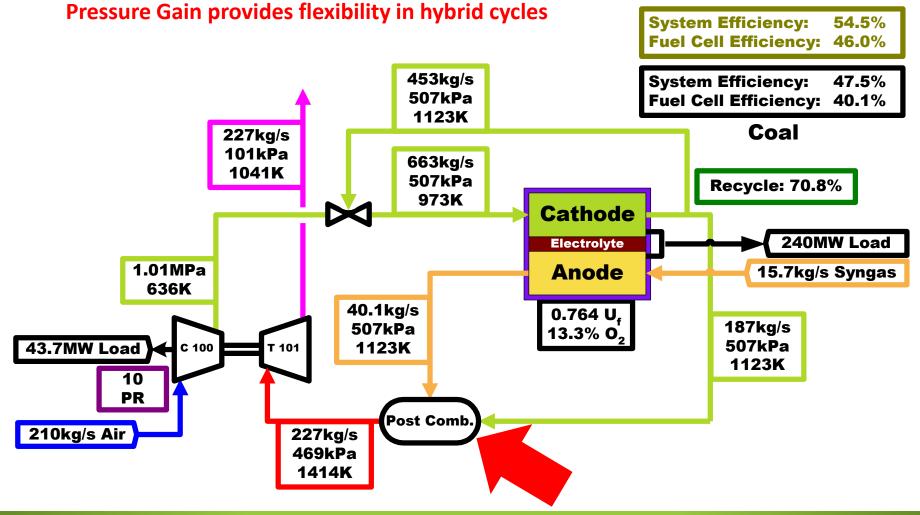
Andrew Naples, John Hoke, Ryan T. Battelle, Matthew Wagner, and Frederick R. Schauer. "RDE Implementation into an Open-Loop T63 Gas Turbine Engine", 55th AIAA Aerospace Sciences Meeting, AIAA SciTech Forum, (AIAA 2017-1747)



## **Cathode Recycle Configuration with Ejector**



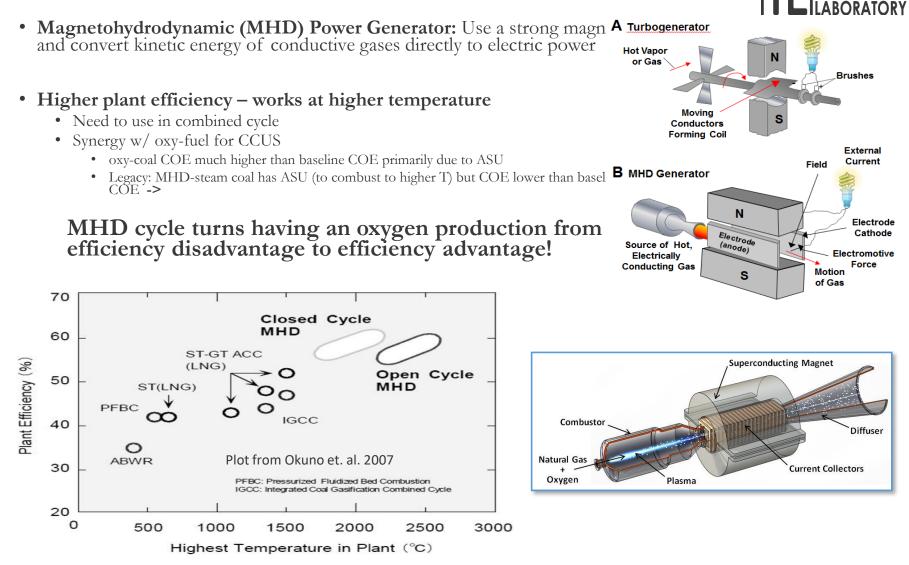
#### **Syngas**





# Making Oxy-fuel an Advantage

Direct Power Extraction (via MHD)









- In-house research effort are complementary to DOE externally funded activities
- In-house work focused on fundamental, computational and lab-scale studies.
- Low NOx appears to be consistent with preliminary modeling and expectations
- Alternative cycle considerations
- Two post-doc / post-grad positions available (Jan 2019 and Jul 2019)
  - https://orise.orau.gov/



# **Acknowedgements**



- This research is funded by the US Department of Energy Office of Fossil Energy through Advanced Combustion and Advanced Turbine Systems.
- Project Funding (DOE NETL)
  - Richard Dennis Advanced Turbine Program
  - John Rockey Advanced Combustion Program





## **Questions?**

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