# Flow of a Cement Slurry Modeled as a Generalized Second Grade Fluid

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### **MOTIVATION & OBJECTIVES**

#### Motivation

- Well cementing is the process of placing a cement slurry in the annulus space between the well casing and the surrounding for zonal isolation
- Rheological behavior of oil well cement slurries is significant in well cementing operation **Objectives**
- Study the impact of constitutive parameters on behavior of cement slurry
- Perform parametric study for various dimensionless numbers



## MATHEMATICAL MODEL

- In this paper, we assume that the cement slurry behaves as a non-Newtonian fluid.
- We use a constitutive relation for the viscous stress tensor which is based on a modified form of the second grade (Rivlin-Ericksen) fluid [2].
- Steady motion and unsteady motion are analyzed with one-dimensional flow.

#### Conservation of mass

$$\frac{\partial \rho}{\partial t} + div(\rho \boldsymbol{v}) = 0$$

 $T = T^T$ 

 $\rho$ : density of cement slurry, which is related to  $\rho_f$  (density of pure fluid);  $\boldsymbol{v}$ : velocity vector;  $\boldsymbol{\rho} = (1 - \boldsymbol{\phi}) \, \boldsymbol{\rho}_f$ ;  $\boldsymbol{\phi}$ : volume fraction Conservation of linear momentum

 $\rho \frac{d \boldsymbol{v}}{d t} = d i \boldsymbol{v} \boldsymbol{T} + \rho \boldsymbol{b}$ d/dt: total time derivative, given by  $\frac{d(.)}{dt} = \frac{\partial(.)}{\partial t} + [grad(.)]v$ *T*: stress tensor; *b*: body force vector

Conservation of angular momentum

Stress tensor of fluid [3]:

 $T_{v} = -pI + \mu_{eff}(\phi, A_{1})A_{1} + \alpha_{1}A_{2} + \alpha_{2}A_{1}^{2}$ p: pressure;  $\alpha_1$ ,  $\alpha_2$  are the normal stress coefficients;  $\mu_{eff}$  is the effective viscosity, which is dependent on volume fraction and shear rate [4]:

$$\mu_{eff}(\phi, A_1) = \mu_0 \left(1 - \frac{\phi}{\phi_m}\right)^{-\beta} \left[1 + \alpha \text{tr}A_1^2\right]$$

 $\phi_m$ : maximum solid concentration packing;  $A_n$ : n-th order Rivlin-Ericksen tensors,

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where  $A_1 = \nabla v + \nabla v^T$ ;  $A_2 = \frac{dA_1}{dt} + A_1 \nabla v + \nabla v^T A_1$ Convection-diffusion equation

 $\frac{\partial \varphi}{\partial t} + div(\phi v) = -\text{div}N$ *Particle flux* [5]: particles collisions; spatially varying viscosity; Brownian diffusive flux  $\mathbf{N} = -a^2 \phi K_c \nabla(\dot{\gamma}\phi) - a^2 \phi^2 \dot{\gamma} K_\mu \nabla(\ln\mu_{eff}) - D\nabla\phi$ where,  $D\nabla \phi = \eta \|A_1^2\| \cdot D_0 [K_1 + K_2(1-\phi)^2 + K_3(\phi_m - \phi)^2 H(\phi_m - \phi)]^2 \nabla \phi$  [6]





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