

### LOAD-Z

Low-NOx, Operable Ammonia Combustor Development for Zero-Carbon Power

### **RTX Technology Research Center**

University Turbine Systems Research (UTSR) & Advanced Turbines Program Review 2023 Meeting, State College, PA 30 Oct. – 1 Nov. 2023

Prime Contractor:RTX Technology Research Center (RTRC)Subcontractor:University of Connecticut (UConn)

### **LOAD-Z Project Team**

Organization	Role in project
RTX Technology Research Center (RTRC)	<ul> <li>Project lead (prime).</li> <li>Experiments in high-pressure staged combustion &amp; swirl-stabilized combustion of NH<sub>3</sub>.</li> <li>Modeling, design, &amp; testing of low-NOx gas turbine combustor for NH<sub>3</sub>.</li> </ul>
University of Connecticut (UConn)	<ul> <li>Fundamental NH<sub>3</sub> combustion experiments:         <ul> <li>counterflow (strained) laminar flames</li> <li>turbulent flame speed &amp; structure</li> </ul> </li> <li>Development of chemical kinetic models/mechanisms.</li> </ul>









Chih-Jen (Jackie) Sung (UConn lead) Flame structure, emissions, and chemical kinetic models



Baki Cetegen Turbulent combustion and diagnostics



James Stevens





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- Project Objectives & Partnership
- Counterflow Flame Studies Reaction Rates for NH<sub>3</sub> Combustion
  - Experiments at 1 6 atm pressure (UConn)
  - Kinetic modeling in 1-D flames w/ radiation (RTRC)
- Burner Studies NOx Emissions
  - Flat-flame burner experiments (30 atm pressure staged reactor rig)
  - Chemical Reactor Network (CRN) modeling of GT combustor
- Next Steps Year-2 plans
  - UConn experiments incl. new rig
  - RTRC high-pressure experiments & modeling





## LOAD-Z Project – Objectives & Partnership

### Low-NOx, Operable Ammonia Combustor Development for Zero-Carbon Power

UConn

- *End Goal:* Demonstrate performance of <u>gas-turbine-capable</u> NH<sub>3</sub>-fuel combustor, at single-nozzle scale.
- <u>Go Get</u>: Obtain fundamental <u>&</u> engineering  $NH_3$ -flame <u>data at gas-turbine-relevant conditions</u>  $\rightarrow P_{inlet}$ ,  $T_{inlet}$ .

#### **RTRC**



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## **Current Gaps for Understanding Ammonia Combustion**

#### **Combustion Challenges**

- Low overall reaction rate
  - Relatively low flame speed & extinction strain rates
- Flame stabilization & efficiency in highly turbulent flow (GT comb.)
- Quantifying NOx formation & emissions



**Decreasing Strain Rate** (Laminar Flame Speed Measurement)

**Increasing Strain Rate** (Extinction Limit Measurement)



### What is needed for improving ammonia models?

- Data at elevated pressure and temperatures relevant to gas turbines ٠
- Extinction strain rate measurements for **both** premixed and non-premixed counterflow flames ٠
  - Local velocity field measurements needed to determine *local* strain rate
  - Quantitative speciation (temperature) profiles (e.g., NO) at elevated pressures and temperatures
- Other data sets (shock tube, etc.) to better constrain reaction rate constant definitions ٠

#### What are highly sensitive reactions with large specific rate constant uncertainty?



### **UCONN Counterflow Strained Flame Rig with Diagnostics**



#### Capability of Counterflow Flame Rig

- Ammonia compatible
- 8+ atm
- 200 °C (now) → 500 °C (later)
- Premixed, non-premixed, and partially-premixed combustion









# **Premixed NH<sub>3</sub> Counterflow Flames**



#### Premixed NH<sub>3</sub> –Air Flames, $\phi$ =1

**Decreasing Nozzle Exit Velocity** Decreasing Strain Rate (Laminar Flame Speed Measurement)





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Flame strain (stretch) rate is represented by the velocity gradient ahead of the flame and is proportional to nozzle exit velocity. 8

# **Premixed** Counterflow NH<sub>3</sub>/Air Flames: Effect of Pressure and Equivalence Ratio



#### **UCONN Counterflow Extinction Experiments**

• Initial reactant temperature  $T_i = 294 - 298 \text{ K}$ 

Effect of Equivalence Ratio on Extinction Strain Rate



Effect of Pressure on  $NH_3$ -Air Flame Extinction ( $\phi = 1$ )





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### **Chemical Kinetic Mechanisms**

Selected published, comprehensive N/H chemical mechanisms

 Open-source computational framework developed by Dave Goodwin at Caltech Cantera

#### Glarborg et al. Mechanism (2018 and 2022 versions)

[Glarborg, Miller, Ruscic, Klippenstein: Modeling nitrogen chemistry in combustion, Prog. Energy Combust. Sci. (2018) 31-68] [Glarborg: The NH<sub>3</sub>/NO<sub>2</sub>/O<sub>2</sub> system: Constraining key steps in ammonia ignition and N<sub>2</sub>O formation, Combust. Flame, Vol. 257 (2023)]

#### Stagni et al. Mechanism

[Stagni, Cavallotti, Arunthanayothin, Song, Herbinet, Battin-Leclerc, Faravelli: React. Chem. Eng. 5 (2020) 696–711]

#### Powell et al. Mechanism- (Referred to as "RTRC")

[Powell, Papas, Dreyer: Hydrogen- and C<sub>1</sub>-C<sub>3</sub> Hydrocarbon-Nitrous Oxide Kinetics in Freely, Propagating and Burner Stabilized Flames, Shock Tubes, and Flow Reactors, Combust. Sci. Tech. 182 (2010) 252-283] [Powell, Papas, Dreyer: Flame Structure measurements of NO in Premixed Hydrogen-Nitrous Oxide Flames, Proc. Combust. Inst. 33 (2011) 1053-1062]

• Two "RTRC" mechanisms differ by only 3 different rate expressions for amine radical reactions:

(1)  $NH_2 + NO \leftrightarrow N_2 + H_2O$ (2)  $NH_2 + NO \leftrightarrow NNH + OH$ (3)  $NH_3 + NH_2 \leftrightarrow N_2H_3 + H_2$ 



# **N/H Chemical Kinetic Mechanisms**

Comparison of selected published N/H chemical mechanisms with laminar flame speed data



*P. Papas, R. Fang, C.-J. Sung, L. L. Smith, J. F. Stevens<sup>,</sup> An Assessment of Kinetic Models for Ammonia Flame Extinction, 13<sup>th</sup> US National Combustion Meeting, College Station, TX, March 19-22, 2023.* 

#### **Premixed** NH<sub>3</sub> <u>Flame Speed</u>: Effect of added H<sub>2</sub>



#### **Non-Premixed** NH<sub>3</sub> Extinction Strain Rate



### **Chemical Kinetic Mechanisms**

Example Data Sets used for "RTRC" N/H Mechanism Validation

Experiment	References
Flow reactor studies	
N <sub>2</sub> O decomposition	Allen et al. (1995)
$\rm H_2/~N_2O/~H_2O/~N_2$	Allen et al. (1998)
Flame speed studies	
$H_2/N_2O/N_2$	Powell et al. (2009)
$CH_4, C_2H_2, C_3H_8/N_2O/N_2$	Powell et al. (2009)
NH <sub>3</sub> / NO/ N <sub>2</sub>	Mei et al. (2020)
NH <sub>3</sub> /H <sub>2</sub>	Lhuiller (2020); Han (2019); Ichikawa (2015)
NH <sub>3</sub> / Air	Hayakawa (2015); Takizawa (2008)
Flame structure studies	
$H_2/N_2O/CO/Ar$	Vandooren et al. (1997)
NH <sub>3</sub> / N <sub>2</sub> O/ Ar	Venizelos and Sausa (1998; 2002)
Shock tube and induction time studies	
H <sub>2</sub> / N <sub>2</sub> O/ Ar	Hidaka et al. (1985); Mével et al. (2009)
CH <sub>4</sub> / N <sub>2</sub> O/ Ar	Drummond (1969); Soloukhin (1971)
$N_2O/CH_4/CO/Ar$	Dean and Johnson (1980)
Counterflow studies	
NH <sub>3</sub> /H <sub>2</sub> (Air)- Extinction	Thomas et al. (2022)

#### Ammonia Oxidation Pathway Schematic



- Radical combinations involving  $NH_i$  to form  $N_2H_i$  important under fuel-rich conditions & not well characterized



### **Feature Sensitivity to Extinction Strain Rate**

#### NH<sub>3</sub>/Air Counterflow Flame



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### **Chemical Kinetic Mechanisms**

Comparison of important N<sub>2</sub>H<sub>i</sub>/NH<sub>i</sub> interactions between Glarborg, Stagni and RTRC mechanisms

Glarborg (2018)	RTRC	Stagni (2020)
$\begin{array}{l} NH_2 + NH_2 \leftrightarrow N_2H_2 + H_2 \\ \mathbf{NH}_2 + \mathbf{NH} \leftrightarrow \mathbf{N}_2H_2 + \mathbf{H} \\ NH_2 + NH_2 (+M) \leftrightarrow N_2H_4 (+M) \\ N_2H_4 + H \leftrightarrow N_2H_3 + H_2 \\ N_2H_4 + H \leftrightarrow NH_3 + NH_2 \\ N_2H_4 + NH_2 \leftrightarrow N_2H_3 + NH_3 \\ N_2H_3 + H \leftrightarrow N_2H_2 + H_2 \\ N_2H_3 + NH_2 \leftrightarrow N_2H_2 + NH_3 \\ N_2H_3 + NH_2 \leftrightarrow N_2H_2 + NH_3 \\ N_2H_3 + NH \leftrightarrow N_2H_2 + NH_2 \\ N_2H_2H_3 + NH \leftrightarrow NNH + H_4 \\ N_2H_2 + H \leftrightarrow NNH + H_2 \\ N_2H_2 + NH_2 \leftrightarrow NNH + NH_3 \\ N_2H_2 + NH_2 \leftrightarrow NNH + NH_3 \\ N_2H_2 + NH \leftrightarrow NNH + NH_3 \\ N_2H_3 + NH \leftrightarrow N_3H_3 \\ N_2H_3 + NH \leftrightarrow N_3 \\ N_3H_3 + NH \leftrightarrow N_3 \\ N_3H_3 + N_3 \\ N_3H_3 + N_3 \\ N_3 \\ N_3H_3 + N_3 \\ N_3H_3 + N_3 \\ N_3 \\ N_3H_3 + N_3 \\ N_3H_3 + N_3 \\ N_3 \\$	$\begin{array}{c} \mathbf{NH_2} + \mathbf{NH_2} \leftrightarrow \mathbf{N_2H_2} + \mathbf{H_2} \\ \mathbf{NH+NH_2} \leftrightarrow \mathbf{N_2H_2} + \mathbf{H} \\ \mathbf{N_2H_4} + \mathbf{M} \leftrightarrow \mathbf{NH_2} + \mathbf{NH_2} + \mathbf{M} \\ \mathbf{N_2H_4} + \mathbf{H} \leftrightarrow \mathbf{N_2H_3} + \mathbf{H_2} \\ \mathbf{N_2H_4} + \mathbf{H} \leftrightarrow \mathbf{NH_2} + \mathbf{NH_3} \\ \mathbf{N_2H_4} + \mathbf{NH_2} \leftrightarrow \mathbf{N_2H_3} + \mathbf{NH_3} \\ \mathbf{N_2H_3} + \mathbf{H} \leftrightarrow \mathbf{N_2H_2} + \mathbf{H_2} \\ \mathbf{N_2H_3} + \mathbf{H} \leftrightarrow \mathbf{N_2H_2} + \mathbf{H_3} \\ \mathbf{N_2H_3} + \mathbf{H} \leftrightarrow \mathbf{N_2H_2} + \mathbf{H_3} \\ \mathbf{N_2H_2} + \mathbf{NH_2} \leftrightarrow \mathbf{N_2H_2} + \mathbf{NH_3} \\ \mathbf{N_2H_2} + \mathbf{NH_2} \leftrightarrow \mathbf{NH+N_2H_3} \\ \mathbf{N_2H_2} + \mathbf{NH_2} \leftrightarrow \mathbf{NNH+H} \\ \mathbf{N_2H_2} + \mathbf{H} \leftrightarrow \mathbf{NNH+H_2} \\ \mathbf{N_2H_2} + \mathbf{NH_2} \leftrightarrow \mathbf{NNH+H_3} \\ \mathbf{N_2H_2} + \mathbf{NH_2} \leftrightarrow \mathbf{NNH+H_3} \\ \mathbf{N_2H_2} + \mathbf{NH_2} \leftrightarrow \mathbf{NNH+NH_3} \\ \mathbf{N_2H_2} + \mathbf{NH_3} \leftrightarrow \mathbf{NNH+NH_3} \\ \mathbf{N_2H_2} + \mathbf{NH_4} \leftrightarrow \mathbf{NNH+NH_3} \\ \mathbf{N_2H_2} + \mathbf{NH} \leftrightarrow \mathbf{NNH+NH_3} \\ \mathbf{N_2H_2} + \mathbf{NH} \leftrightarrow \mathbf{NNH+NH_3} \\ \mathbf{N_2H_2} + \mathbf{NH} \leftrightarrow \mathbf{NNH+NH_3} \\ \mathbf{N_2H_3} + \mathbf{M} \leftrightarrow \mathbf{N_3H_3} + \mathbf{H} + \mathbf{M} \end{array}$	$\begin{array}{c} N_{2}H_{4}+H\leftrightarrow N_{2}H_{3}+H_{2} \\ N_{2}H_{3}+NH_{2}\leftrightarrow N_{2}H_{2}+NH_{3} \\ N_{2}H_{4}+NH_{2}\leftrightarrow N_{2}H_{3}+NH_{3} \\ N_{2}H_{3}+H\leftrightarrow N_{2}H_{2}+H_{2} \\ N_{2}H_{2}\leftrightarrow NNH+H \\ N_{2}H_{2}+H\leftrightarrow NNH+H_{2} \\ N_{2}H_{3}\leftrightarrow N_{2}H_{2}+H \\ N_{2}H_{2}+NH_{2}\leftrightarrow NNH+NH_{3} \\ N_{2}H_{2}+NH_{2}\leftrightarrow NNH+NH_{2} \end{array}$ $\begin{array}{c} \text{NNH+NH}_{2}\leftrightarrow N_{2}+NH_{3} \\ N_{2}H_{2}\leftrightarrow H_{2}NN \\ H_{2}NN\leftrightarrow NNH+H \\ H_{2}NN+H\leftrightarrow N_{2}H_{2}+H \\ H_{2}NN+H\leftrightarrow NNH+H_{3} \end{array}$
$\begin{array}{l} NH_{2}H_{1}\leftrightarrow N_{2}H_{3} \\ NH_{2}+NH_{2}\leftrightarrow H_{2}NN+H_{2} \\ H_{2}NN\leftrightarrow NNH+H \\ H_{2}NN+H\leftrightarrow NNH+H_{2} \\ H_{2}NN+H\leftrightarrow N_{2}H_{2} \\ H_{2}NN+H\leftrightarrow N_{2}H_{2}+H \\ H_{2}NN+NH_{2}\leftrightarrow NNH+NH_{3} \\ N_{2}H_{4}\leftrightarrow H_{2}NN+H_{2} \\ N_{2}H_{3}+NH_{2}\leftrightarrow H_{2}NN+NH_{3} \end{array}$ $\begin{array}{l} Pros:  - \mbox{ Comprehensive N kinetics for NOx} \\ - \mbox{ Extended to low-temp. ignition chemistry} \\ Ons:  - \mbox{ Flame-speed predictions vs. data} \end{array}$	$\begin{array}{c} N_{2}H_{3}+H\leftrightarrow NH_{2}+NH_{2} \\ NNH+NH_{2}\leftrightarrow N_{2}+NH_{3} \\ NNH+NH\leftrightarrow N_{2}+N_{2} \\ NNH+NH\leftrightarrow N_{2}+H_{2} \\ NNH+NH\leftrightarrow N_{2}+H+M \\ N_{2}H_{4}+M\leftrightarrow N_{2}H_{3}+H+M \\ N_{2}H_{3}+M\leftrightarrow NH_{2}+NH+M \\ N_{2}H_{3}+M\leftrightarrow NH_{2}+NH+M \\ N_{2}H_{3}+H\leftrightarrow NH+NH_{3} \\ NH_{3}+NH_{2}\leftrightarrow N_{2}H_{3}+H_{2} \\ N_{2}H_{4}+NH\leftrightarrow NH_{2}+N_{2}H_{3} \\ N_{2}H_{4}+N_{2}H_{2}\leftrightarrow N_{2}H_{3}+N_{2}H_{3} \\ N_{2}H_{3}+N_{2}H_{2}\leftrightarrow N_{2}H_{4}+NNH \end{array}$	<ul> <li>In 2 NN+INH ↔ NH 11+12 H2NN+NH2 ↔ NH3+NNH N2H4 ↔ H2NN+H2 N2H3+NH2 ↔ H2NN+NH3</li> <li>Pros: - Flame-speed predictions match existing data Cons: - Limited NOx data validation</li> <li>S: - Validated N/ O/ H chemistry for NOx, N2O - Flame-speed predictions match existing data</li> </ul>
© 2023 RTX. All Rights Reserved.	$N_2H_2+N_2H_2 \leftrightarrow NNH+N_2H_3$ <u>TBL</u>	<u>D</u> : - Counterflow predictions $\rightarrow$ <b>Newly added UConn data</b> (for

K RTX

15 all mechs.)

# **Non-Adiabatic Premixed Ammonia Counterflow Flames**

Modified Counterflow Model scripts to account for radiative heat loss Radiative heat loss per unit volume

$$q_r = -4\sigma\kappa_p(T^4 - T_o^4)$$

( $\sigma$  = Stefan-Boltzmann constant,  $\kappa_p$  is the Planck mean absorption coefficient;  $T_o$  = ambient unburnt reactant temperature,  $\kappa_p$  = total Planck's mean absorption coefficient)





- Overall burning rate  $S \sim (Le^{-1} 1)\kappa$
- NH<sub>3</sub> counterflow flames exhibit radiative-induced and stretch-induced extinction limits near lean flammability limit

# **Non-Adiabatic Premixed Ammonia Counterflow Flames**

Ammonia flames exhibit both stretch- and radiative-induced extinction states near lean flammability limit



C-shaped curve for counterflow premixed fuel-lean, ammonia-air flames showing computed adiabatic stretch-induced stretch rate  $\kappa_{ext,ad}$  (solid line) as well as non-adiabatic stretch-induced stretch rates  $\kappa_{ext,R}$  (dashed line) and radiative-induced stretch rates  $\kappa_{ext,R}$  (+ symbols).



# **Premixed** Counterflow NH<sub>3</sub>/Air Flames: Effect of Pressure on Extinction Strain Rate

Comparison with available data from Colson et al. (2016) and N/H chemical mechanisms



Colson et al. (1 atm)

#### Stoichiometric Premixed NH<sub>3</sub>/Air Flames





NH<sub>3</sub>/Air

NH<sub>3</sub>/Air

stagnation plane

Twin flames

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# High-Pressure Staged Reactor Rig (RTRC) – NOx Evaluations

### **Capability of High-Pressure Reactor**

- 30+ atm
- Vessel shell rated >500 K
- Coflow / purge enables higher preheat & flame temperatures
- Staged reaction-zones for fuel-rich & fuel-lean measurements
- Planned diagnostic techniques
  - Extractive probe with in-line analyzers for species measurements (NO, NH<sub>3</sub>, ...)



pump liquid

NH<sub>3</sub> to >500psi



New NH<sub>3</sub> Flat Flame

Burner

# **RTRC High-Pressure Staged Flame Reactor Rig**

#### - High-pressure burner rig modifications for NH<sub>3</sub> compatibility

- Removal of copper components from inside pressure vessel & burner
- Modified burner insert for NH<sub>3</sub> operation
- For staged-burner testing (RQL), chimney modification for staged air addition



Shakedown Burner Testing Set-up



Flat Flame Burner







# **Chemical Reactor Network (CRN) Modelling**



- Validation against available simulation data from Li et al., Fuel 355 (2024) 129509.
- Overall "theoretical" NOx levels <30 ppm for a RQL architecture appear feasible</li>
- Established N/H mechanisms show wide variability for NOx

 $\phi_{R} = 1.25$ 

Total Residence time τ (ms)	τ <sub>PSR_I</sub> (ms)	τ <sub>PFR_I</sub> (ms)	τ <sub>PSR_II</sub> (ms)	τ <sub>PFR_II</sub> (ms)	Pressure (atm)	Inlet Temp. (K)	Outlet Temp. (K)	NOx* (ppm)
20	3	14	2	1	12	600	1850	38.5
20	3	14	2	1	30	700	1850	30.1
30	3	24	2	1	30	700	1850	22.9



\* 15% O<sub>2</sub> dry

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### **Next Steps: 2024 Experiments**

- UConn Counterflow testing continuing with preheat
- UConn Turbulent Flame Rig
  - Turbulent flame speed measurements (NH PLIF for flame surface area)
  - Effects of pressure, equivalence ratio, and turbulent intensity (Turbulent intensity range: 15–25%)
  - Pressure range: 1–7 atm; up to 500 K preheat



- **RTRC High-Pressure Staged Reactor Rig**
- System pressure up to 30 atm
- Air preheat up to 800K
- NOx measurements using probe extraction technique
- FTIR Analysis and other diagnostics

#### UConn Turbulent Flame Rig



# **Questions?**

Please e-mail any questions to:

Lance Smith (lance.smith@rtx.com) or Paul Papas (paul.papas@rtx.com)



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