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# Electrochemically-mediated Sorbent Regeneration in CO<sub>2</sub> Scrubbing Processes

NETL Pittsburgh, PA | August 26, 2019

## **Principal Investigator**

Professor T. Alan Hatton  
tahatton@mit.edu

## **Submitted to**

U.S. Department of Energy  
Office of Fossil Energy  
National Energy Technology Laboratory

# Project Overview

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**Award Name:** Electrochemically-Mediated Sorbent Regeneration in CO<sub>2</sub> Scrubbing Processes (FE0026489)

**Funding:**

□DOE	\$1,202,052
□Cost Share	\$ 310,601
□Total	\$1,512,653

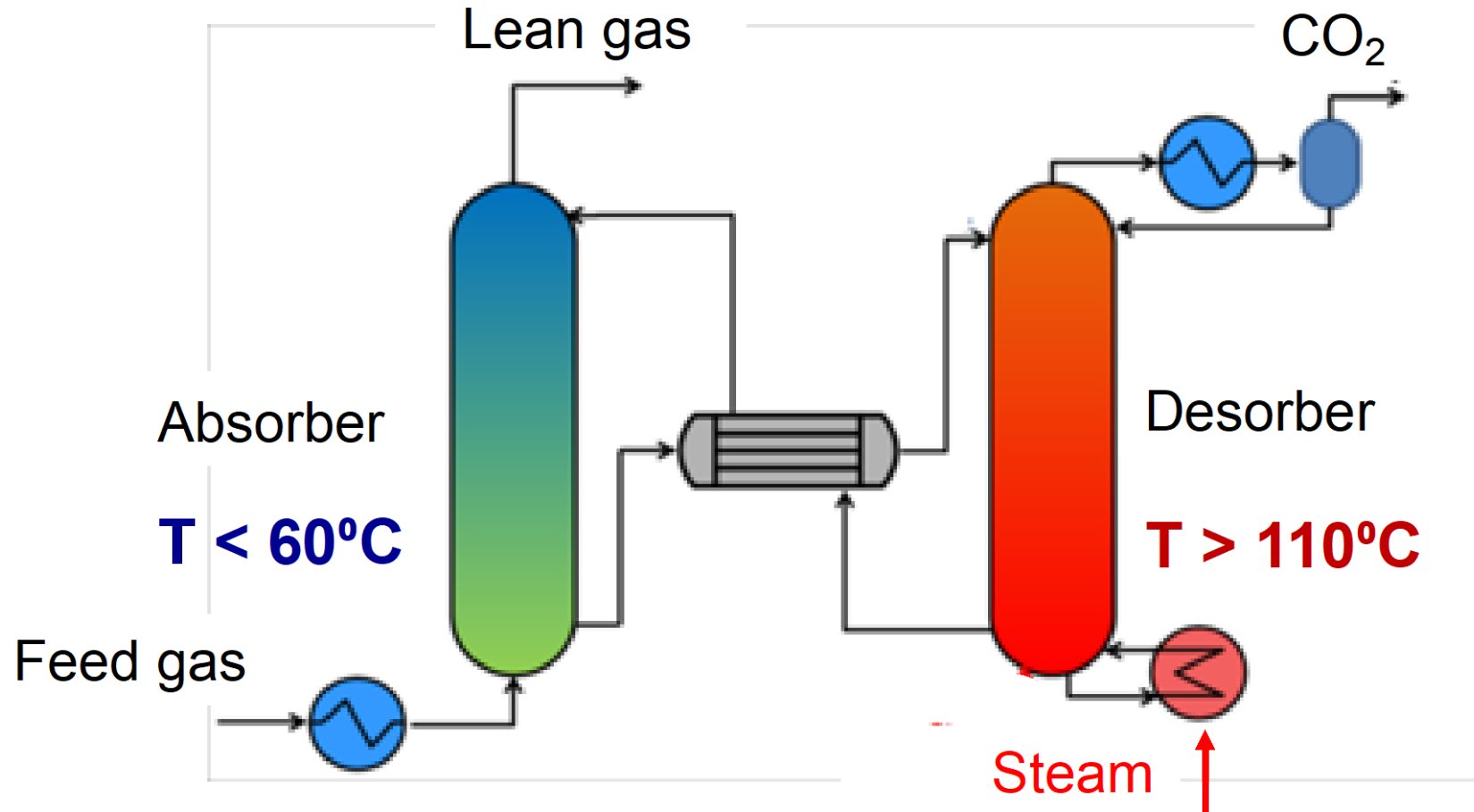
**Project Period:** August 1, 2017 – December 31, 2020

**Project PIs:** T. Alan Hatton, Howard Herzog

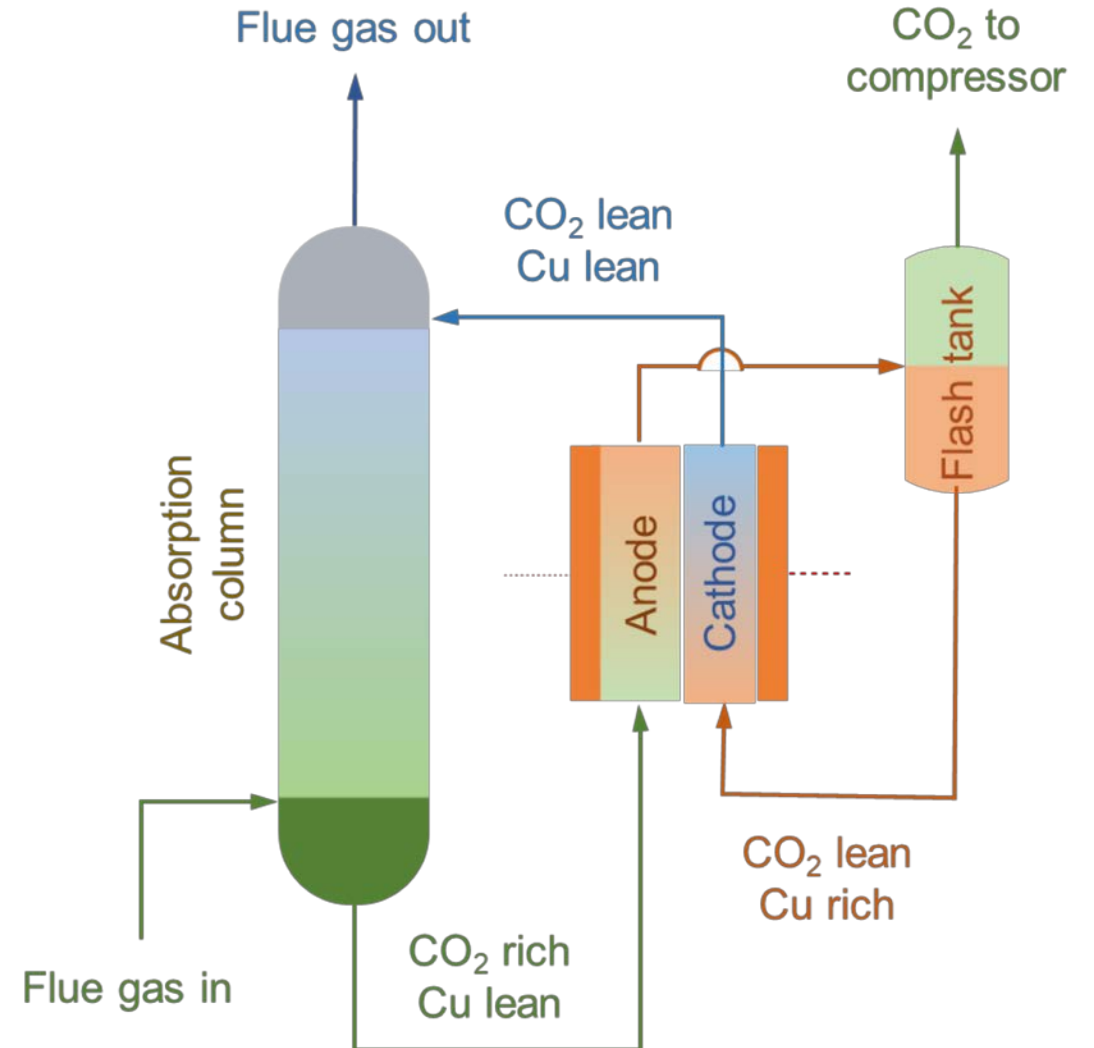
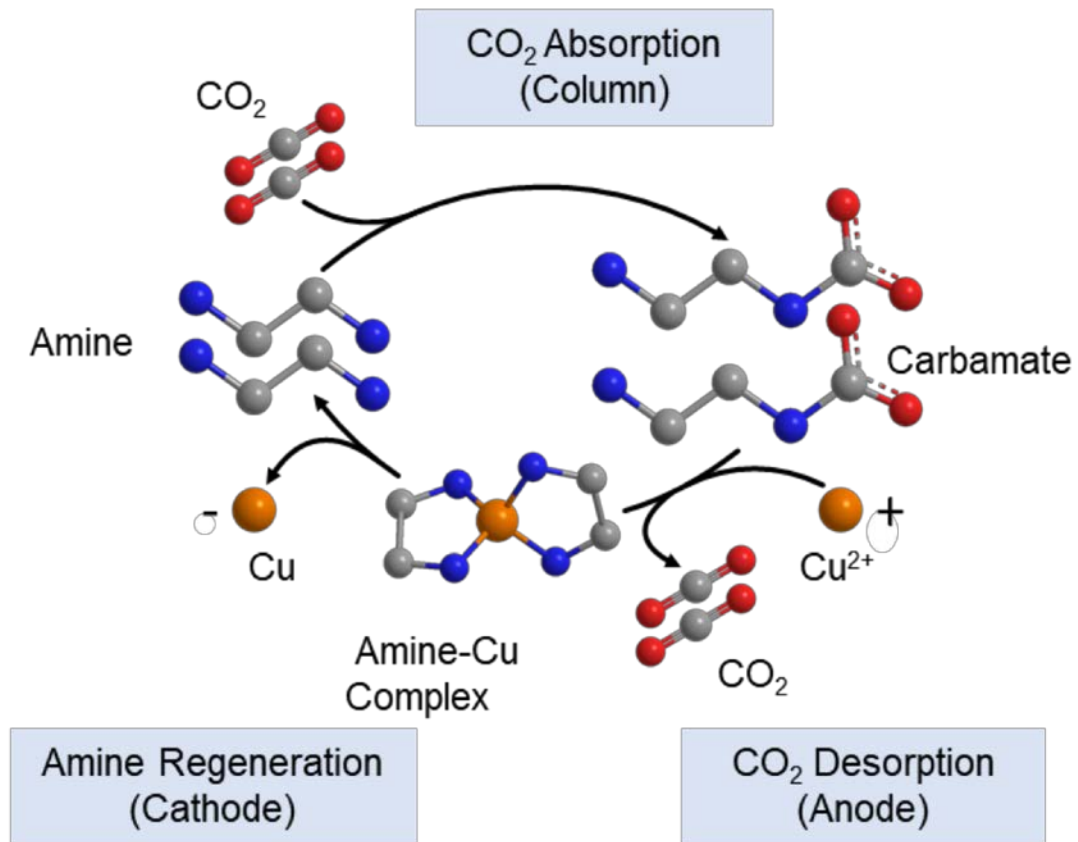
**DOE Project Manager:** Ted McMahon, Bruce Lani, David Lang

**Overall Project Objectives:** Develop, characterize and implement electrochemically mediated sorbent regeneration and CO<sub>2</sub> release in amine scrubbing processes

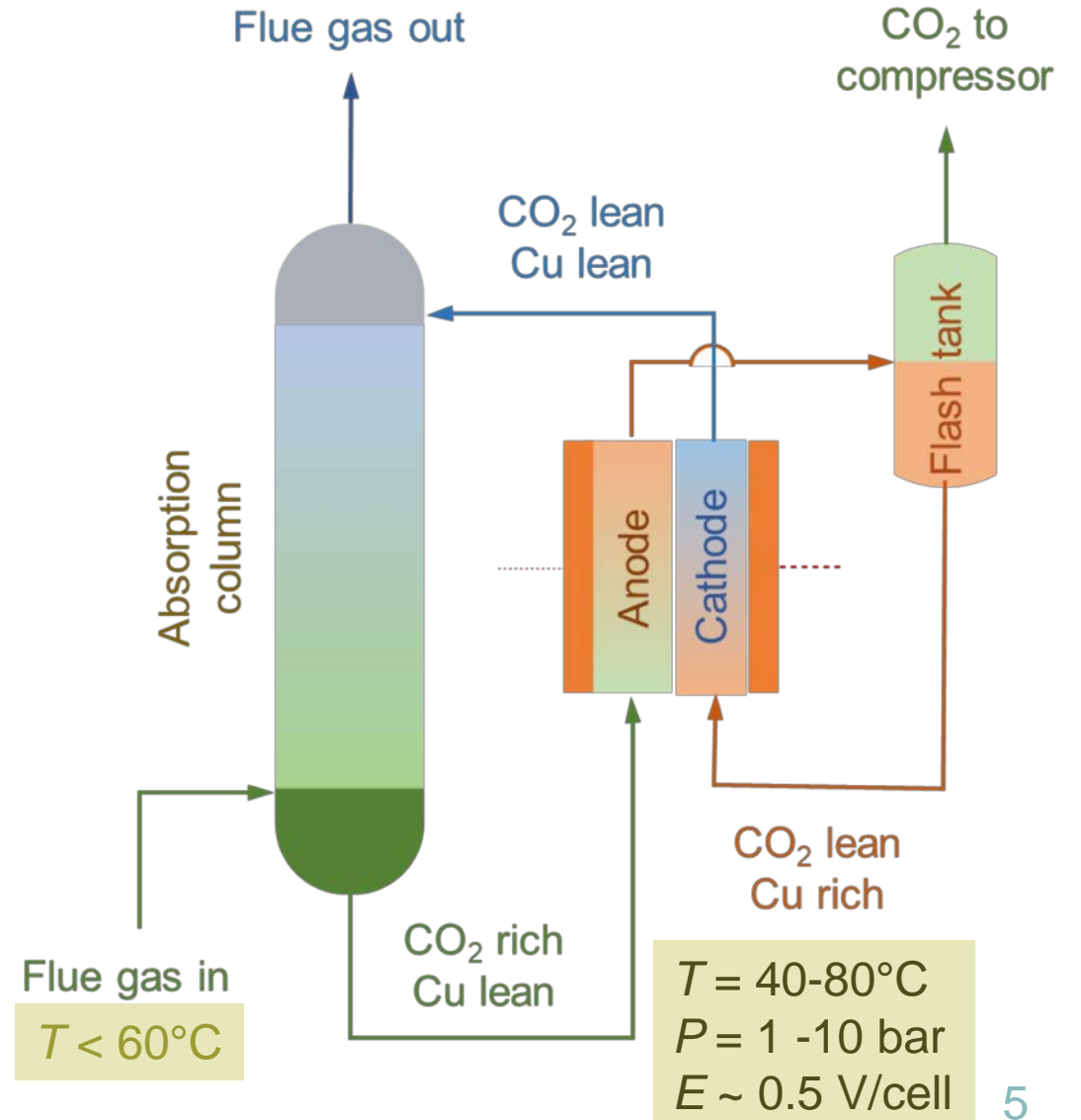
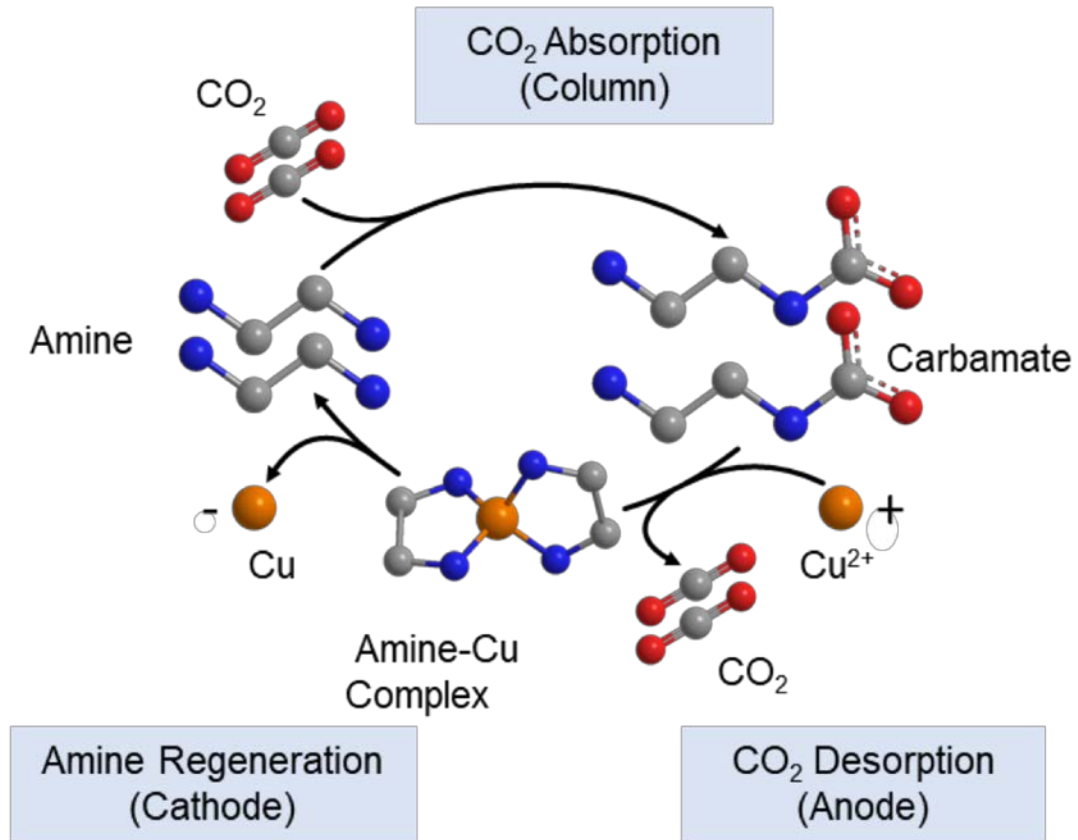
# Amine Regeneration in CO<sub>2</sub> Capture



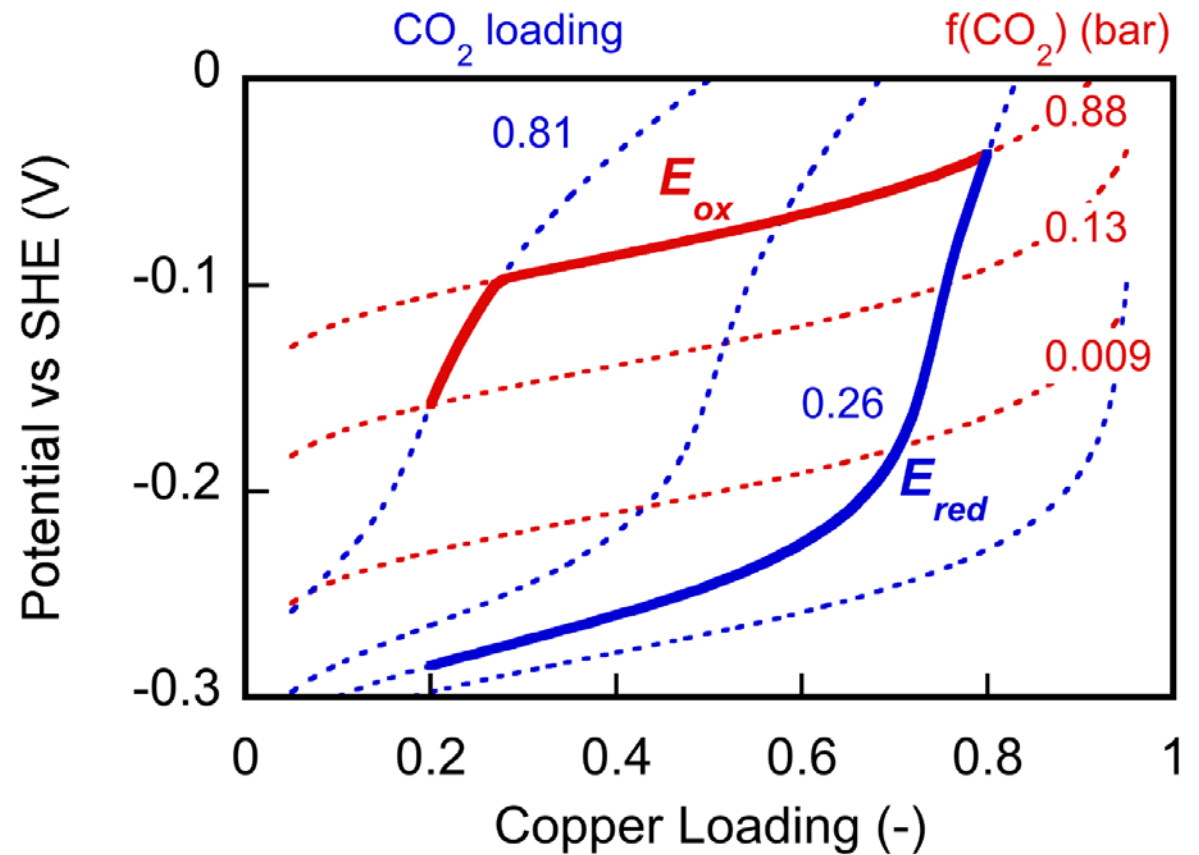
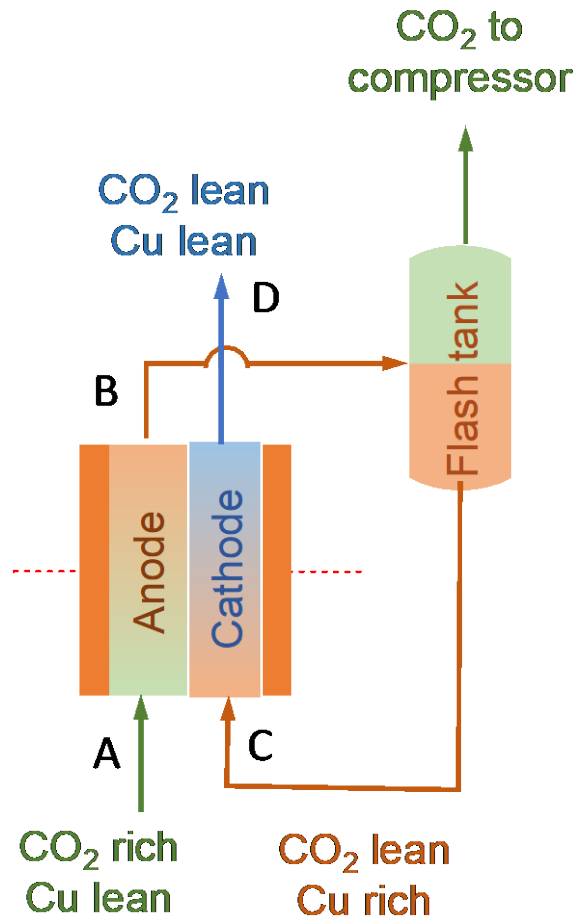
# Electrochemically Mediated Amine Regeneration



# Electrochemically Mediated Amine Regeneration



# Nernstian Description of Electrochemical Gas Separation Cycle

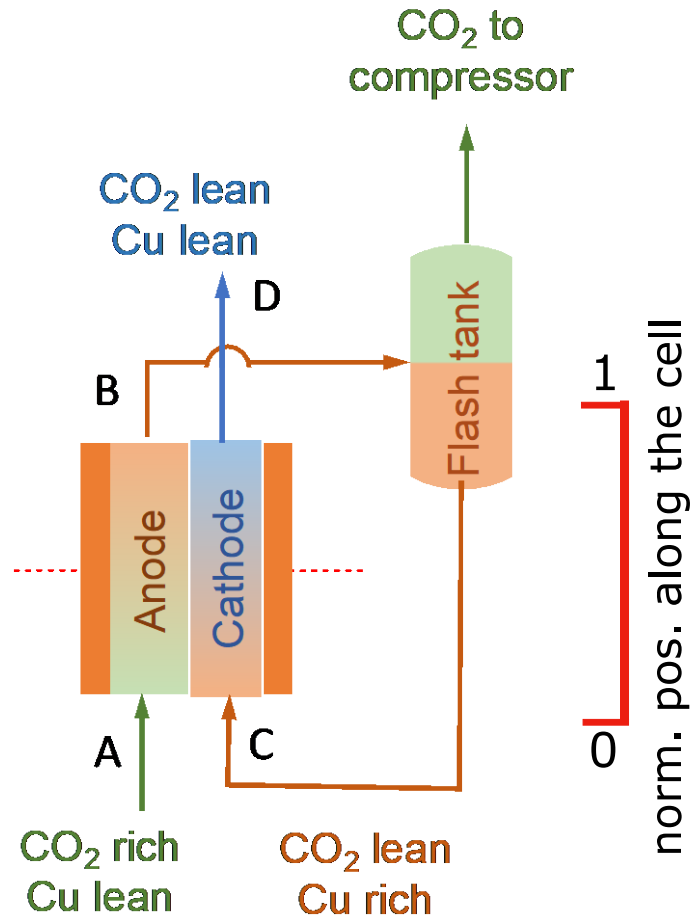


$$E_{cell} = \frac{RT}{nF} \ln \left( \frac{a_{\text{Cu}_{anode}^{2+}}}{a_{\text{Cu}_{cathode}^{2+}}} \right)$$

$$\text{copper loading} := \frac{\text{Cu}^{2+}}{2Am_o}$$

$$E = f(a_{\text{Cu}_o^{2+}}, K_1, \dots, K_{17}, y_{\text{CO}_2in}, C_{Am})$$

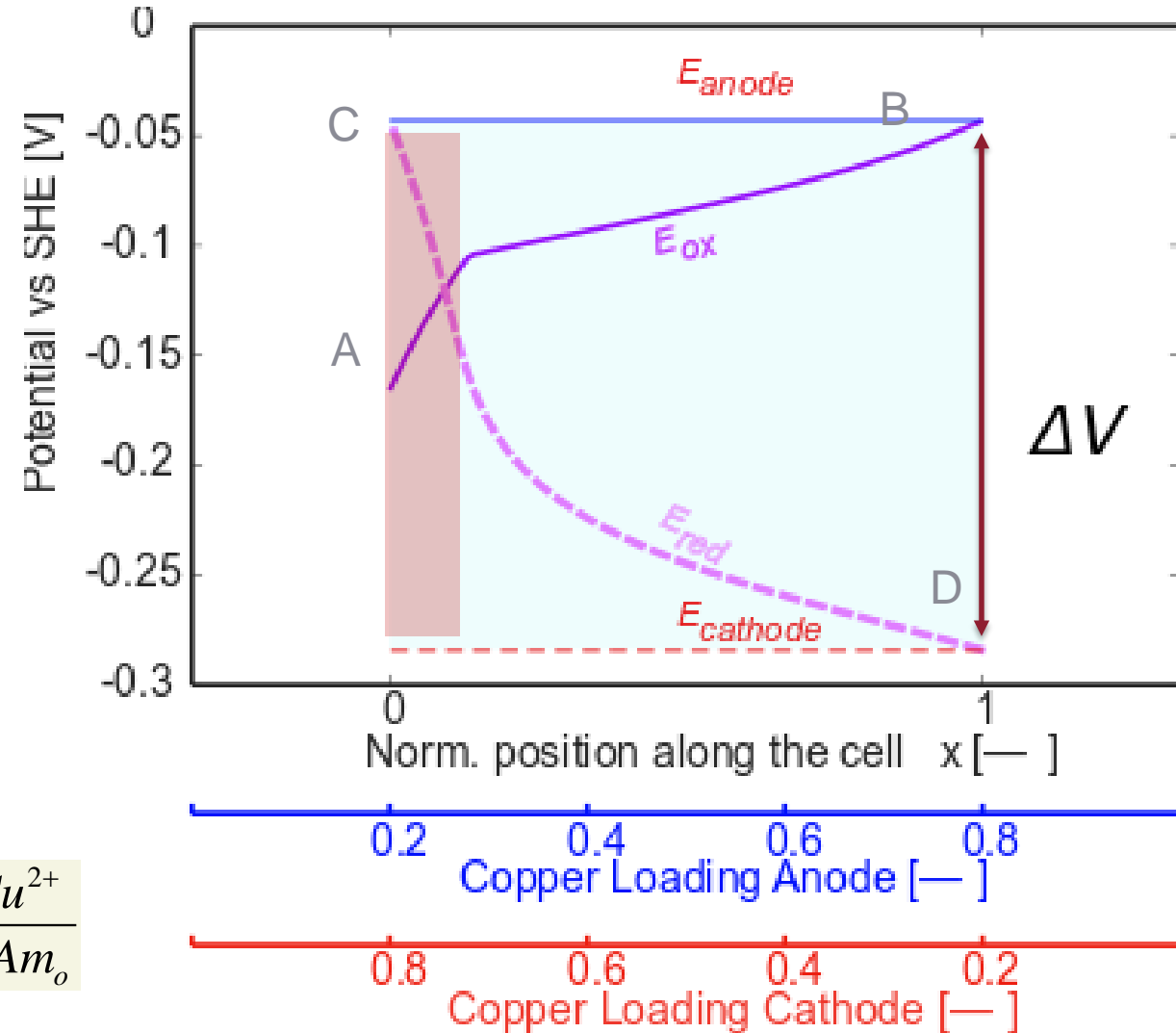
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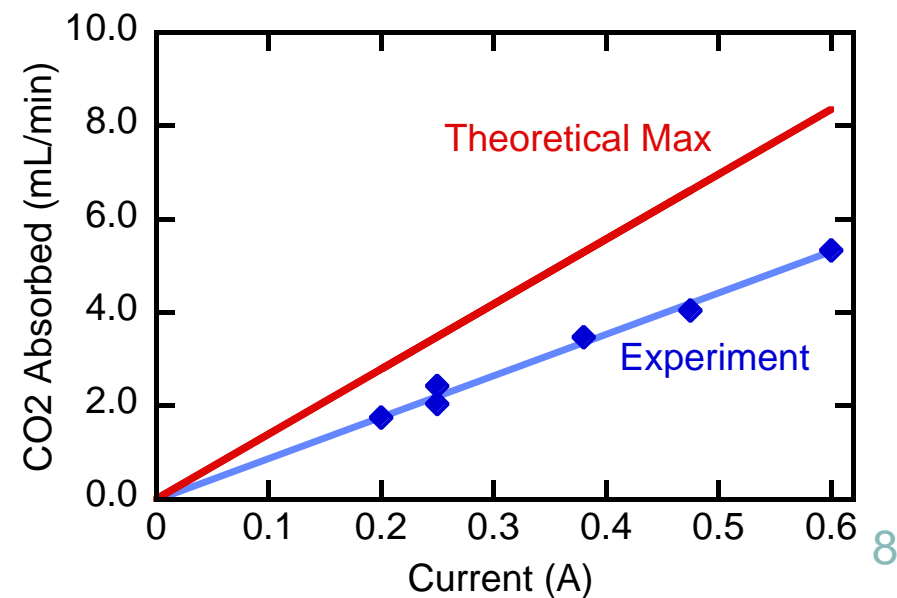
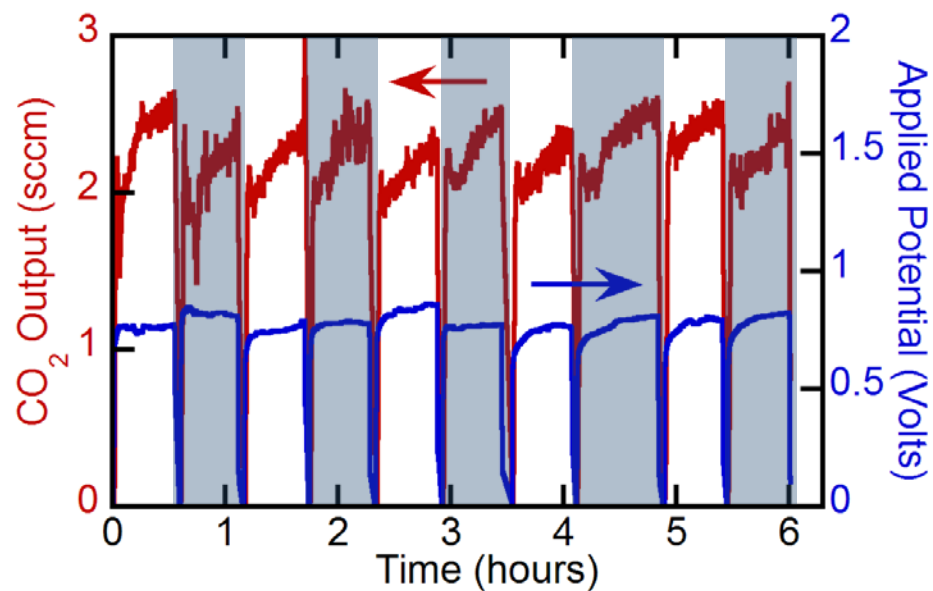
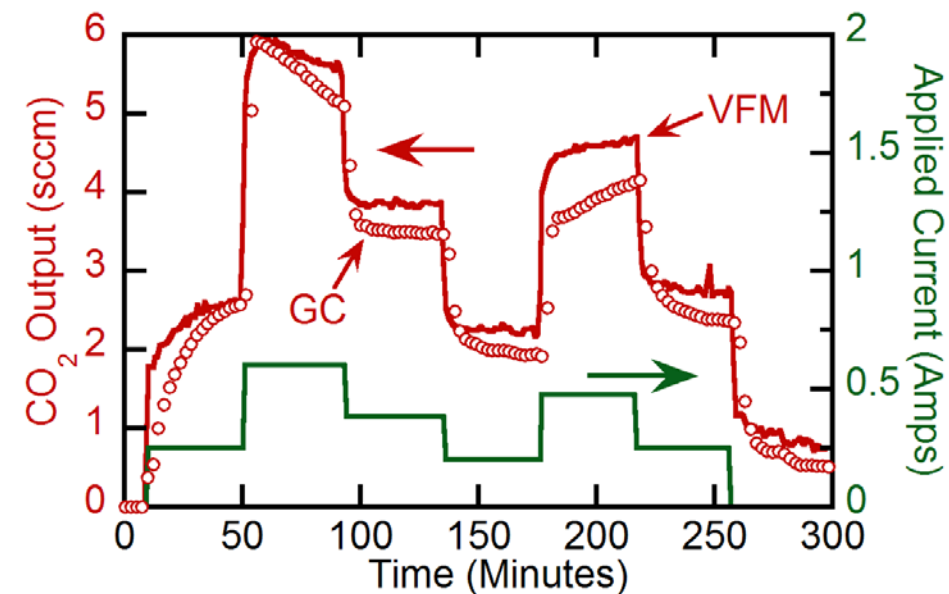
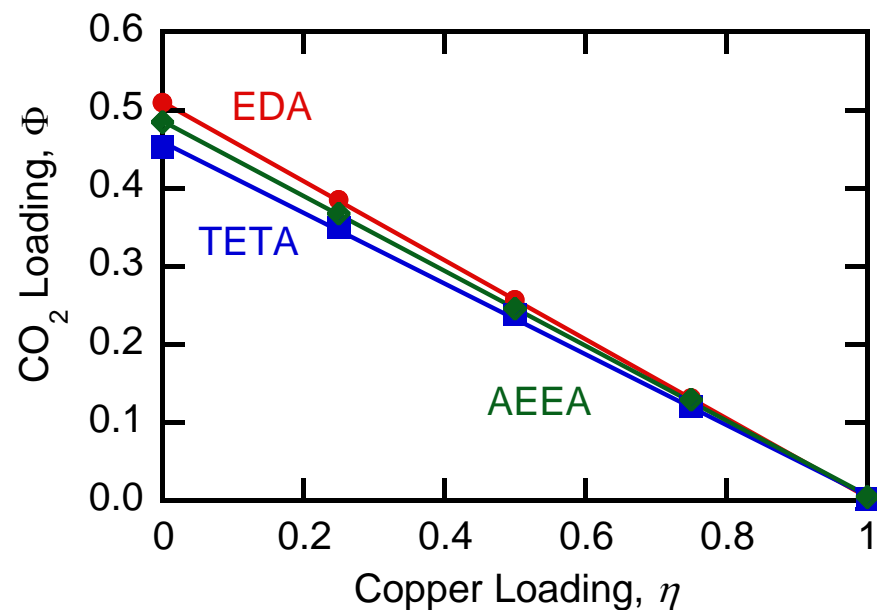
$$E_{cell} = \frac{RT}{nF} \ln \left( \frac{a_{Cu_{anode}^{2+}}}{a_{Cu_{cathode}^{2+}}} \right)$$

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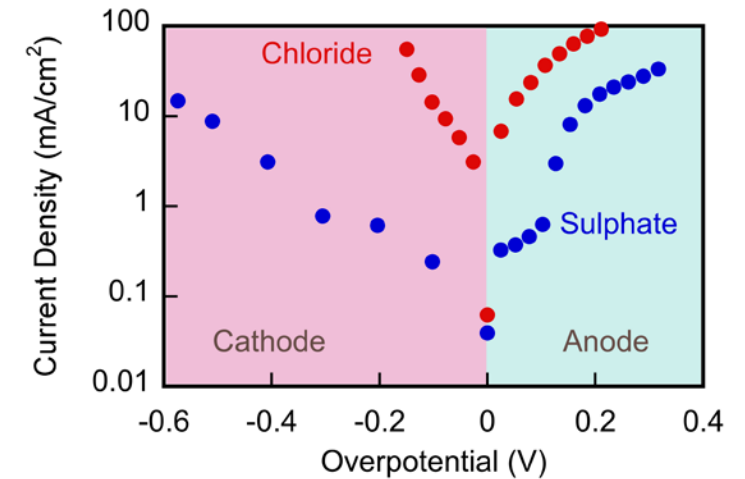
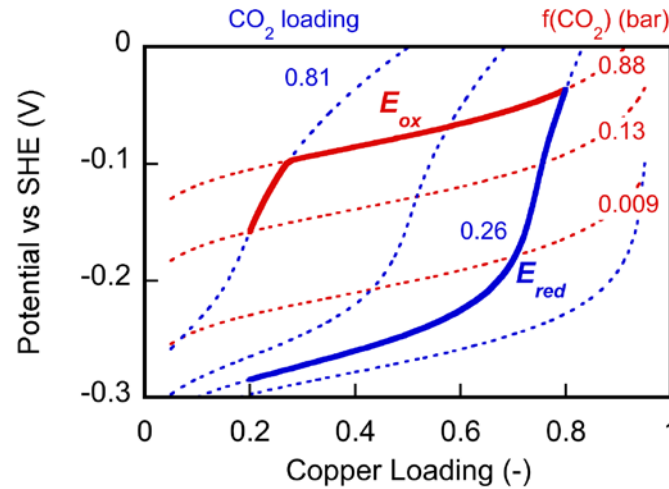
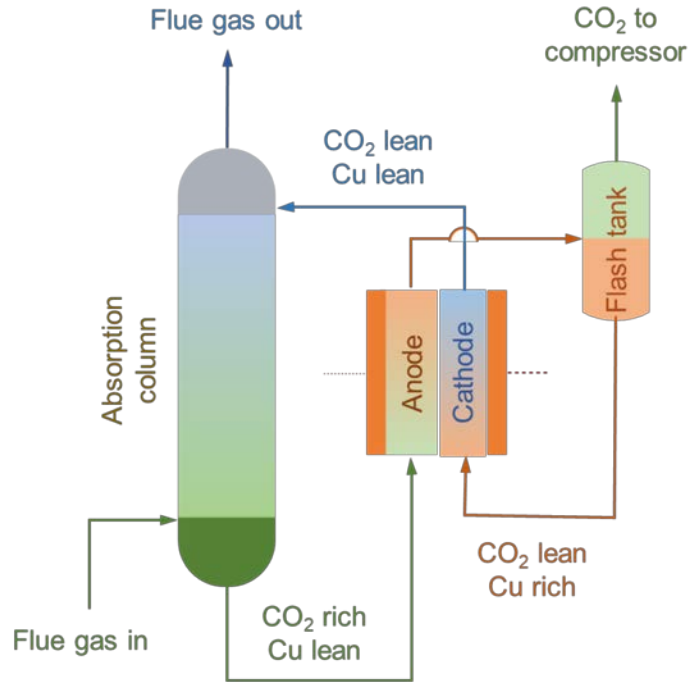


# Prior effort: EMAR CO<sub>2</sub> capture





# EMAR Advantages and Challenges



## Advantages:

- Does not need steam and extensive retrofitting
- Lower operation temperature
- Can desorb at pressure
- Can utilize low grade waste heat to improve efficiency

## Challenges:

- Overpotentials intrinsic to electrochemical systems
- Efficiency losses due to ion migration
- Stable cyclic operation

# Technical Approach

## Evaluation of amine-metal pairs

- Thermodynamics
- Kinetics

## Electrochemical characterization

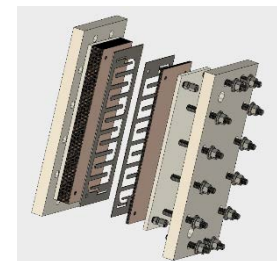
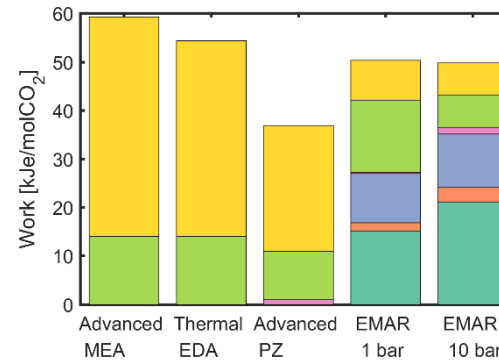
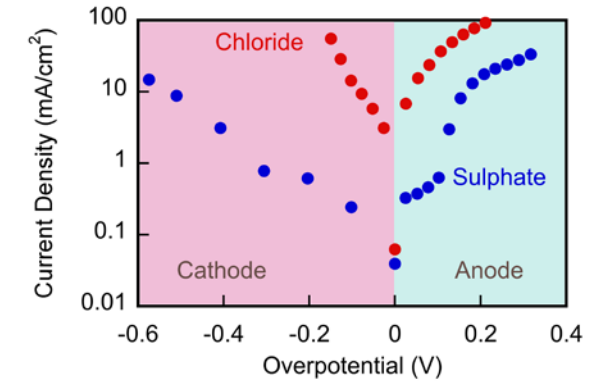
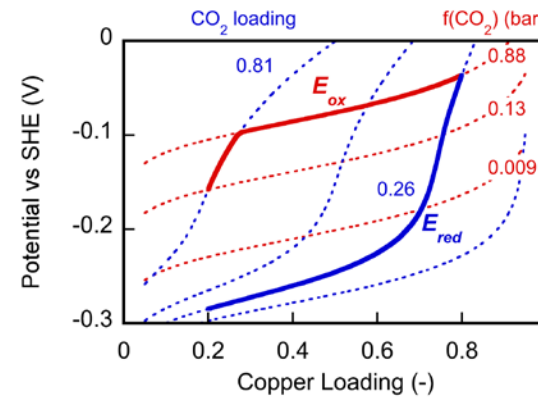
- Evaluate supporting electrolyte
- Overpotentials required

## Electrochemical cell modeling

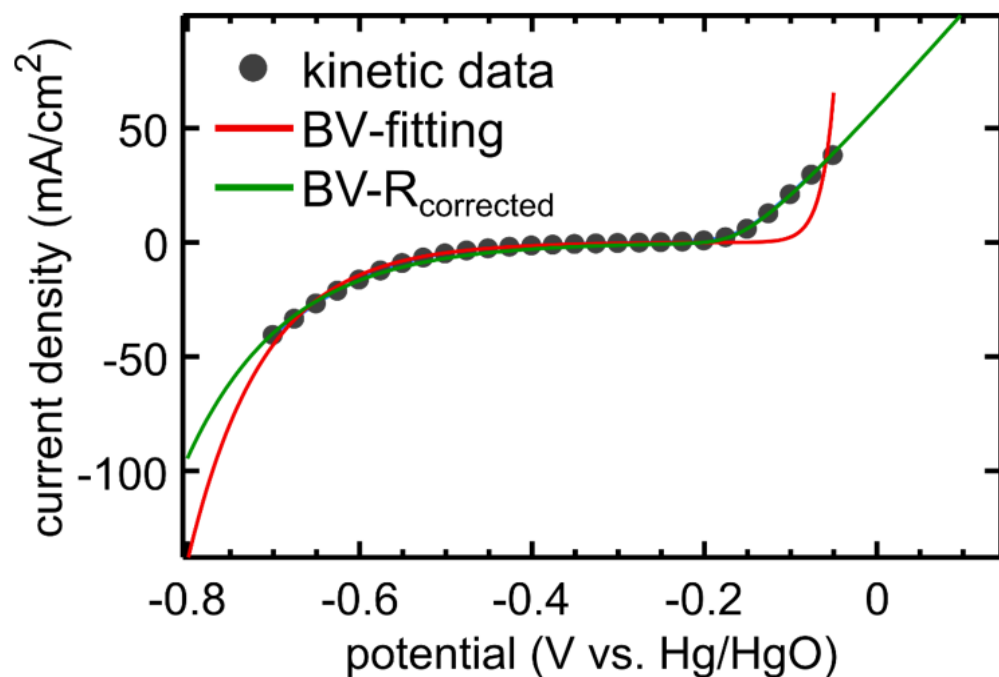
## Process modeling

- Energetics
- Techno-economic analysis

## Bench scale demonstration



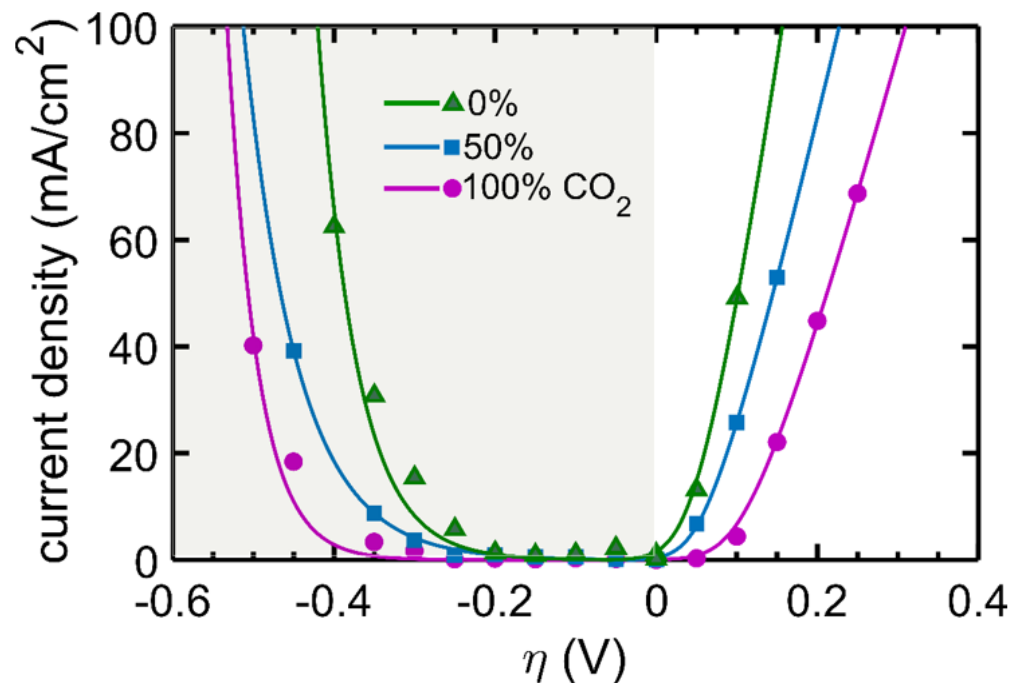
# RDE results imply asymmetrical electrode polarization



- Chronoamperometry on rotating disk electrode shows overpotential ( $\eta$ ) for cathodic reaction

$$i_o = 2Fk_o[EDA]^{2\alpha}[Cu(EDA)_2^{(2+)}]^{(1-\alpha)}$$

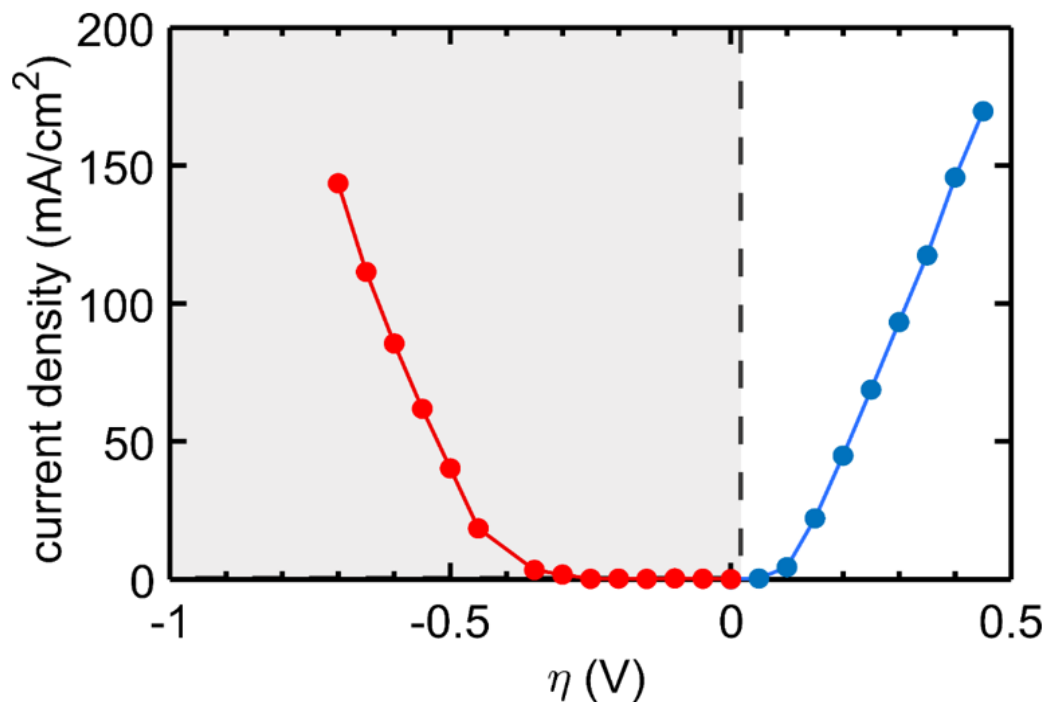
$$i_o \sim \sqrt{2}(1-\eta)^{1/2}\eta^{3/4}$$



- Higher overpotential with increasing CO<sub>2</sub> content

$$\frac{i_o(EDA-CO_2)}{i_o(EDA)} \sim \left( \frac{P_o}{K_{CO_2}P_{CO_2}} \right)^\alpha \sim 0.3$$

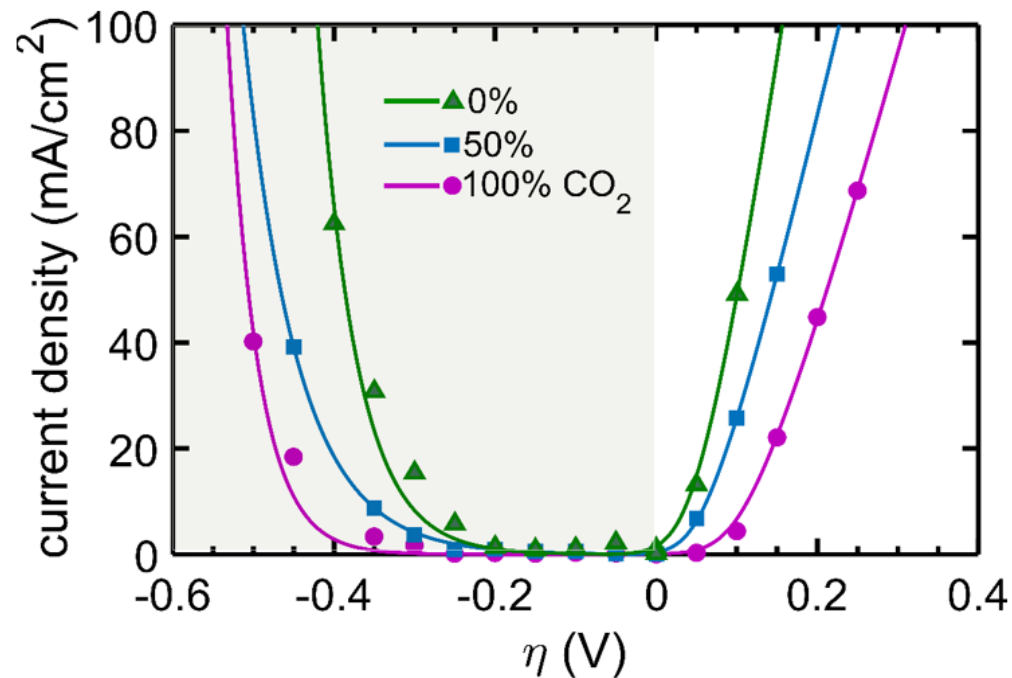
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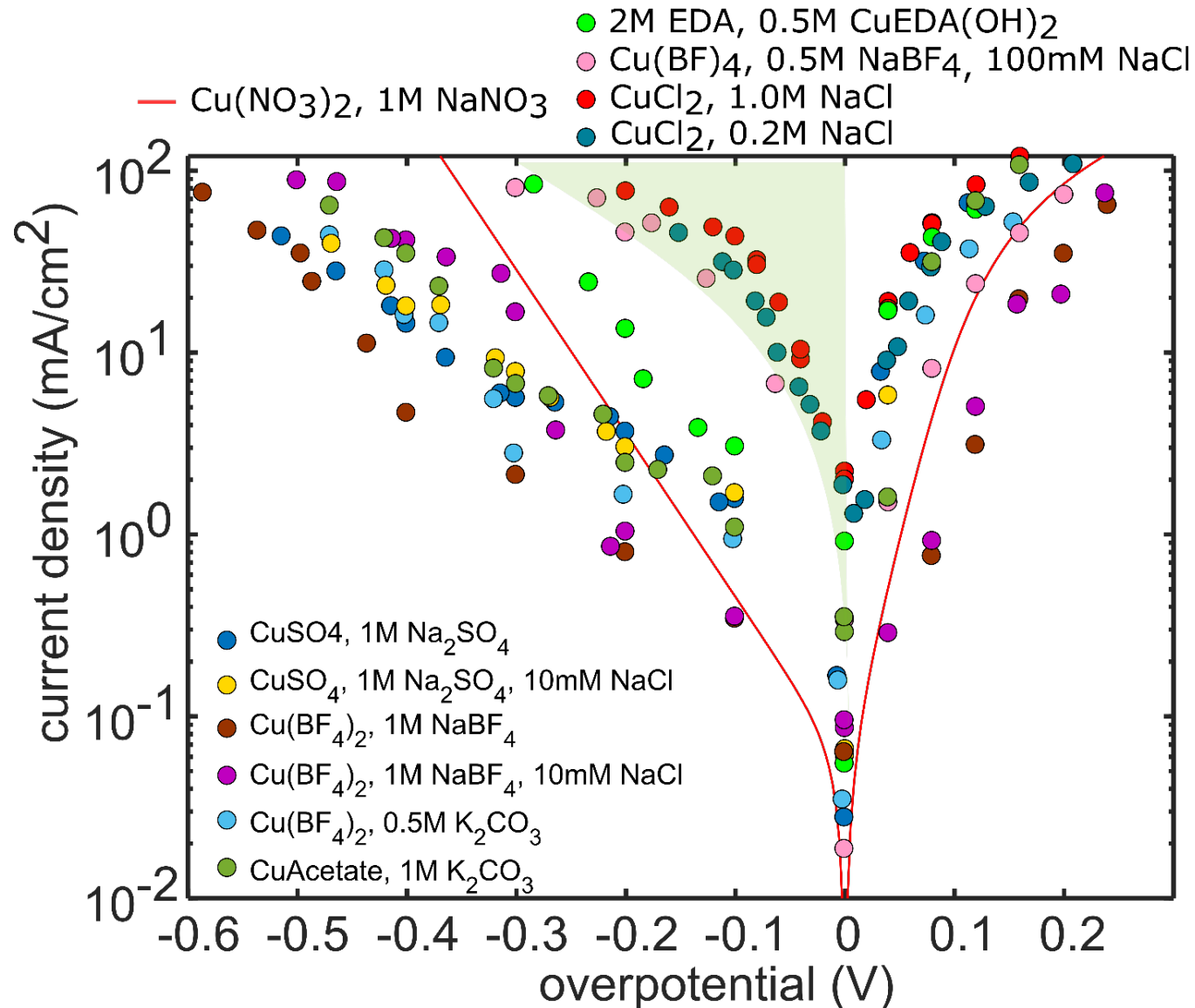
$$i_o \sim \sqrt{2}(1-\eta)^{1/2}\eta^{3/4}$$



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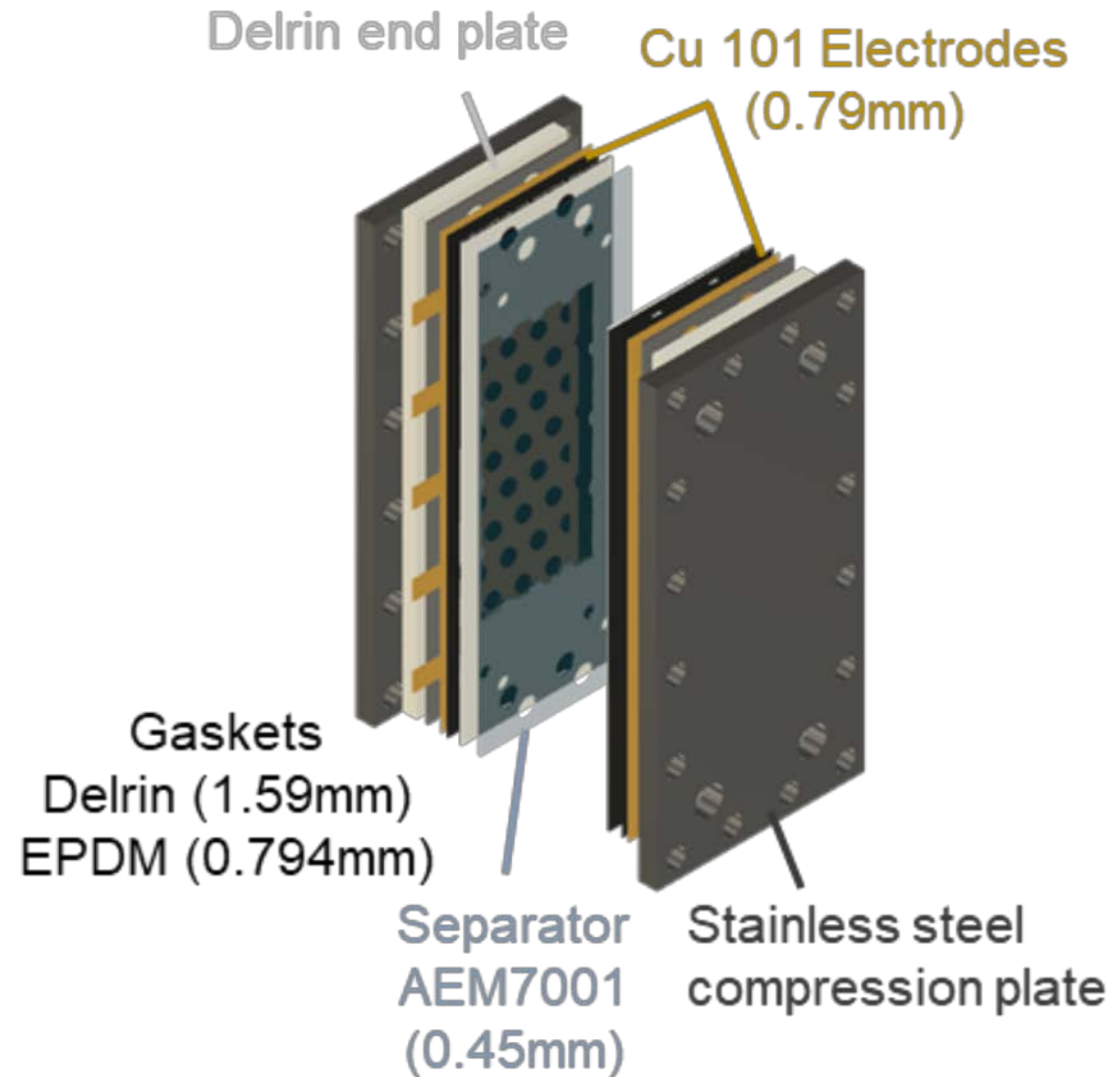
$$\frac{i_o(EDA - CO_2)}{i_o(EDA)} \sim \left( \frac{P_o}{K_{CO_2} P_{CO_2}} \right)^\alpha \sim 0.3$$

# Supporting salt affects kinetics



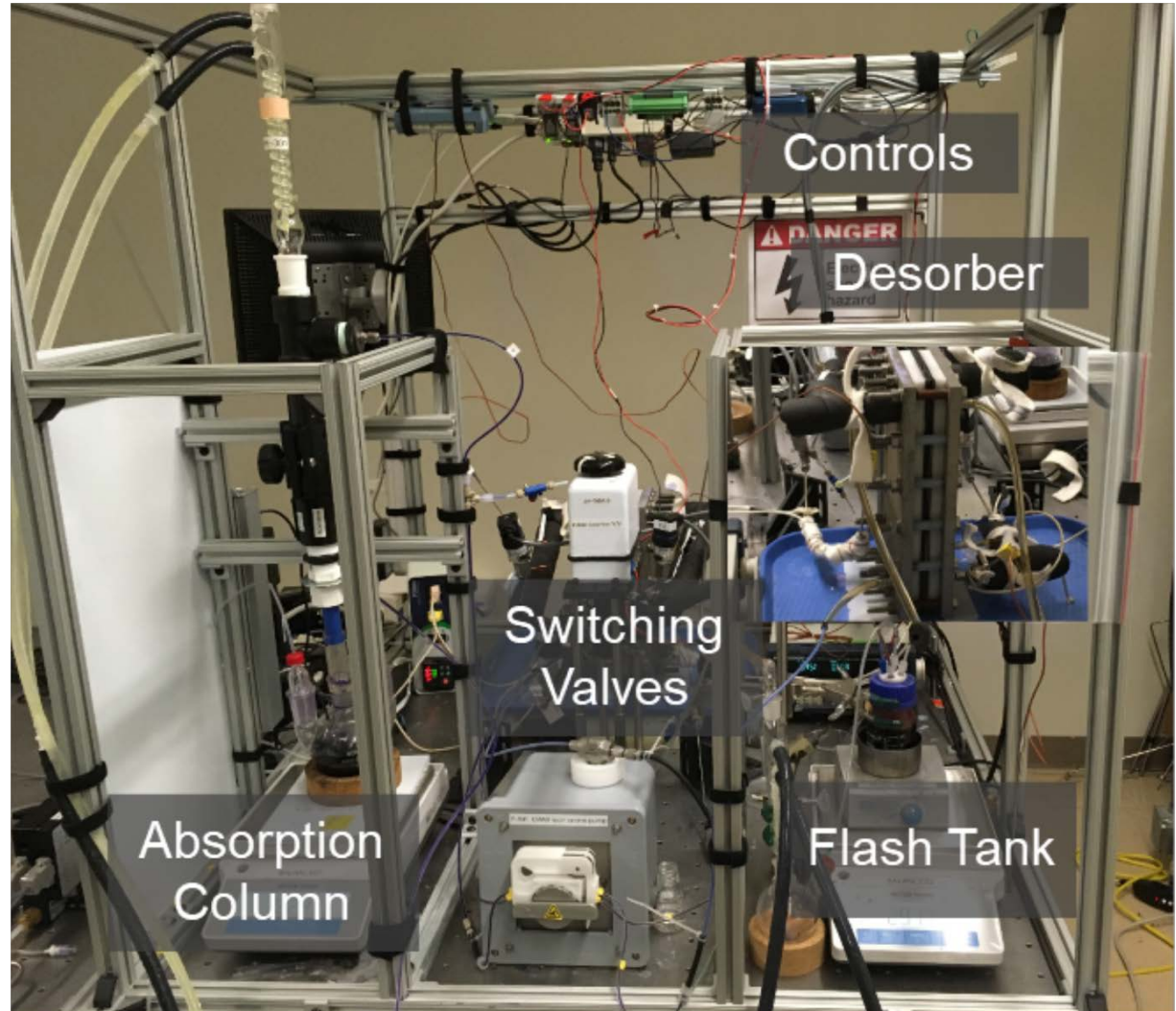
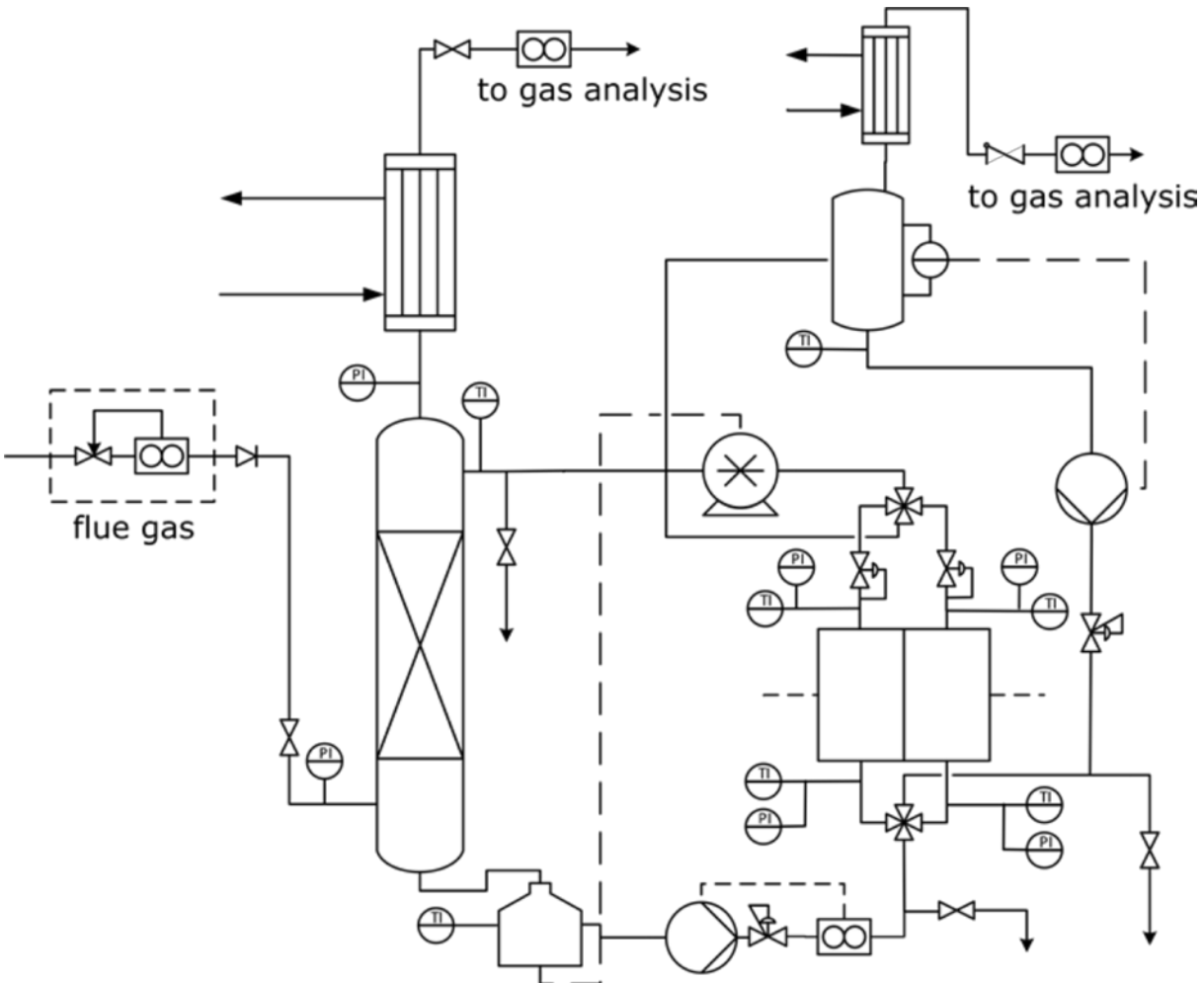
- Changing electrolyte can increase current density from  $<10 \text{ mA/cm}^2$  to  $>50 \text{ mA/cm}^2$
- Addition of Cl<sup>-</sup> increases current density to  $100 \text{ mA/cm}^2$

# EMAR Cell Construction

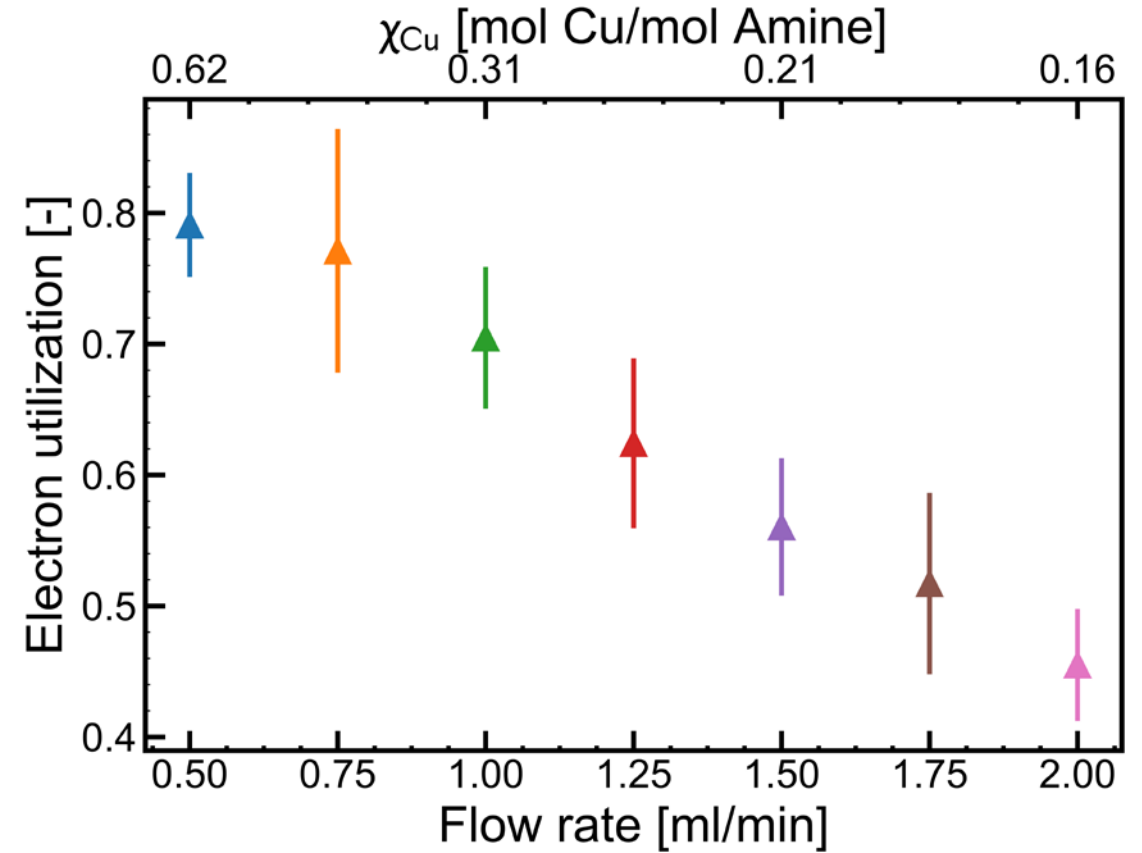
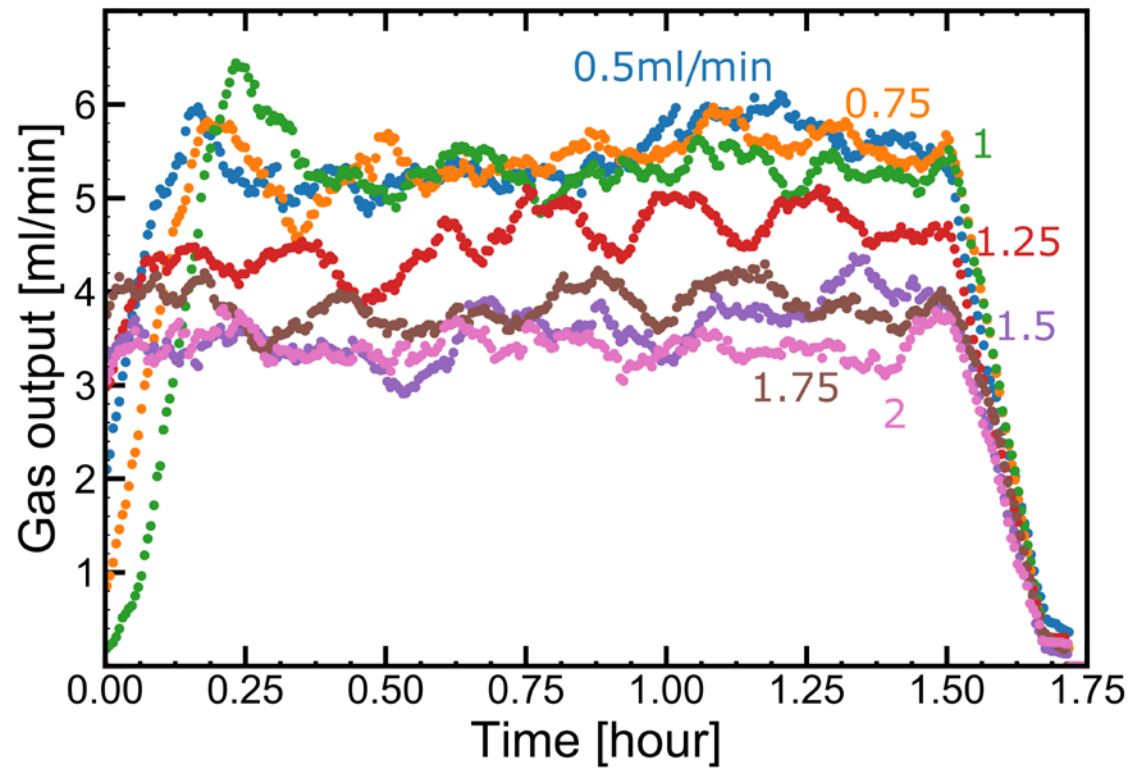




# Continuous Bench Scale EMAR

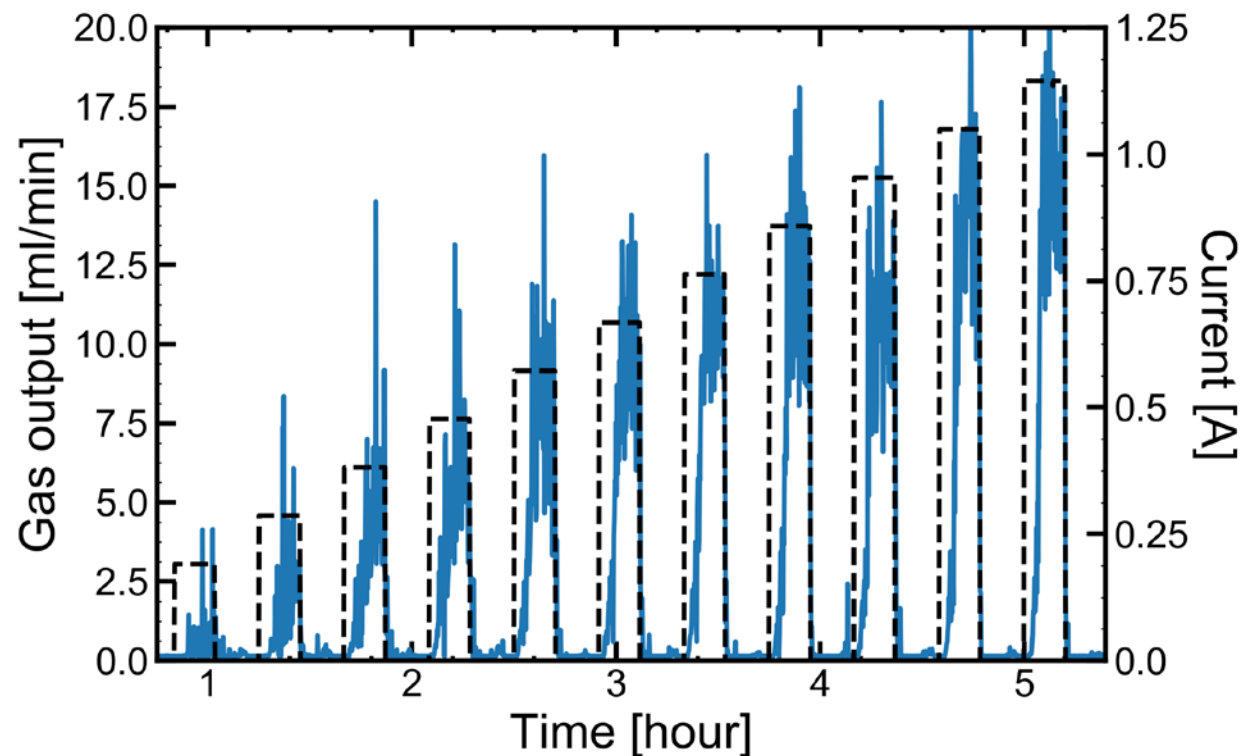
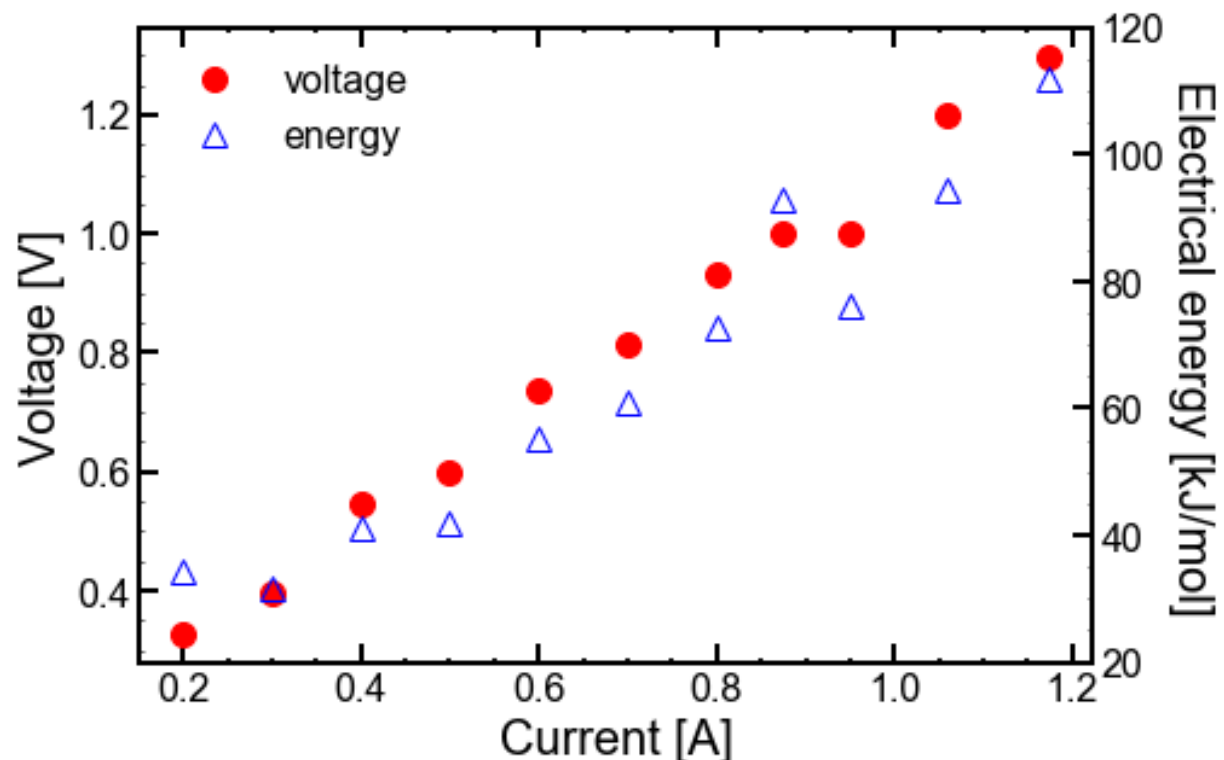


# Gas Separation and Electron Utilization: Effect of Flow Rate

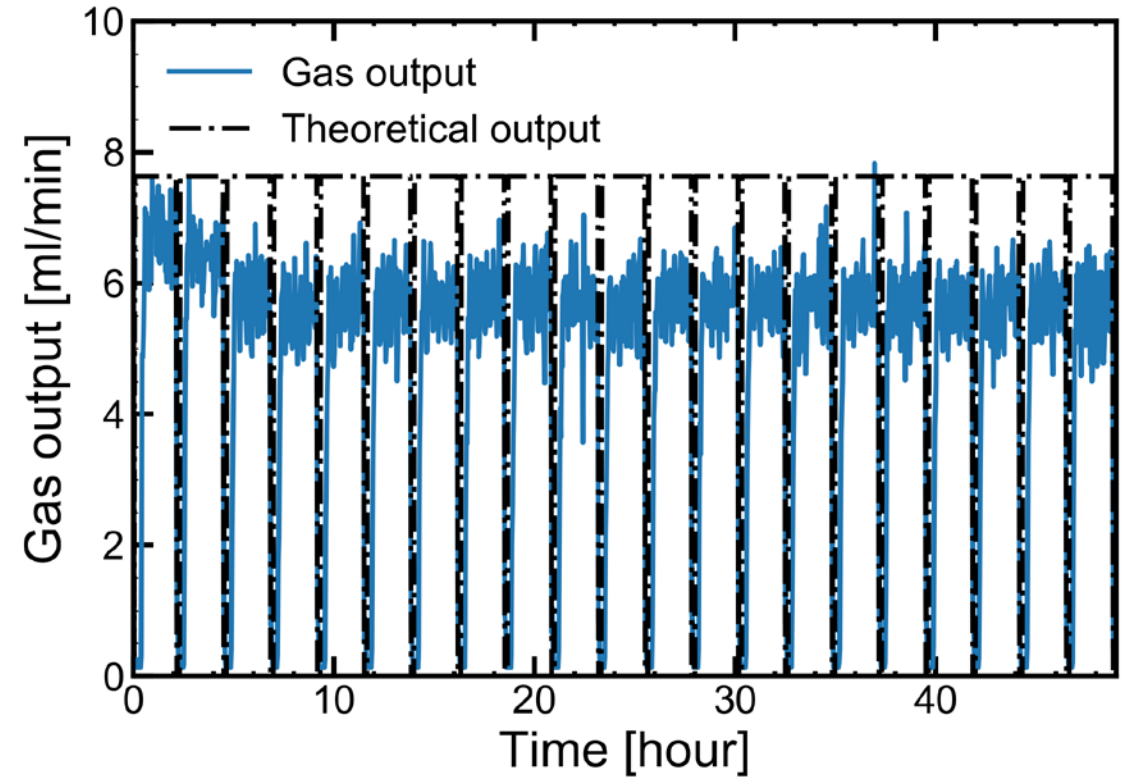
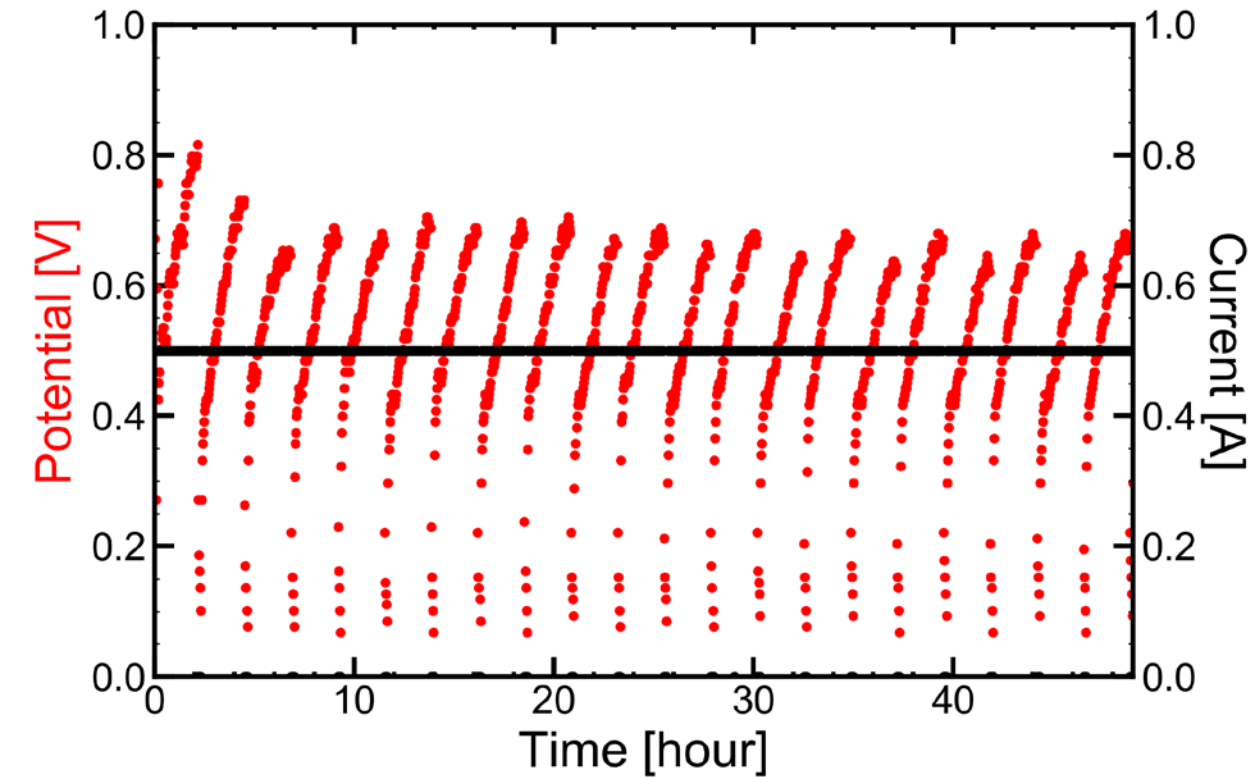




# Voltage and Gas Evolution with Varying Current

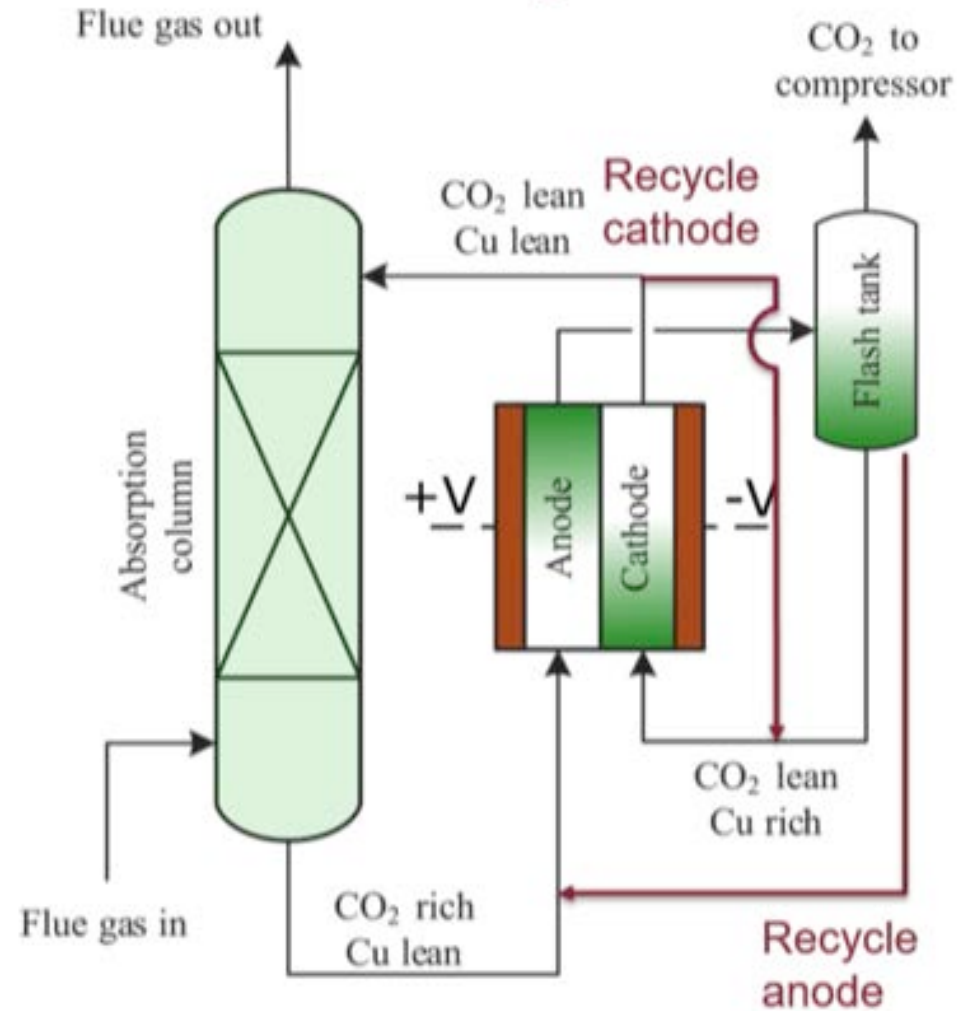


# Continuous Operation under Constant Current



# Enhanced Electrode Stability with Recycle

40 hr with no recycle

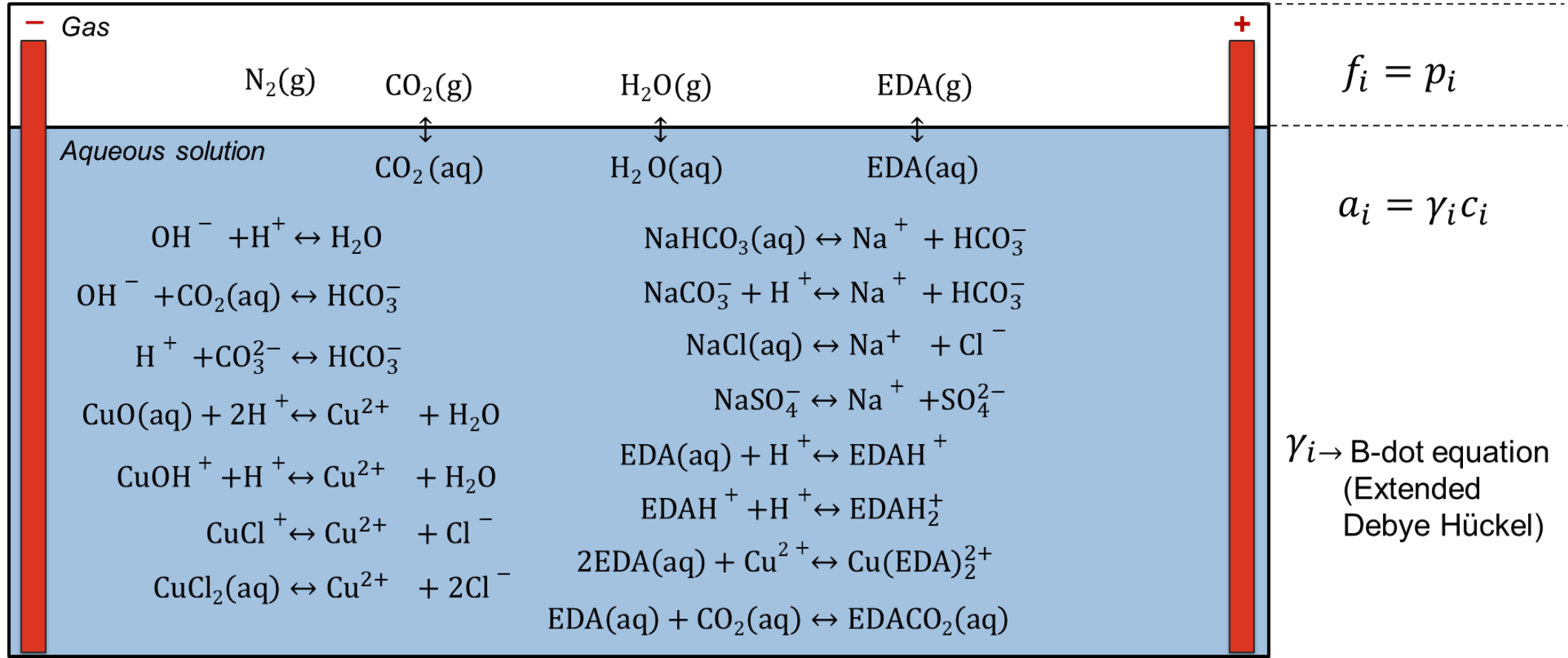


200 hr with recycle



# EMAR thermodynamics modeling

EMAR electrolyte speciation with copper electrodes and EDA as the amine



To calculate:

- Electrochemical Energetics
- Process energetics (compressor, pump, hot water utilities, etc.)

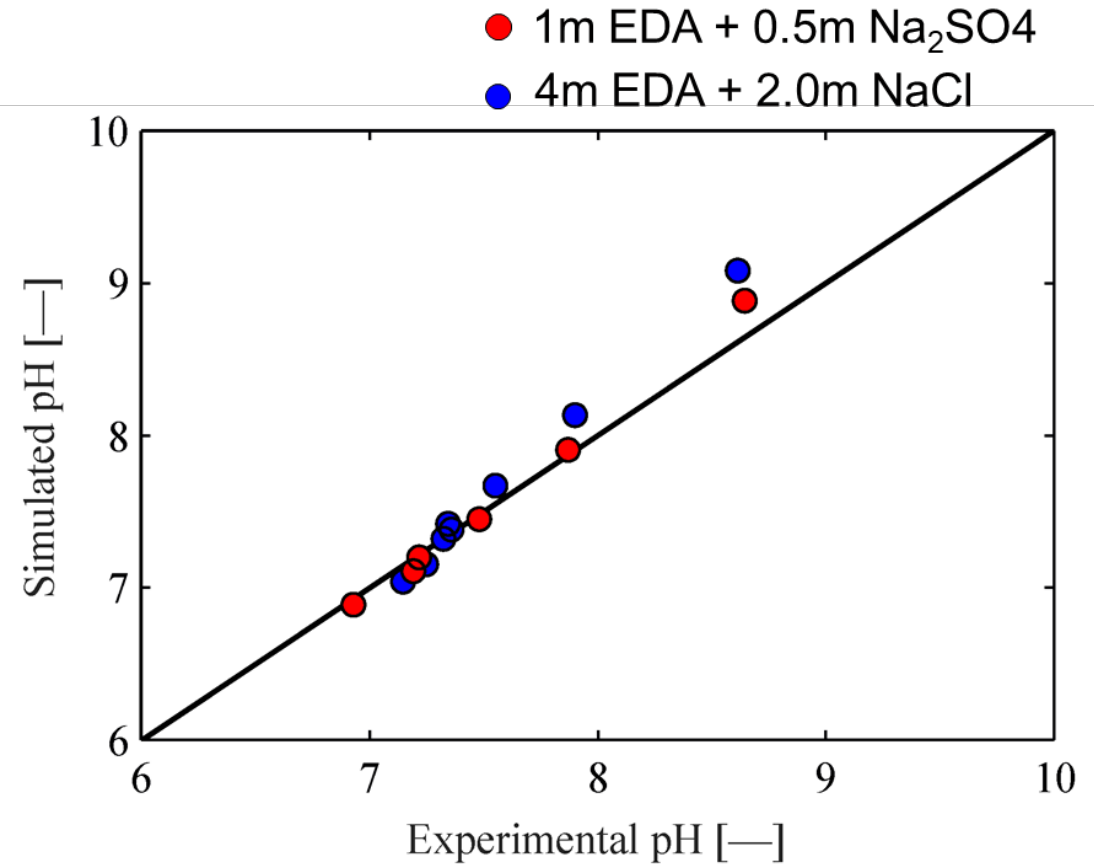
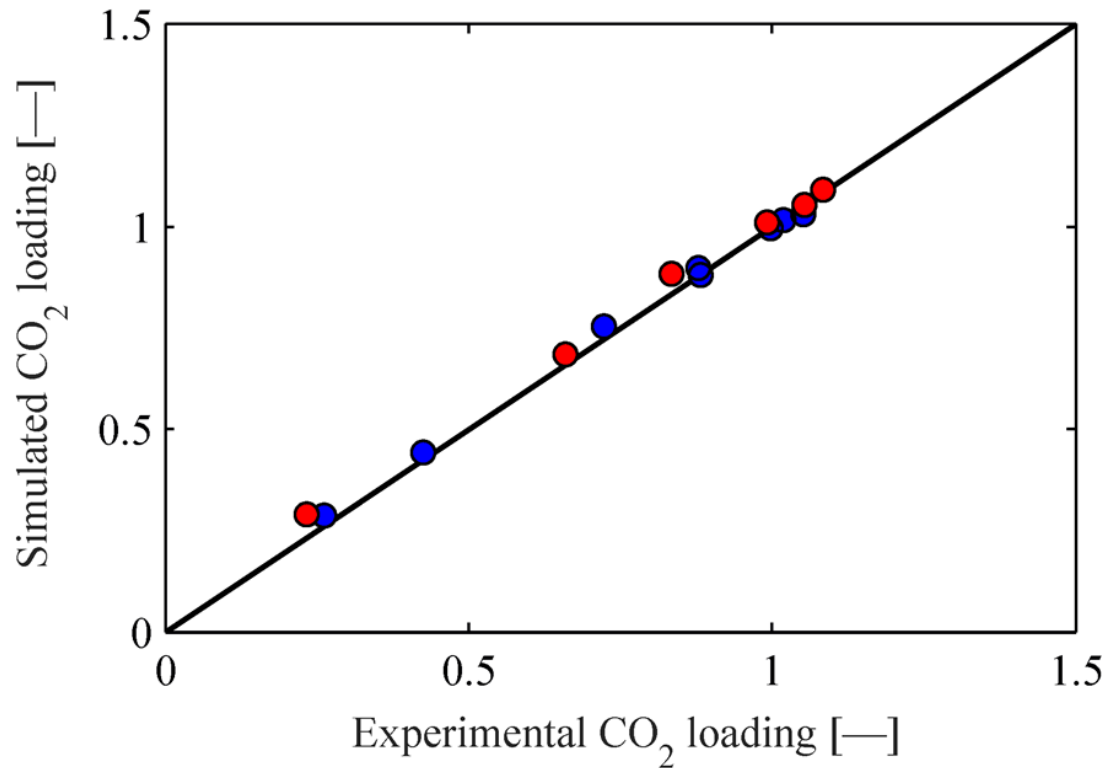
Wolery, (2002); Paoletti, *Pure Appl Chem*, 56, (1984): 491-522; Stern, *PhD Thesis*, (2013)

Hatton Group, *Int. J. Greenhouse Gas Control*. 2019, 82, 48-58.

# Thermodynamics modeling validation

CO<sub>2</sub> capacity/loading measurements at 50°C under different  $f_{\text{CO}_2}$  and  $c_{\text{Cu}}$

$$\text{CO}_2 \text{ loading} = x_{\text{C}} = \frac{c_{\text{C}}}{c_{\text{EDA}}}$$

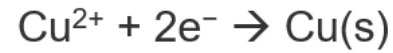


# Electrochemical Energetics

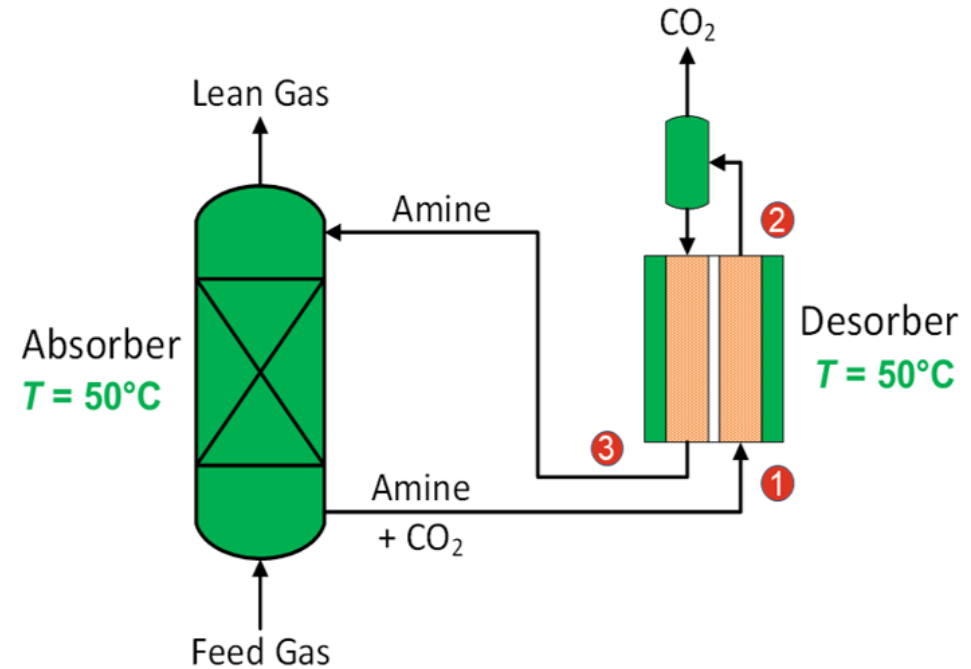
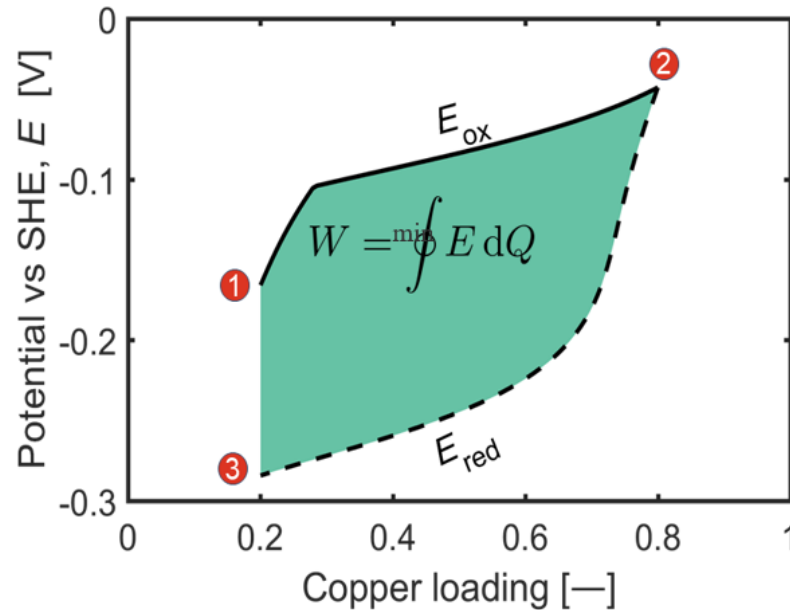
① to ② : Oxidation



② to ③ : Reduction



$T = 50^\circ\text{C}$ , 1m EDA + 0.5m  $\text{Na}_2\text{SO}_4$  + 0.25m  $\text{CuSO}_4$



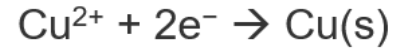
$$W_{\min} = \frac{1}{F_{\text{m,CO}_2}} \left( \int_{x_{\text{Cu}}} E_{\text{ox}} dI - \int_{x_{\text{Cu}}} E_{\text{red}} dI \right)$$

# Electrochemical Energetics

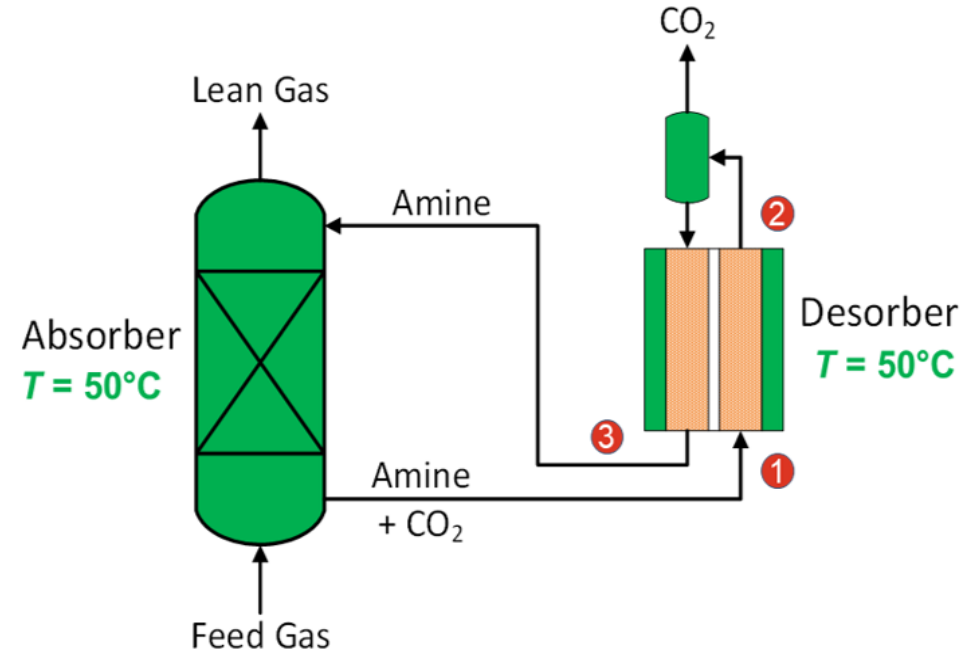
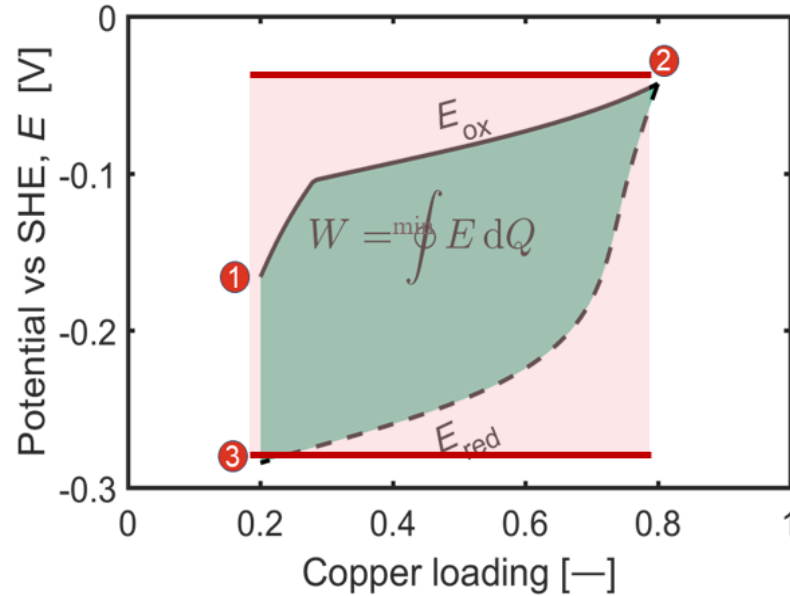
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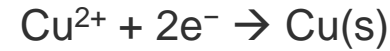
$$W_{\min, \text{corrected}} = \frac{1}{F_{\text{m,CO}_2}} \left( \int_{x_{\text{Cu}}} E_{\text{ox}} dI - \int_{x_{\text{Cu}}} E_{\text{red}} dI \right)$$

# Electrochemical Energetics

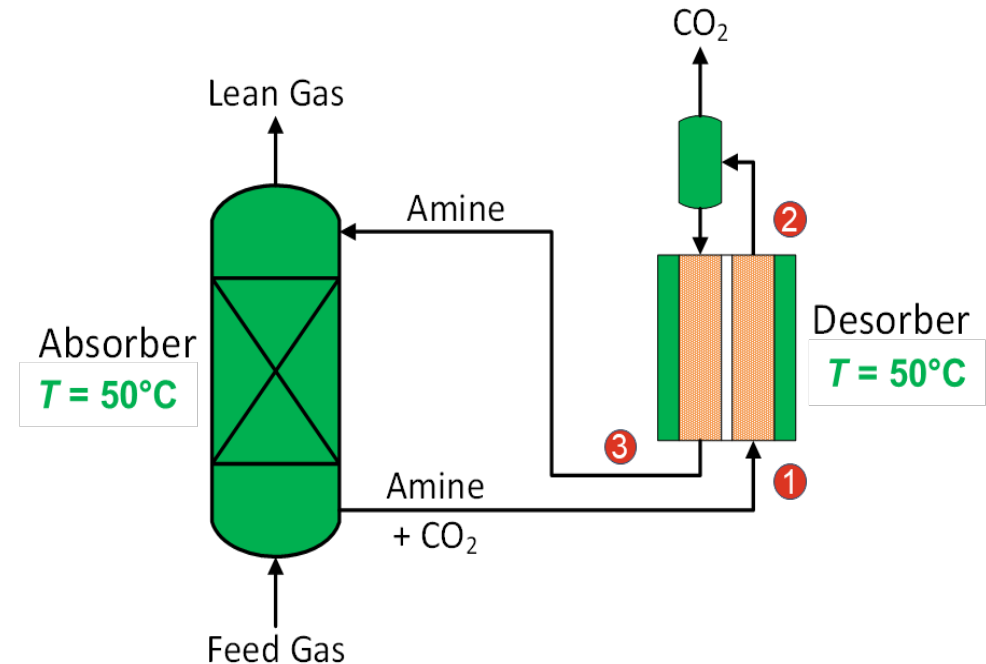
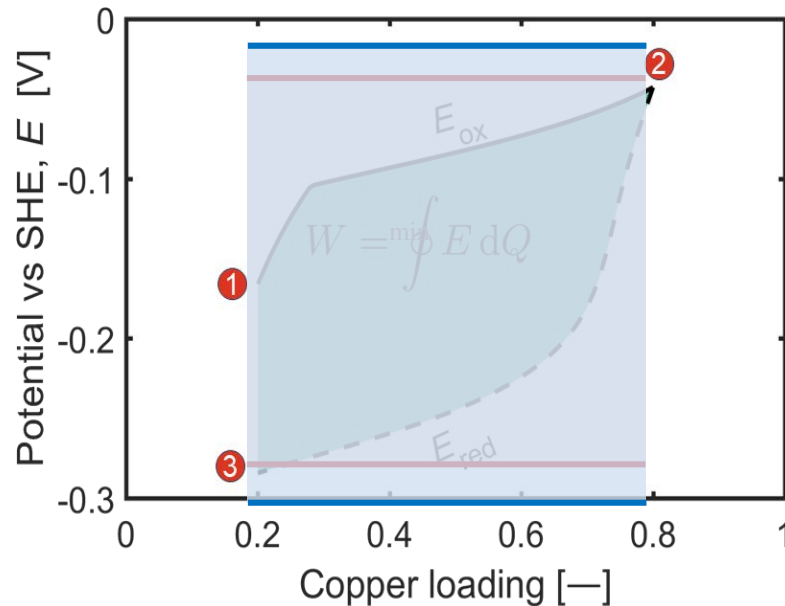
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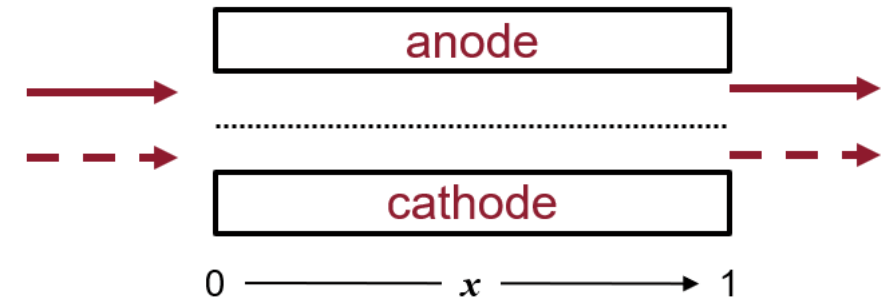
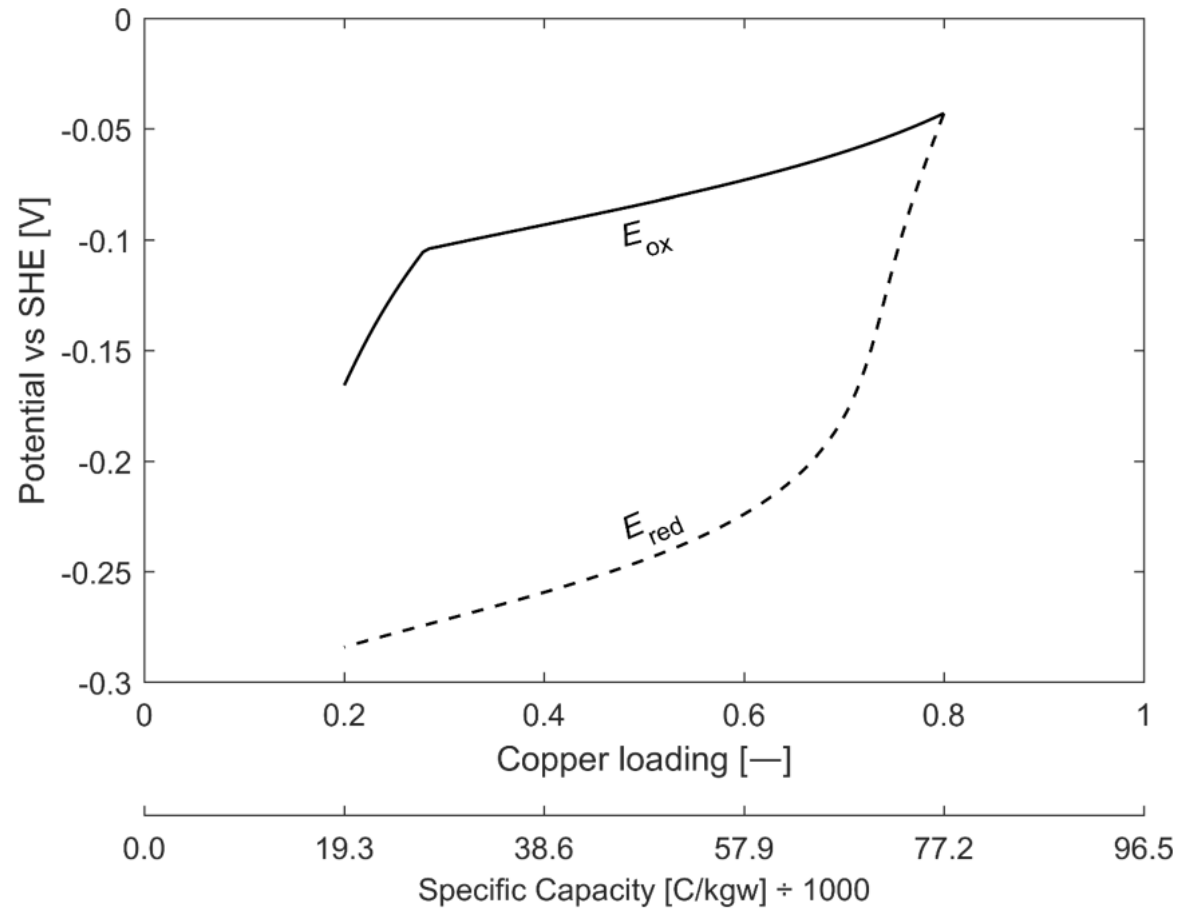
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$$W_{\text{EMAR}} = \frac{1}{F_{\text{m,CO}_2}} \left( \int_{x_{\text{Cu}}} E_{\text{ox}} dI - \int_{x_{\text{Cu}}} E_{\text{red}} dI \right)$$



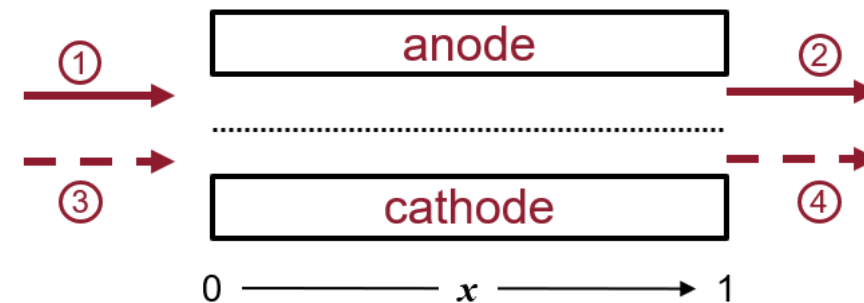
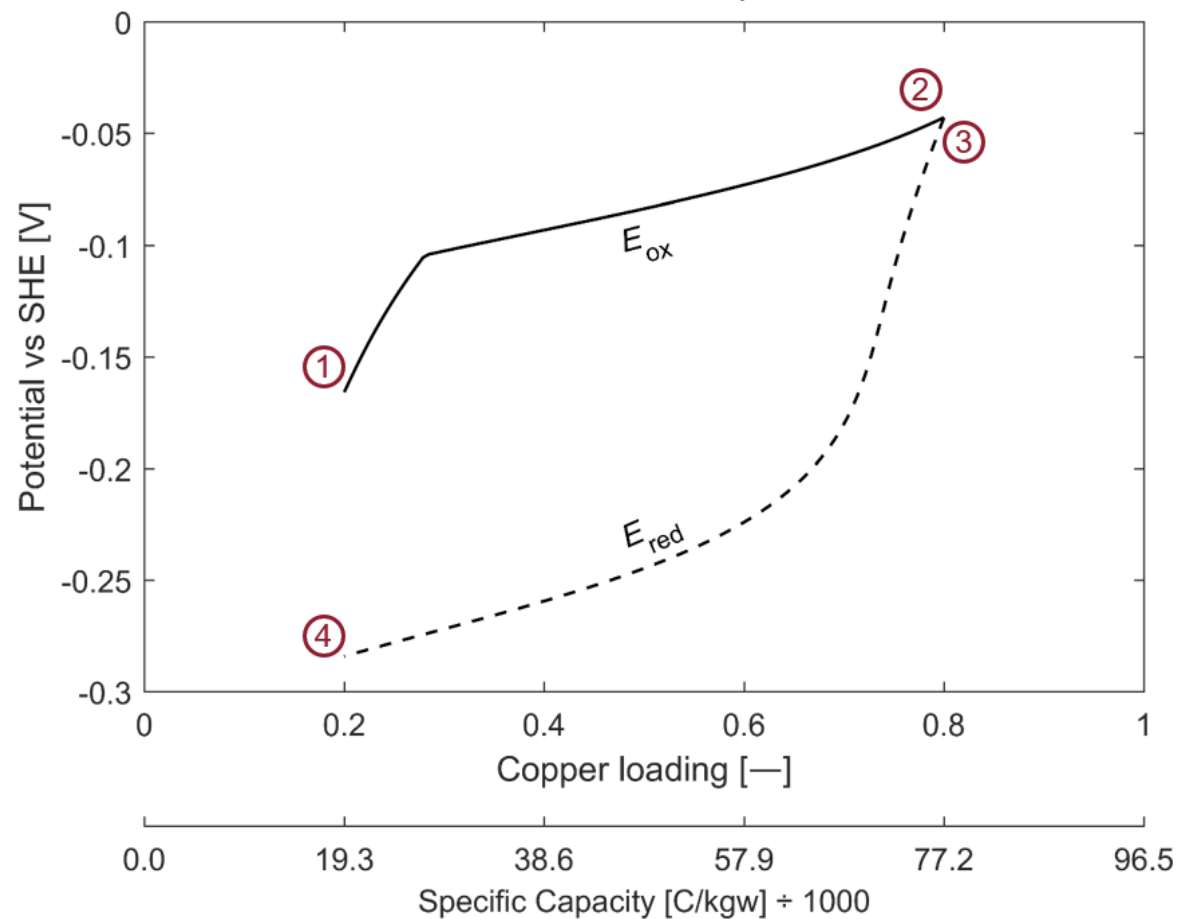
# Minimum EMAR Work: Co-Current Operation

$T = 50^\circ\text{C}$ , 1m EDA + 0.5m  $\text{Na}_2\text{SO}_4$  + 0.25m  $\text{CuSO}_4$   
Ionic current via  $\text{SO}_4^{2-}$  migration



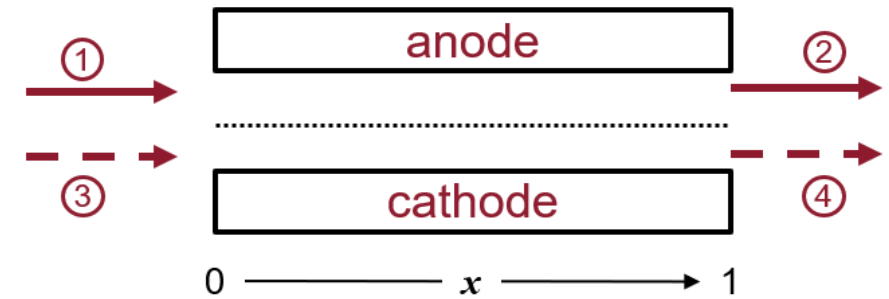
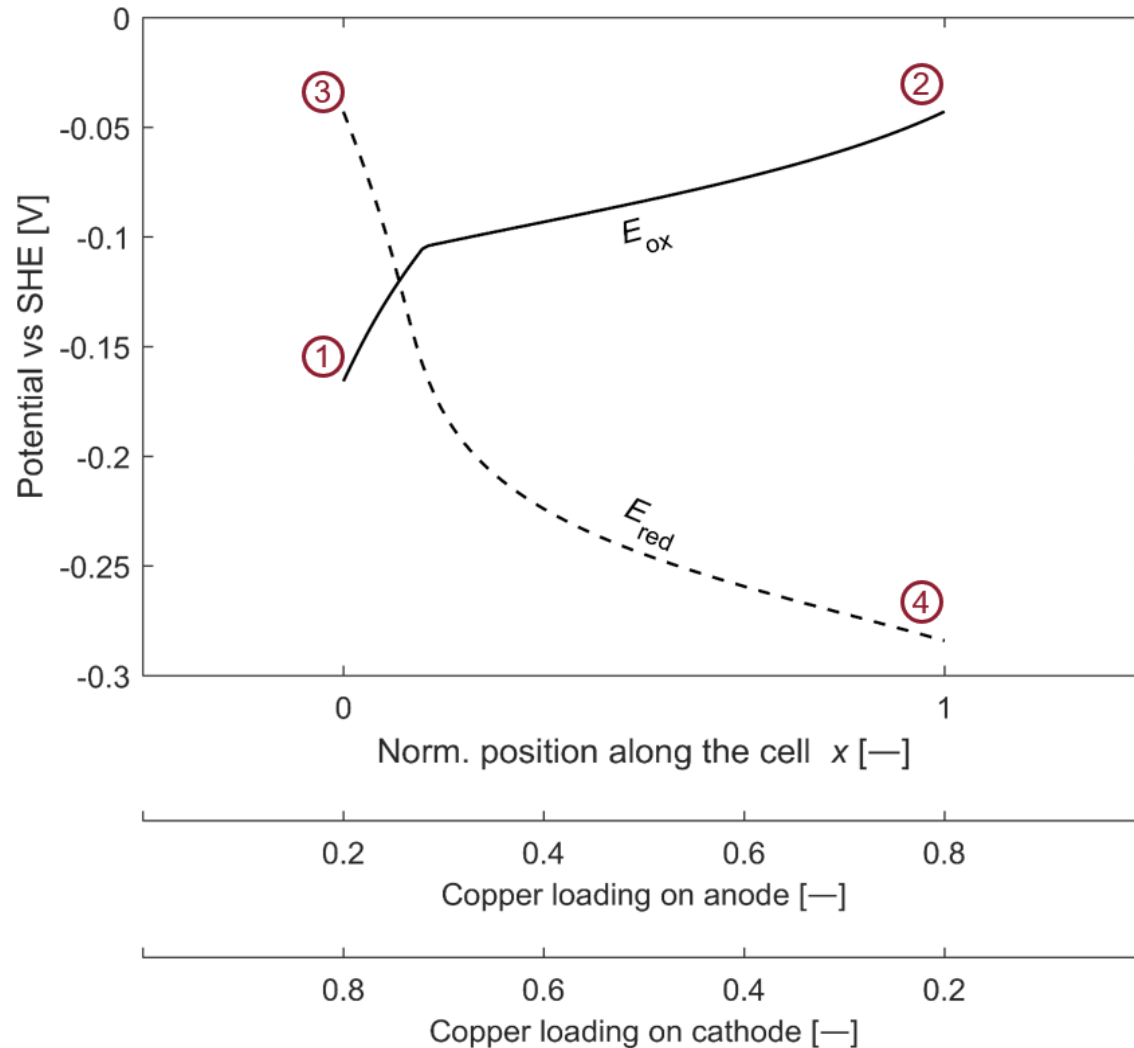
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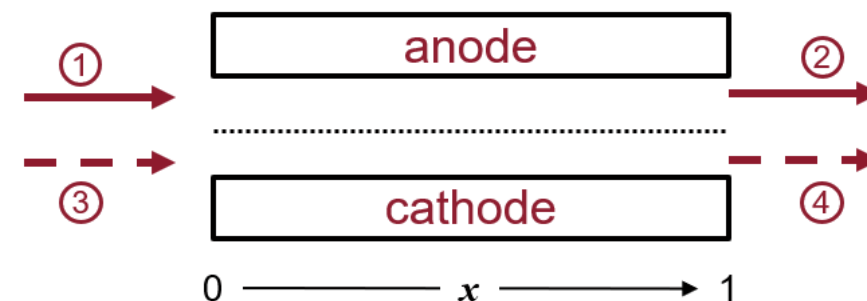
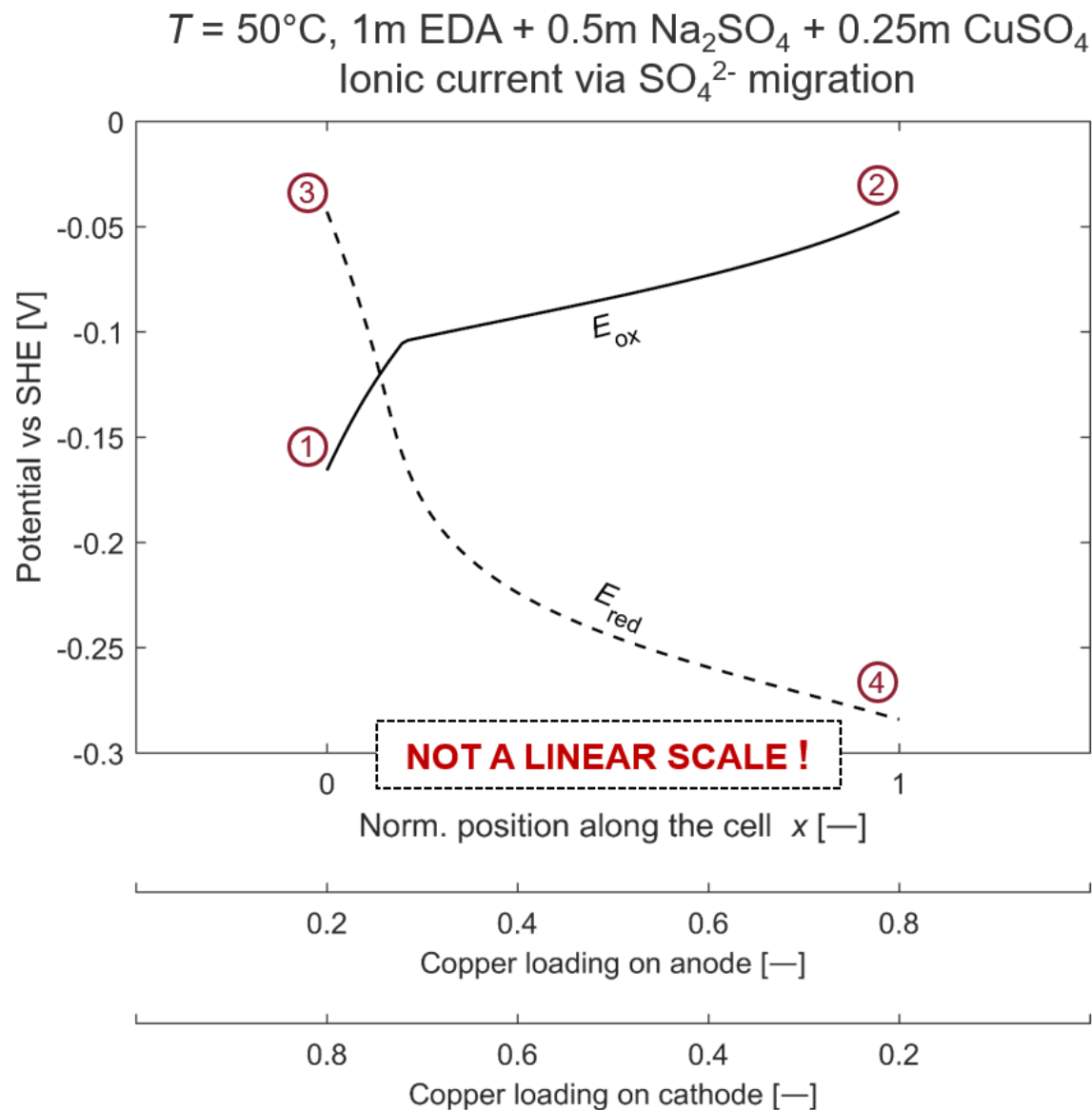


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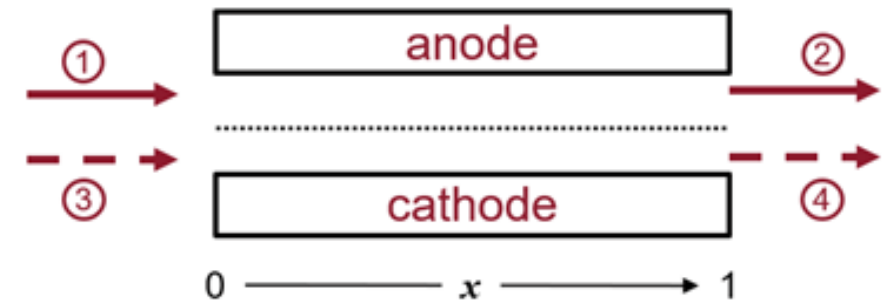
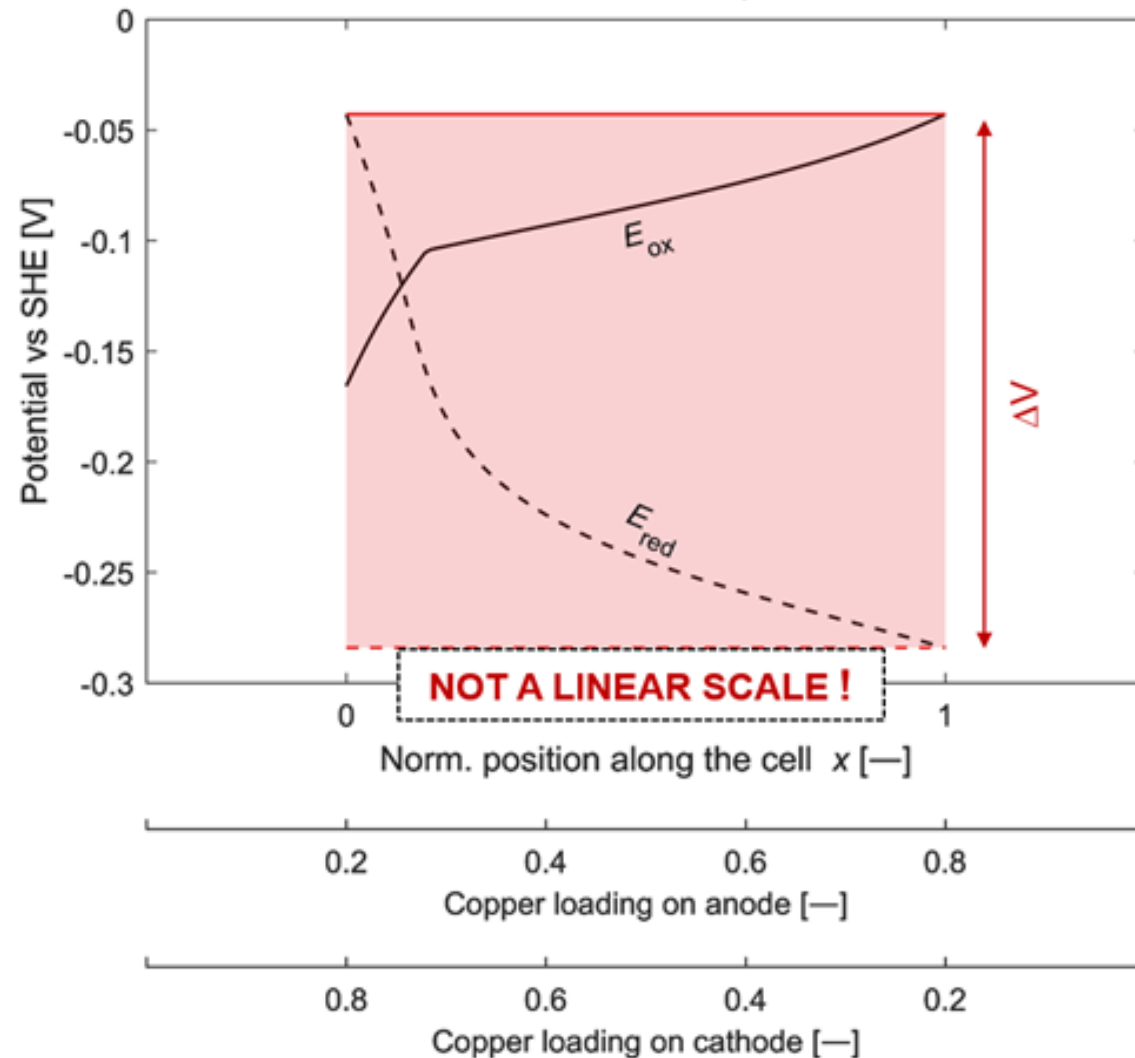


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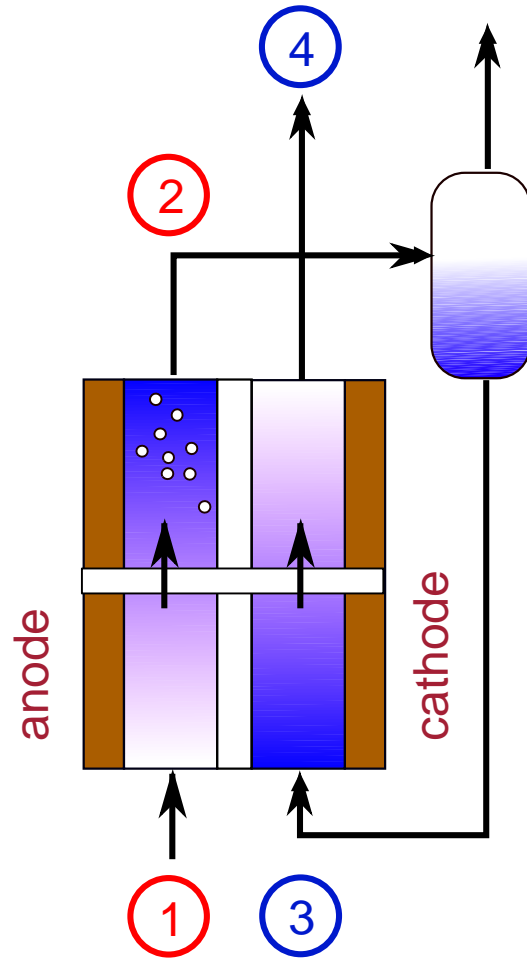


# Minimum EMAR Work: Co-Current Operation

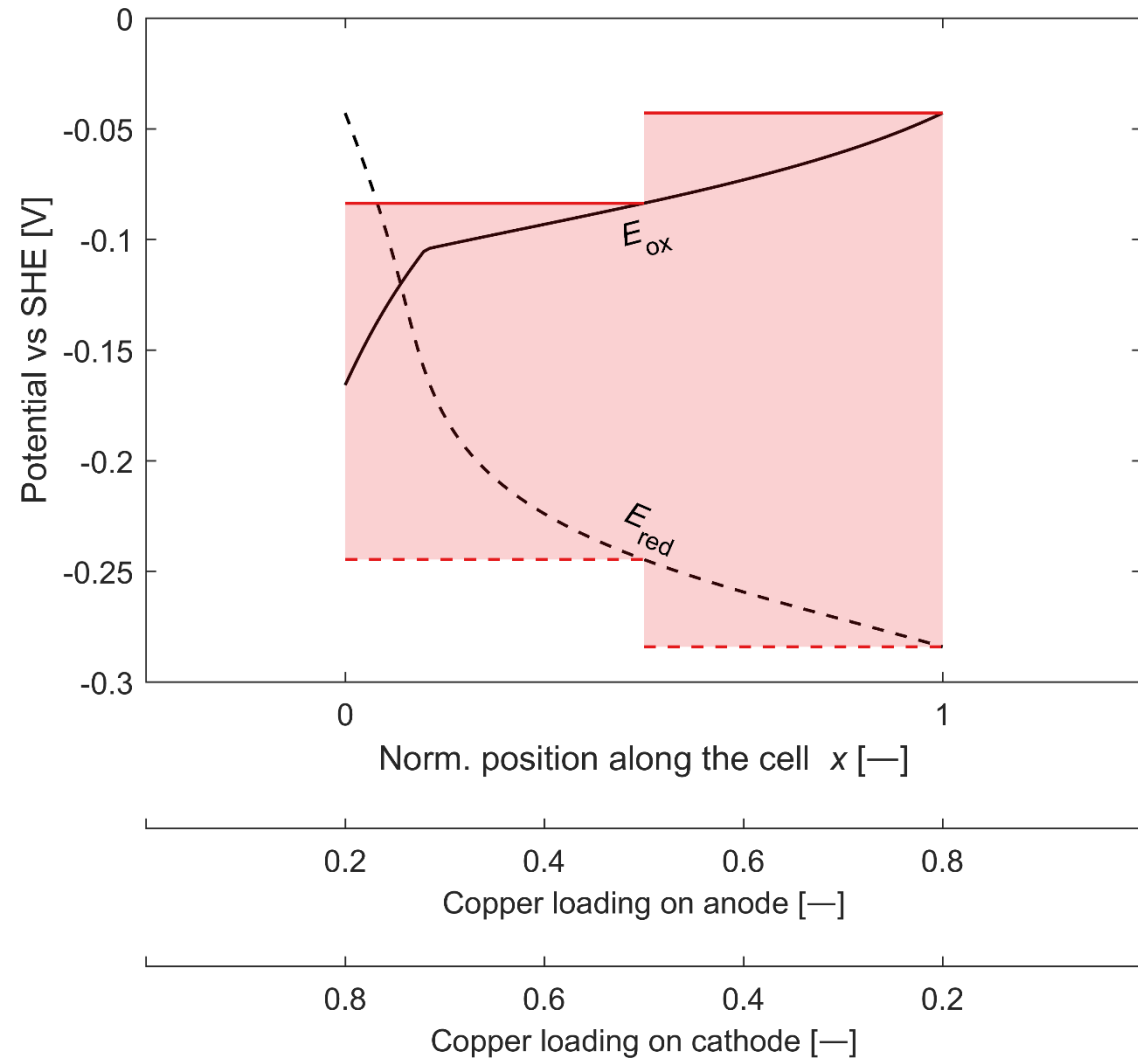
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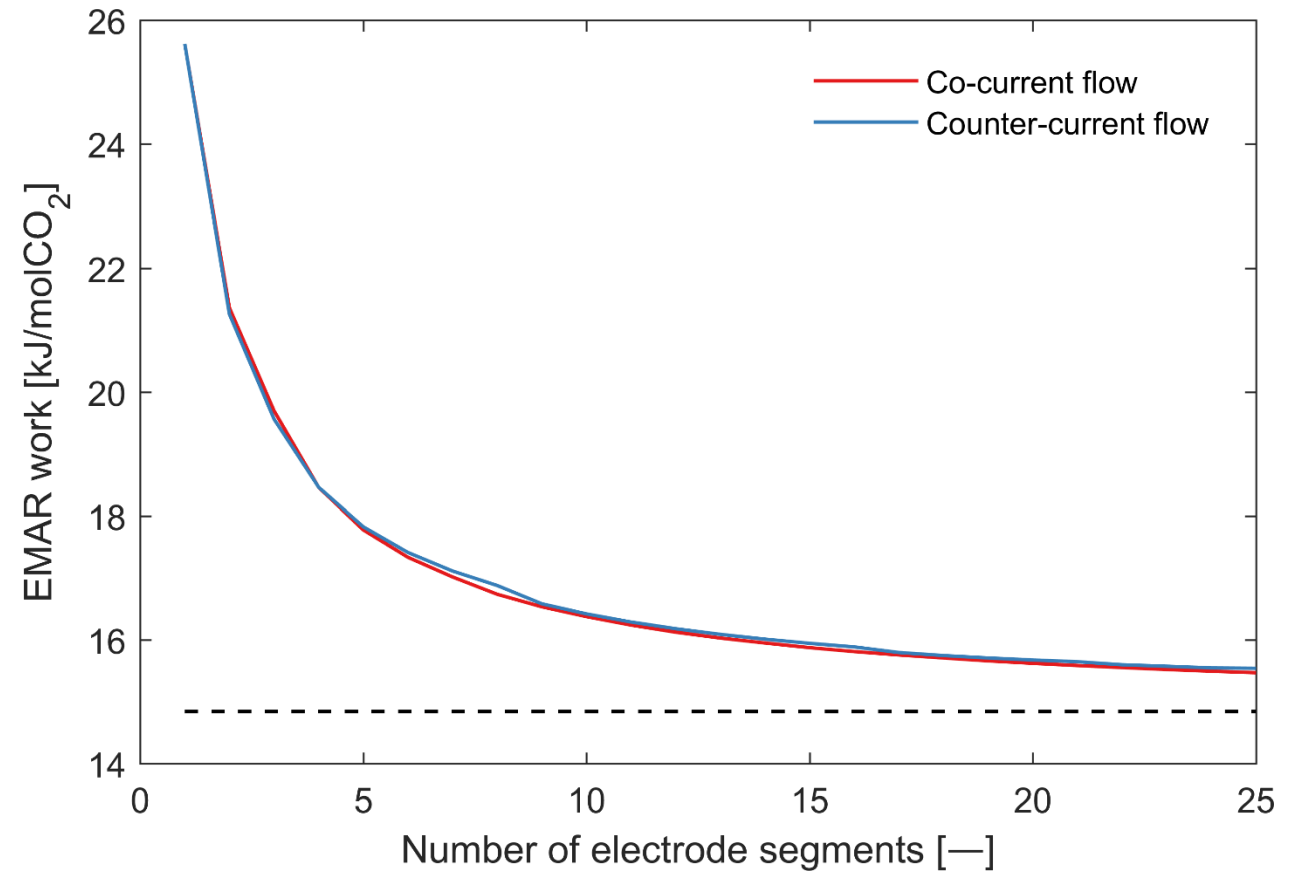
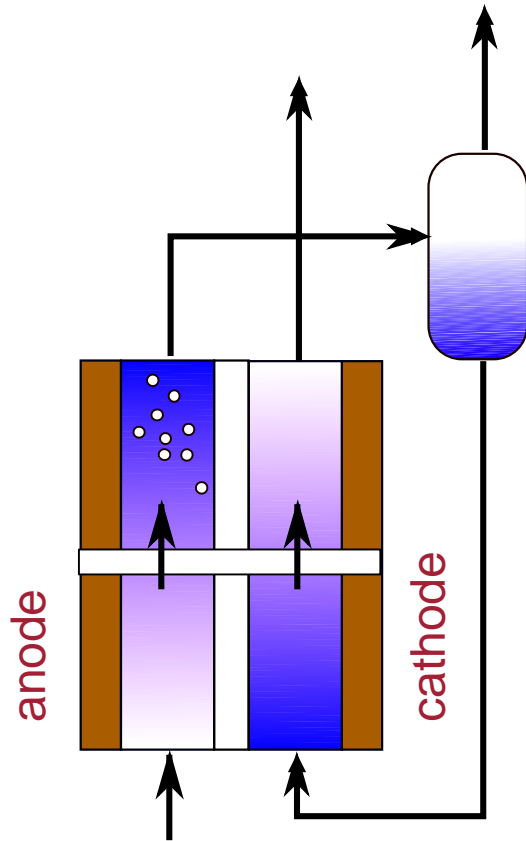
# Finite Electrode Overpotential: Segmented Electrodes



$T = 50^\circ\text{C}$ , 1m EDA + 0.5m  $\text{Na}_2\text{SO}_4$  + 0.25m  $\text{CuSO}_4$   
Ionic current via  $\text{SO}_4^{2-}$  migration



# EMAR Work with Segmented Electrodes



# Effect of Operating Parameters on Overall Energetics

## Base case

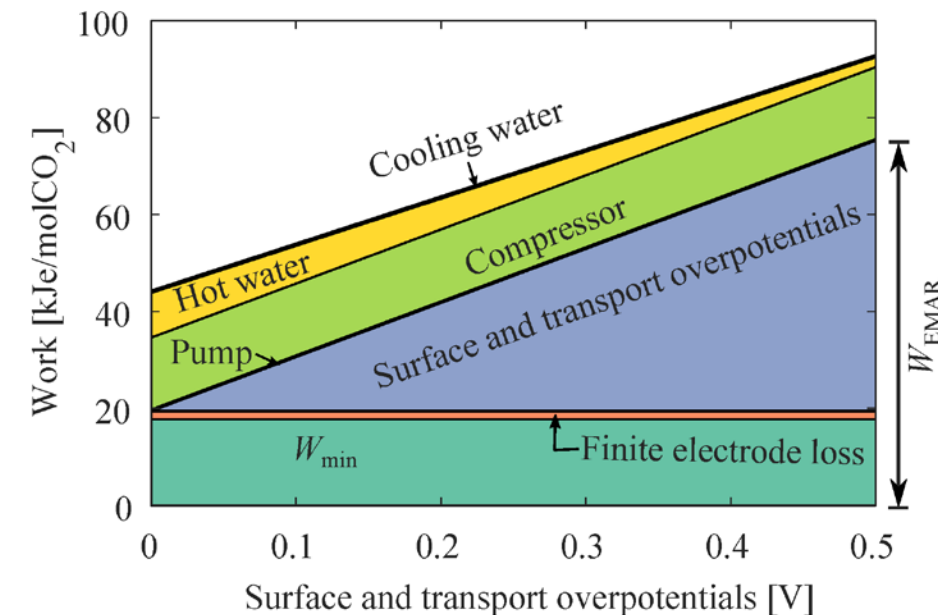
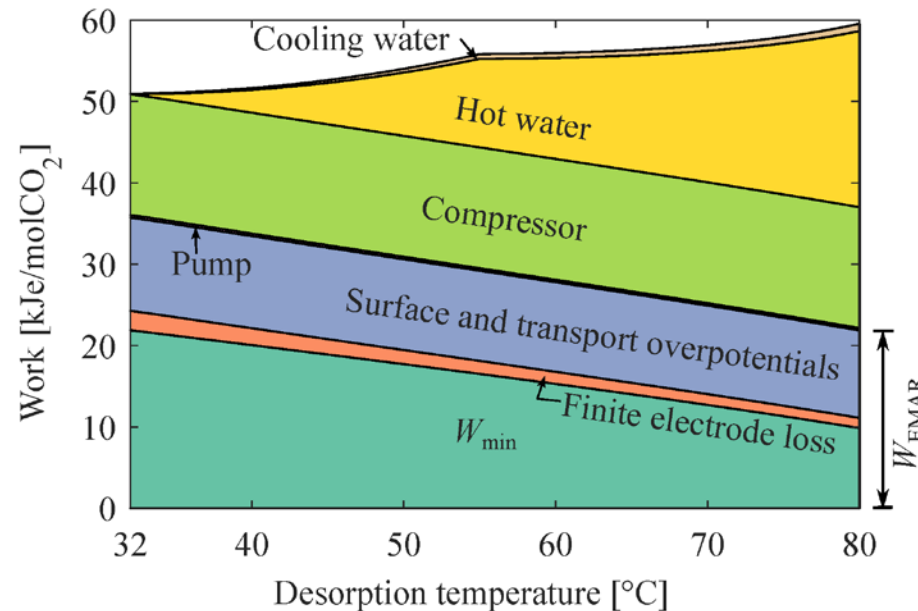
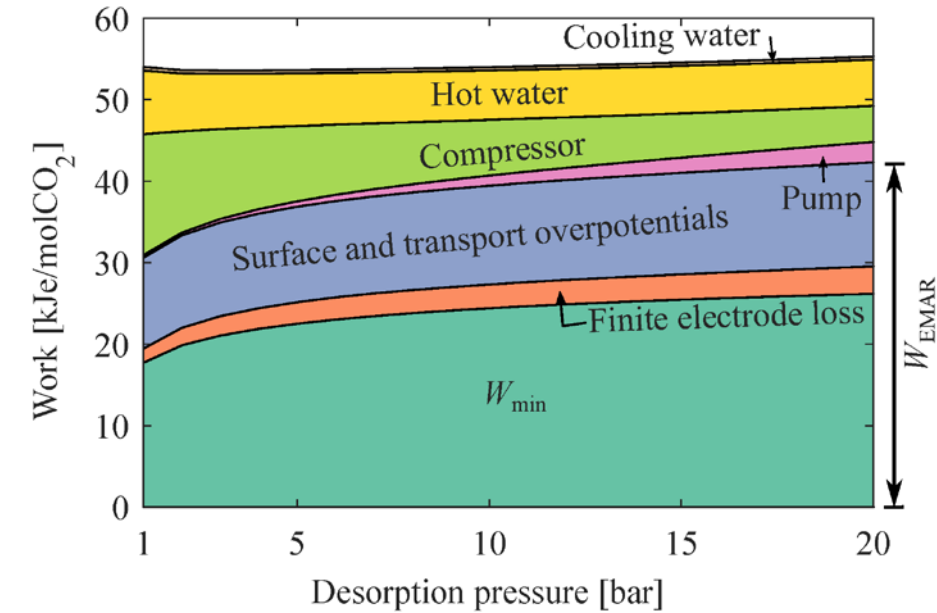
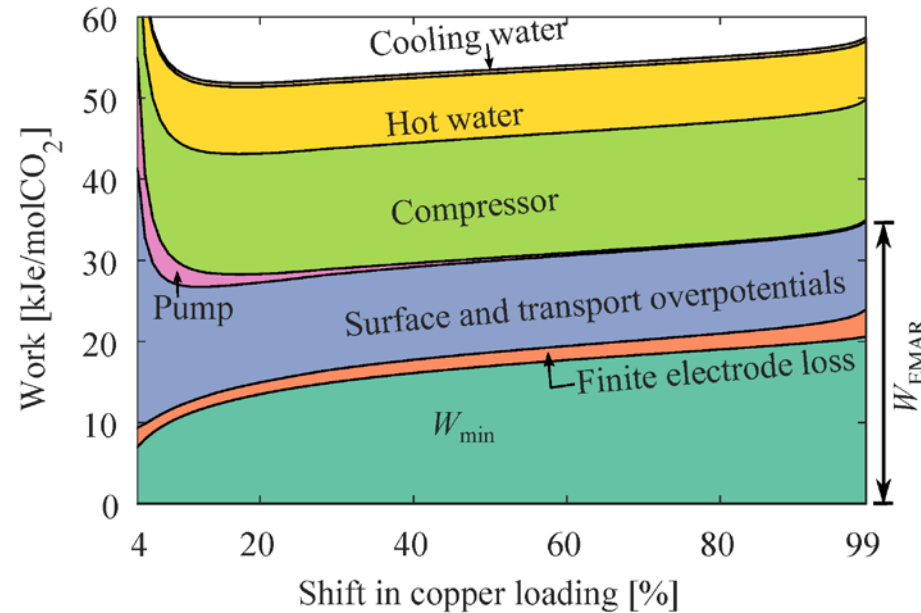
$$T_{\text{abs}} = 50^{\circ}\text{C},$$

$$T_{\text{des}} = 50^{\circ}\text{C}$$

$$\text{Cu Shift} = 60\%$$

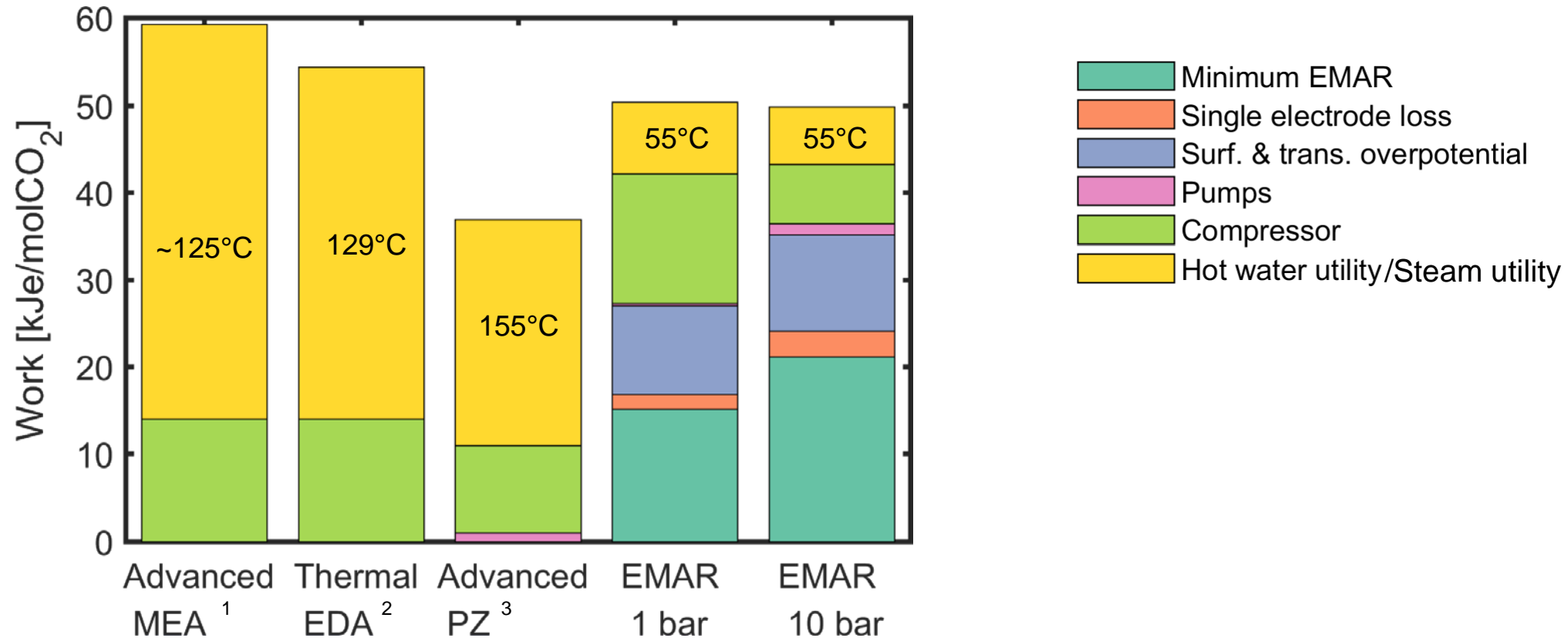
$$P_{\text{des}} = 1 \text{ bar},$$

$$\text{overpotential} = 0.1 \text{ V}$$





# Process Energetics comparison

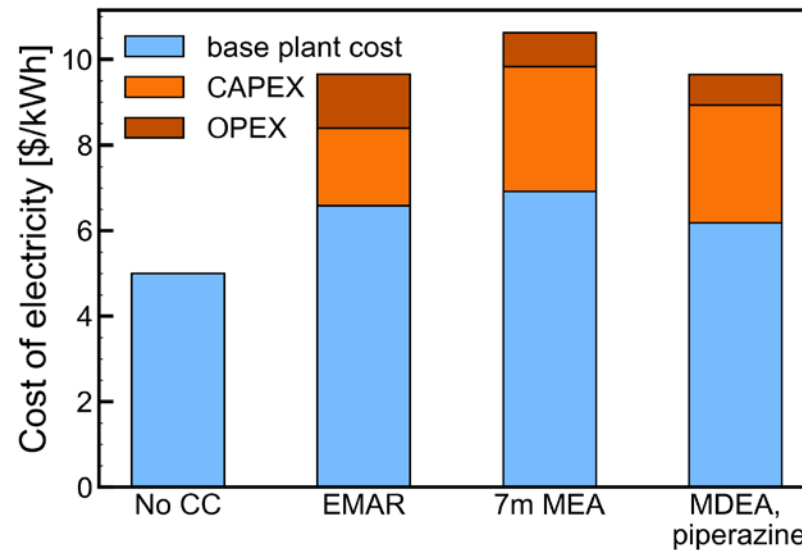
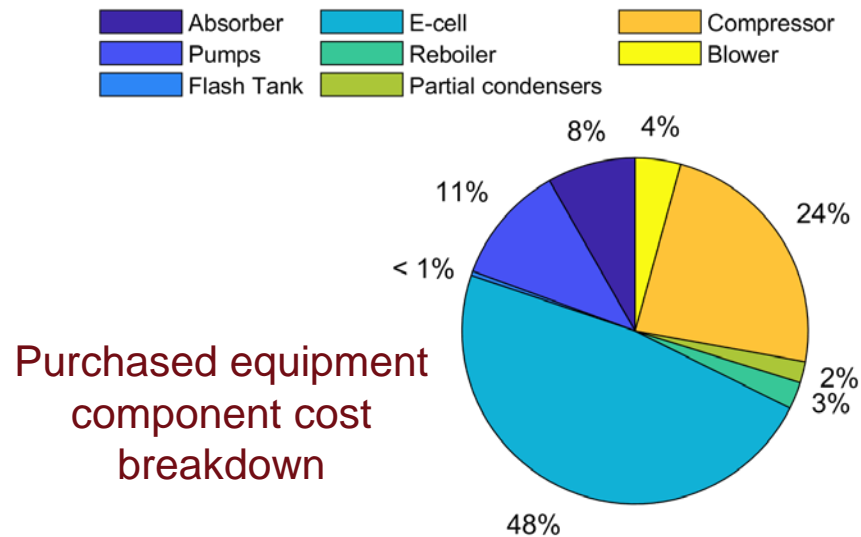
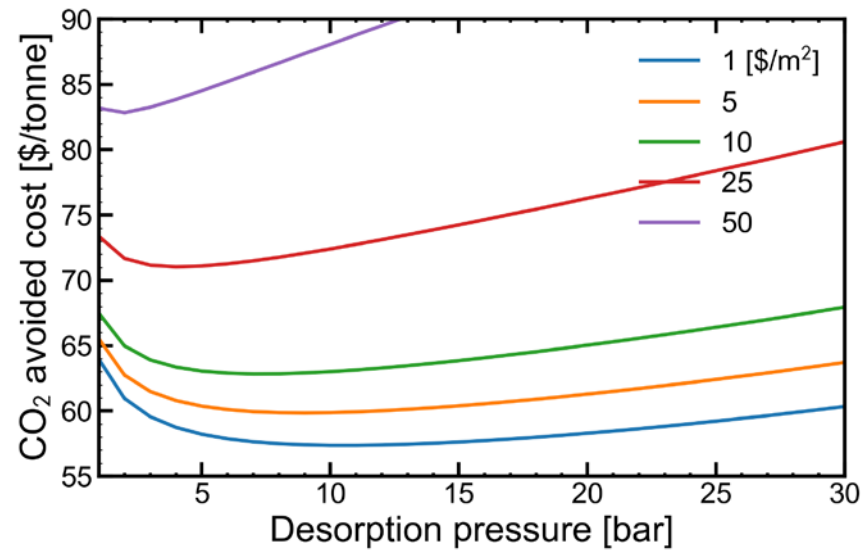
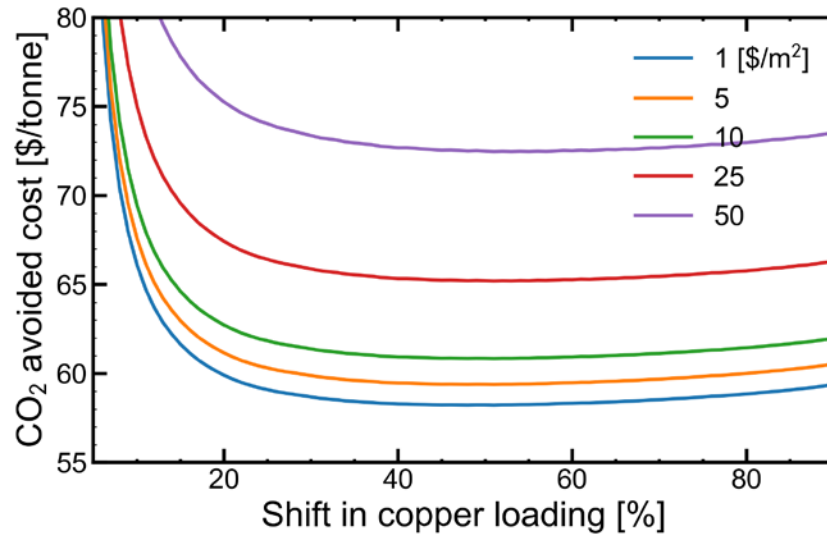


[1] Econamine process, Case10, Rev.2a, NETL (2013)

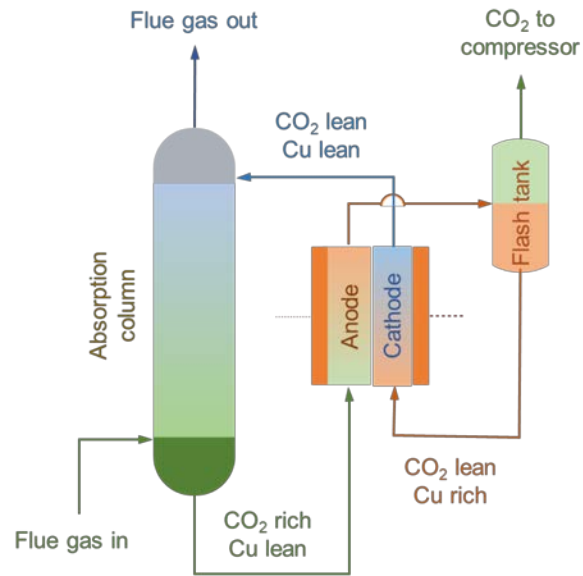
[2] Rabensteiner et al., *Int J Greenh Gas Con*, 27 (2014), 1-14

[3] Lin and Rochelle, *Chem Eng J*, 283, (2016): 1033-1043

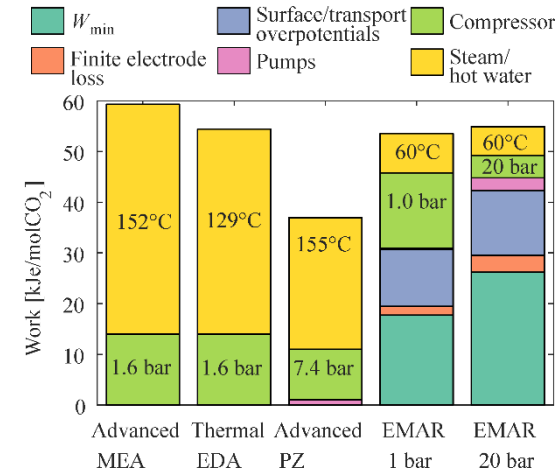
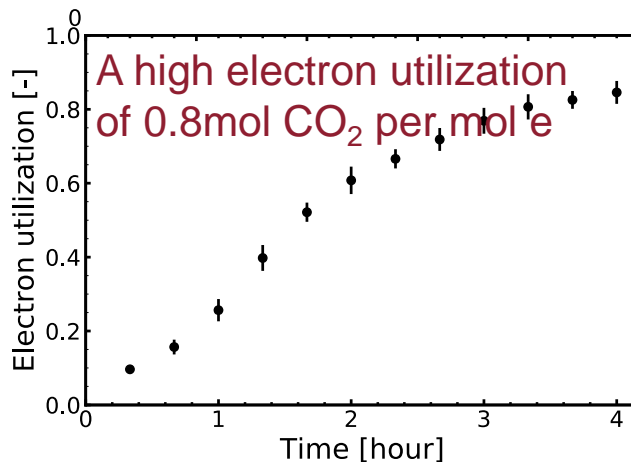
# Cost of Electricity and CO<sub>2</sub> Avoided



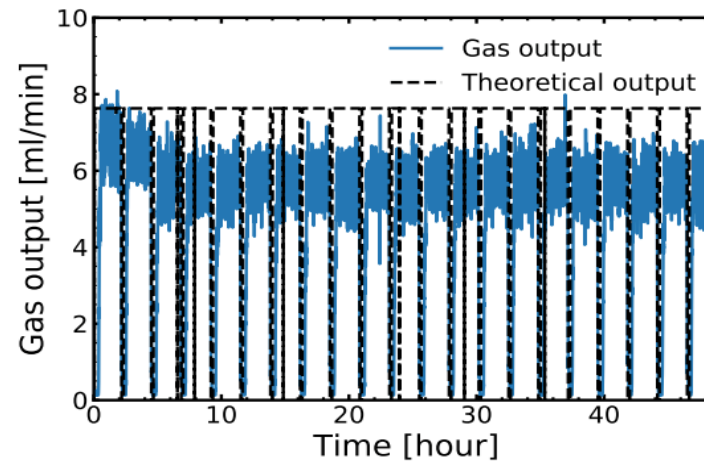
# Conclusion



EMAR is an alternative  $\text{CO}_2$  desorption at low temperature (less amine degradation) and with electricity (easier retrofit)



Favorable energetics and costs relative to conventional thermal amine processes



Effective and stable approach for flue gas  $\text{CO}_2$  capture

# Project Risks and Mitigation Strategies

Technical Risks	Probability	Impact	Risk Mitigation
CO <sub>2</sub> sorbents and metal ion systems unsuccessful	Medium	Low	Wide range of candidate sorbents available. Initial results are promising
Electrochemical cell models low in fidelity and do not permit optimization	Moderate	Low	Complexity of underlying mechanisms in electrochemical cell presents risk for modeling. Parametric experiments will generate sufficient data for empirical optimization.
Process found to be too sensitive for long-term operations and disturbances	Moderate	Moderate	Preliminary testing is encouraging. Degradation of electrodes or sorbents possible, but can be mitigated through design of electrode configurations

# Resource and Management Risks

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Resource Risks	Probability	Impact	Risk Mitigation
Cost of bench-scale system after optimization more expensive than planned	Low	Low	Most of the components of the system have been procured and operated in previous work, but the optimized system might involve more expensive equipment, especially for automation.

Management Risks	Probability	Impact	Risk Mitigation
Process performance reaches a plateau that does not satisfy DOE research goals	Moderate	High	The progress reports will allow the project team to evaluate the performance of the process and determine whether it is possible to explore new dimensions for performance improvements.

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