Flashback Measurements in Hydrogen Enriched Low Swirl Flames Using High Speed OH-PLIF

Pradeep Parajuli and Peter Strakey

National Energy Technology Laboratory, 3610 Collins Ferry Road, Morgantown, WV 26505, USA

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Presentation Outline

Motivational Factors and Background

- Issues with hydrogen gas turbine systems
- Potential of low swirl flames with hydrogen-enriched systems

Experimental Apparatuses

- High-repetition rate ns-pulse laser system
- An optically accessible laboratory-scaled, swirl-stabilized burner

Results and Discussions

- Characterization of low swirl-stabilized flame
- Flashback characterization in low swirl burner
- Effects of fuel composition and varying swirler geometries
- Jet-in-Cross-Flow experiments.

Summary and Ongoing Work

• Jet-in-cross-flow experiments, computational fluid dynamics (CFD) modeling.

Introduction

Hydrogen – a clean and sustainable energy source

- Significantly different combustion characteristics compared to natural gas – higher flame speed and adiabatic temperature
- Supports net zero carbon policy, however, NO_x emissions pose a problem with non-premixed systems
- Ultra-lean premixed hydrogen combustion has a great NO $_\mathrm{\mathsf{x}}$ reduction potential
- Higher flame speed increases the risk of flashback and equipment damage

Source: GE Gas Power

Introduction

- **Swirl-stabilized flames are well-known methods to stabilize premixed flames**
	- Low swirl burners (LSBs) have gained increasing attention
	- Increases flame intensity reduces the flame length
	- LSBs have non-swirling core surrounded by a swirling shroud and produce freely propagating lifted flames
- **OH-PLIF diagnostic technique – a well-known laser diagnostic tool to gain insight into flashback phenomena**

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• Study reported two peak values of turbulence intensities showing presence of inner and outer shear layer and credited its role for the flame flashback [1]

Objective of the current study:

Characterize the flashback process observed in a swirlstabilized, atmospheric-pressure burner with hydrogenenriched flames.

- Develop correlations
- Validate CFD models

Experimental Apparatuses – Laser and Imaging System

Laser system

- Pump laser: A ns-duration Nd:YVO4 laser (INNOSLAB, Model: IS400-2-L), P ~ 75 W @ 20 kHz-repetition rate emitting a unique 3 mm \times 8 mm rectangular beam
- Dye laser: Frequency-tunable dye laser (Sirah, Model: CREDO-DYE-N) filled with a solution of rhodamine-6G dye diluted in pure ethanol
- Excitation wavelength: 283.9 nm, $E \sim 0.05$ mJ/pulse

Imaging system

- Camera: A high-speed CMOS camera (Photron, Model: FASTCAM SA-Z)
- Intensifier: A high-speed intensifier (Invisible Vision, Model: UVi 1850-10 S25)
- UV lens (Cerco, Objectif UV, f/1.8)
- Filter

Experimental Apparatuses – Burner System

Burner configuration

- A 21.2-mm ID low swirl burner with optically accessible pre-mixer system
- Fuel (H $_{\rm 2}$ and CH $_{\rm 4}$) with 50%–90% H $_{\rm 2}$ by mole
- Thermocouple (inserted in pre-mixer unit) senses the rise in temperature and shuts off fuel

- Swirling vane angles (α) 26^o and 33^o.
- Perforated plate hole diameters 1.08, 1.12 and 1.16 mm.
- Blockage ratio (BR) 0.783, 0.767, and 0.75.
- Radius ratio -0.65 .

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Results and Discussion: Stable Flames

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Characterization of Low Swirl Burner Flame – Variation of Fuel Compositions

Effects of Pre-mixer Velocities (V)

- Velocity varied: $5.5 \le V \le 10$ m/s
- Lift-off length (L) tends to increase linearly with Velocity
- The local gas velocity is increased compared to flame speed and becomes less flashback prone

Effects of Hydrogen Content (X_{H2})

- \cdot Increasing X_{H2} tends to decrease lift-off length and increase the chances of flashback – due to a increase in flame speed
- Expected rise of flame temperature as hydrogen flame is hotter than methane flame at same ϕ

Effects of Equivalence Ratio ϕ **on Stable Flames**

- Increasing φ decreases *L*, i.e., it brings the flame closer to the burner surface, increasing the risk of flashback
- Increasing $φ$ increases flame speed
- Lifted-to-attached flame transition can be observed
- OH-PLIF signal increases with increasing ϕ

70%H² /30%CH⁴ -air flame, V = 7.5 m/s

Investigation of Flame Flashback Events

Flashback Characterization in Low Swirl Burner

Experimental test conditions: $5 \le V \le 10$ m/s and $50\% \le X_{H_2} \le 90\%$

- At low ϕ or H₂, the flame is lifted and has V shape.
- Increasing ϕ or H₂ pulls the flame closer to the tube exit; however, the general shape remains unchanged.
- Significant change in flame shape occurs at $\phi = 0.65$ or H₂ = 75%.
- High-speed OH-PLIF images show intermittent burning in the outer shear layer.

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Changes in flame shape and stabilization pattern as a function of ϕ or H_2 at V = 10 m/s

Investigation of Flame Flashback Events

1 kHz frame rate (100 msec video)

Flashback initiation

• Burning of outer shear layer pulls the flame upstream into the nozzle.

Flashback propagation inside the nozzle

• Inner shear layer above the center channel wall (between swirled and unswirled flows) facilitates upstream flame propagation inside the nozzle.

Post-flashback flame holding

- Once a part of flame is attached to the rim of the swirler, it ignites the incoming fresh mixture (likely along the inner shear layer) forming a conical flame
- The flame structures anchor inside the mixing tube between the swirling and non-swirling regions.

70%H² /30%CH⁴ -air flame, = 10 m/s

Effects of Fuel Composition

- **As XH2 increases, the burner system is more prone to flashback**
- **Φ_{FB}** decreases linearly with an increase in X_{H2} **in the reactant mixture**

- **As V increases, the flashback resistance of the burner system increases**
- **ϕFB increases linearly with an increase in pre-mixer velocity**

Effects of Varying Swirler Geometries

- Dependence of ϕ_{FB} on X_{H_2} for three different perforated plated hole diameters (d) keeping $'a'$ fixed at 33°.
- An increase in '*d'* decreases the blockage ratio which increases the flow via the center-body and the burner system becomes less flashback prone.

- Another interesting observation is on the slope of the flashback lines which shows a greater negative slope with increasing '*d'*
- The error bar represents a 2-sigma standard deviation of φ _{FB} obtained from five different experimental tests

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Effects of Varying Geometry

- **Dependence of ϕFB on XH2 for two different swirler vane angles keeping perforated plate hole diameter (d) fixed at 1.16 mm.**
- **ϕFB increases with an increase in** α **especially at lower pre-mixer velocities of 5 and 7.5 m/s.**
- **Higher** α **may be increasing the core flow.**
- **ϕFB lines almost overlap for two** α**s at V = 10 m/s**

- **Objective - Characterize flashback and flameholding with a jet-in-cross-flow fuel injection strategy. Validate CFD codes.**
- **JICF used in conventional swirlers as well as micro-mixers for fuel injection.**
- **Swirler removed and flat plate installed on back side.**
- **0.063" fuel jet located in flat plate.**
- **Lean flame attached to burner tube exit.**
- **Ramp up equivalence ratio while maintaining H2/CH4 ratio and air flow.**

Jet in Cross Flow Experiments

70%H² /30%CH⁴ -air flame; ϕFB =0.665; at V = 4 m/s

Jet in Cross Flow Experiments

Time-Averaged OH PLIF Images After Flashback

- As momentum flux ratio increases, the flame detaches from the fuel port completely and stabilizes in the form of a lifted flame.
- As r increases, the fuel jets penetrate further into the crossflow and the combustion zone shifts away from the fuel ports.

Jet in Cross Flow Modeling

- **Fluent Large Eddy Simulation.**
- **9M cells (0.2 mm).**
- **Skeletal methane-air mechanism (16 species, 45 reaction).**
- **No turbulence chemistry interaction.**
- **BCD for momentum, SOU for scalars, 2nd ddt implicit PB solver.**
- **Chemiluminescence sub-mechanism from Petersen.**

```
H+O+M=OH*+M 3.1E+14 0.0 10000.
OH*+H2O=>OH+H2O 5.92e12 0.5 -861.
OH*+H2=>OH+H2 2.95e12 0.5 -444. 
OH*+O2=>OH+O2 2.1e12 0.5 -482.
OH*+OH=>OH+OH 1.5e12 0.5 0.0
OH*+H=>OH+H 1.5e12 0.5 0.0
OH*+O=>OH+O 1.5e12 0.5 0.0
OH*+N2=>OH+N2 1.08e11 0.5 -1238.
OH*=>OH 1.4e6 0.0 0.0
!chemiluminescent reactions
!J. Hall, E. Petersen, Int. J. Chem. Kin. 38 (2006) 714–724.
!
```


Comparison to Fluent Simulations

- **Simulations at highest flowrate shows fuel jet impingement on opposing wall and "horseshoe" shaped flame.**
- **Limits effectiveness of using planar techniques.**
- **Integrated line-of-sight chemiluminescence more useful.**

 1.25 el 1
6.23 el 2

Mean Chemiluminescence (line-of-sight integrated) 436611 3.74611 3.12e11 2.49e11
- 1.87e11

Mean OH slices*

Jet in Cross Flow Experiments

Comparison to Fluent Simulations

- **CFD results qualitatively similar.**
- **Testing sensitivity to air inflow boundary conditions.**
- **Testing PaSR combustion model.**

Mean Chemiluminescence $(line-of-sight integrated)$ $V = 5 m/s$, $H = 70\%$, $\Phi_{FB} = 0.73$

$V = 3$ m/s, H = 70%, $\Phi_{\text{FR}} = 0.5$

Summary and Ongoing Work

- **OH-PLIF fluorescence provides an excellent marker of the lift-off length and can capture transient phenomenon.**
- **Flashback occurs at high ϕ or XH2 when burning occurs in the outer shear layer and the leading flame brush ingresses into the pre-mixer tube.**
- **Post-flashback flame is anchored on the rim of center-body between the swirling and non-swirling regions with conical flame front.**
- **Additional work includes CFD model validation at experimental conditions.**
- **JICF experiments and CFD modeling continuing.**

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CONTACT: Pradeep Parajuli pradeep.parajuli@netl.doe.gov

(304) 285-1615

