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Thermal Management of Zero-to-Near-Zero CO₂ Emission Gas Turbines

Tom I-P. Shih

School of Aeronautics and Astronautics, Purdue University

Mark Bryden Ames National Laboratory, U.S. Dept. of Energy

Richard Dalton and John Crane

National Energy Technology Laboratory, U.S. Dept. of Energy

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Our nation's goal to reach 100% carbon-free electricity by 2035 opens many challenges and opportunities for gas turbines.

There are many pathways to transition from what we have today to one that is 100% carbon free!

For the gas-turbine hot section:

- Need to continue pushing the limits of

 all technologies: combustion (RDE), aerothermal, materials, control
 all fuels and working fluid: NG, NG + H₂, H₂, ammonia, ammonia + H₂, ...; sCO₂ for reliable operation, increased <u>efficiency</u>, and increased service life.
- On GT aerothermal, the need for any fuel or working fluid continues to be
 - Reducing aerodynamic loss for efficiency.
 - $\circ~$ Reducing cooling flow for efficiency and service life.



Challenges and Opportunities for Aerothermal: NG \rightarrow NG + H₂ \rightarrow H₂

RDC: thermal management **sCO2:** efficient HX



Objective:

Advance thermal management of gas turbines that enable near-zero to zero CO_2 emissions.

Approach:

- **1** Assess and encapsulate the literature/knowledge base.
- 2 Assess and develop tools.
- **3** Advance fundamentals.
- 4 Advance applications.
- 4 Work and coordinate with NETL on the research.



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Assess & Encapsulate the Literature

Turbine Aerodynamics, Heat Transfer, Materials, and Mechanics, 2014.

This is the first book that integrates design, aerothermal, mechanics, materials, and failure modes for the turbine component.

Gas Turbine Compressors and Fans: Fundamentals, Design, and Analysis, 2024 or 2025



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PART I: The Compressor and Fan Systems

Forward: Alan Epstein (MIT, P&W), Frank Haselbac (AirBus)

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Steve Wellborn

Tom Shih

Vigor Yang

- 1.1 Intro to Gas Turbines
- 1.2 Intro to compressors and Fans
- 1.3 Challenges and Opportunities

Chapter 2: Design-Build-Test Process - Steve Wellborn (Rolls-Royce)

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- 2.4 Multidisciplinary Design Process
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- Chapter 4: Aerodynamic Design of Fan Rotors for Ultra-High-Bypass Ratio Turbofan Engines – Ernersto Benini (U. of Padova) and Aspi Wadia (GE)
- Chapter 5: Computational Fluid Dynamics for Turbomachinery Feng Liu & Yalu Zhu(UC Irvine)
- Chapter 6: Computational Solid Mechanics and Fluid-Structure Interactions Wei Zhao (Oklahoma State U.), Sameer Mulani (U. Alabama), Rakesh Kapania (Virginia Tech), and Mani Sadeghi (Pratt & Whitney)
- PART III: Physical Processes in Compressors and Fans
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Recent and Current Efforts

Tools

- Hybrid LES-RANS methods (2 papers in IJNMF in 2021 and 2022)
- ROM for tapered cooling ducts in 1st stage turbine (2024 IGTI).
- ROM for conjugate HT in conical cooling ducts with tip leakage in 2nd stage turbine.
- Physics-based ROM for internal cooling of vane & blade w/ 3-D effects.
- Physics-based ROM for internal cooling of RDC
- ROM + Optimization + machine learning for design

Fundamentals Applications







Max errors in ρ , V, and T relative to steady RANS are 4.9%, 7.1%, 0.9%, 4.7% for a ribbed duct.

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Recent and Current Efforts

Tools

Fundamentals

hot gas T_h $T_c \wedge q_s''$ cooling air T













Revisit film cooling dimensionless parameters (2024 IGTI \rightarrow accepted JTM)

Applications

- Internal cooling w and w/o rotation and taper (2024 IGTI \rightarrow JTM) ٠
- Internal cooling of RDC walls. ٠
- Transition duct from RDC to turbine ٠
- New film-cooling holes: downstream VG with cross flow; ٠ Y-shaped hole (Doug Straub & Justin Weber)
- New film-cooling design paradigms from machine ٠ learning (w/ Doug Straub & Justin Weber)
- Biot no. analogy to study TBC in sCO2 turbine cooling ٠ (w/ Matthew Searle)
- Rotationally & externally-induced rim-seal ingress • (2papers in Energies in 2023).
- Blade-tip leakage in a 1.5 stage turbine via RANS and ٠ LES (2025 IGTI, ...)





Hybrid LES-RANS and RANS Study of Tip Leakage Flow in a 1.5 Stage Power-Generation Gas Turbine under Engine-Relevant Conditions

Purdue: DoE Ames Lab: DoE NETL: Adwiteey Shashodia and Tom I-P. Shih Mark Bryden John Crane

Acknowledgement: Jay Kim



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LES-RANS of Tip-Leakage Flow in a 1.5 Stage Turbine

- Introduction
- Literature Review
- Objective
- Problem Description
- Problem Formulation
- Numerical Method of Solution
- Verification and Validation
- Results
- Summary and Conclusions



In gas turbine, there is a gap between the rotating blades and the shroud.

- \approx 1 to 2% of blade span during cold start
- hot gas flows across this gap

Tip-leakage flow (TLF) accounts for 1/3 of total turbine stage efficiency loss^{(Booth, 1985).}

Thus, want to **reduce TLF.** 1% decrease in tip gap/span can improve stage efficiency by 2%^(Yoon, 2013 & Maesschalck, 2014)







Previous Work

Parameters Studied	Range	Experiment/ CFD
Exit Mach Number	Subsonic, Supersonic	Wheeler et al. (2009 & 2012); Zhang & He (2011); Zhang et al. (2011)
Tip Gap size	0.5 to 2% blade span	Yoon et al. (2014) ; Zhang et al. (2011); Maesschalck et al.(2014); Rahman et al. (2013)
Rotor RPM	1200 to 12000 RPM	Rezasoltani et al. (2015); Rahman et al. (2013)
Tip Design	flat, many variations of squealer, contoured	Mischo et al. (2008); Mischo et al. (2008); Maesschalck et al. (2014 &2016); Zhang & He (2013)
Film-Cooling Design	blade tip, blade's PS, shroud	Rezasoltani et al. (2015); Tamunobere and Acharya (2016); Andreoli V et al. (2019)



Gaps in the Literature

CFD:

 No LES or hybrid LES-RANS studies to date on the details of the flow in the tip gap including the effects of stator, stator-rotor interaction, and downstream stator.

Benchmark data:

- No time and spatially resolved turbulence and heat transfer data that could be used to improve RANS models and develop reduced order models.
- Changing load with constant RPM varying mass flow rate

Lab vs Engine-Relevant Conditions:

 No experimental data at engine conditions due to high temperatures. Most experiments are conducted under scaled down operating conditions with simplified blade geometries.

Objectives

Use **hybrid LES-RANS** to study the flow and heat transfer about the blade tips in a **1.5 stage** power-generation gas turbine **at engine relevant conditions**.

Examine where RANS fails to predict in the 1.5 stage turbine fails and where it succeeds in predicting the flow and performance parameters relative to LES-RANS.

Examine effects of loading with engine speed fixed on flow and heat transfer mass flow rate by using RANS.

Problem Description: Hybrid LES-RANS



Problem Description: RANS

inviscid outlet not shown <u>m</u>, T_t Stator 1

 \dot{m} (kg/s) + velocity profile 324 (design) T_{in} (K) P_b (kPa)

324 (design), 376 (115%), 250 (75%) 1700 700 $Re_{D_H} = 1.786 \times 10^6$

Electric-power generation GT with twist but no taper on blade.

Added an upstream duct to get "fully developed" flow upstream,]m of stator (length = $20C_{s1,ax}$).

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Assumptions Invoked

ASSUMPTION INVOKED IN THIS CFD STUDY

- "Fully-developed" flow at inflow boundary. Did not consider the largescale turbulent structure that exit the combustor.
- Adiabatic wall. Vanes, blades, and endwalls do not have internal or film-cooling and no conjugate heat transfer.
- No trailing-edge film cooling. Thus, get vortex shedding in addition to Kevin-Helmholtz instability.
- Did not account for hot-gas path cross-sectional area changes.
- Did not consider endwall and vane/blade contouring.
- Accounted for twist in the blade, but not its taper.

Problem Formulation & Numerical Method: Hybrid LES-RANS

- Problem Formulation
 - Inertial frame for stators and non-inertial frame for rotor
 - Favre-averaged "3D, unsteady" continuity, compressible Navier-Stokes, and total energy for RANS part of IDDES
 - Filtered "3D, unsteady" continuity, compressible Navier-Stokes, and total energy for LES part of IDDES
 - RANS to/from LES via IDDES

closed by

- thermally perfect gas
- temperature-dependent transport properties
 - Sutherland's model for viscosity and thermal conductivity
 - Specific heat, $c_p(T) = 1.1529 \cdot 10^3 9.5080 \cdot 10^{-1}T + 2.2003 \cdot 10^{-3}T^2 1.8939 \cdot 10^{-6}T^3 + 7.4571 \cdot 10^{-10}T^4 1.1197 \cdot 10^{-13}T^5$
 - Prandtl number, $Pr(T) = c_p(T) \times \mu / k(T)$
- LES RANS: Modified Shear-Stress-Transport (SST) model (wall functions not used) **BCs:** specify \dot{m} (with velocity profile), T, and turbulent quantities at inflow; p_b at outflow
- Code
 - cell-centered finite volume code, SIEMENS STAR-CCM+ V.2206 (double precision)

Numerical Method

- fully coupled implicit algorithm
- 2nd order Roe upwind for inviscid fluxes
- algebraic multigrid with V-cycle to accelerate convergence at each time step (20 to 30 iterations)

Problem Formulation & Numerical Method: RANS

Problem Formulation

- Inertial frame for stators and non-inertial frame for rotor
- Favre-averaged continuity, compressible Navier-Stokes, and total energy

closed by

- thermally perfect gas
- temperature-dependent transport properties
 - Sutherland's model for viscosity and thermal conductivity
 - Specific heat, $c_p(T) = 1.1529 \cdot 10^3 9.5080 \cdot 10^{-1}T + 2.2003 \cdot 10^{-3}T^2 1.8939 \cdot 10^{-6}T^3 + 7.4571 \cdot 10^{-10}T^4 1.1197 \cdot 10^{-13}T^5$
 - Prandtl number, $Pr(T) = c_p(T) \times \mu / k(T)$
- Shear-Stress-Transport (SST) model (wall functions not used)

BCs:

- specify \dot{m} (with uniform velocity profile), T, and turbulent quantities at inflow; p_b at outflow
- mixing plane at rotor-stator interface
- Code
 - cell-centered finite volume code, SIEMENS STAR-CCM+ V.2206 (double precision)

Numerical Method

- fully coupled implicit algorithm
- 2nd order Roe upwind for inviscid fluxes
- algebraic multigrid with V-cycle to accelerate convergence to steady state

V&V: Grid-Sensitivity Study

Domain	$\begin{array}{c} \textbf{Coarse} \\ r \times \theta \times z \text{ (O-grid)} \\ \hline \text{total} \end{array}$	$\begin{array}{c} \textbf{Baseline} \\ r \times \theta \times z \text{ (O-grid)} \\ total \end{array}$	Fine $r \times \theta \times z$ (O-grid) total
Inlet	60×40×75	140×75×150	200×100×180
Duct	0.18 mil	1.57 mil	3.6 mil
Stator 1	75×75×150 (25)	150×145×275 (50)	225×240×390 (80)
(10 deg)	1.1 mil	7.7 mil	39.45 mil
Rotor	130×65×165 (30)	225×130×335 (55)	345×240×540 (70)
(5 deg)	1.6 mil	15.65 mil	63.51 mil
Stator 2	80×50×150 (25)	150×100×265 (50)	210×145×285 (65)
(10 deg)	0.84 M	5.59 M	11.83 M
TOTAL RANS	3.8 M	31 M	106 M





45, 75, and 125 in the radial direction inside the tip gap.

1st cell next to wall: $y^+ < 1$



Verification: Blade-Tip Region



V&V: Grid- and Time-step Sensitivity Study



Verification



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Instantaneous Flow: Temperature



On shedding+Kelvin-Helmholtz at trailing edge, note that there are **no film-cooling from trailing edge**.

Instantaneous Flow: Temperature



Instantaneous Flow: Temperature





Pressure Profile variation with time at 50% span

Hybrid LES-RANS vs RANS: P & T on Blade Surface



Summary and Conclusions

To be presented at the 2025 IGTI!!!







Current Efforts to Meet Our Nation's Goal of Carbon-Free Electric-Power Generation by 2035

Tools

- ROM for conjugate HT in conical cooling ducts with tip leakage in 2nd stage turbine.
- Physics-based ROM for internal cooling of vane & blade w/ 3-D effects.
- Physics-based ROM for internal cooling of RDC
- ROM + Optimization + machine learning for design

Fundamentals

Revisit T_{adiabatic} on its physical meaning & how to measure (directly to journals in 2024, 2025)

Applications

- Tip-leakage flow in 1.5 stage turbine.
- Internal cooling of RDC walls.
- Transition duct from RDC to turbine
- New film-cooling holes: **downstream VG with cross flow**; **Y-shaped hole** (Doug Straub & Justin Weber)
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- Biot no. analogy to study TBC in sCO2 turbine cooling (w/ Matthew Searle)







My current students...



Eric Chen, Abhi Victor, Dylan Hsieh, Jiekun Wu, Robert Gillespy, Tom Shih, Jay Kim, Jack Buechler, Madeleine Yee, Brandon Hay

Not shown: James Peck, Sharouk Reza, Adwiteey Shishodia

