

# Dual-Loop Solution-Based Carbon Capture System for Net Negative Carbon Dioxide Emissions with Lower Costs (DE-FE0032134) and Enhancement of Carbon Capture Reactor Performance (DE-FE0032217)

Heather Nikolic,  
Jesse Thompson and Kunlei Liu

*IDEA at PPL R&D Center  
University of Kentucky  
Lexington, KY*

<https://idea.engr.uky.edu/>

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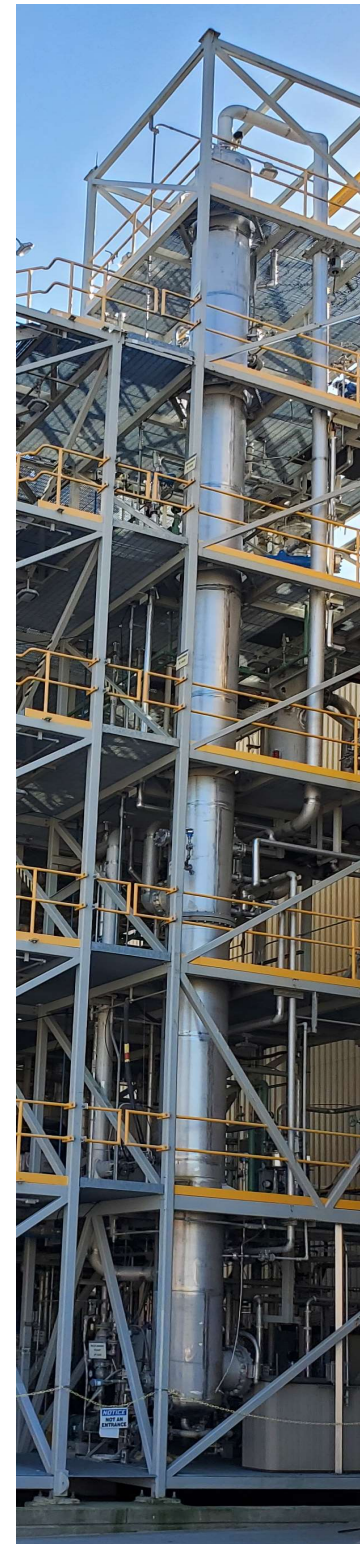
# UK IDEA Approach

1. Match the capture technology to the driving force
2. Intensify mass transfer
3. Utilize H<sub>2</sub> production to offset cost
4. Allow power generation unit to run with less cycling by flexibly operating separate CO<sub>2</sub> capture loops
5. Integration with existing plant
6. Continue to minimize solvent degradation, recover heat from steam condensate to improve HRSG performance, maximize capture unit capacity factor by eliminating the flue gas blower

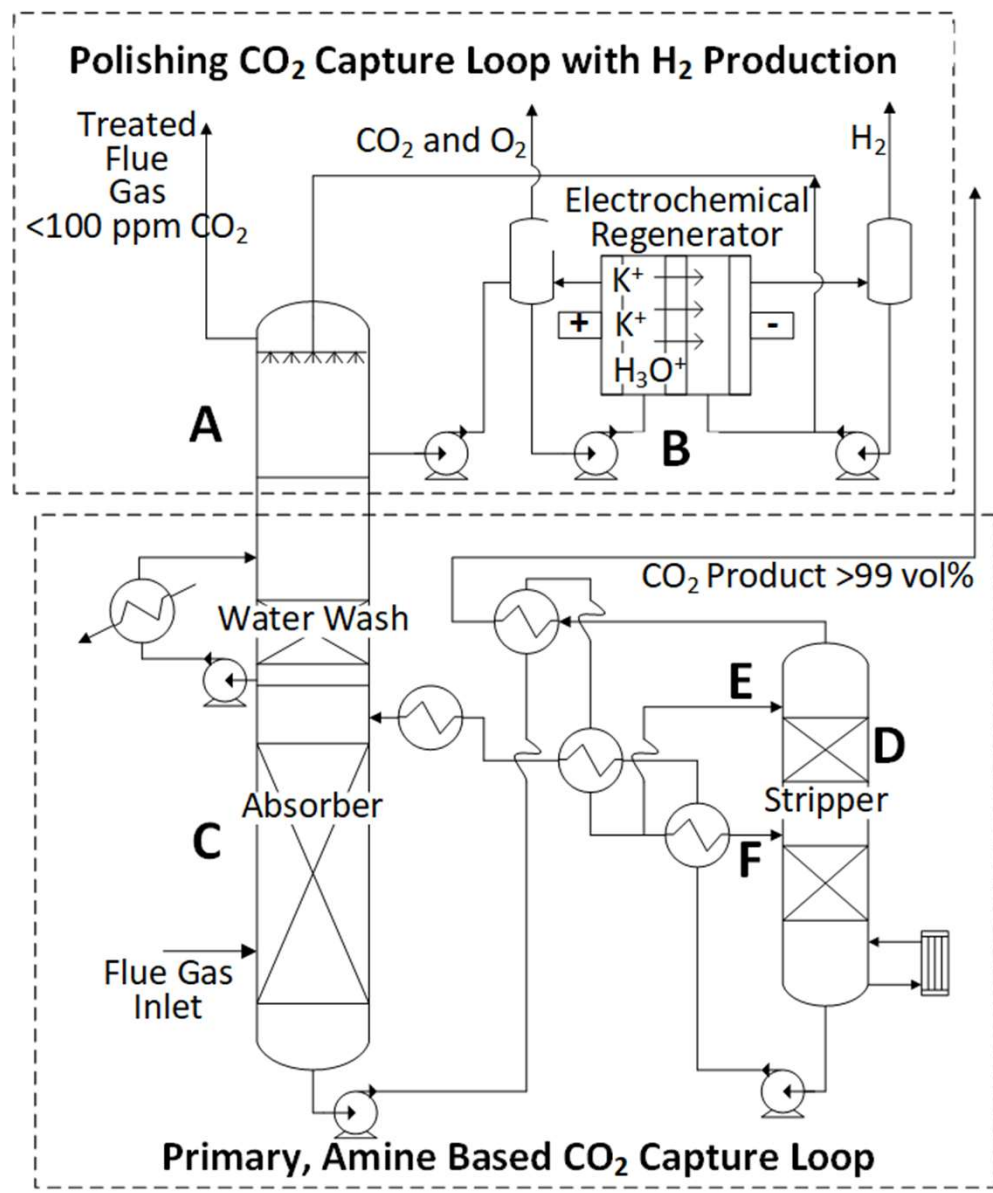
$$CO_2 \text{ Mass Transfer} = A K_G (P_{CO_2}^g - P_{CO_2}^*)$$

$$\frac{1}{K_G} = \frac{1}{k_g} + \frac{1}{k'_g}$$

$$k'_g = \frac{\sqrt{D_{CO_2} K_2 [Am]}}{H_{CO_2}}$$



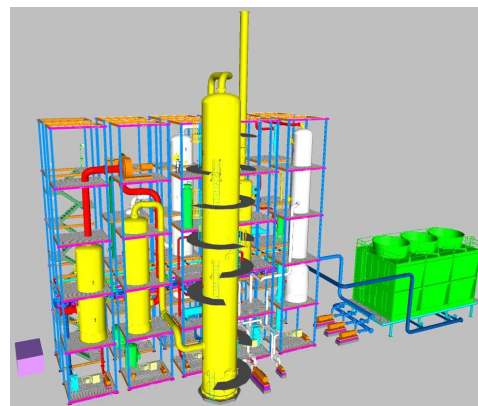
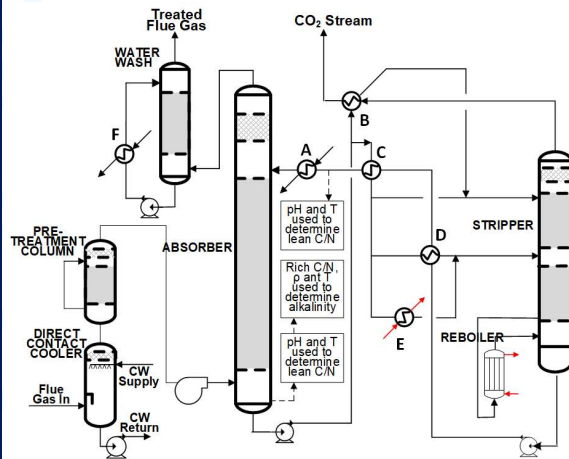
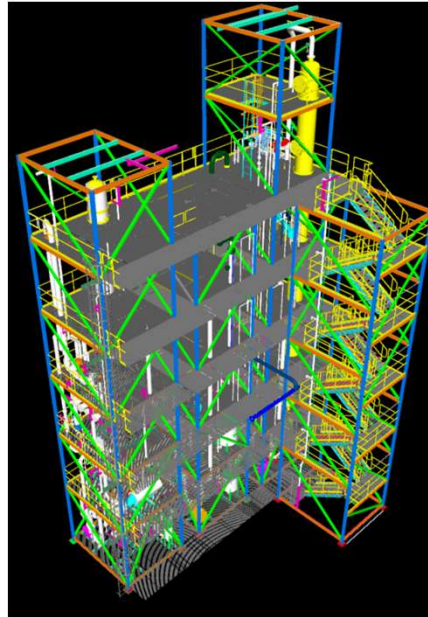
# UK Dual Loop Approach for Point Source Treated Flue Gas with <100 ppm CO<sub>2</sub>



Adaptation of  
 UK DAC with  
 H<sub>2</sub> Production  
 Technology

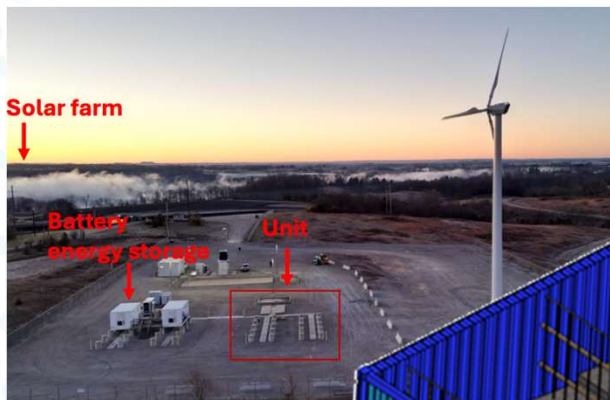
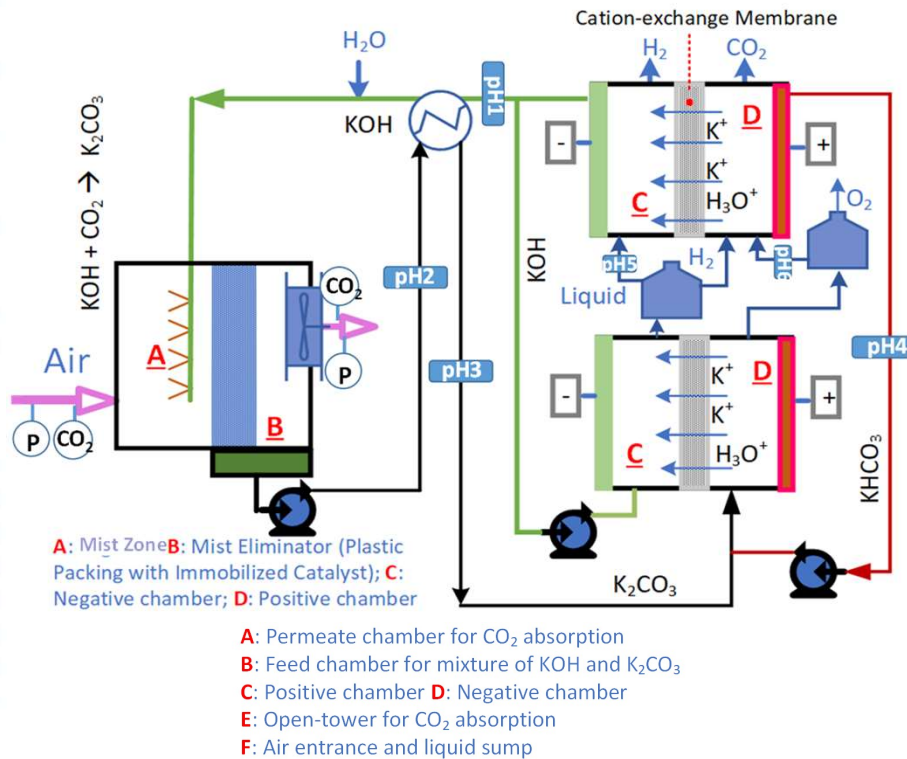
UK Point  
 Source CO<sub>2</sub>  
 Capture  
 Technology,  
 such as for  
 NGCC

# Building on Point Source Technology



- ❑ Bench Scale Since 2009
- ❑ Engineering Scale, 15 TPD, Since 2015 at EW Brown Generating Station, a PPL Corporation Facility
- ❑ 3 TPD, Nucor Steel Gallatin, 2025
- ❑ 9.3 TPD, Vitro Architectural Glass,
- ❑ 215 TPD, Cane Run Generating Station (CRGS), a PPL Corporation Facility, 20230
- ❑ 1.7M TPY, CRGS, FEED complete 8/2025
- ❑ Favorable carbon intensity scenario: 114.81 kg CO<sub>2</sub>e/MWh<sub>net</sub> cradle to delivered electricity was found, 13% reduction from 2019 B31B

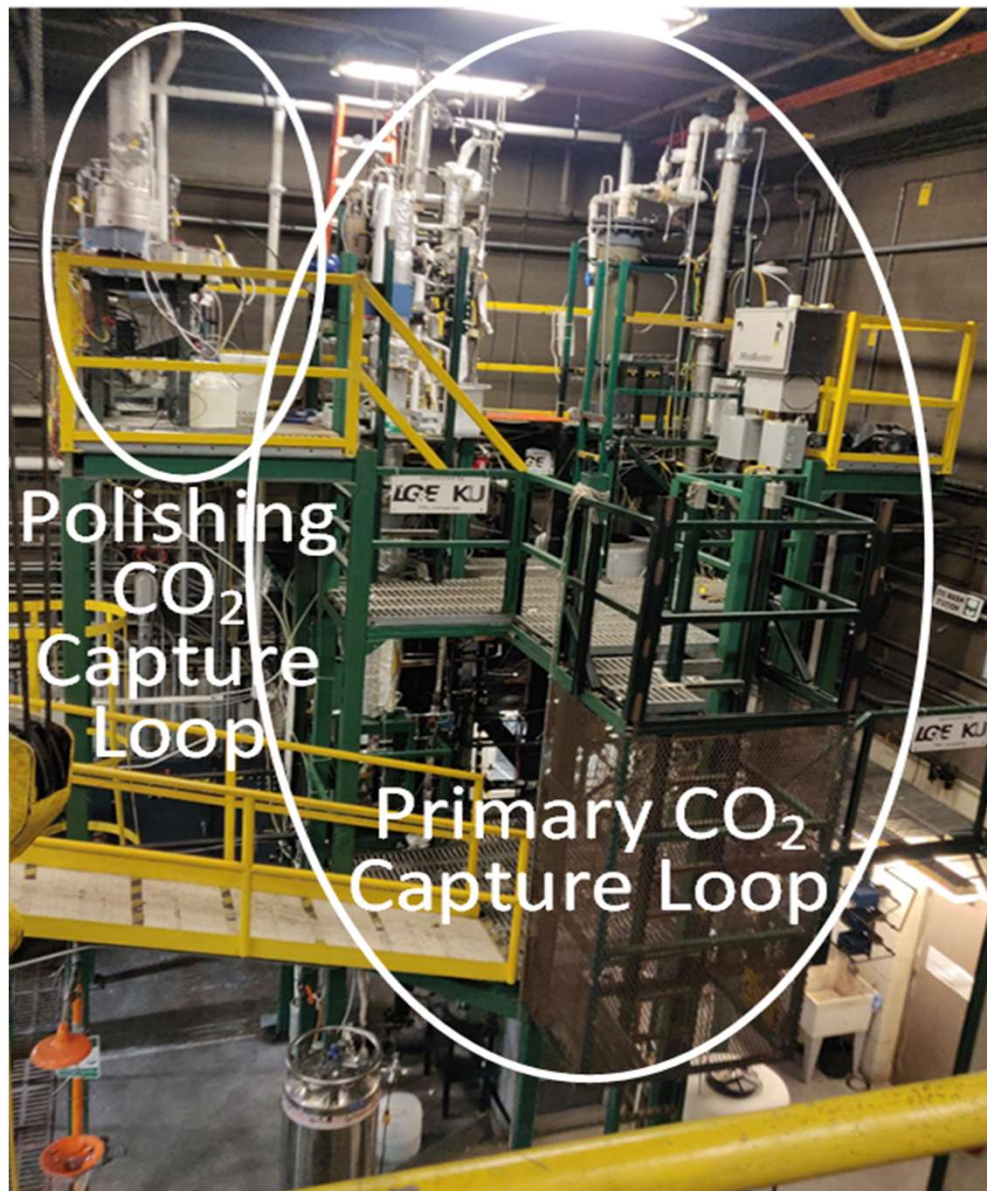
# Building on DAC with H<sub>2</sub> Production Technology



- Inorganic, solvent-based
- Catalyzed capture at mild pH for DAC energy cost minimization
- Simplified Process and Operation
- Electrochemical regeneration with H<sub>2</sub> and O<sub>2</sub> production
- 7,700 kg CO<sub>2</sub>/year Demo at EW Brown Generating Station, a PPL Corporation Facility, 350 kg H<sub>2</sub>/year, 470 W Regenerator, 2025-2026
- DAC Hub Feasibility Study, ≥3,500 tonne CO<sub>2</sub>/year per capture location with 160 tonne H<sub>2</sub>/year and 1040 kW regenerator
- Favorable carbon intensity found: 0.32 kg CO<sub>2</sub> is estimated to be abated per kg of CO<sub>2</sub> captured and permanently sequestered for the case where the H<sub>2</sub> production displaces H<sub>2</sub> produced via electrolysis, based on the expected 2050 U.S. grid carbon intensity

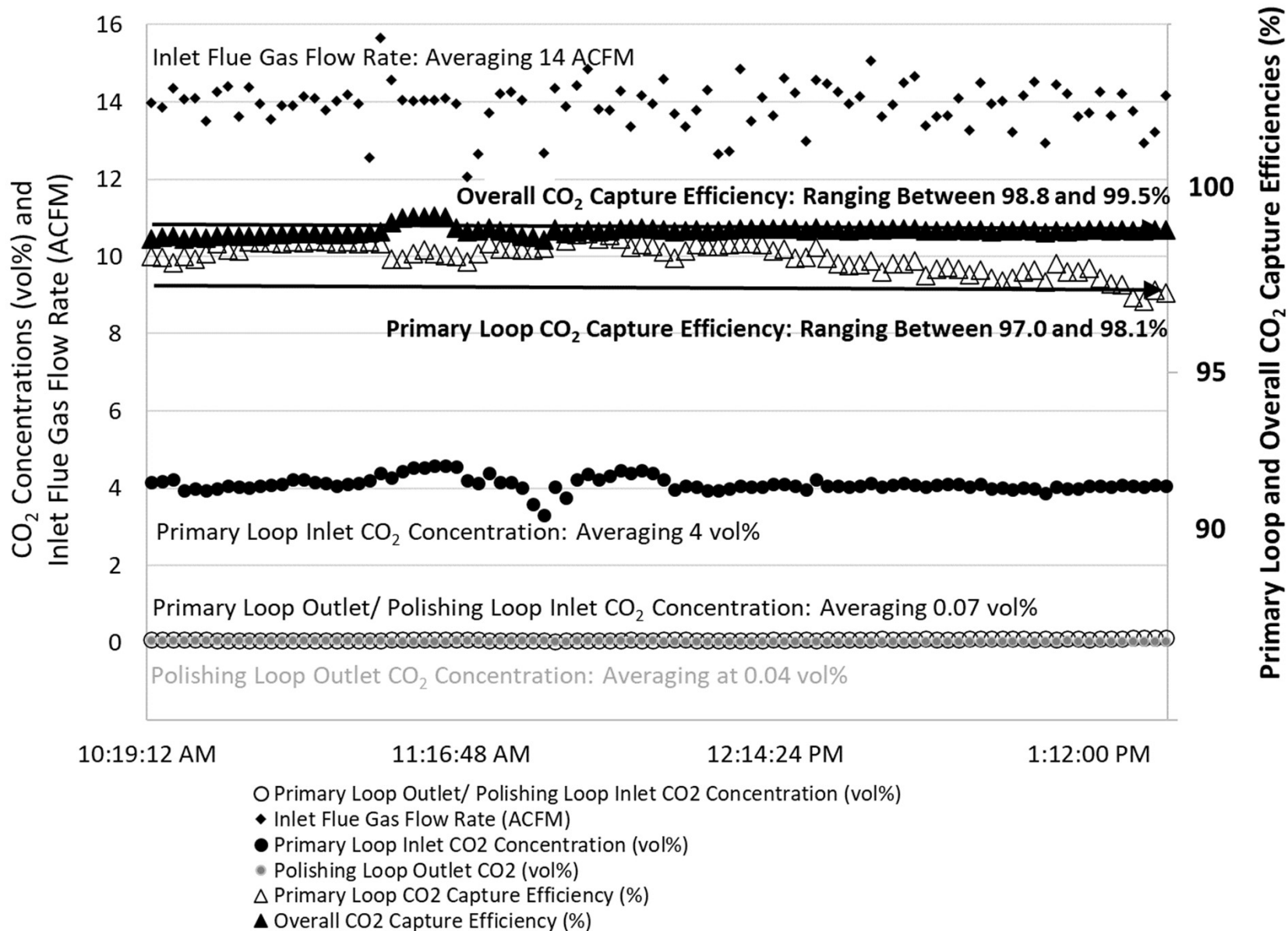
# DE-FE0032134

## Dual-loop Solvent-based CCS for Net Negative CO<sub>2</sub> Emissions with Lower Cost



- ❑ Bench Scale Demonstration
- ❑ 3/1/2022 to 8/31/2025
- ❑ Resulting TRL 4
- ❑ Existing UK Amine-Based CO<sub>2</sub> Capture Unit Applied as Primary Loop
- ❑ Polishing Loop Designed, Integrated, Operational and Being Tested
- ❑ Variable CO<sub>2</sub> Capture Efficiency in the Primary Loop
- ❑ TEA, LCA, EH&S Upcoming

# Bench Scale Operational Data



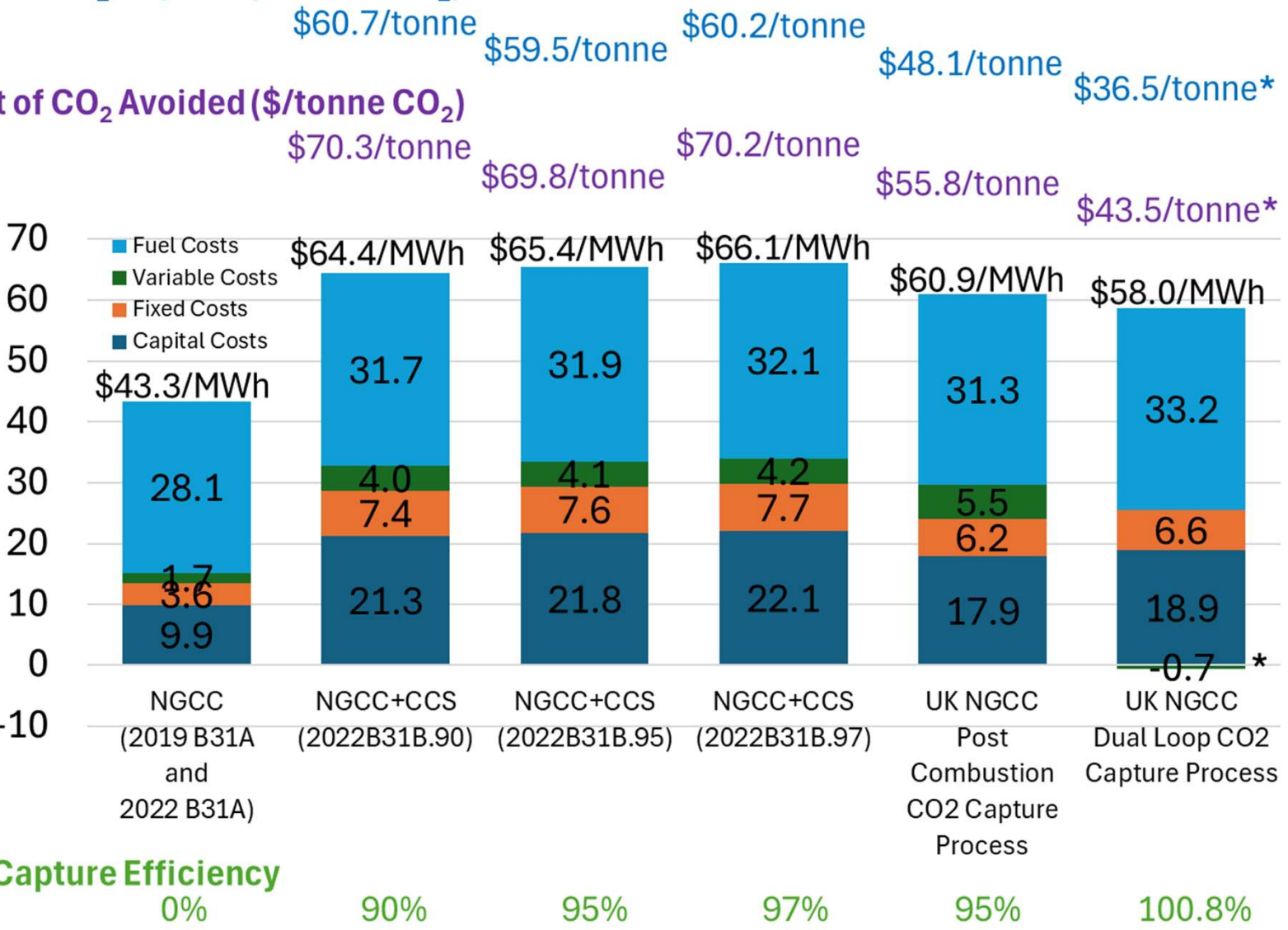


# Preliminary TEA

## Cost of CO<sub>2</sub> Capture (\$/tonne CO<sub>2</sub>)

## Cost of CO<sub>2</sub> Avoided (\$/tonne CO<sub>2</sub>)

Levelized Cost of Electricity (\$/MWh) (Ex. T&S)



## CO<sub>2</sub> Capture Efficiency

\* Assuming a H<sub>2</sub> sales price of \$8/kg and a credit for CO<sub>2</sub> capture from air of \$100/tonne

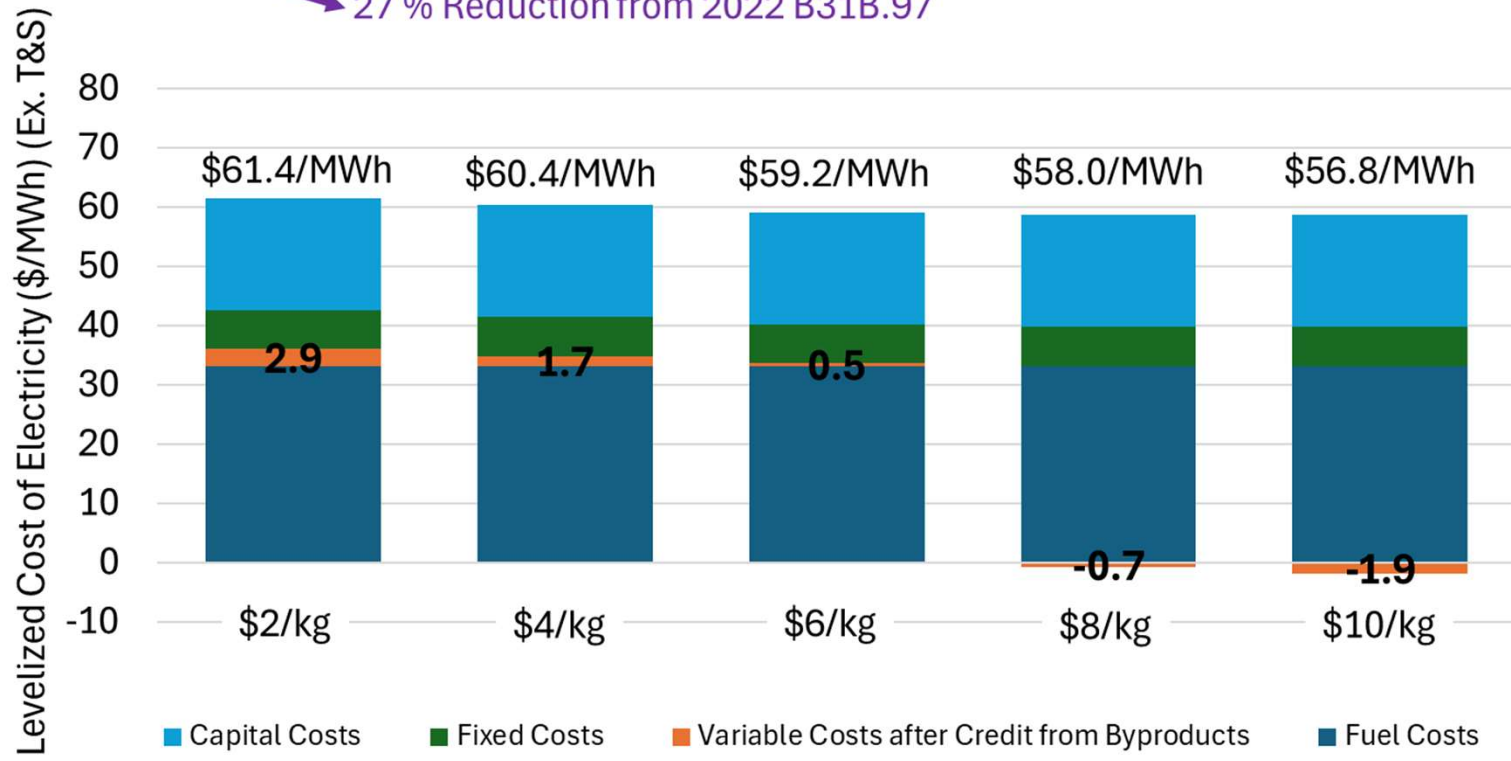
# Effect of H<sub>2</sub> Sales Price on the UK Dual Loop CO<sub>2</sub> Capture Process Costs

## Cost of CO<sub>2</sub> Capture (\$/tonne CO<sub>2</sub>)

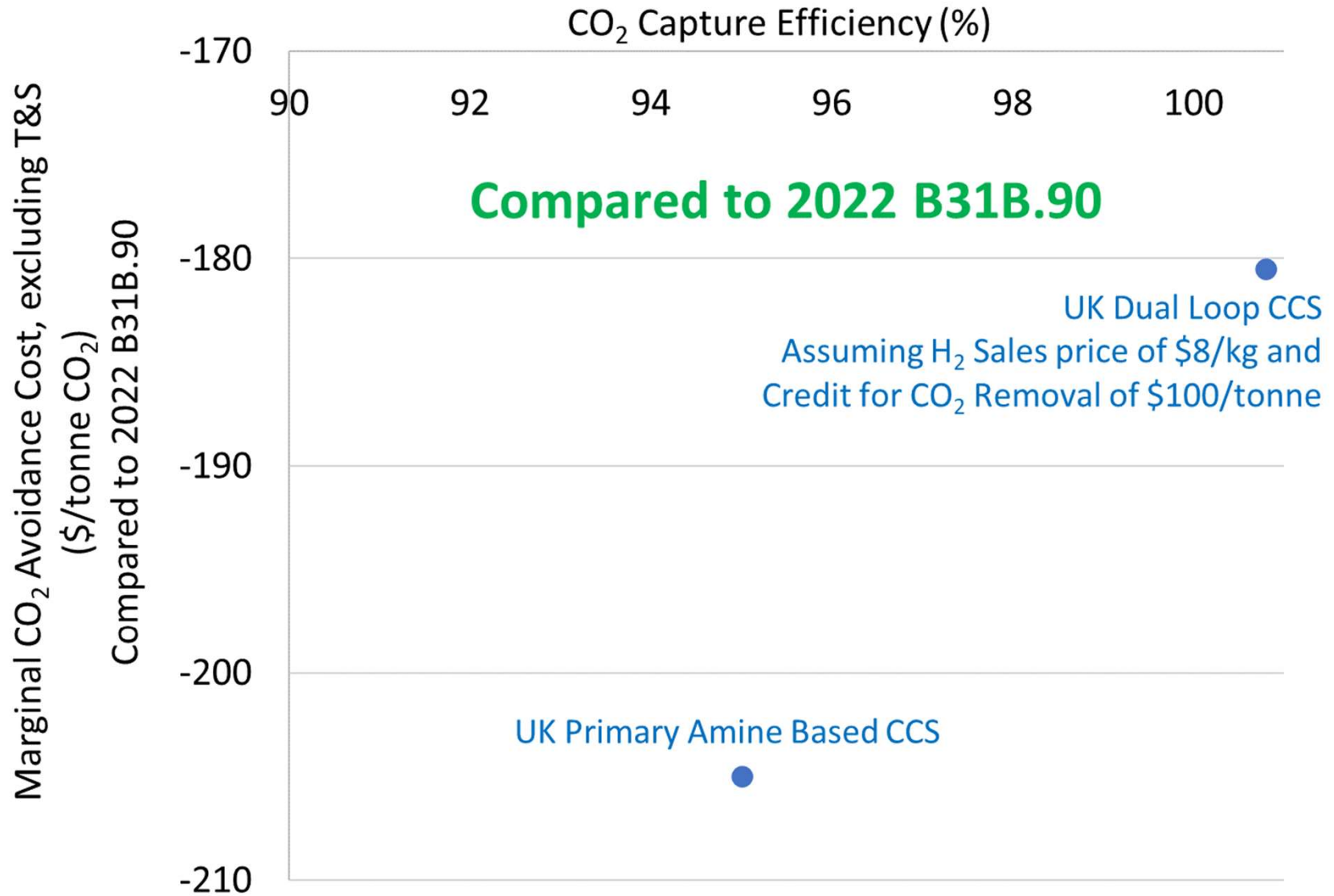
\$45.3/tonne    \$42.4/tonne    \$39.5/tonne    \$36.5/tonne    \$33.6/tonne  
 ↘ 25% Reduction from 2022 B31B.97

## Cost of CO<sub>2</sub> Avoided (\$/tonne CO<sub>2</sub>)

\$51.4/tonne    \$50.6/tonne    \$47.0/tonne    \$43.5/tonne    \$39.9/tonne  
 ↘ 27% Reduction from 2022 B31B.97

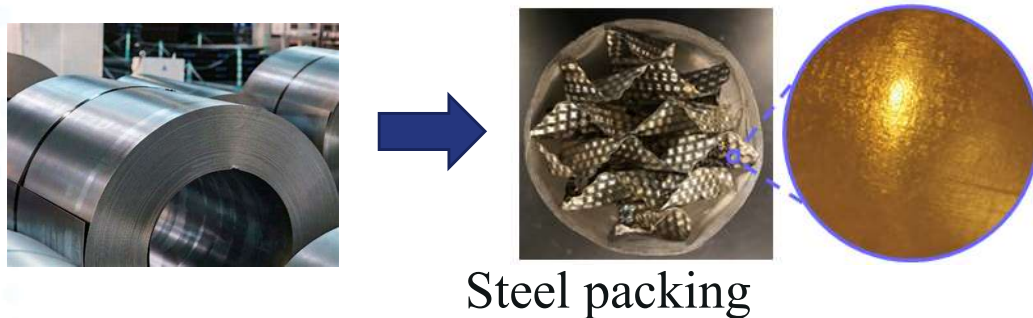


# UK Marginal CO<sub>2</sub> Avoidance Costs



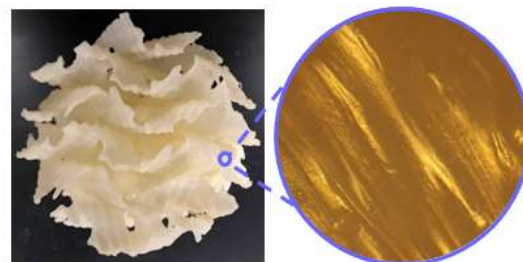
# Process Intensification for High Capture & Short Absorber – Decrease Diffusion Resistance

## Commercially Available Packing

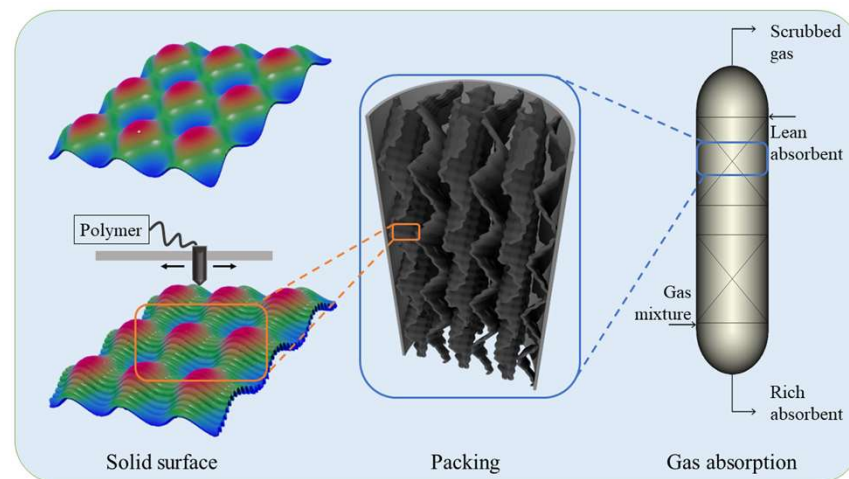
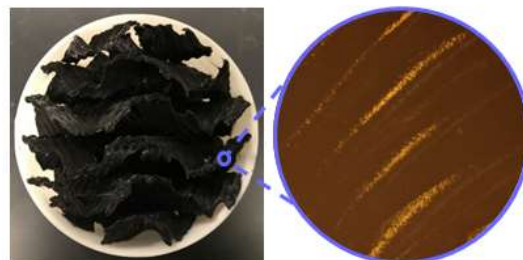
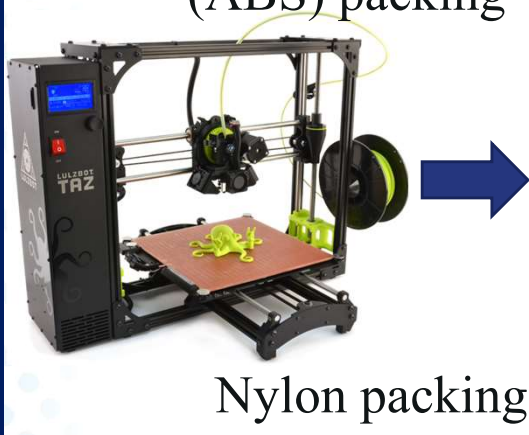


## 3D Printed Polymer Packing

Acrylonitrile  
butadiene styrene  
(ABS) packing

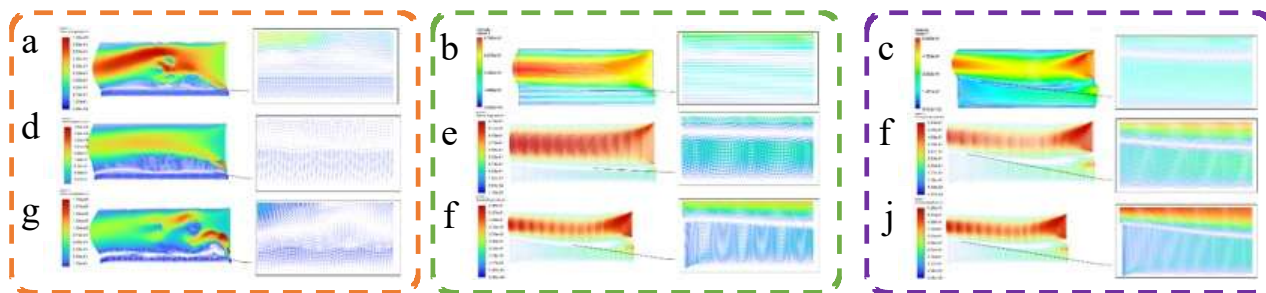
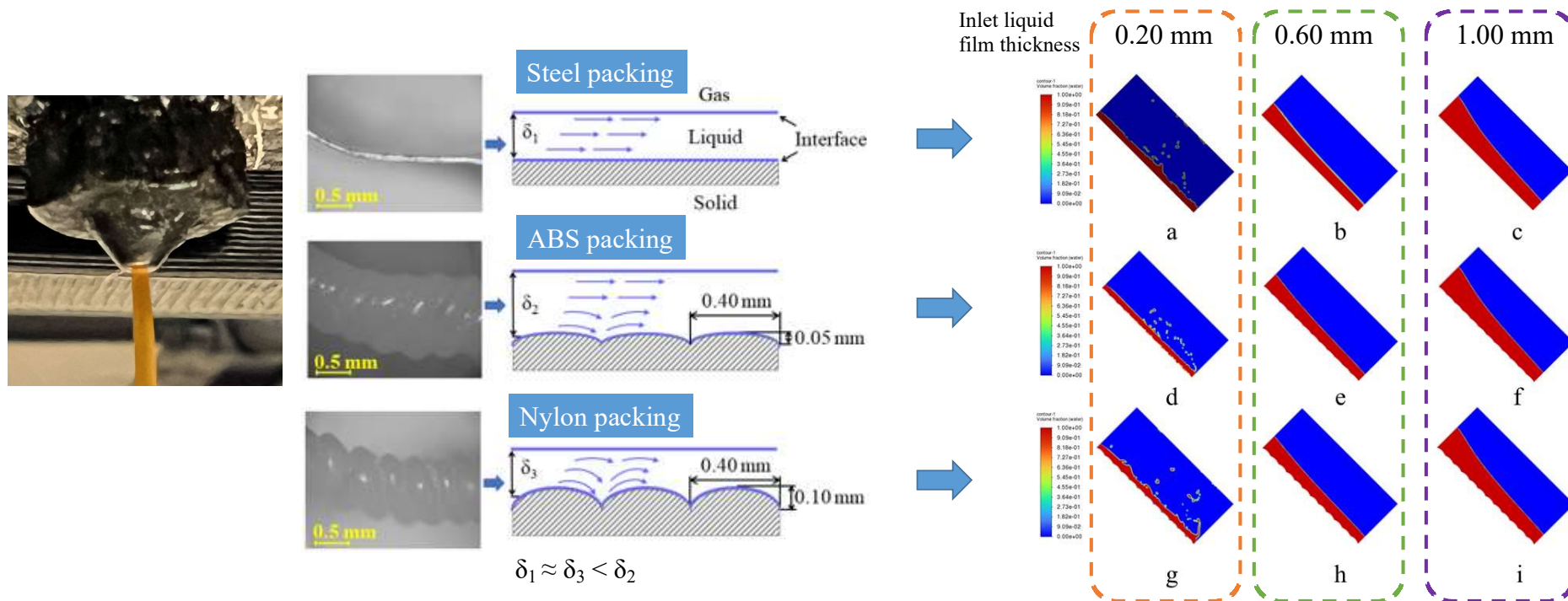


Nylon packing



3D printed polymer packing has additional wavy sub-texture that further improves liquid turbulence on the surface translating to improved CO<sub>2</sub> capture rates

# Process Intensification for High Capture & Short Absorber – Decrease Diffusion Resistance

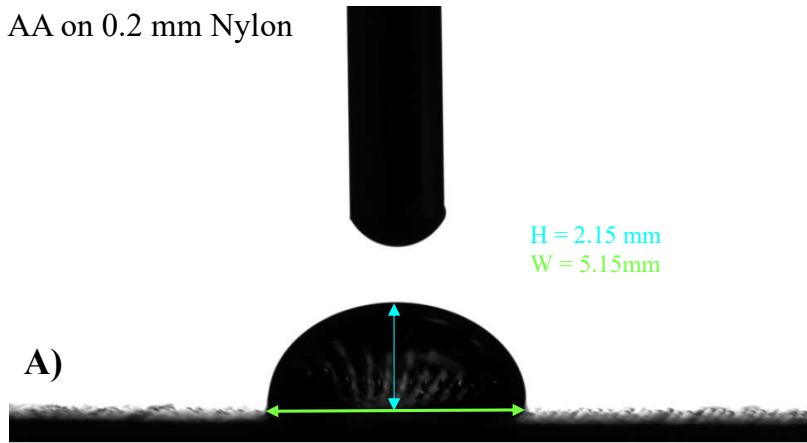


- Surface texture amplitude
  - Liquid film thickness
- Local mixing within the liquid

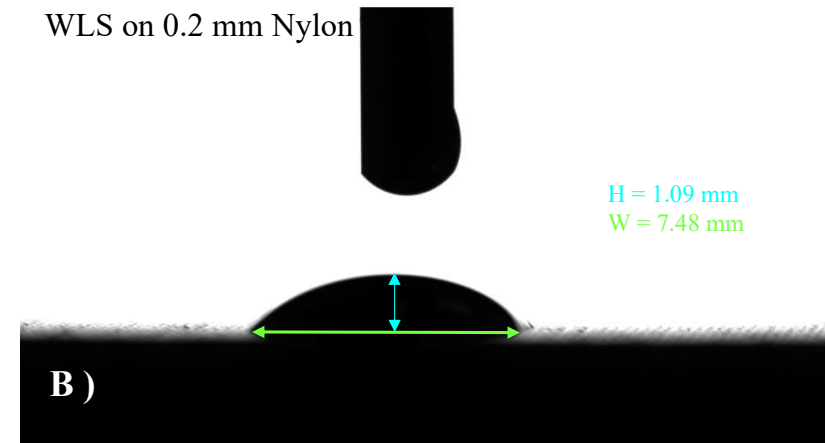
# Process Intensification for High Capture & Short Absorber – Increase Liquid-Gas Contact Area

## Solvent Contact Angle (Wetting)

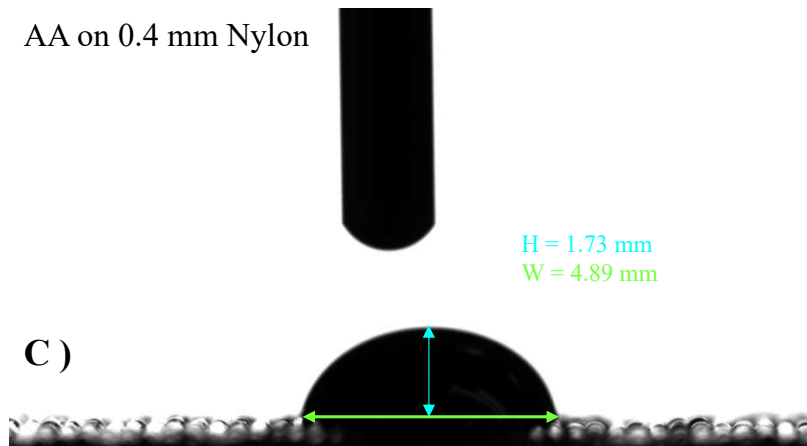
AA on 0.2 mm Nylon



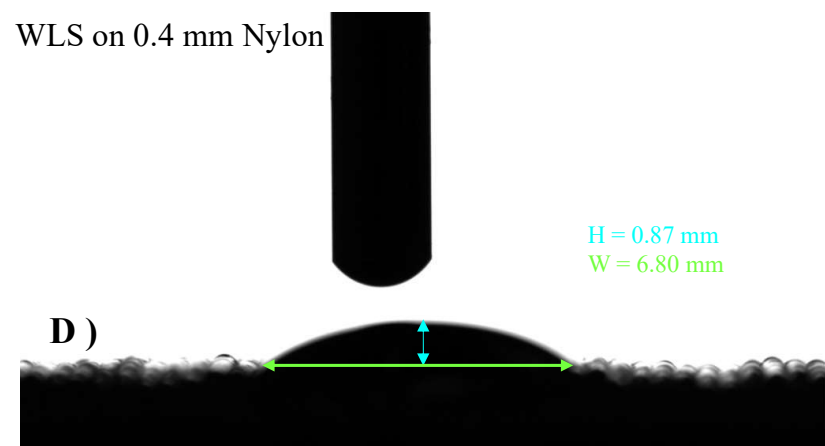
WLS on 0.2 mm Nylon



AA on 0.4 mm Nylon



WLS on 0.4 mm Nylon

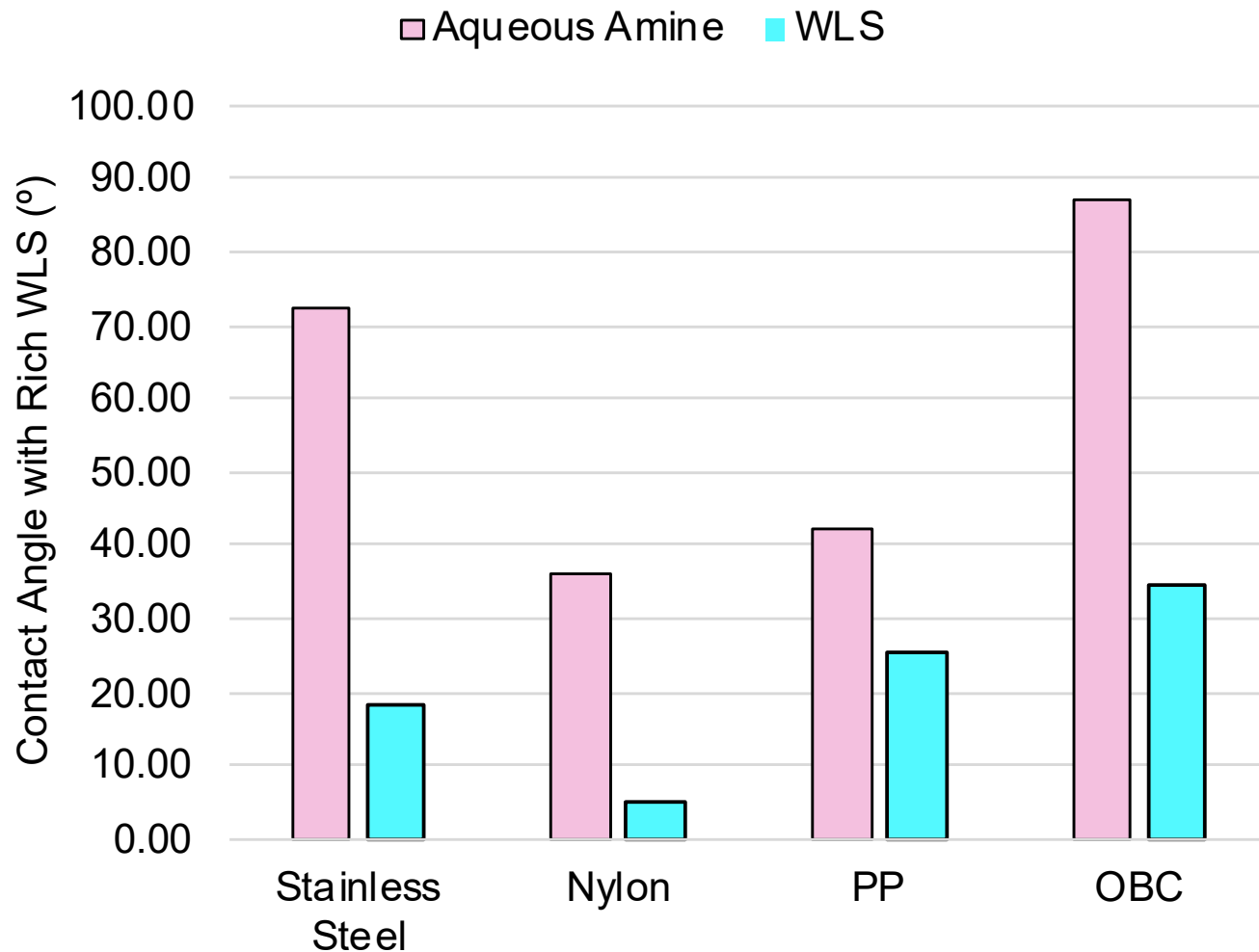


The initial drop, prior to rolling, of A) AA on 0.2 mm nylon, B) WLS on 0.2 mm nylon, C) AA on 0.4 mm nylon, and D) WLS on 0.4 mm nylon.

# DE-FE0032217

## Enhancement of Carbon Capture Reactor Performance

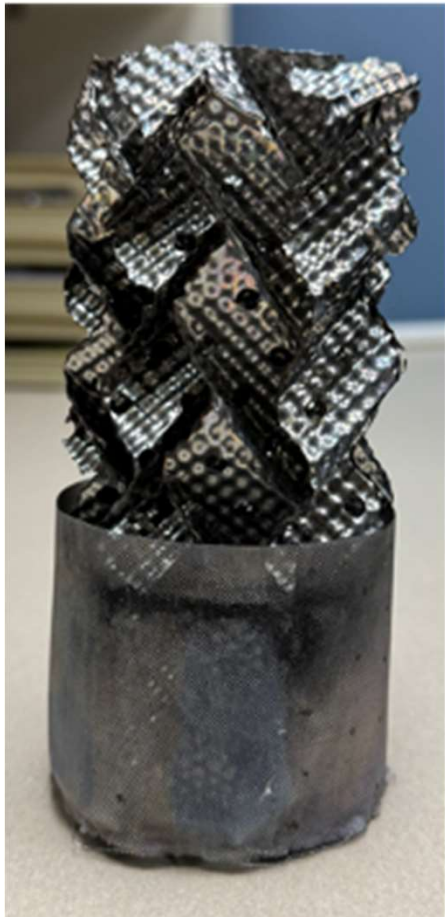
### Summary of Solvent Wetting on Stable 3D Printed Polymers



# 3D Printed Packing

Bench testing of steel packing with WLS as baseline, then with Nylon and PP packing to see benefit from improved wetting in the absorber leading to better CO<sub>2</sub> mass transfer

Stainless Steel



Nylon



PP





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