



# LOAD-Z

## Low-NOx, Operable Ammonia Combustor Development for Zero-Carbon Power



F T4000® Aeroderivative Dual Fuel Gas Turbine Engine.

### RTX Technology Research Center

2024 FECM/NETL Spring R&D Project Review Meeting  
April 24, 2024

*Prime Contractor:* RTX Technology Research Center (RTRC)

*Subcontractor:* University of Connecticut (UConn)

**RTRC**

RTX Technology  
Research Center

**UCONN**

UNIVERSITY OF CONNECTICUT

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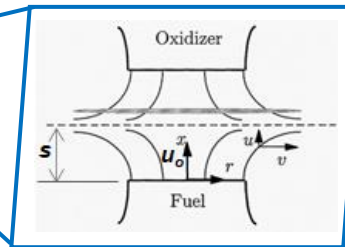
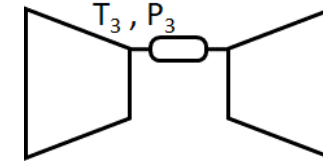
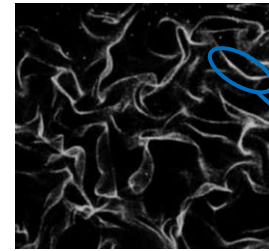
# Key Project Goals .... WHAT / WHY

## Low-NOx Operable Ammonia-Combustor Development (LOAD-Z)

(1)  
EXPERIMENTS  
4 lab-scale  
facilities

### – Fundamental NH<sub>3</sub> flame data relevant to turbines:

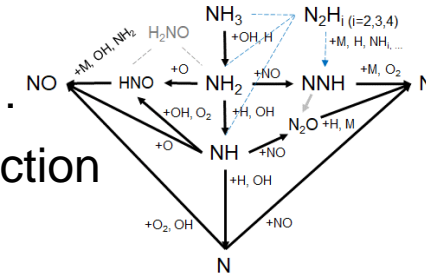
- P, T >> ambient → relevant to compressor exit conditions .....
- strained & turbulent flames .....
- Targeted outcome: expand published data w/ new, useful data (previously unreported)



(2)  
MODELING

### – Predictive capability for NH<sub>3</sub> combustion & emissions

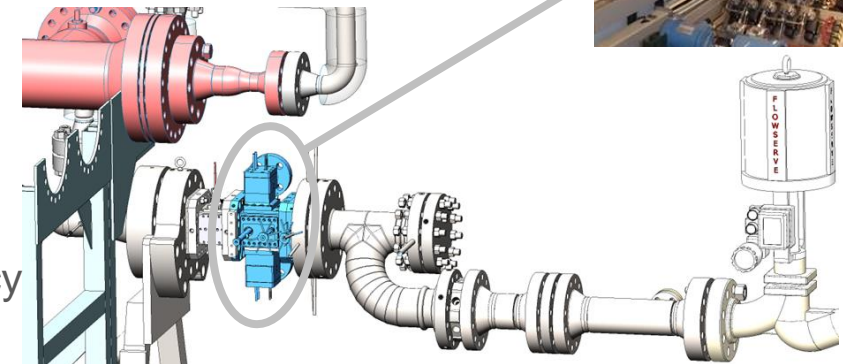
- NO<sub>x</sub> formation kinetics integral w/ NH<sub>3</sub> comb. kinetics .....
- CFD of turb. NH<sub>3</sub> flames w/ NO<sub>x</sub> & NH<sub>3</sub> slip ( $\eta_{\text{COMB}}$ ) prediction
- Targeted outcome: capability for GT combustor design



(3)  
DESIGN & DEMO.

### – Develop & test NH<sub>3</sub> gas-turbine combustor “@ scale”

- Single-nozzle-rig (SNR) scale demo. @ high P, T .....
- Pure NH<sub>3</sub> combustion @ 75% – 100% power
- Targeted outcome: < 30ppm NO<sub>x</sub>\*\* & >99.99% efficiency



\*\*Note recent ETN recommendations for NO<sub>x</sub> reporting with hydrogen-containing fuels

# Approach & Progress .... How

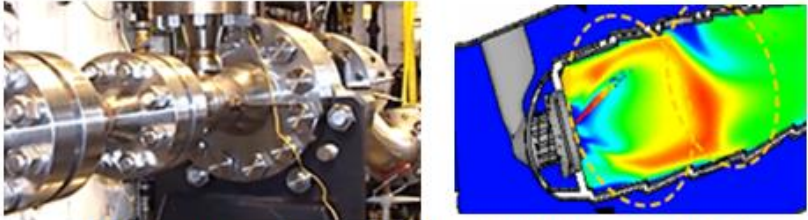
- 4-year PoP: Oct. 2022 – Sept. 2026 (currently at year-1.5)
- \$3.3M Federal DOE funding
- \$0.9M Customer funding - RTRC & UConn (21.8% cost-share)

## RTRC

## UConn

Time ↑

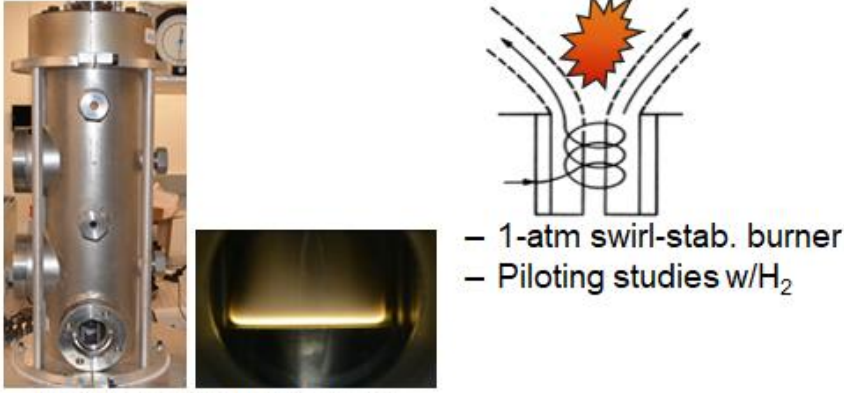
Year-4



- Single-nozzle high-pressure combustor, fired w/ $\text{NH}_3$  fuel
- Measure emiss. & performance:  $\text{NO}_x$ , efficiency, stability

Year-3

Year-2

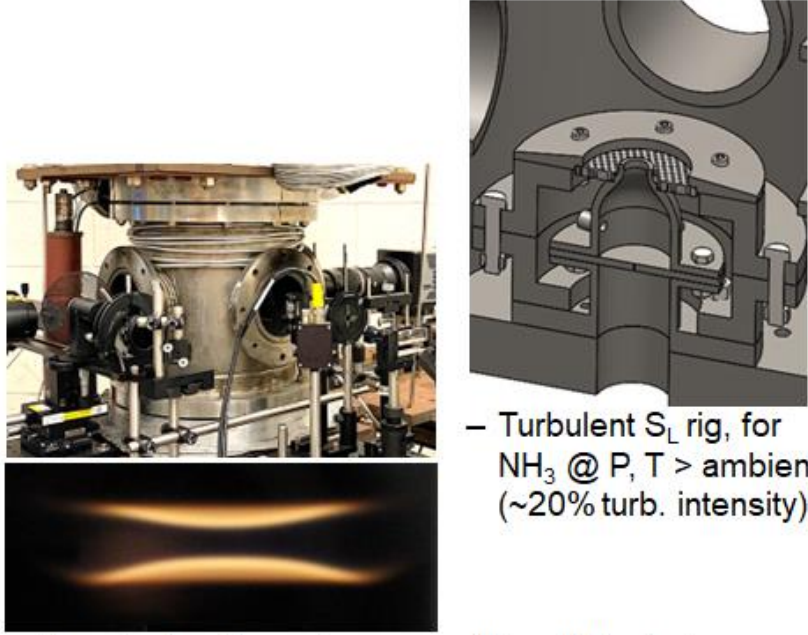


- Flat-flame high-P burner (>>1-atm) for  $\text{NO}_x$  eval.
- 1-atm swirl-stab. burner
- Piloting studies w/ $\text{H}_2$

Year-1

**Modeling:**

- CFD for design
- Kinetic improve. w/ exp. data
- CFD & validation
- Turb. models for  $\text{NH}_3$  comb. &  $\text{NO}_x$  (no post-process.)
- CRN modeling
- Counterflow
- Kinetic mech.



- Counterflow flame rig, compatible w/ $\text{NH}_3$  fuel
- Measure strained flames w/ inlet P, T > ambient
- Turbulent  $S_L$  rig, for  $\text{NH}_3$  @ P, T > ambient (~20% turb. intensity)

### • Outcomes/Publications (to-date):

- *Proceedings of the Combustion Institute* – 40<sup>th</sup> CI Symposium paper in press for July 2024
- *AIAA SciTech 2024* – paper # AIAA-2024-2019 ( DOI:10.2514/6.2024-2019 )
- *Combustion Institute Meetings* – 2023 US National & ESS Spring 2024 meeting papers

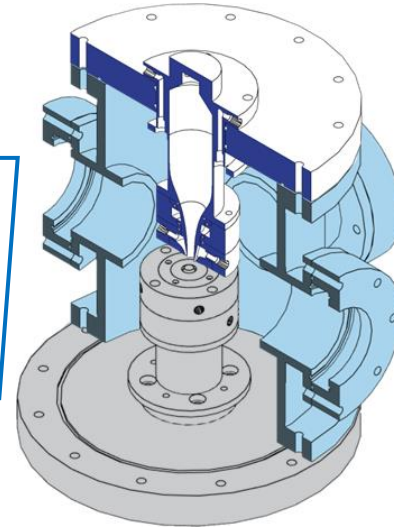
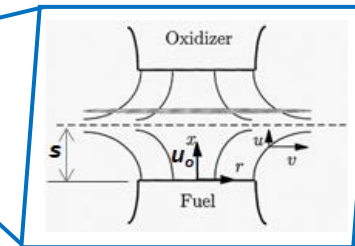
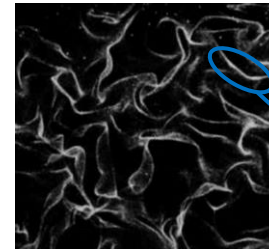
# 1st Technical Task .... EXPERIMENTS .....

## Low-NOx Operable Ammonia-Combustor Development (LOAD-Z)

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EXPERIMENTS  
4 lab-scale  
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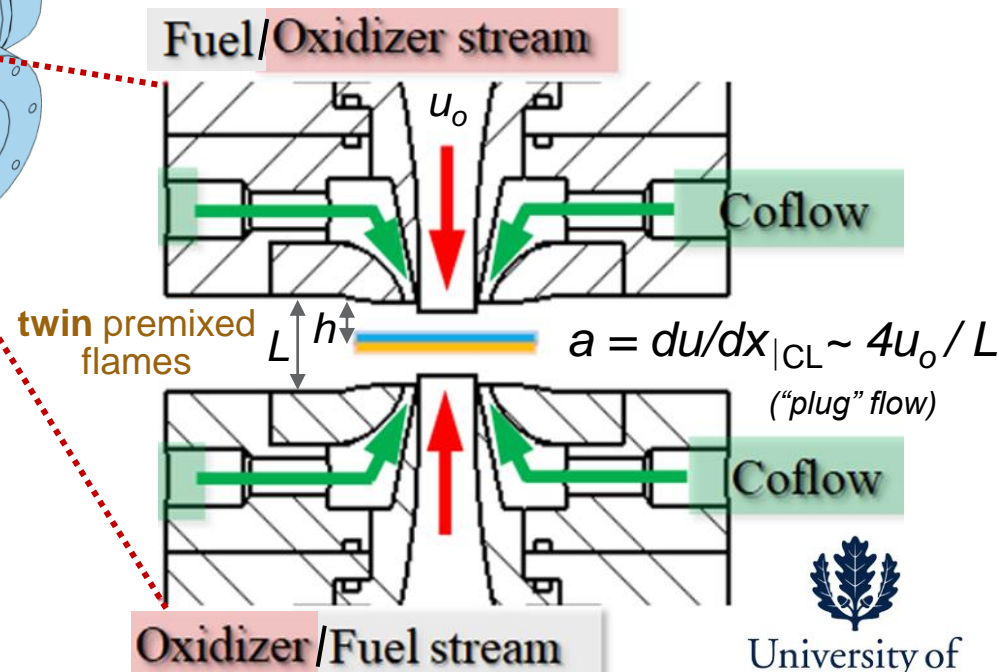
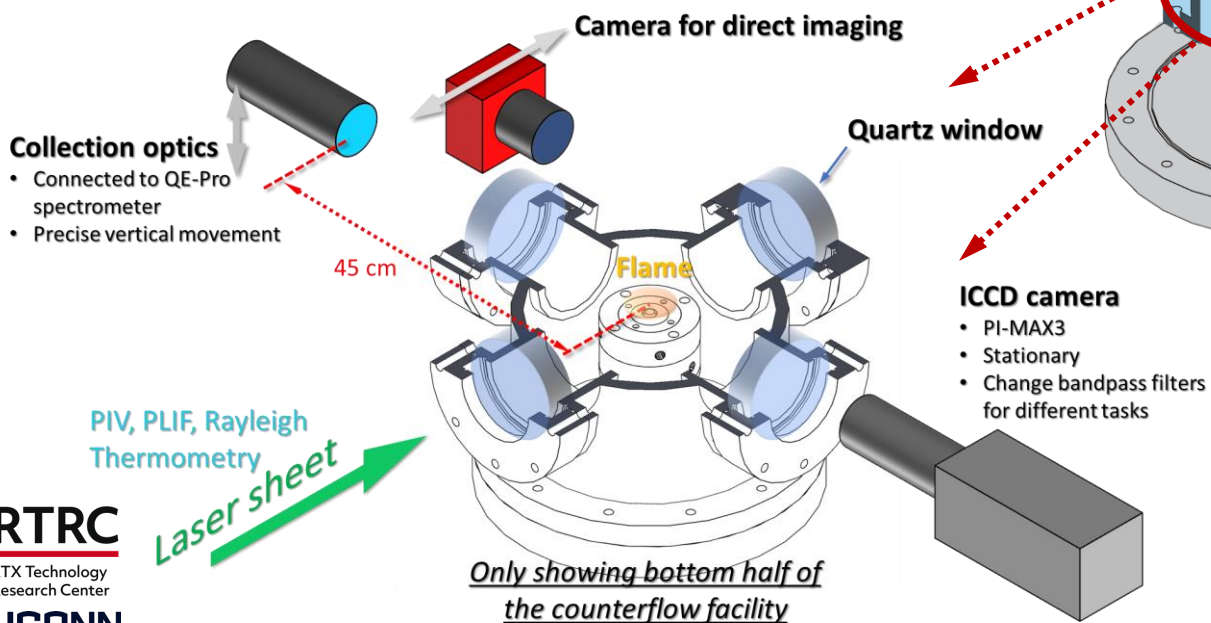
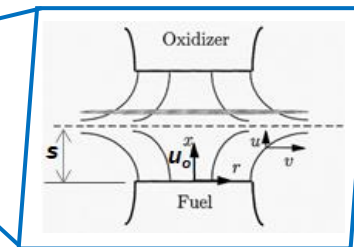
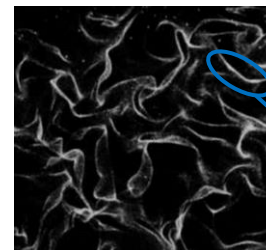
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  - Pure  $\text{NH}_3$  combustion @ 75% – 100% power
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# Lab-Scale Experiment #1: Counterflow Flame Rig | *Laminar (2D)*

- Relevance:**
- Scarce data on  $\text{NH}_3$  flame extinction, esp. @  $P, T > \text{ambient}$ .
  - Stringent test of kinetic mechanisms, for comb. model development
  - Canonical representation of turbulent “flamelet”

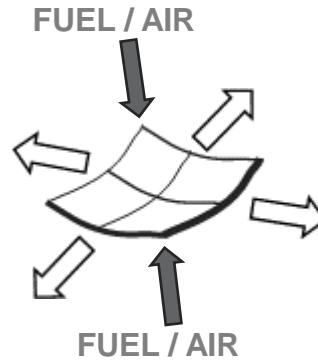
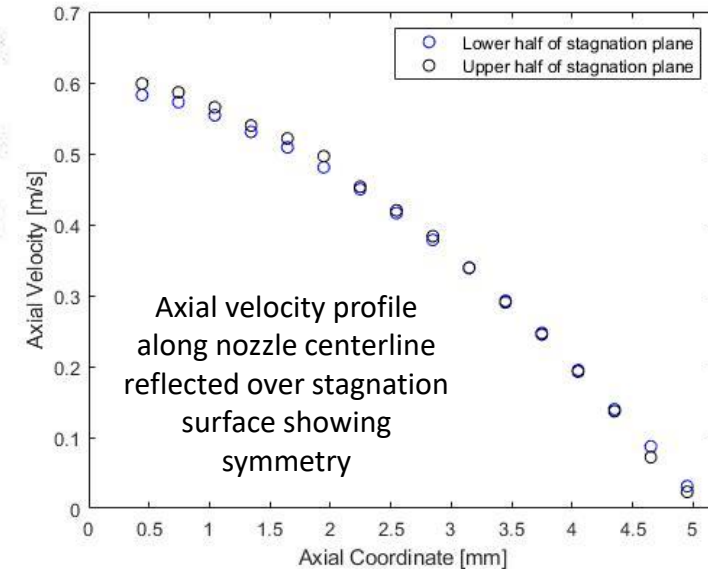
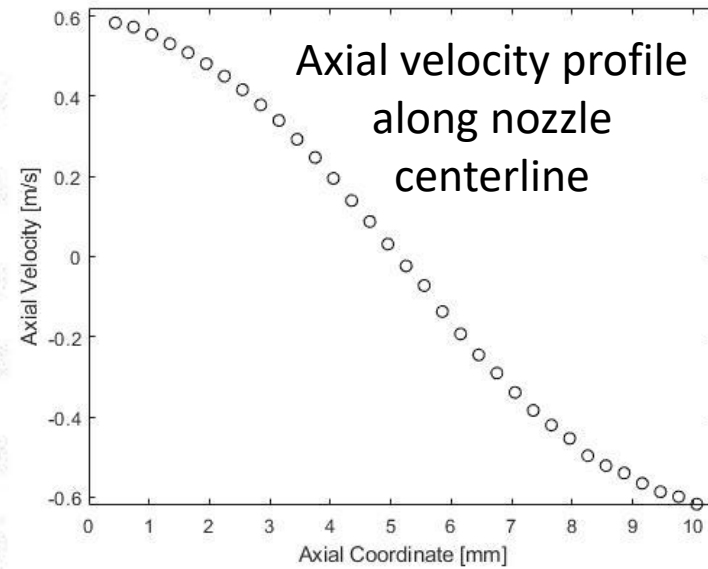
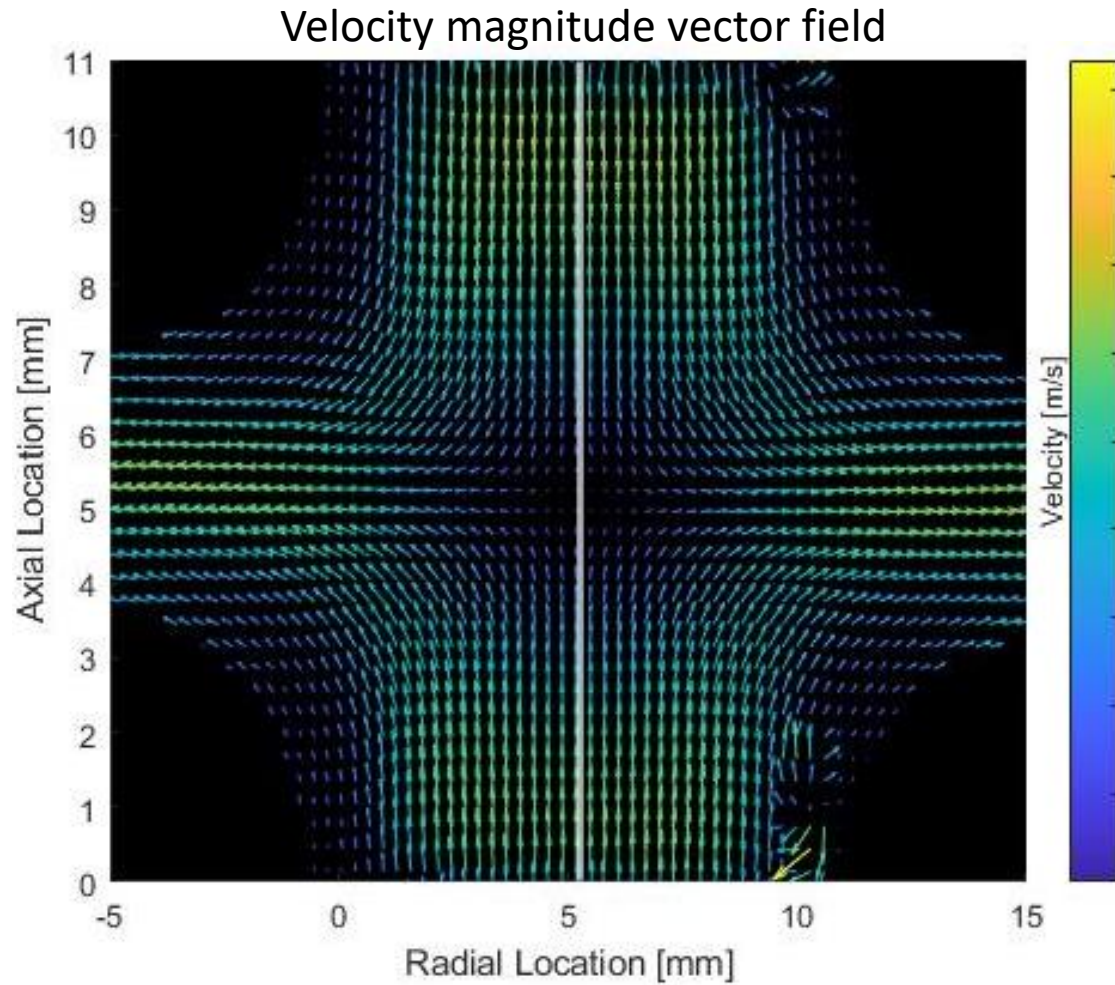
## UConn configuration & capability:

- >7-atm pressure vessel & feeds
- up to 500 K preheat capability



University of Connecticut

# Counterflow Experiments – Measure Flow Uniformity & Strain

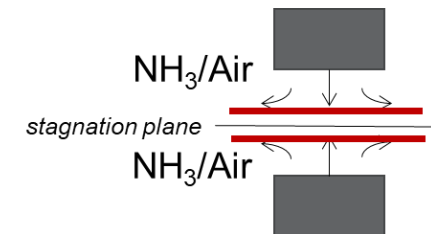


Flame stretch:

$$a_{STRETCH} = \frac{1}{A} \frac{dA}{dt}$$

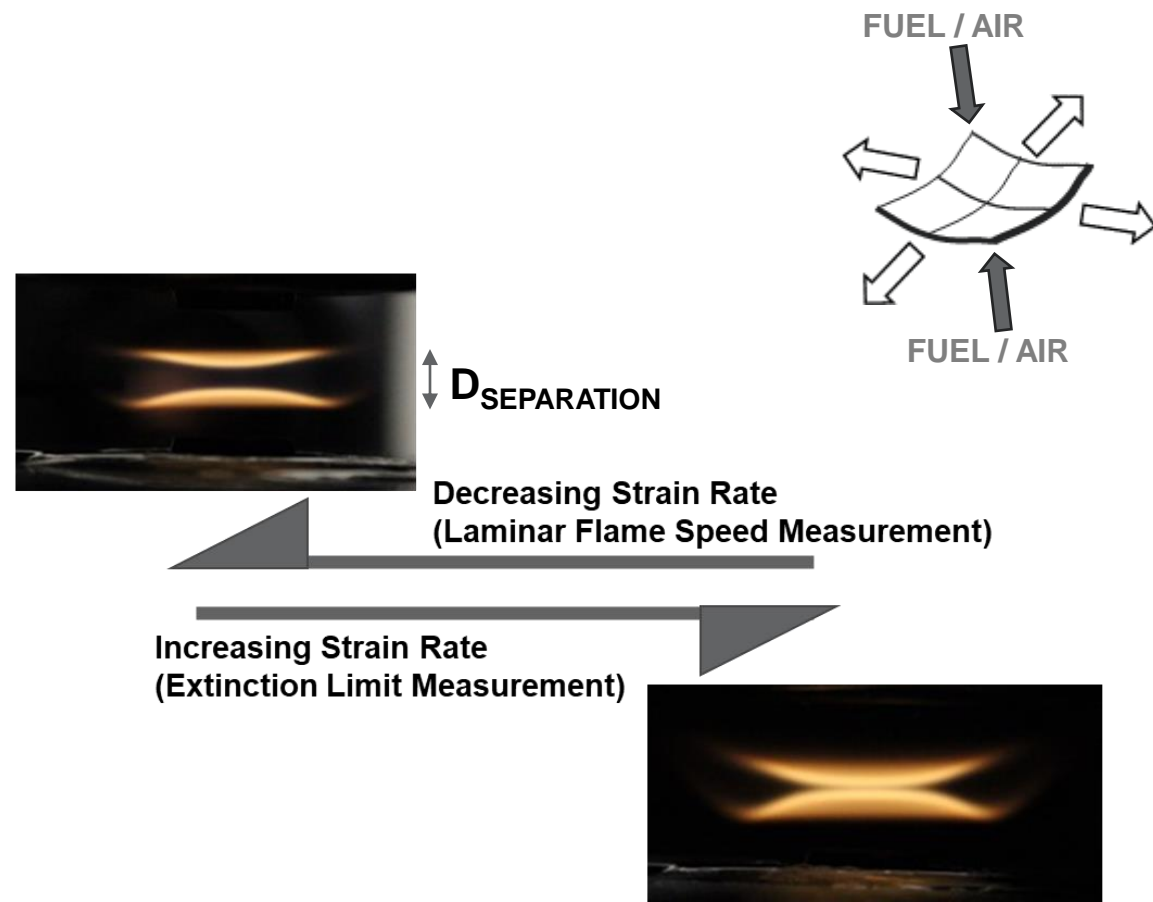
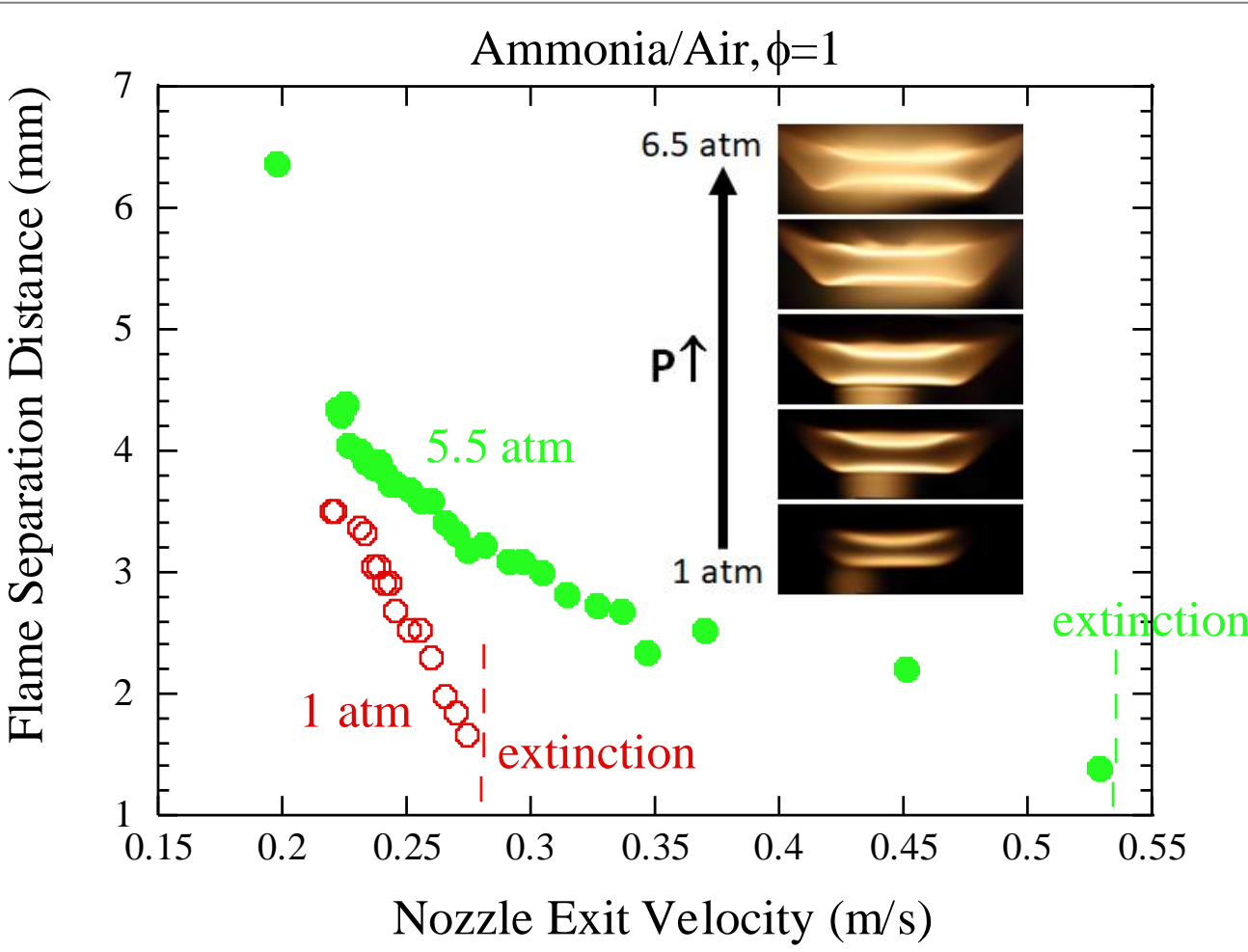
Define:  
Global / Centerline strain rate (for “plug” flow):

$$a_{GLOBAL} \sim \frac{4U_{JET}}{L}$$



Air at 5 SLPM flowrate + N<sub>2</sub> shroud ( $a \sim 200 \text{ s}^{-1}$ )  
1 atm, 295 K  
 $L = 10.4 \text{ mm}$ ;  $D = 10 \text{ mm}$

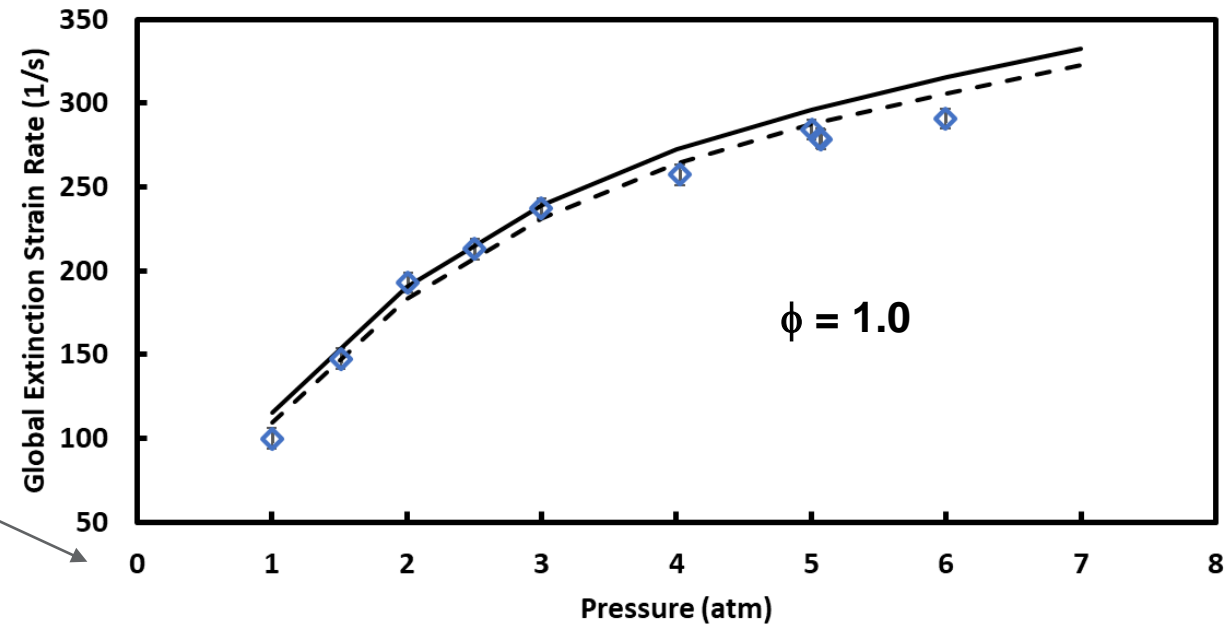
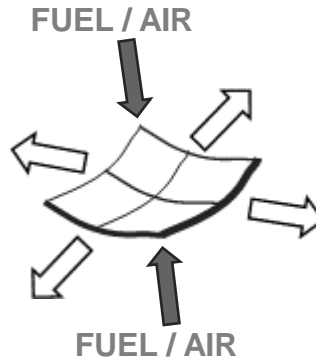
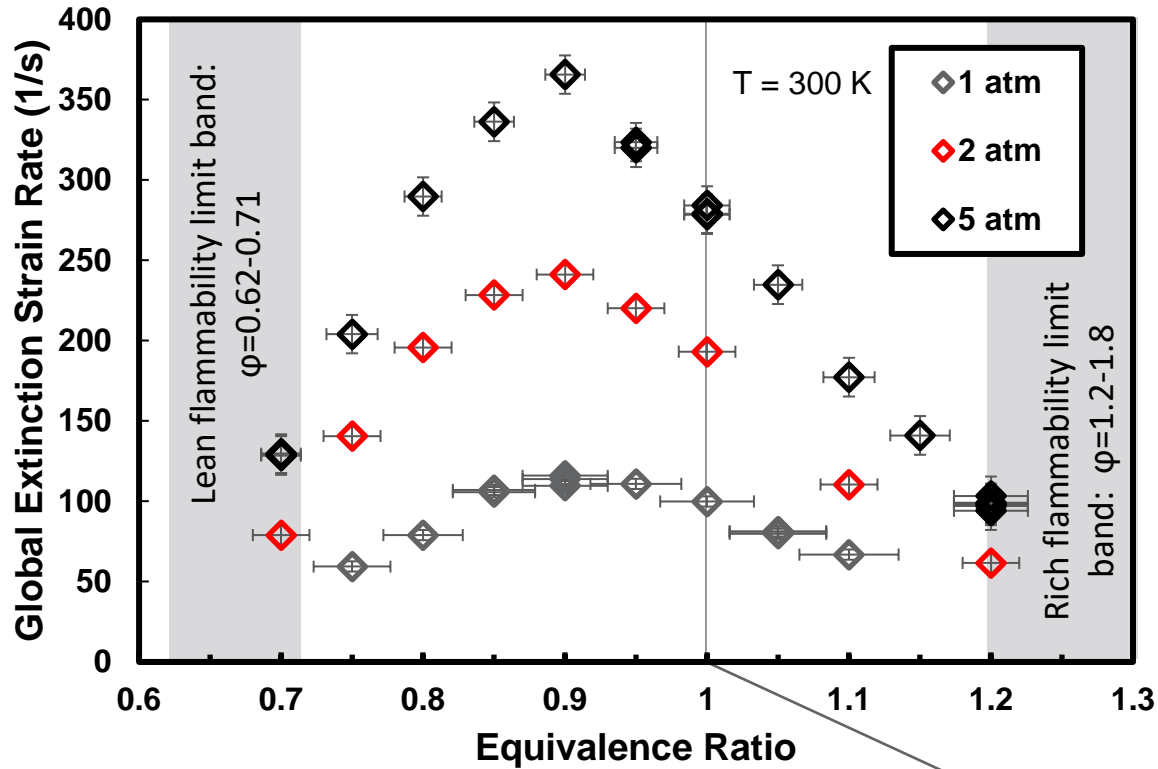
# Counterflow Experiments – Procedure for Measuring Extinction



- Sequence:**
- Establish stable, premixed  $NH_3$  / air flames @ initial  $D_{SEPARATION}$  ..... twin flames fixed in space
  - At fixed  $P, \phi$ : uniformly increase  $U_{JET}$  & observe  $D_{SEPARATION} \downarrow$
  - Quasi-steady approach to  $U_{EXT}$  at extinction  $\rightarrow \frac{4U_{EXT}}{L} = a_{EXT\_GLOBAL}$

...for both  
experiments  
& modeling

# Counterflow Experiments – Extinction Strain Rate vs. $\phi$ , $p$



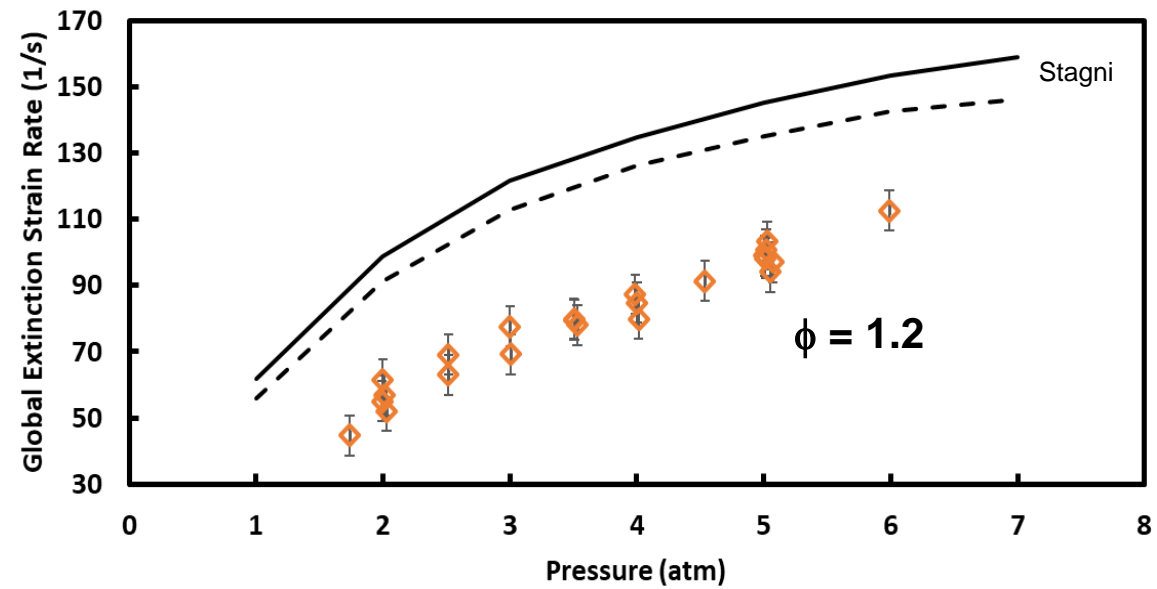
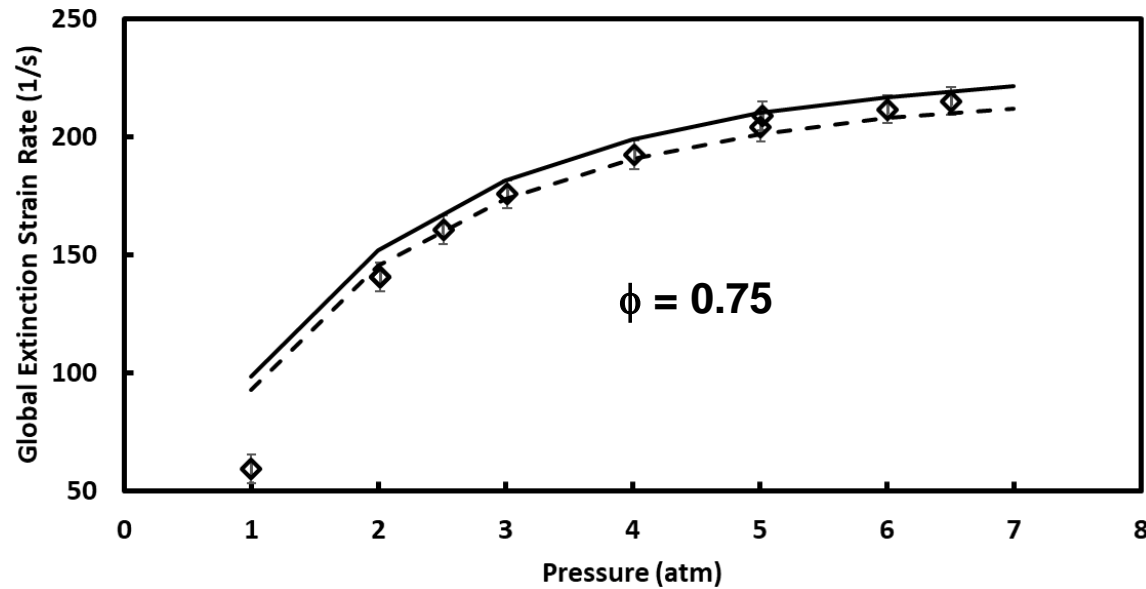
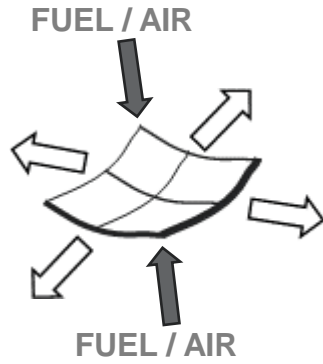
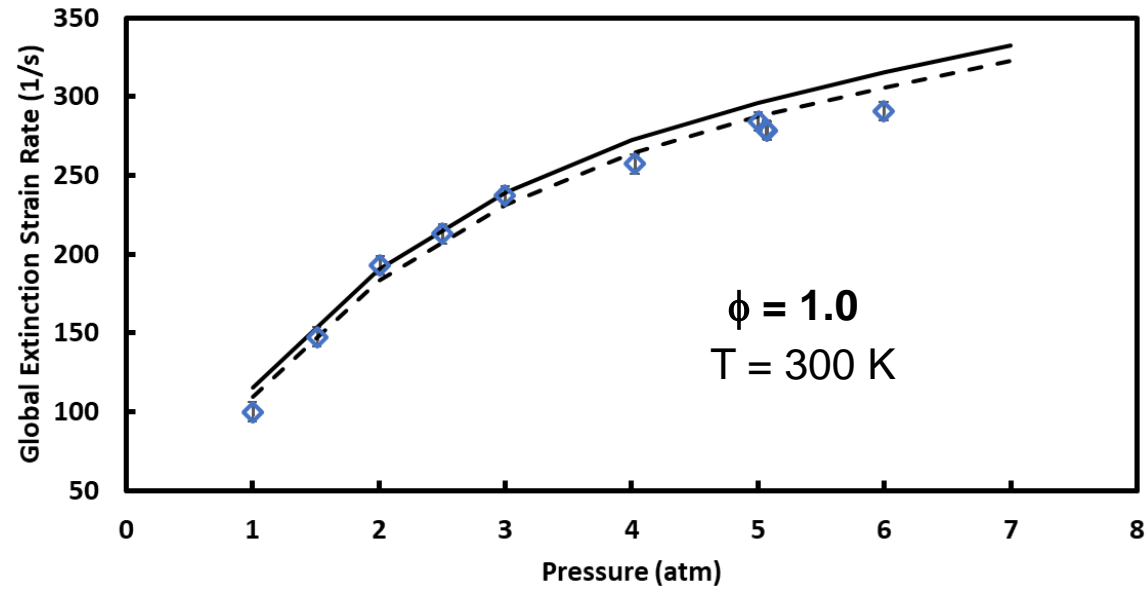
## Accuracy / Error Assessment:

- Flowmeter precision incl. accuracy & calibration
- (Many) representative data points repeated to establish variability / repeatability

Roll-off in  $a_{EXT}$  with pressure (non-linear)



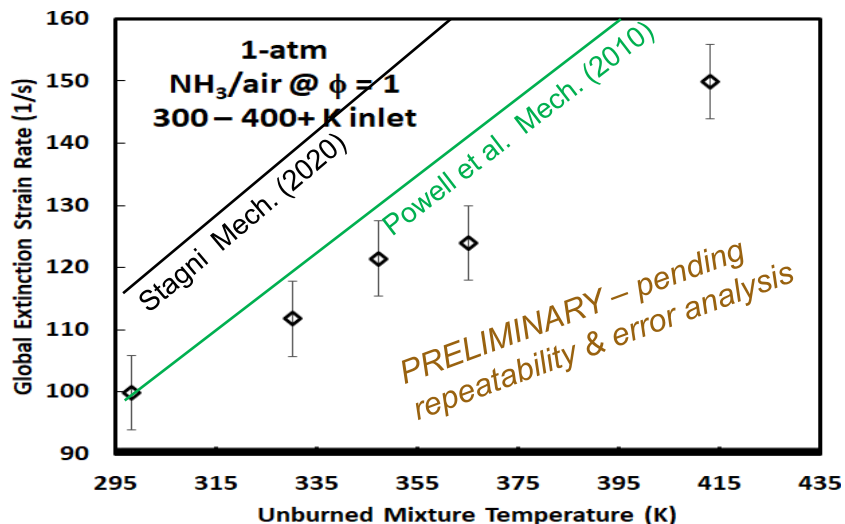
# Counterflow Experiments – Pressure Effect on Extinction (3 $\phi$ 's)



# UConn Next Steps – $T_{INLET} \uparrow$ , PIV ... Turb. Flame Speed Rig

## Ongoing Counterflow Flame Rig Work:

- PIV measurements for local velocities  $\rightarrow S_L$  &  $a_{EXT}$
- 300K to 500K  $T_{INLET}$  experiments  $\rightarrow a_{EXT}$  vs.  $T, P, \phi$



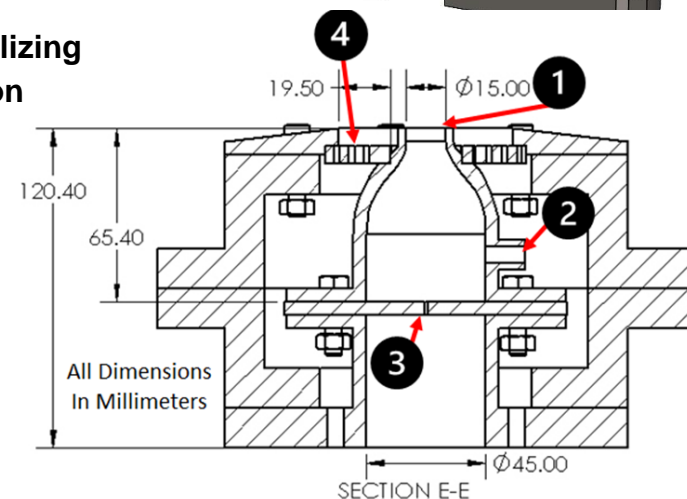
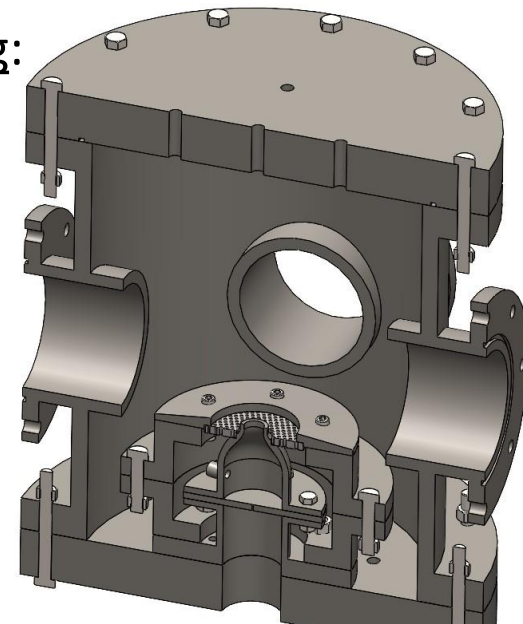
## Q3- Fabricate **Turb. Flame Speed Rig**:

Turbulent intensity range: 15–25%

1. NH<sub>3</sub> Bunsen Burner Outlet
2. Jet In Crossflow Port
3. Sharp-Edged Orifice Plate
4. H<sub>2</sub> Pilot Burner Plate

- NH PLIF for turbulent flame structure imaging
- High-speed PIV for turbulent flow-velocity characterization
- Turbulent intensity enhancement utilizing jet-in-crossflow & contraction section [e.g. Michigan\*/Lund\*\* Hi-Pilot/DRZ]

\*J.Driscoll, Univ. of Mich.; \*\*M.Alden, Lund Univ.



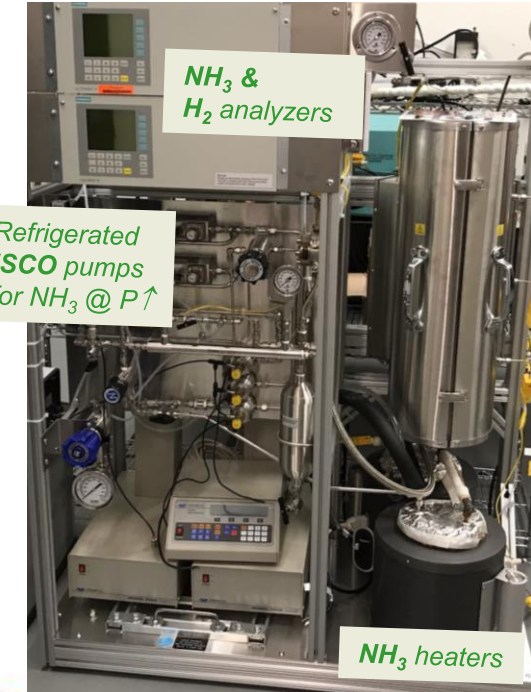
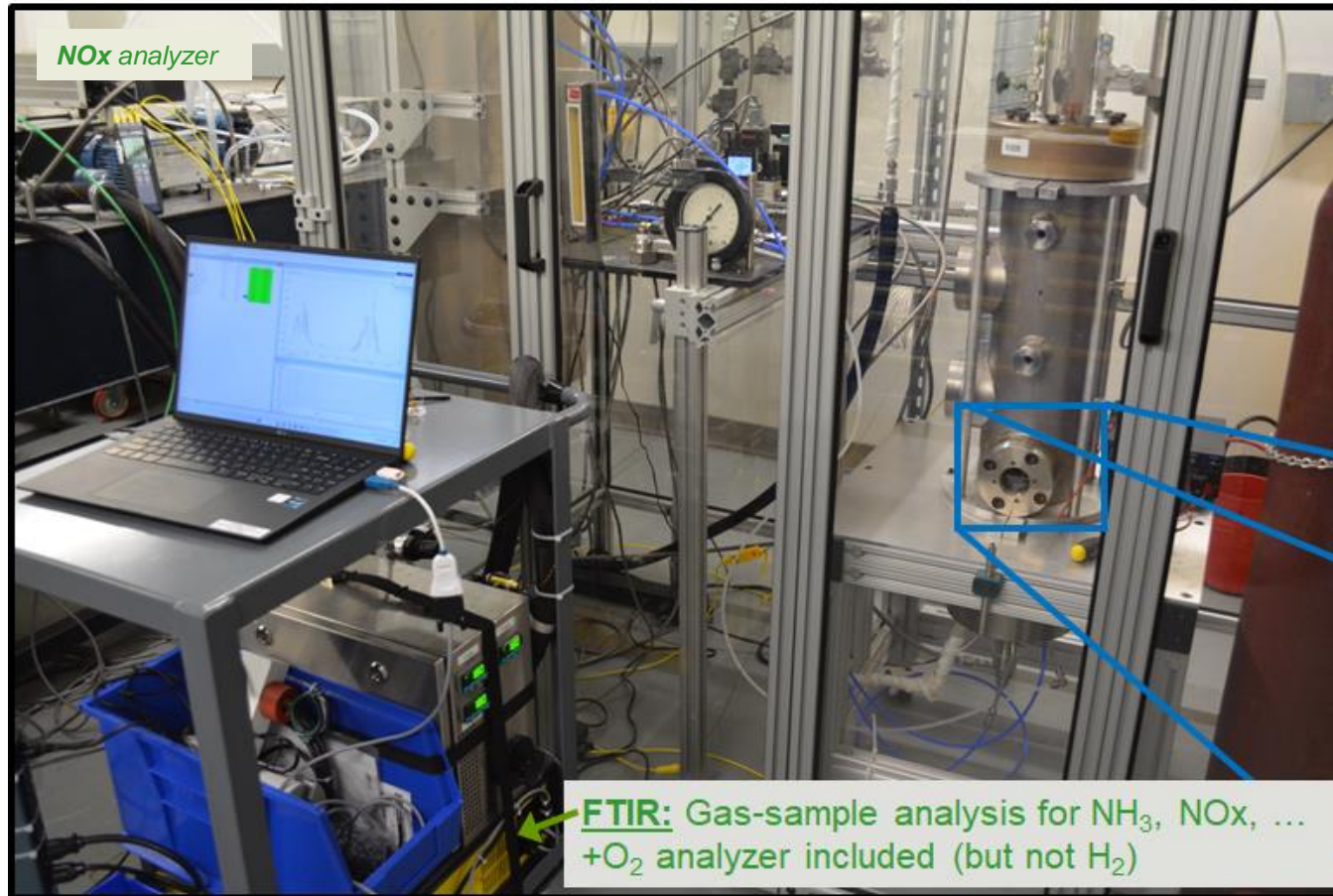
# Lab-Scale Experiment #2: High-P Flat-Flame Rig | *Laminar (1D)*

Relevance:

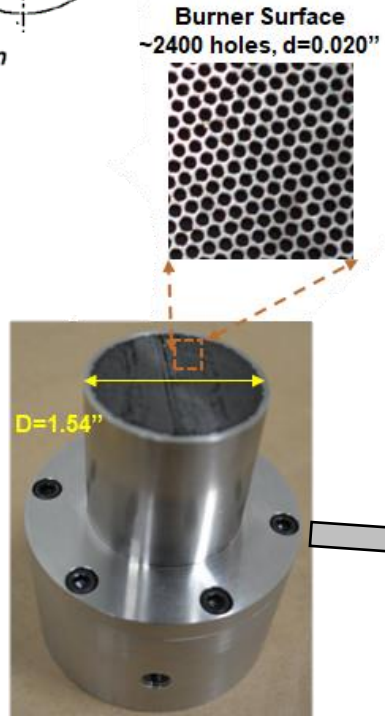
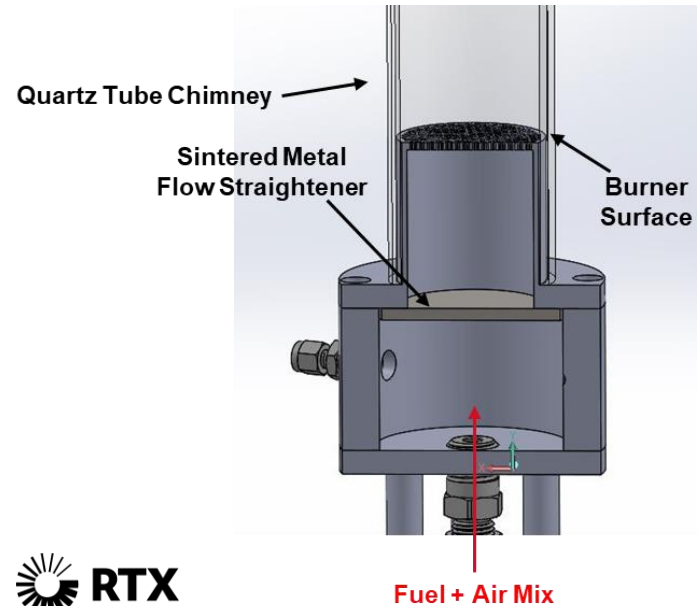
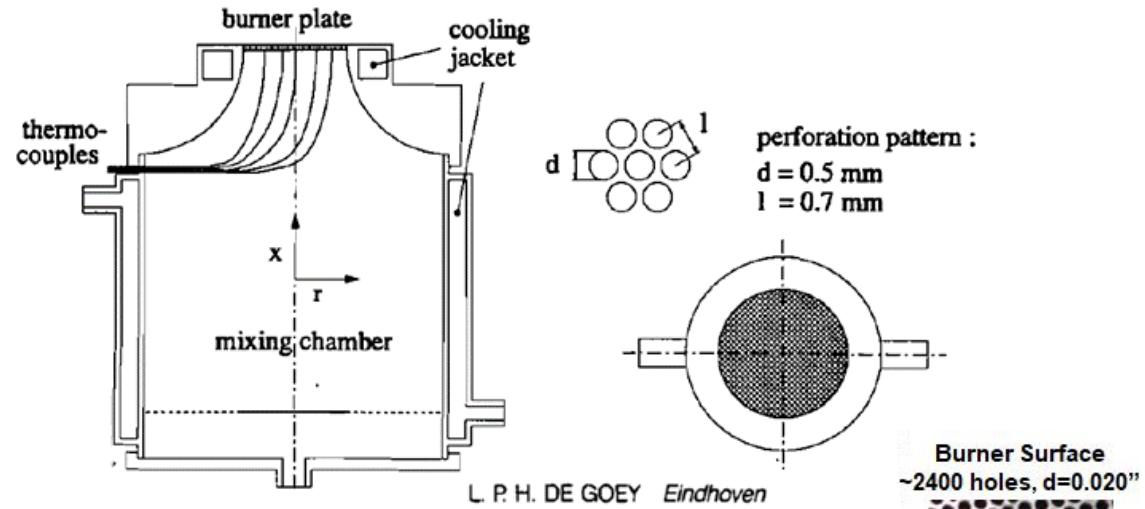
- Scarce data on  $\text{NH}_3$  flames &  $\text{NO}_x$  formation at  $\gg 10$ -atm.
- Capability to evaluate staged (RQL or “RRQL”) combustion of  $\text{NH}_3$

## RTRC configuration & capability:

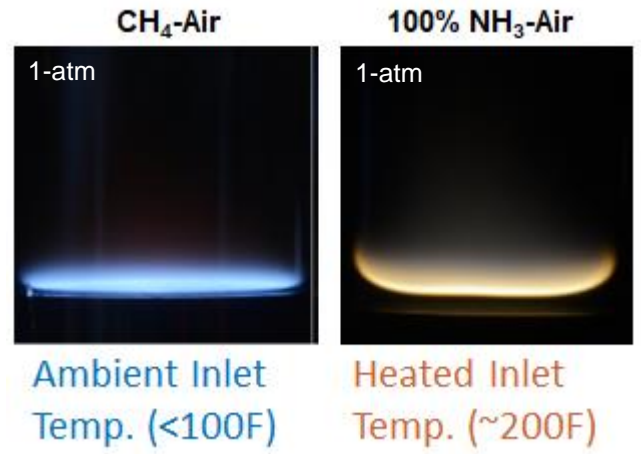
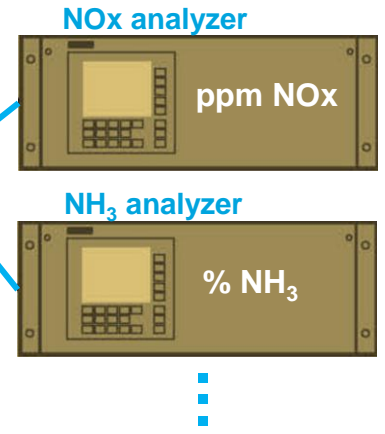
- **450** to  $>500+$  K preheat capability ( $>25$ -atm w/new heater install.)
- **10** to  $>25$ -atm pressure vessel & feeds ... fuel, air, &  $\text{N}_2$  chamber flow



# Flat-Flame Exper. – Premixed “Adiabatic” Burner & Emissions

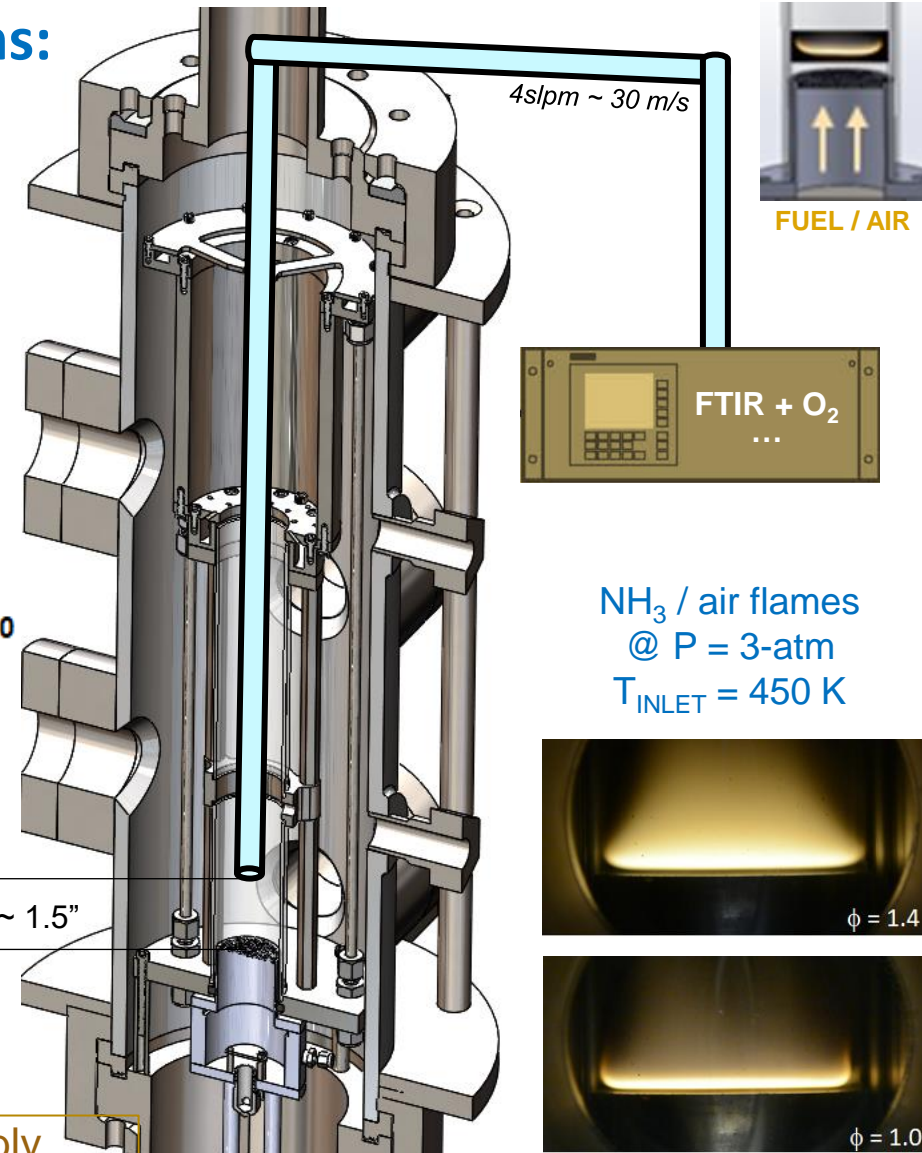
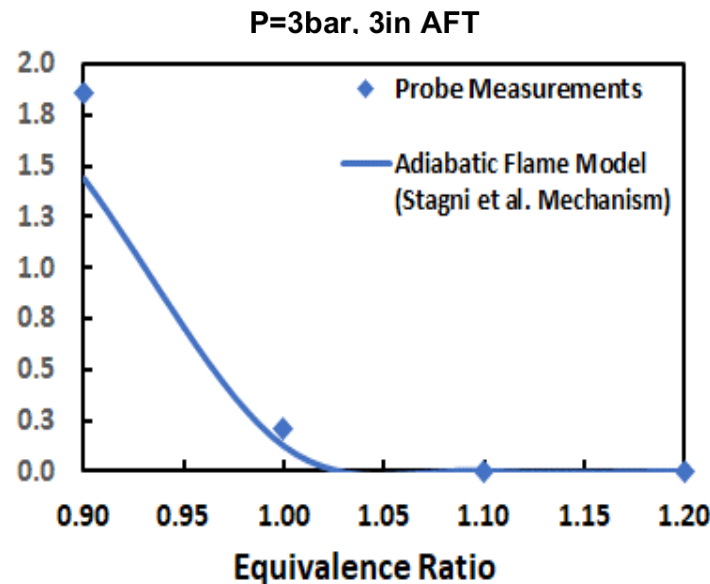
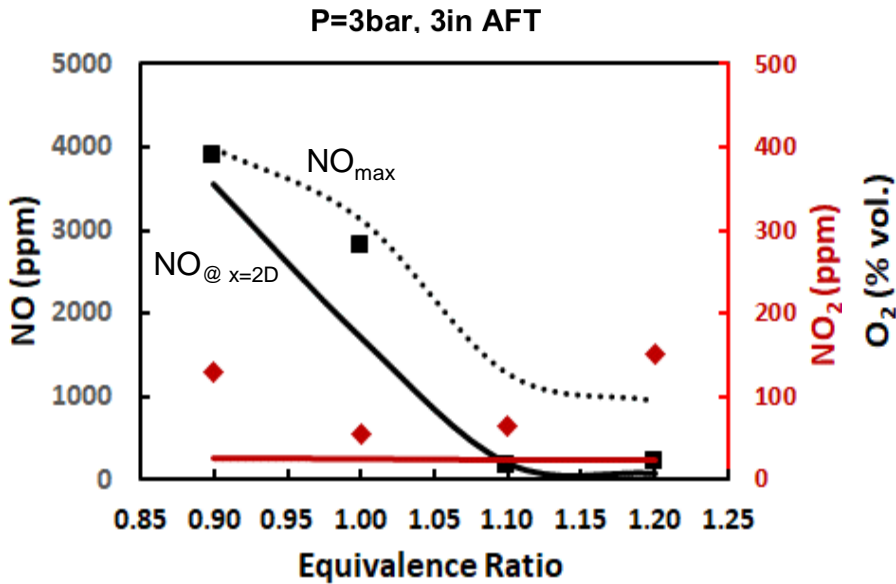


Traversable Emissions Probe (Air-Cooled)



# Flat-Flame Experiments – FTIR Measurements of NO<sub>x</sub> & NH<sub>3</sub>

## Measured NO<sub>x</sub> Values – Rich vs. Lean NH<sub>3</sub> Flame Emissions:



- 450 K preheat
- 12 cm/s burner face velocity
- $\tau \sim 60$  ms to 1D sample-probe location
- NEXT STEPS:
  - NH<sub>3</sub> & air preheat  $\uparrow$  as P  $\uparrow$  for stable flat flames
  - Rich, lean, & staged NO<sub>x</sub> / NH<sub>3</sub> studies vs. P, T
  - Burner instrumentation & Q<sub>LOSS</sub> characterization / control

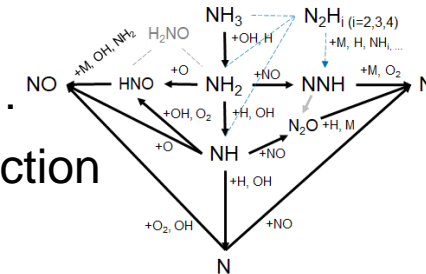
Note NH<sub>3</sub> flames do not anchor stably w/out preheat, especially @ P > P<sub>AMBIENT</sub>

# 2<sup>nd</sup> Technical Task .... MODELING .....

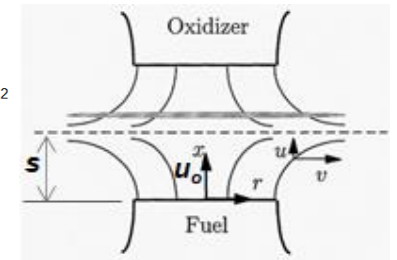
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FOCUS HERE:



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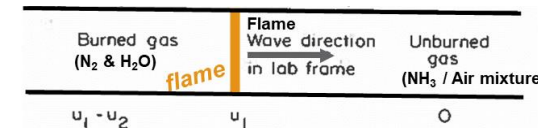
(2)  
MODELING

# Computational Methods

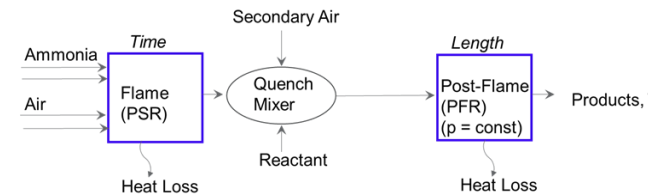


- Cantera, open-source computational framework developed by Dave Goodwin at Caltech
- Models developed for flame speed, chemical reactor networks (CRN), and counterflow flames (premixed & non-premixed)
- Additional tools developed to perform sensitivity analysis, including feature sensitivity (e.g. extinction strain rate), reaction path, chemical mechanism reduction and other diagnostic tools

## (i) Freely Propagating Premixed Flames (Flame Speed)

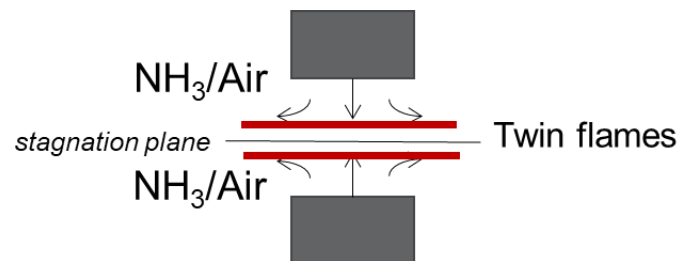


## (ii) NH<sub>3</sub> Chemical Reactor Network (CRN) Models

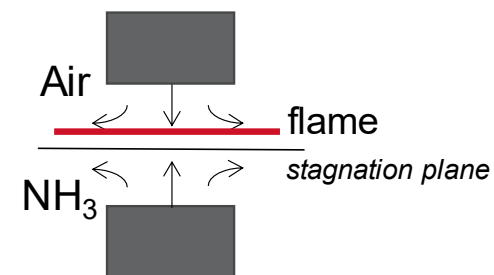


## (iii) NH<sub>3</sub> Counterflow Flames: Premixed and Non-Premixed

### Premixed Counterflow Flames



### Non-Premixed Counterflow Flames



FOCUS HERE

# Chemical Kinetic Mechanisms

Selected published, comprehensive N/H chemical mechanisms

- Open-source computational framework developed by Dave Goodwin at Caltech  Cantera

- **Glarborg et al. Mechanism (2018 & 2022 versions)**

[Glarborg, Miller, Ruscic, Klippenstein: Modeling nitrogen chemistry in combustion, Prog. Energy Combust. Sci. (2018) 31-68]

[Glarborg: The NH<sub>3</sub>/NO<sub>2</sub>/O<sub>2</sub> system: Constraining key steps in ammonia ignition and N<sub>2</sub>O formation, Combust. Flame, Vol. 257 (2023)]

- **Stagni et al. Mechanism (2020)**

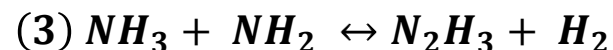
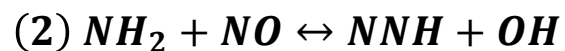
[Stagni, Cavallotti, Arunthanayothin, Song, Herbinet, Battin-Leclerc, Faravelli: React. Chem. Eng. 5 (2020) 696–711]

- **Powell & Papas et al. Mechanism- (2010 & 2011 versions) → RTRC**

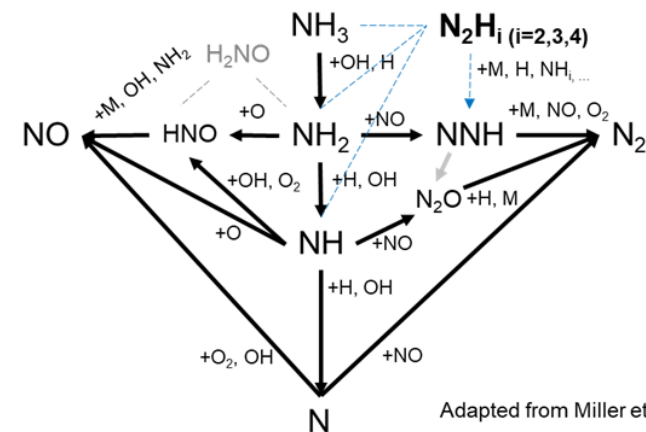
[Powell, Papas, Dreyer: Hydrogen- and C<sub>1</sub>-C<sub>3</sub> Hydrocarbon-Nitrous Oxide Kinetics in Freely, Propagating and Burner Stabilized Flames, Shock Tubes, and Flow Reactors, Combust. Sci. Tech. 182 (2010) 252-283]

[Powell, Papas, Dreyer: Flame Structure measurements of NO in Premixed Hydrogen-Nitrous Oxide Flames, Proc. Combust. Inst. 33 (2011) 1053-1062]

- Two “Powell” mechanisms differ by only 3 different rate expressions for amine radical reactions:



**Ammonia Oxidation Pathway Schematic**

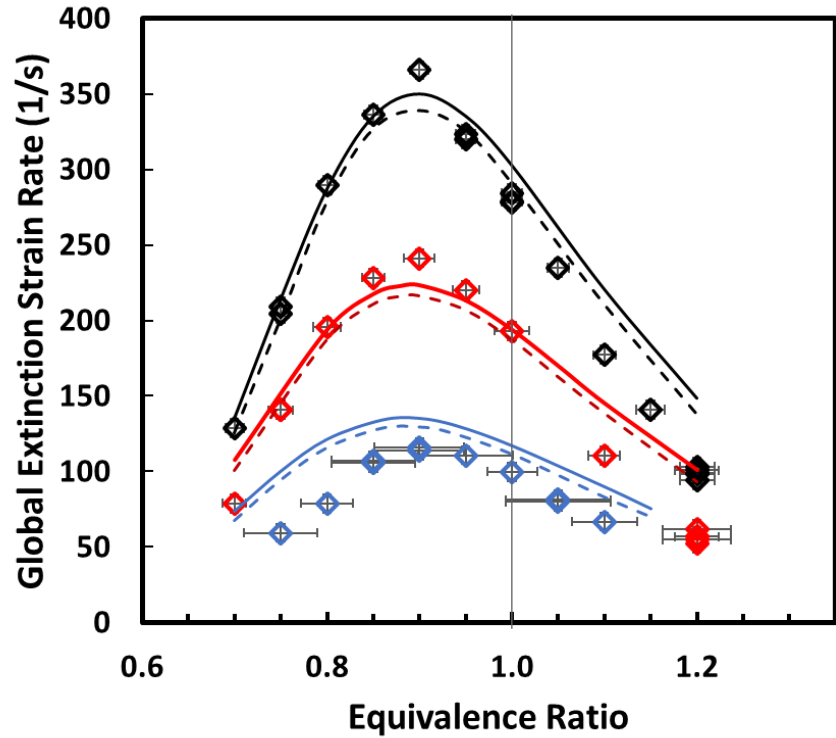
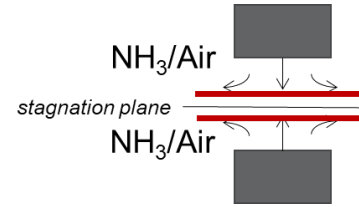


Adapted from Miller et al. (1983)

Approved for public release. © 2024 RTX. 16



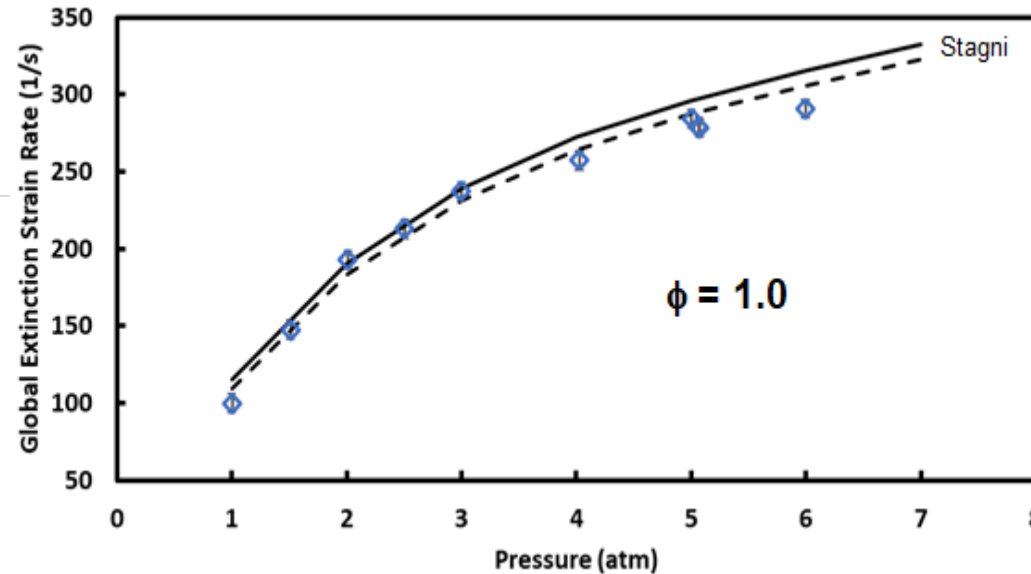
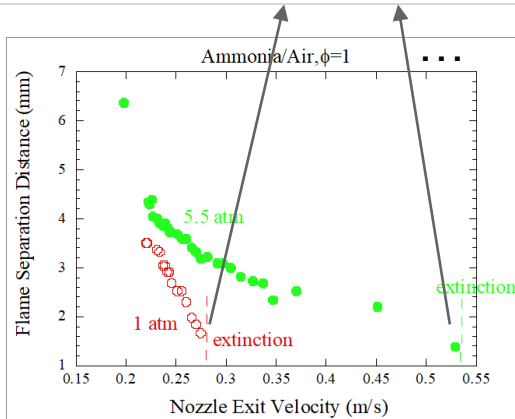
# RTRC Predictions vs. UConn Measurements (1/2)



- Stagni Mechanism
- ◆ 1 atm
  - ◆ 2 atm
  - ◆ 5 atm
  - Stagni\_2atm\_Adiabatic
  - Stagni\_5atm\_Adiabatic
  - Stagni\_1atm\_Adiabatic
  - - Stagni\_1atm\_Radiation\_Loss
  - - Stagni\_2atm\_Radiation\_Loss
  - - Stagni\_5atm\_Radiation\_Loss

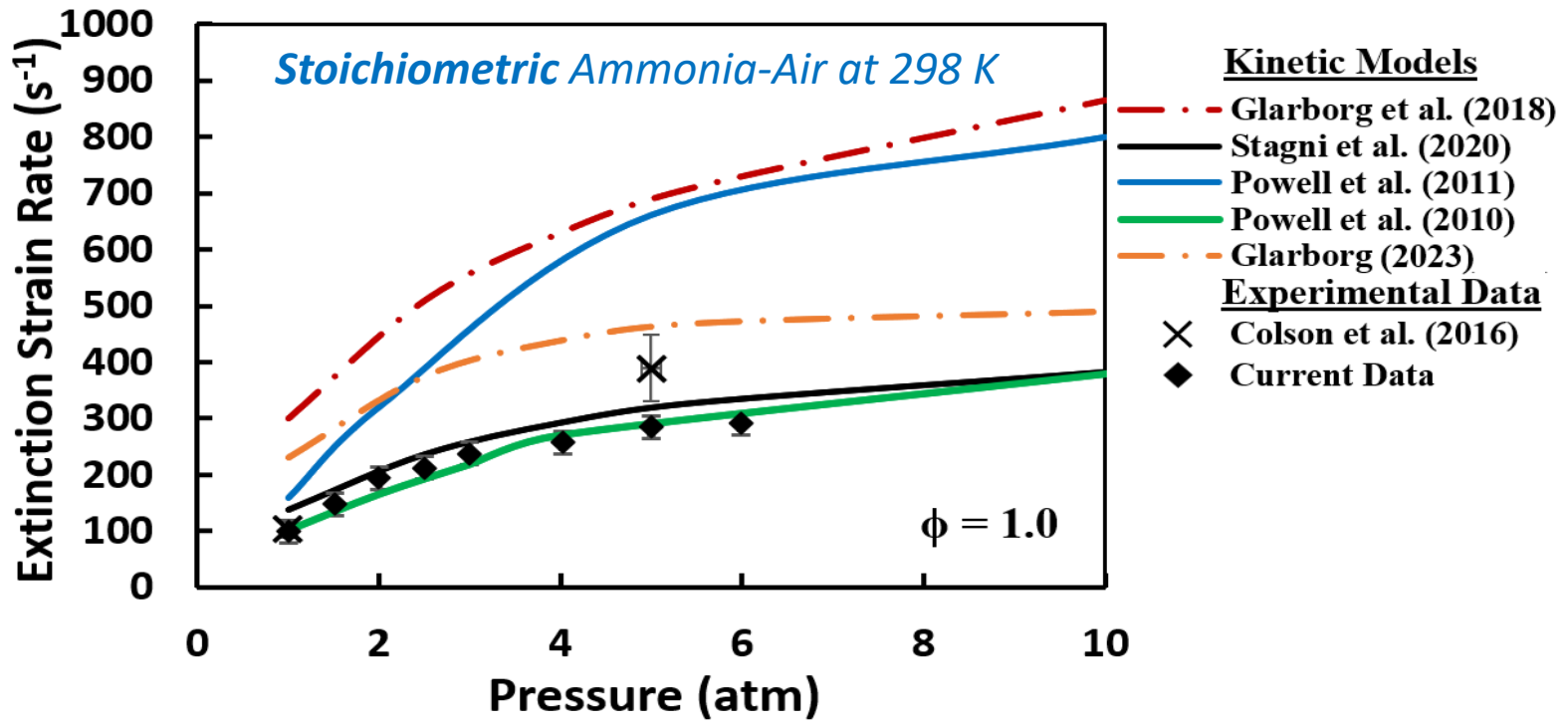
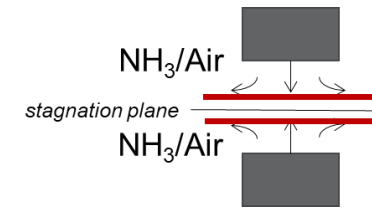
$$q_r = -4\sigma\kappa_p(T^4 - T_o^4)$$

Modified Counterflow Model scripts to account for radiative heat loss  
**Radiative heat loss per unit volume**  
 ( $\sigma$  = Stefan-Boltzmann constant,  $T_o$  = ambient unburnt reactant temp.,  
 $\kappa_p$  = total Planck's mean absorption coefficient)

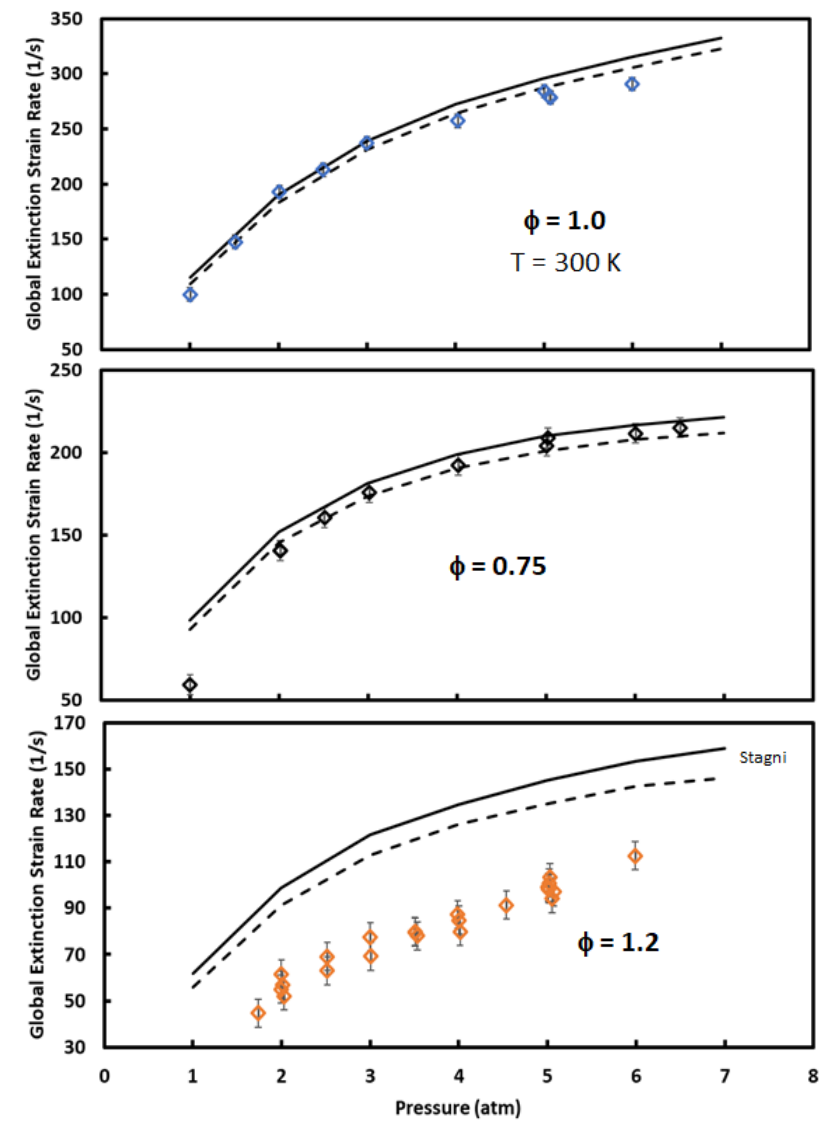
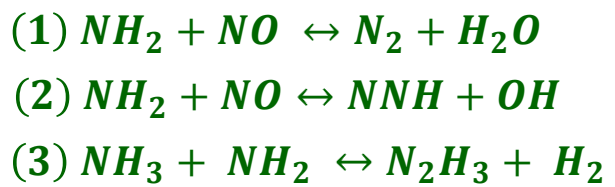


Roll-off in  $a_{EXT}$  with pressure (non-linear)

# RTRC Predictions vs. UConn Measurements (2/2)



• Two “Powell” mechanisms differ by only 3 different rate expressions for amine radical reactions:

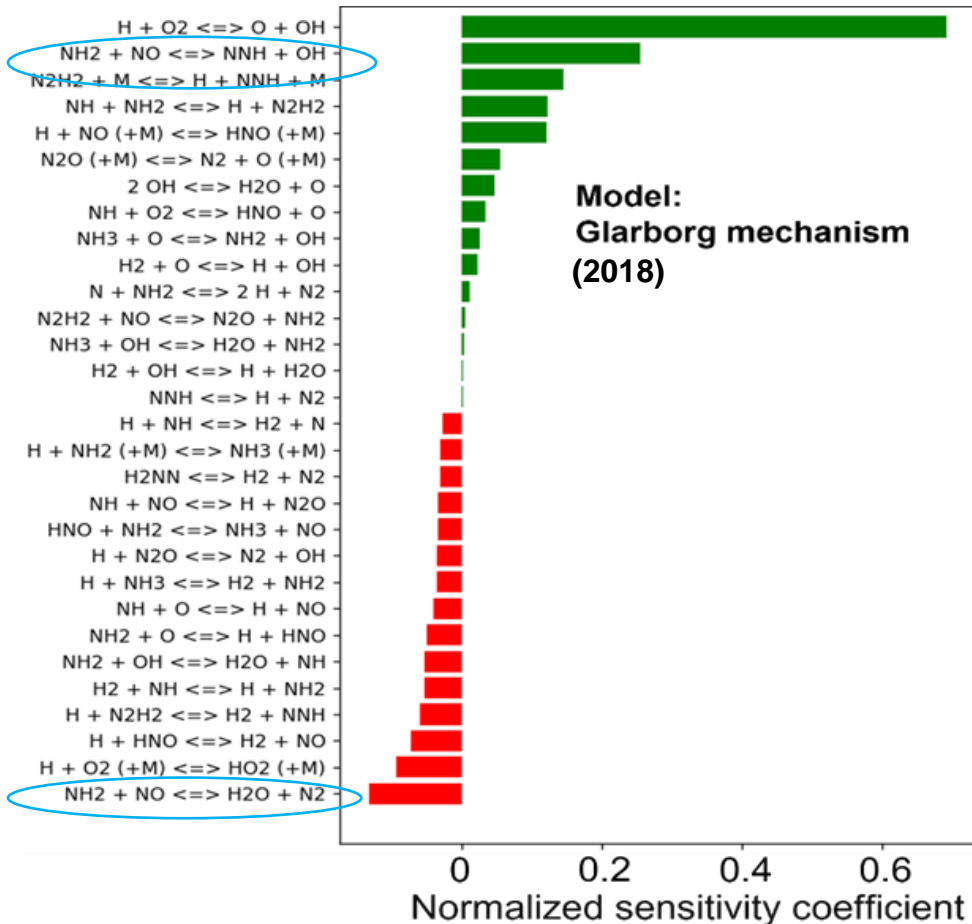


# Feature Sensitivity to Extinction Strain Rate

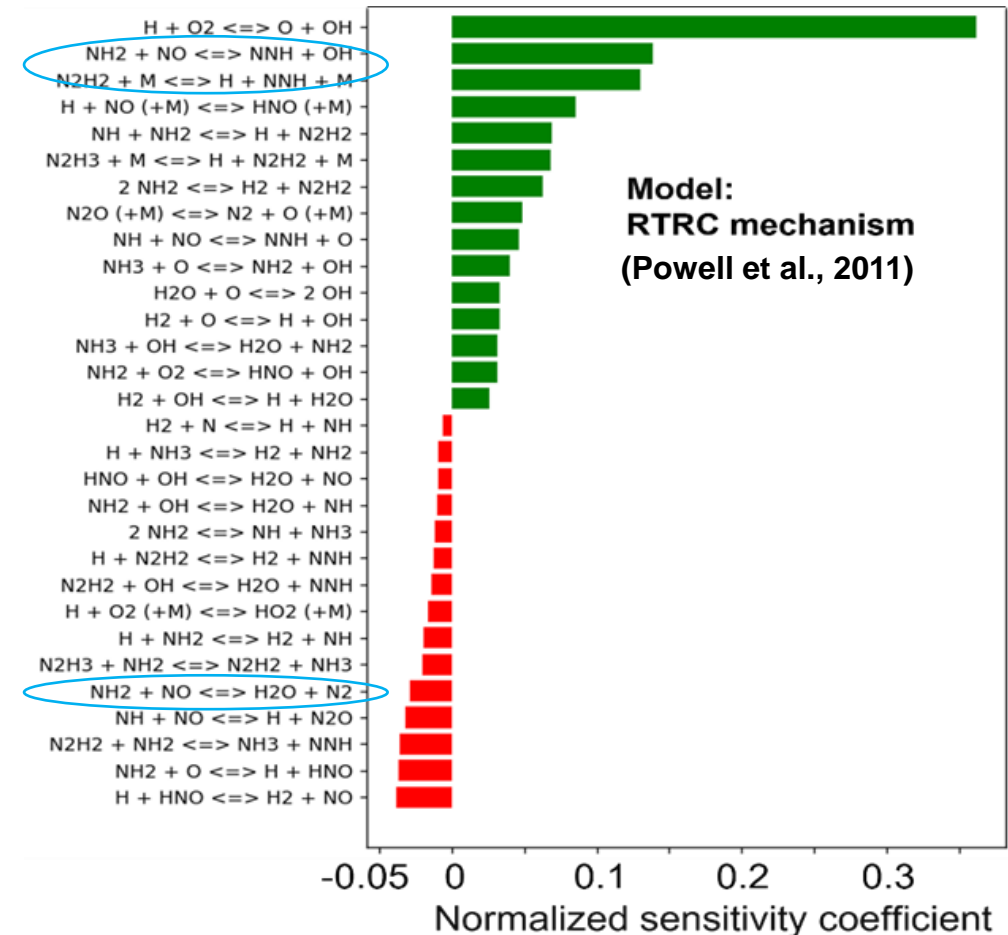
## NH<sub>3</sub>/Air Counterflow Flame

- (1)  $NH_2 + NO \leftrightarrow N_2 + H_2O$
- (2)  $NH_2 + NO \leftrightarrow NNH + OH$
- (3)  $NH_3 + NH_2 \leftrightarrow N_2H_3 + H_2$

T<sub>i</sub> = 301/333 K; P = 0.1 MPa



T<sub>i</sub> = 301/333 K; P = 0.1 MPa



**Sensitive rate constants:**

### NH<sub>2</sub>/NO Interactions

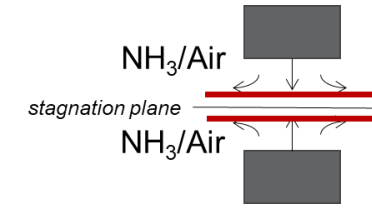
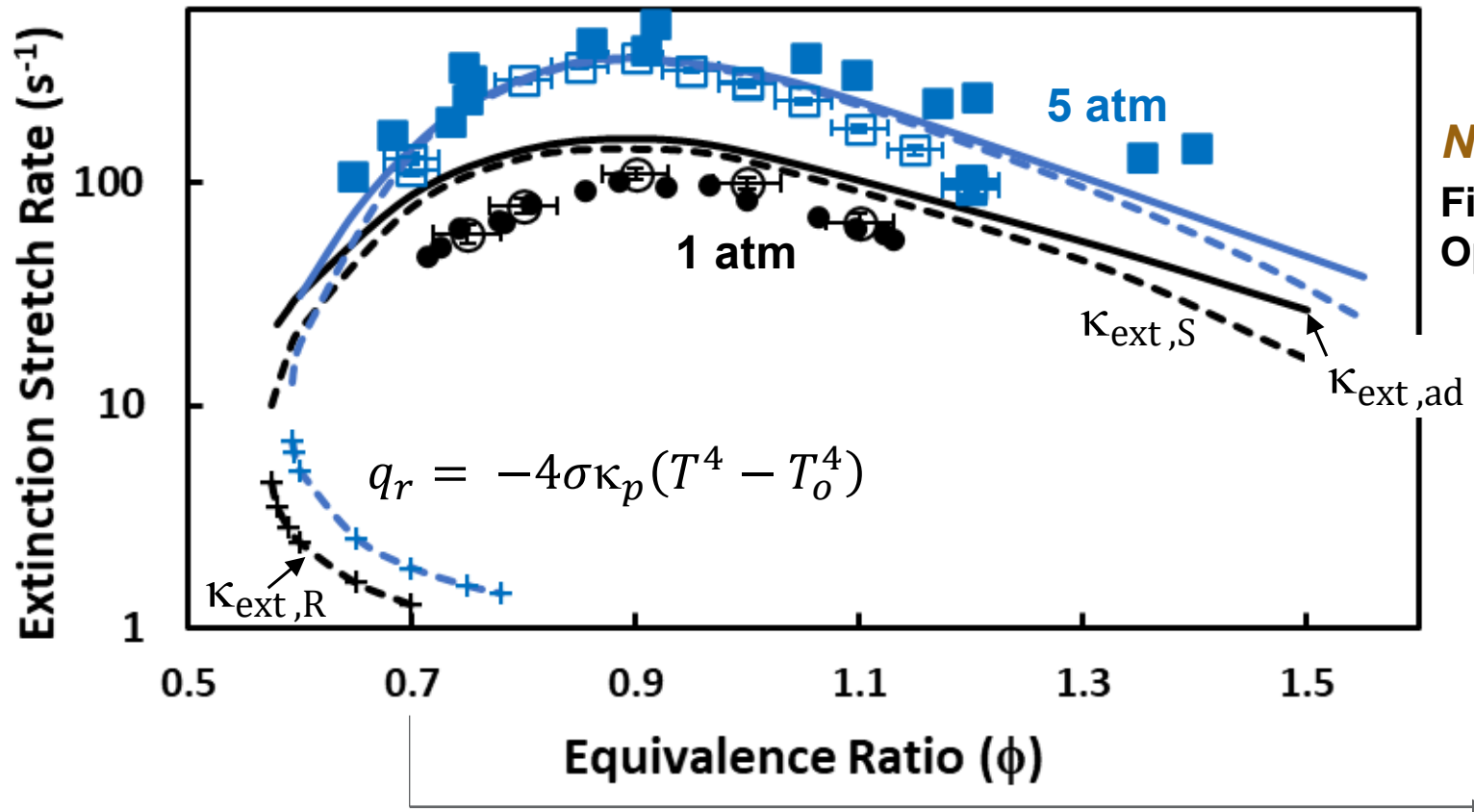
- (1a)  $NH_2 + NO \leftrightarrow N_2 + H_2O$
- (1b)  $NH_2 + NO \leftrightarrow NNH + OH$

### NH<sub>i</sub>/N<sub>2</sub>H<sub>i</sub> Reactions

- (2a)  $N_2H_2 + M \leftrightarrow NNH + H + M$
- (2b)  $N_2H_3 + M \leftrightarrow N_2H_2 + H + M$

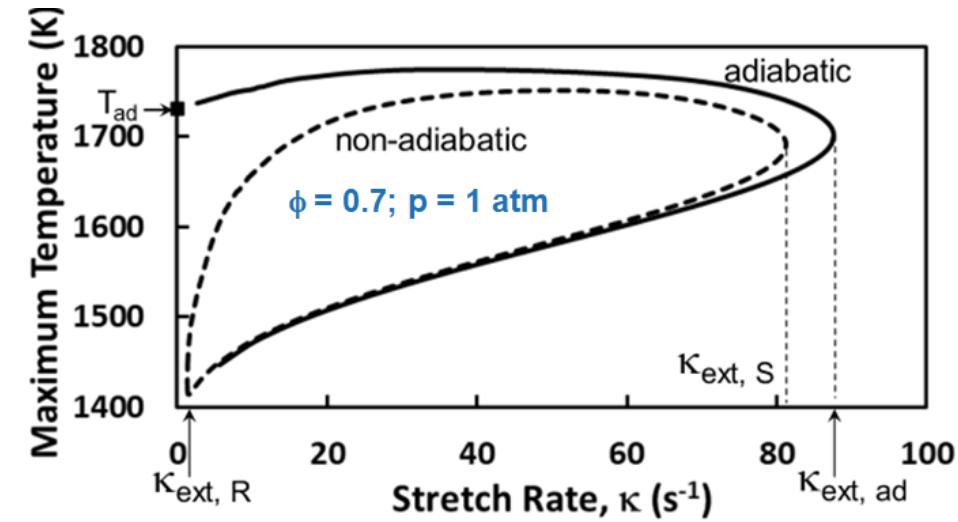
**Sensitive and Uncertain rate constants**

# Counterflow NH<sub>3</sub> Flames w/Heat Loss → Impact & Lean Limit



## NH<sub>3</sub>/Air Counterflow Flames

Filled Symbols: Colson et al. (2016)  
 Open Symbols: UConn Data (2023-4)

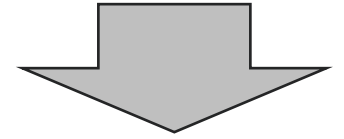


C-shaped curve for counterflow premixed fuel-lean, ammonia-air flames showing **i.** adiabatic stretch-induced stretch rate  $\kappa_{ext,ad}$  (solid line), **ii.** non-adiabatic stretch-induced stretch rates  $\kappa_{ext,S}$  (dashed line), and **iii.** radiative-induced stretch rates  $\kappa_{ext,R}$  (+ symbols).

# Modeling Activities & Next Steps ..... Toward GT Design

- Outcomes/Publications (to-date):

- *Proceedings of the Combustion Institute* – 40<sup>th</sup> CI Symposium paper in press for July 2024
- *AIAA SciTech 2024* – paper # AIAA-2024-2019 ( DOI:10.2514/6.2024-2019 )
- *Combustion Institute Meetings – 2023 US National & ESS Spring 2024* meeting papers



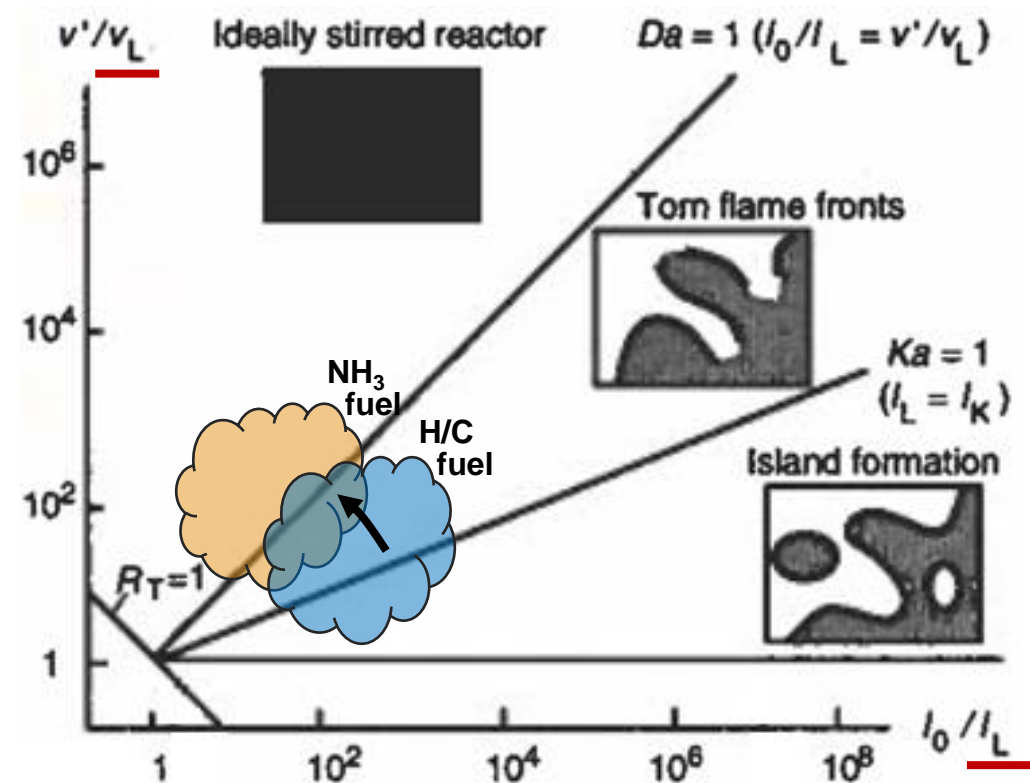
## Turbulent combustion regime for NH<sub>3</sub>-fueled gas turbines:

- $v'$  &  $l_0 \sim$  independent of fuel type (only aero dependent)
- $v_L \downarrow$  w/ NH<sub>3</sub> fuel
- $l_L \uparrow$  w/ NH<sub>3</sub> fuel
- shift by  $\sim 5 - 10x$

validate w/ turb. flame  
rig measurements

## CFD modeling of NH<sub>3</sub>-fueled gas turbine combustor:

- Challenges:
  - Efficient flamelet models uncertain (regime = ??)
  - NO<sub>x</sub> cannot be post-processed (integral to comb. rxns)
- For efficient GT design calculations, *possible approaches*:
  - Reduced NH<sub>3</sub>/NO<sub>x</sub> kinetics w/transport, e.g. EDC\*\*
  - Steady RANS turbulence model saves computational power for chemistry/transport

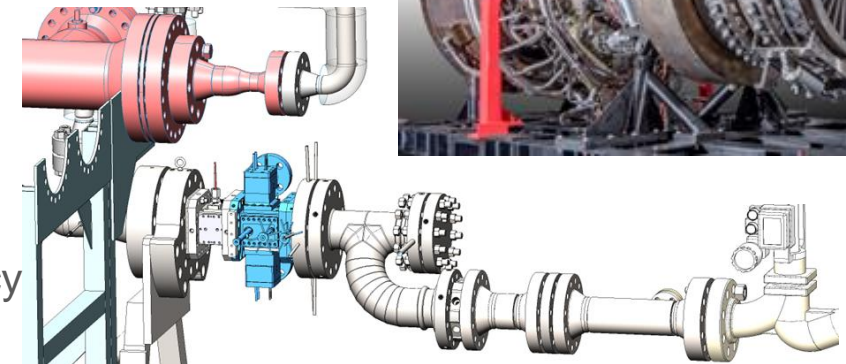


# 3<sup>rd</sup> Technical Task .... GAS TURBINE COMBUSTOR DESIGN (PREP) .....

## Low-NOx Operable Ammونيا-Combustor Development (LOAD-Z)

- Fundamental NH<sub>3</sub> flame data relevant to turbines:
  - P, T >> ambient → relevant to compressor exit conditions .....
  - strained & turbulent flames .... ..
  - Targeted outcome: expand published data w/ new, useful data (previously unreported)
- Predictive capability for NH<sub>3</sub> combustion & emissions
  - NO<sub>x</sub> formation kinetics integral w/ NH<sub>3</sub> comb. kinetics .....
  - CFD of turb. NH<sub>3</sub> flames w/ NO<sub>x</sub> & NH<sub>3</sub> slip ( $\eta_{\text{COMB}}$ ) prediction
    - Targeted outcome: capability for GT combustor design
- **Develop & test NH<sub>3</sub> gas-turbine combustor “@ scale”**
  - Single-nozzle-rig (SNR) scale demo. @ high P, T .....
  - Pure NH<sub>3</sub> combustion @ 75% – 100% power
    - Targeted outcome: < 30ppm NO<sub>x</sub>\*\* & >99.99% efficiency

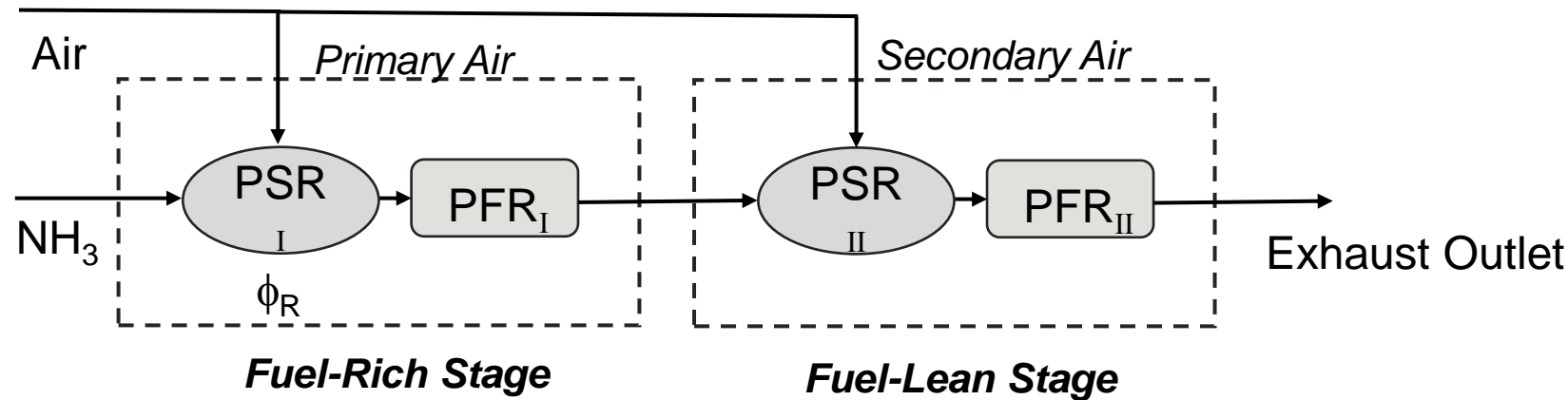
(3)  
DESIGN & DEMO.



\*\*Note recent ETN recommendations for NO<sub>x</sub> reporting with hydrogen-containing fuels

# Chemical Reactor Network (CRN) Modeling

## CRN Model Schematic for RQL Combustor



- Validation against available simulation data from Li et al., Fuel 355 (2024) 129509.
- Overall “theoretical” NO<sub>x</sub> levels <30 ppm for a RQL architecture appear feasible**
- Established N/H mechanisms show wide variability for NO<sub>x</sub>

$$\phi_R = 1.25$$

Total Residence time $\tau$ (ms)	$\tau_{\text{PSR}_I}$ (ms)	$\tau_{\text{PFR}_I}$ (ms)	$\tau_{\text{PSR}_{II}}$ (ms)	$\tau_{\text{PFR}_{II}}$ (ms)	Pressure (atm)	Inlet Temp. (K)	Outlet Temp. (K)	NO <sub>x</sub> * (ppm)
20	3	14	2	1	12	600	1850	38.5
20	3	14	2	1	30	700	1850	30.1
30	3	24	2	1	30	700	1850	22.9

\* 15% O<sub>2</sub> dry

**END**