



THE OHIO STATE UNIVERSITY

Hydrogen Fuel Effects on Stability and Operation of Lean-Premixed and Staged Gas Turbine Combustors

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University Turbine Systems Research and Advanced Turbines Program Review Meeting

October 30, 2023

Awarded under DE-FOA-0002397 (Project number FE0032076)

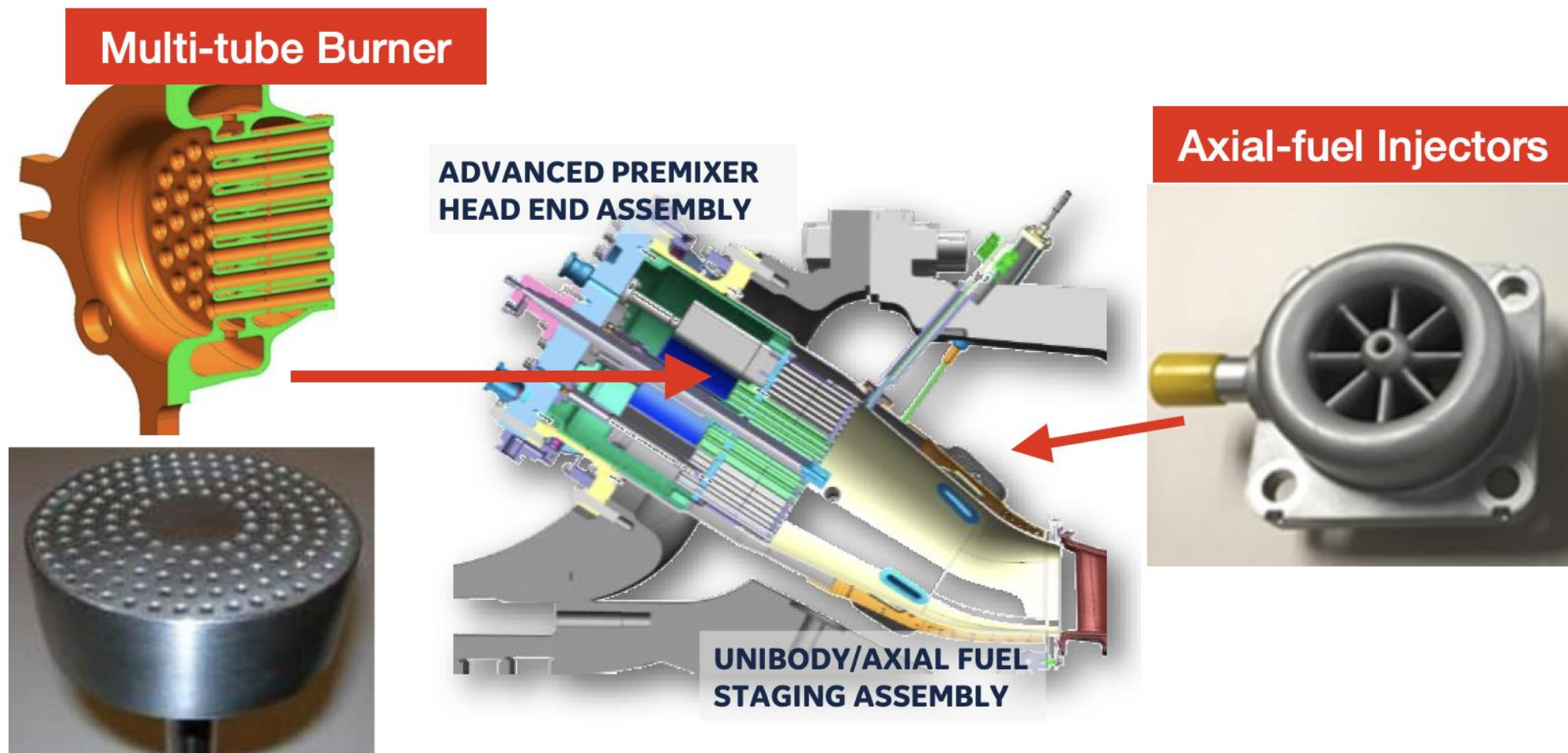




- Background
- Project Objectives, Scope, and Technical Approach
- Experimental Update – Year 2 (OSU – Jeff Sutton)
- Computational Updates – Year 2 (UM – Vansh Sharma)



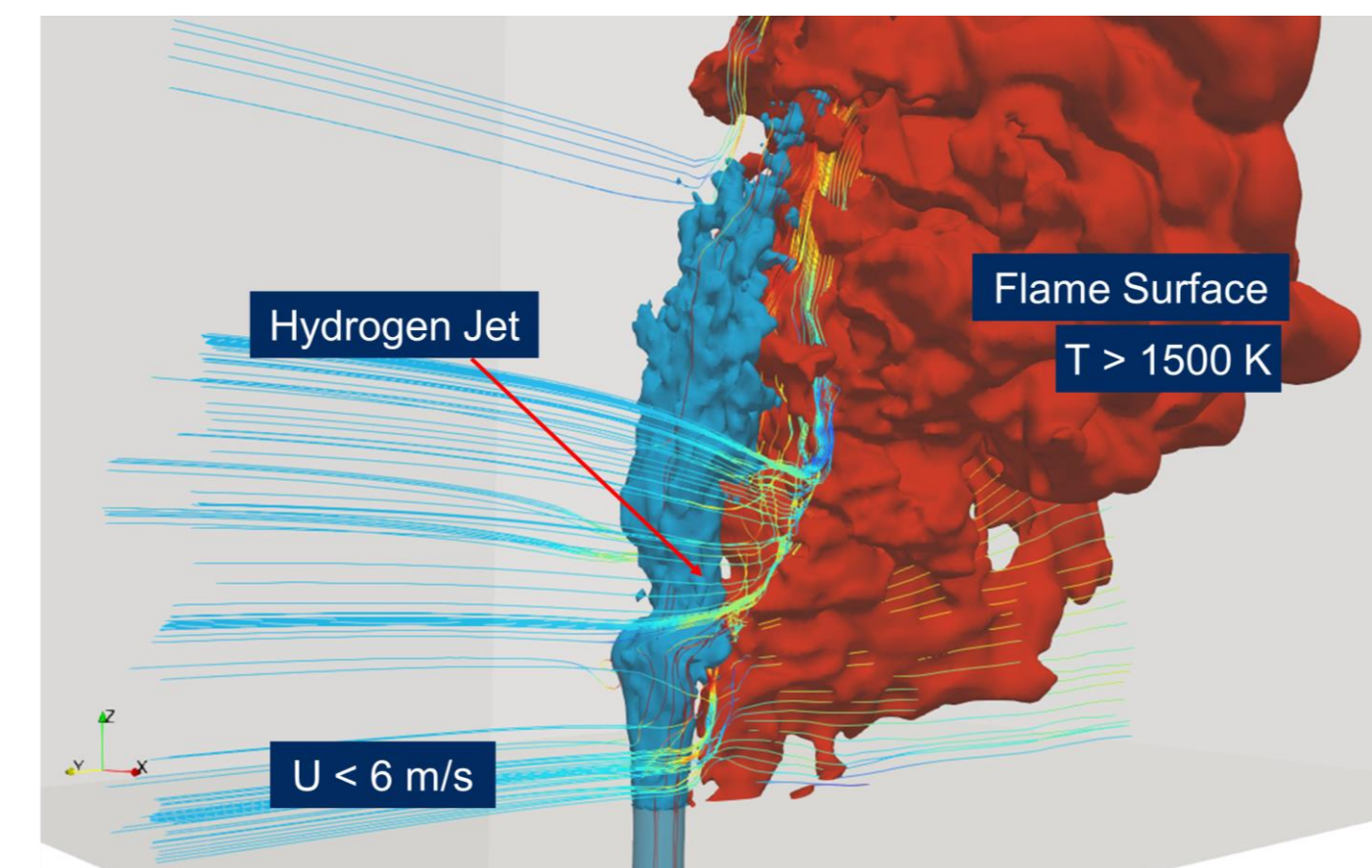
The focus of this work is on core flow physics and flame processes that control combustor operation using hydrogen and hydrogen-containing (HC) fuels (i.e., H₂/HC blends)



GE 9HA and 7HA machines with premixer/primary combustor and axial fuel staging

- Modern gas turbine designs use a lean, premixed primary burner and an axially staged secondary burner
- Significant development of hydrogen combustion technology with DoE support (up to 50% by vol)
- Limiting design constraints are dictated by hydrogen level

- Hydrogen is more reactive than HCs and has a high molecular diffusivity
- The limiting processes (flame holding, blowout, and flashback) are controlled by several fluids/heat transfer phenomena that interplay with one another
- There is a need for a broad set of experiments/computations to address issues
 - Advanced tools (laser diagnostics/DNS/LES)
 - Relevant conditions (H₂ content, pressure, confinement/wall effects, etc)



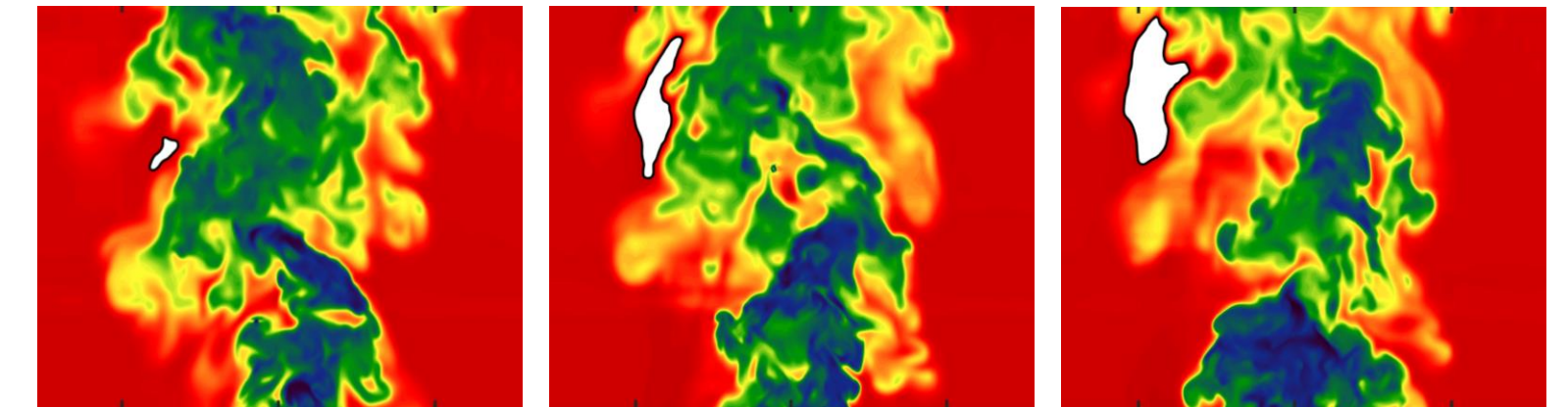
Sharma, Tang, Raman, AIAA Scitech, 2024



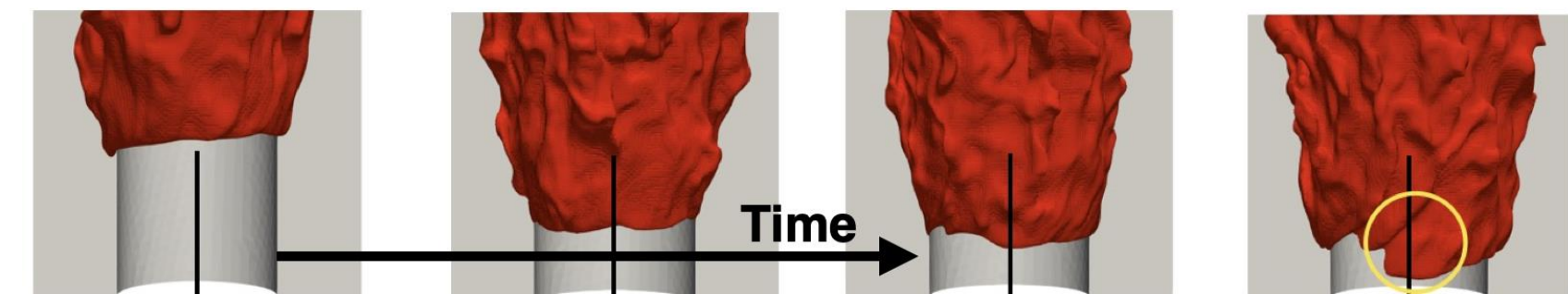
Technical Objectives: Joint experimental and computational effort to (1) investigate physics governing flame stabilization and flashback (2) develop predictive computational tools for simulating gas turbine combustion **when burning hydrogen-containing (HC) fuels**

Project Objectives:

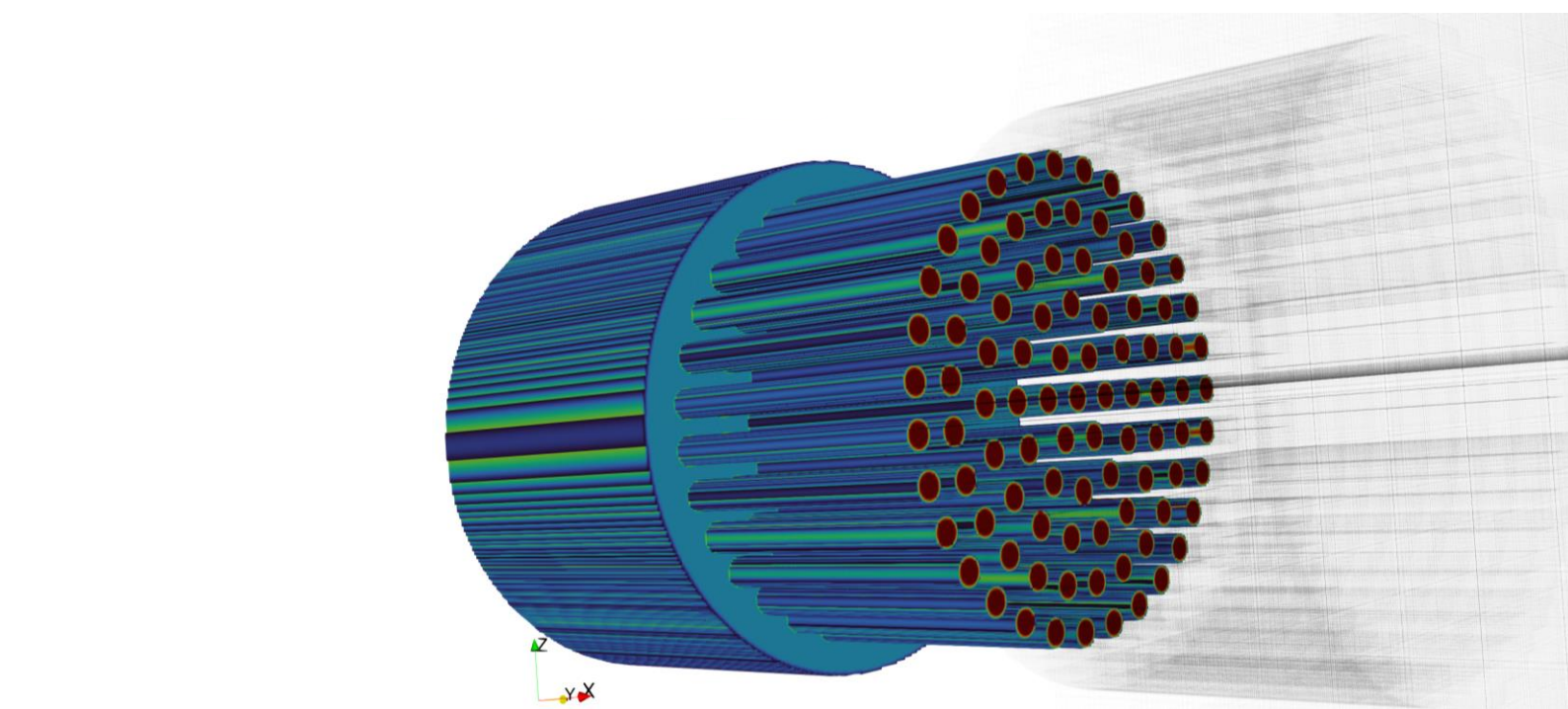
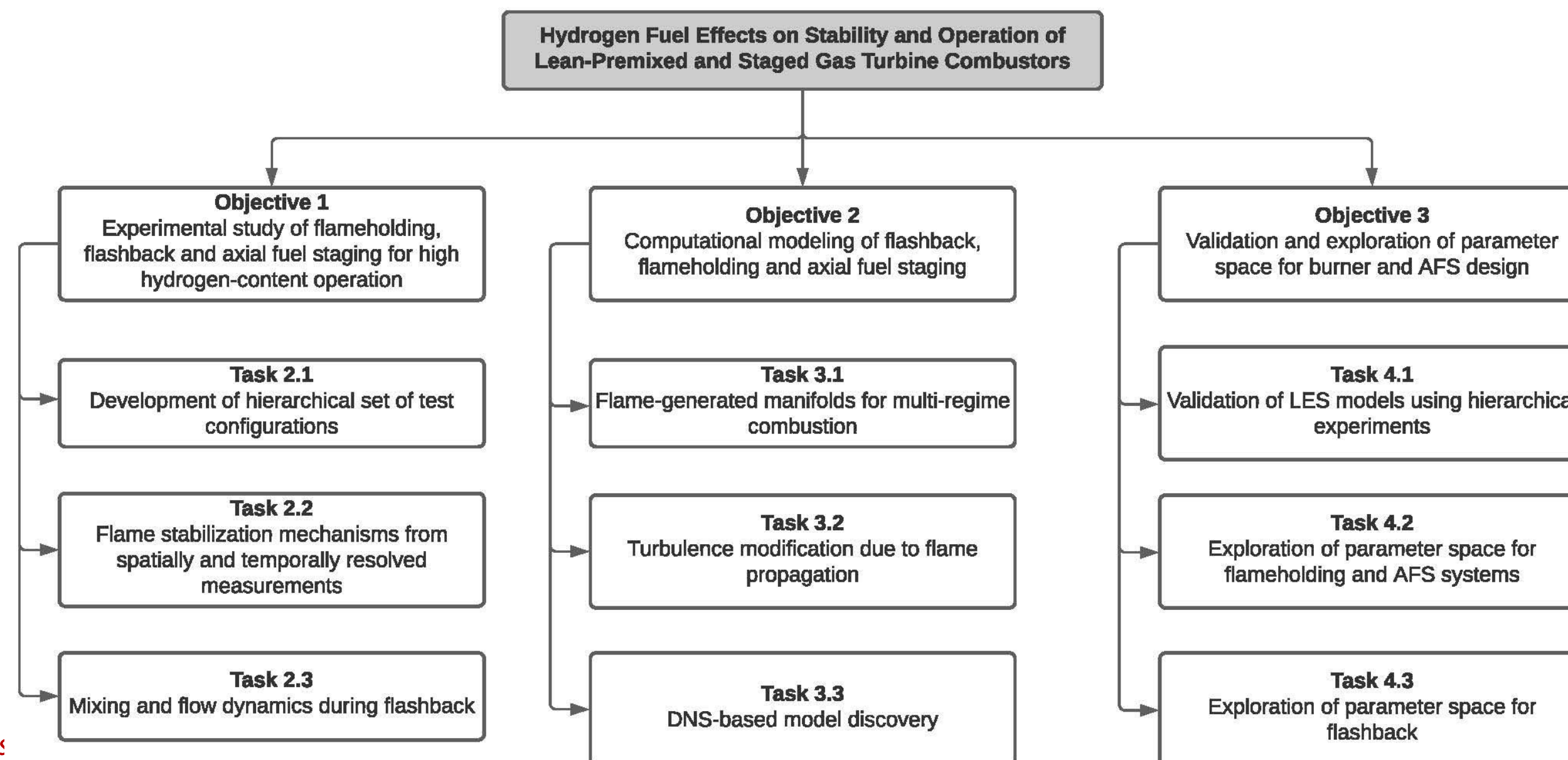
- Objective 1 – use hierarchy of experiments/laser diagnostics to quantify rate-limiting physics; what physics need to be captured in models?
- Objective 2 – develop suite of validated, multi-regime computational models
- Objective 3 – characterize operability and operational limits (exploration of parameter space) for burner and AFS systems



Time-resolved temperature fields during auto-ignition



Simulation of flashback along a centerbody in swirling flow using LES



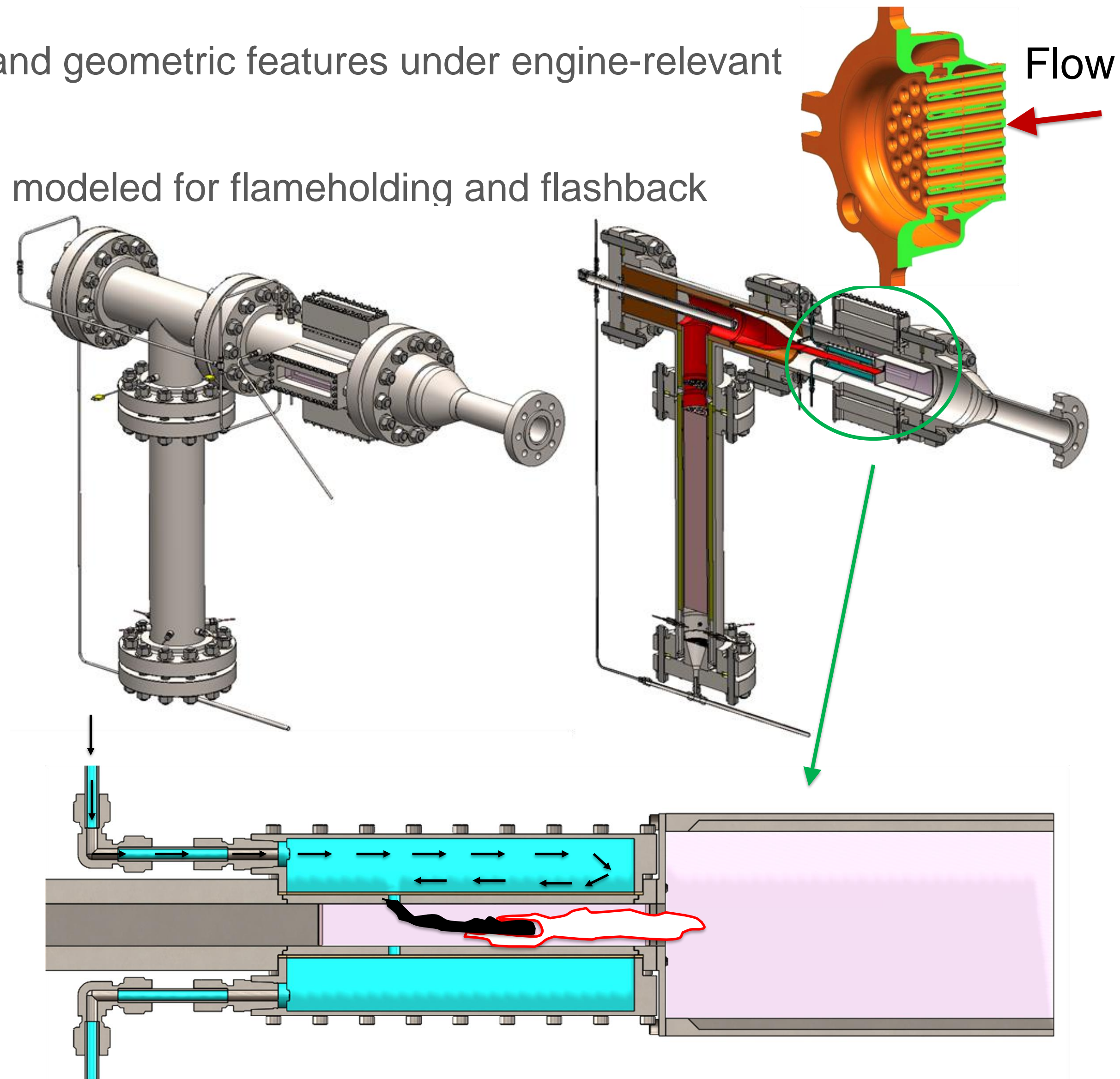
DNS of full-scale micromixer (discussed later by V. Sharma)



Goals:

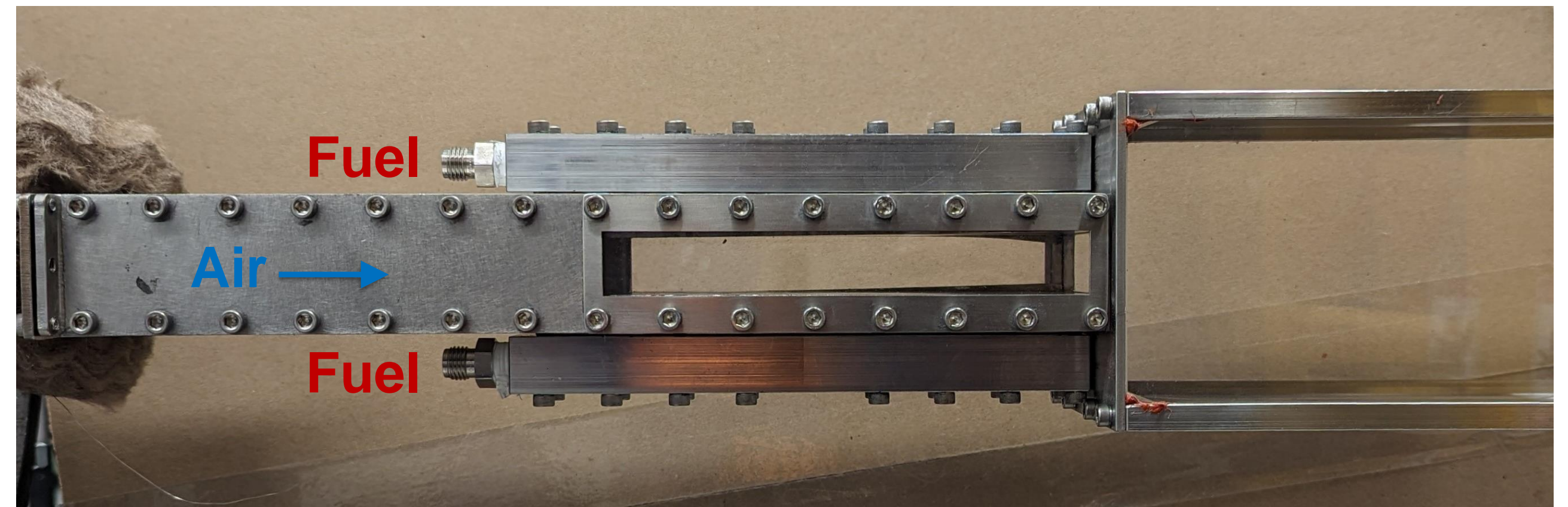
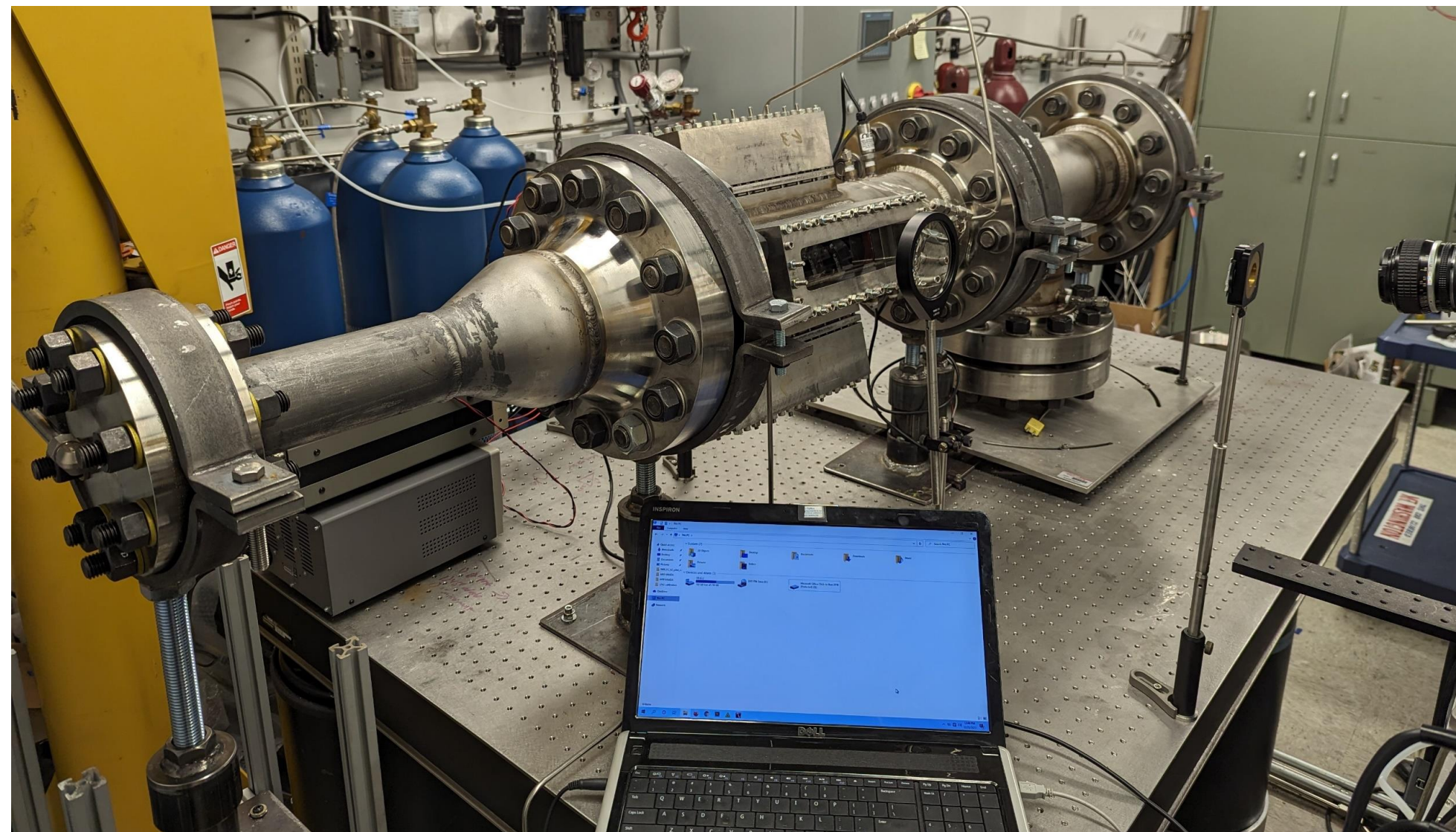
- Configurations and test conditions model important flow and geometric features under engine-relevant conditions
- NOT a duplication – captures key features that should be modeled for flameholding and flashback

	SEPB 1	SEPB 2	SEPB 3	SEPB 4
Air tube ID / channel H x W (inch)	0.75 x 3	0.75 x 3	0.75 x 3	0.75 x 3
Fuel hole D (inch)	0.205	0.205	0.205	0.205
Number of fuel holes	2			
Fuel hole angle (deg)	0			
Pressure (bar)	17.2	8.0	4.0	1.0
Inlet air temperature (K)	670			
Inlet air velocity (m/s)	2.51	5.41	10.80	43.30
Inlet air Re (based on channel height)	23400	23400	23400	23600
Air mass flow rate (slpm)	1510	1510	1510	1530
Heat addition to air (kW)	13.0	13.0	13.0	13.1
Fuel composition (% vol)	40/60 CH ₄ /H ₂			
Inlet fuel temperature (K)	590	590	590	590
Inlet fuel velocity (m/s)	7.47	16.10	32.10	128.00
Inlet fuel Re	9390	9390	9390	9480
Total fuel mass flow rate (slpm)	150	150	150	152
Flame power (kW)	52.0	52.0	52.0	52.5
Fuel/air momentum ratio	2.64			
Fuel/air mass flow rate ratio	0.026			





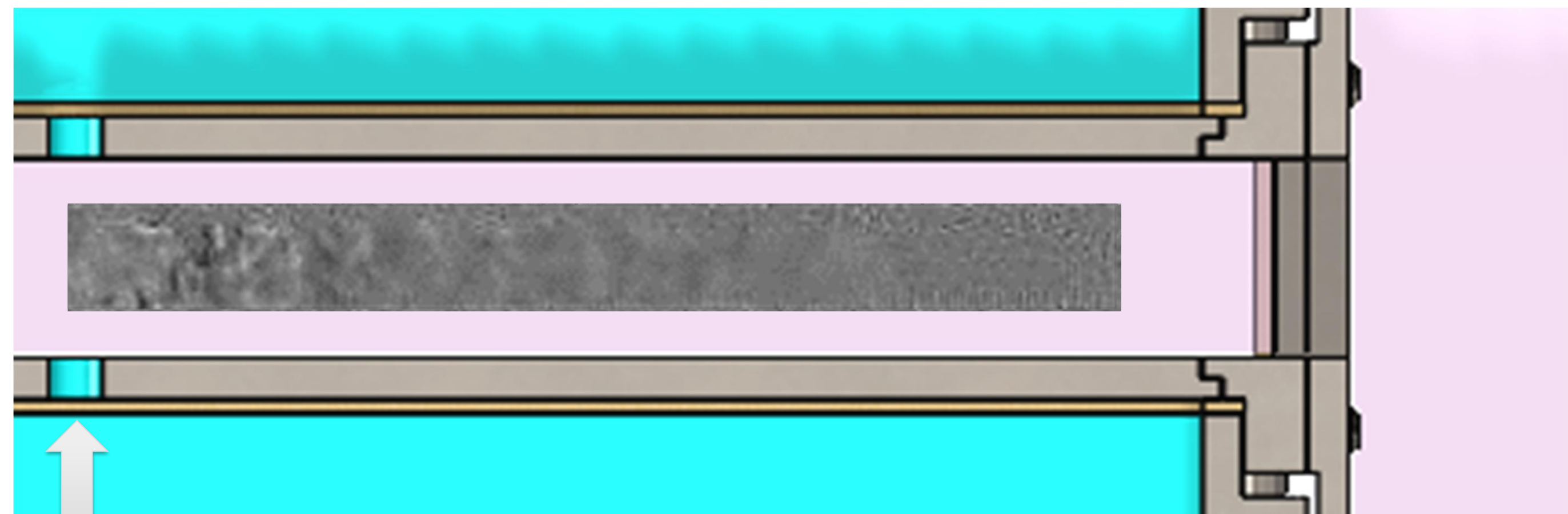
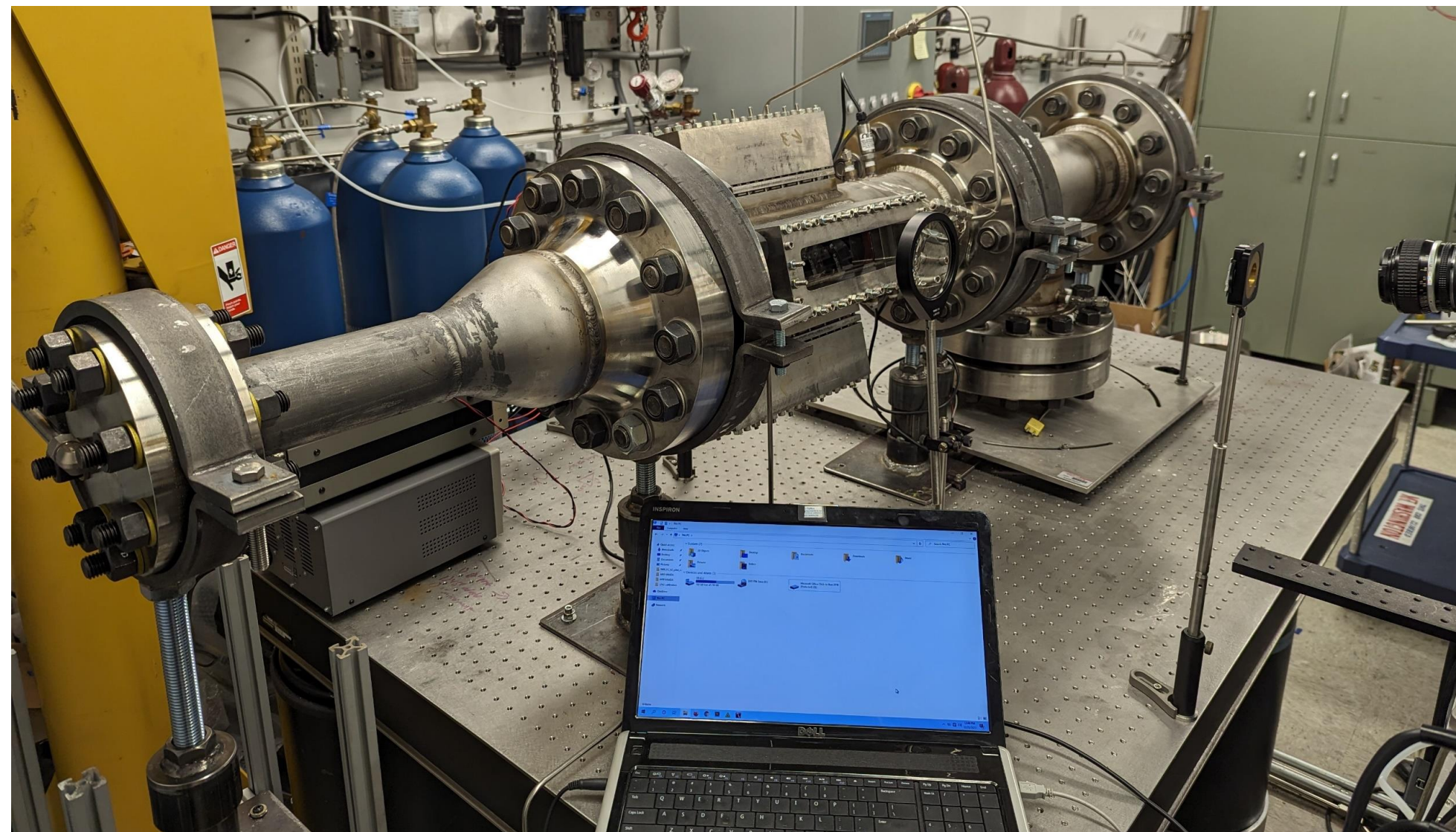
- A number of delays that impacted construction
 - Initial fabrication of many parts were delayed by 3+ months
 - Many major/minor parts had to be fabricated twice due to machinist error
 - Personnel issues – new postdocs only started July 2023 (1-year gap between staff)
 - University halted work with an existential crisis about hydrogen and its usage
- Test rig has now been assembled
- System control (temperature, pressure, flow rates, etc) has been installed and tested



Burner Assembly



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 - University halted work with an existential crisis about hydrogen and its usage
- Test rig has now been assembled
- System control (temperature, pressure, flow rates, etc) has been installed and tested
- Facility shakedown has begun (atmospheric and pressurized cold flow cases)



CH₄

t = 140 ms



- During system fabrication and construction, we have optimized laser-based measurements

DLR turbulent premixed burner (5 bar)

Flow direction

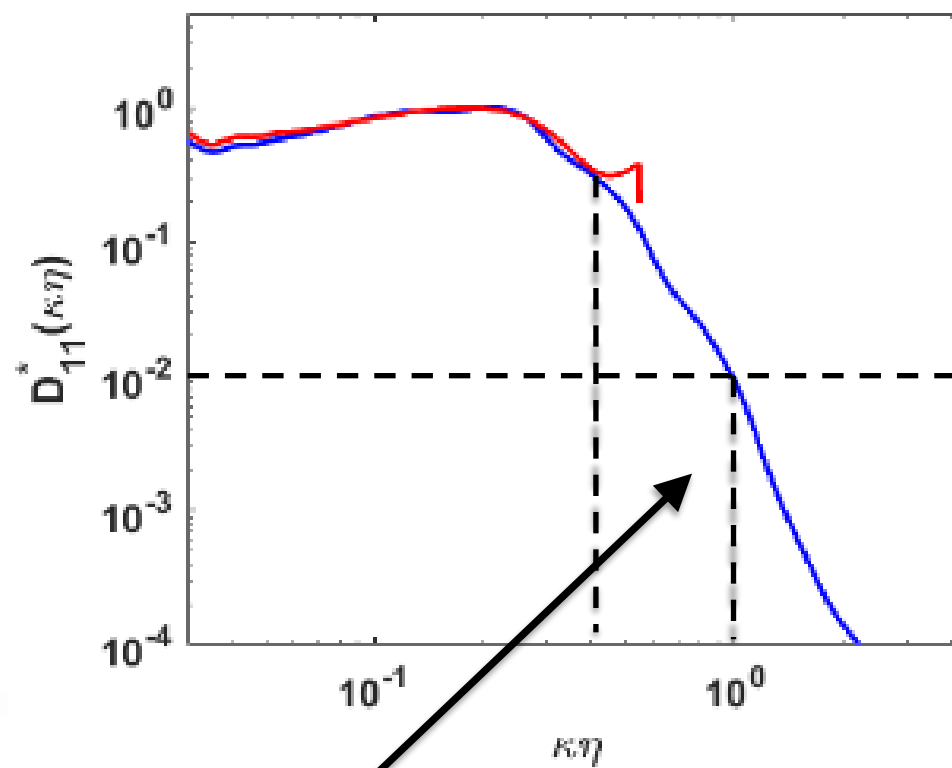
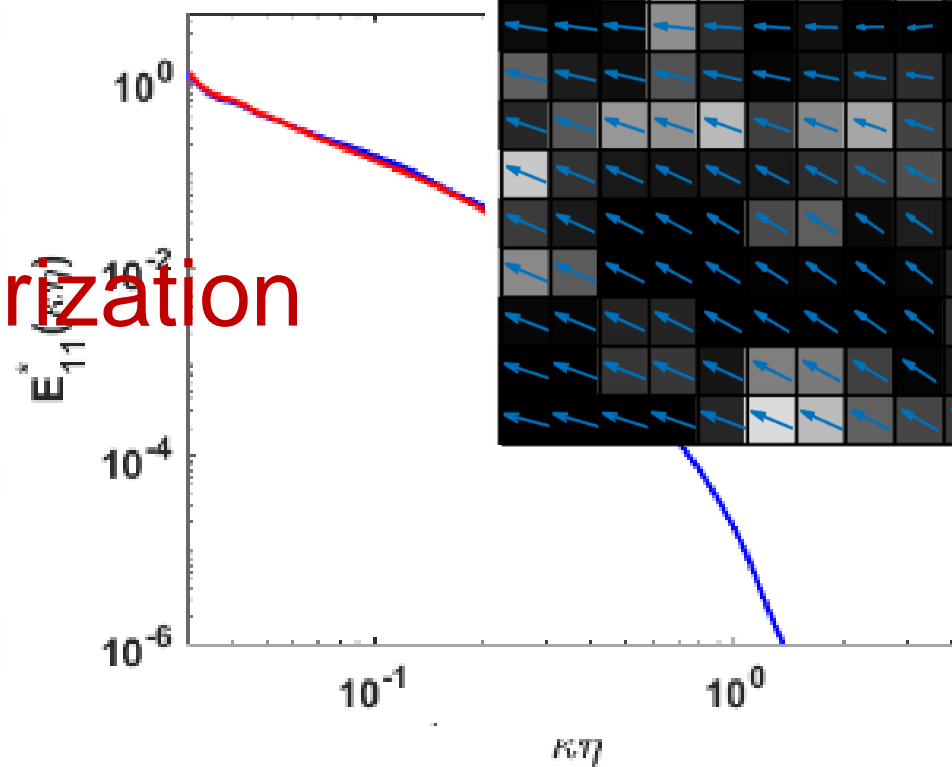
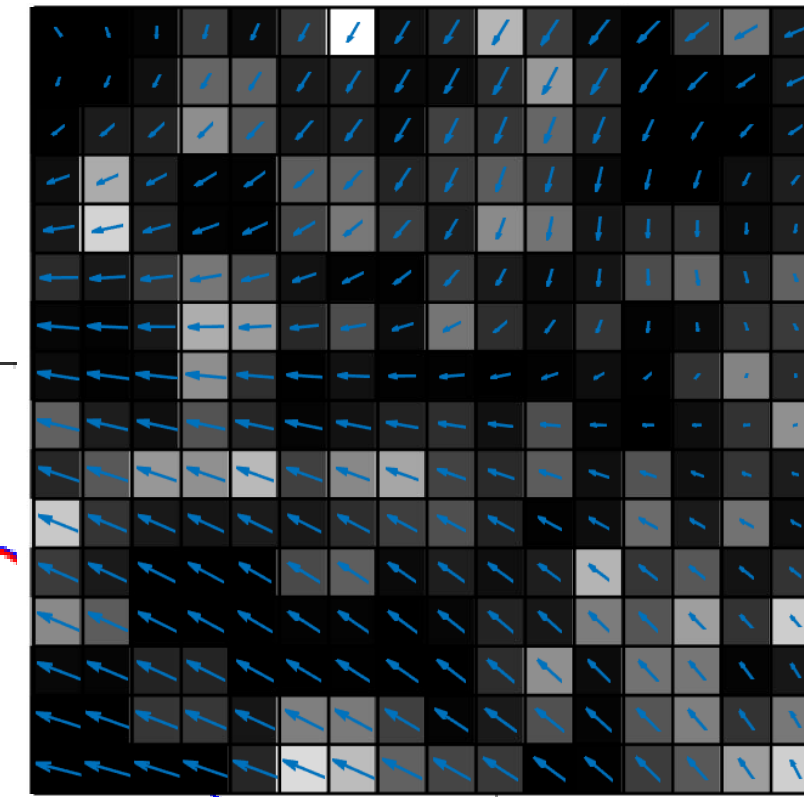
Axial (m/s)

Vorticity (1/s)

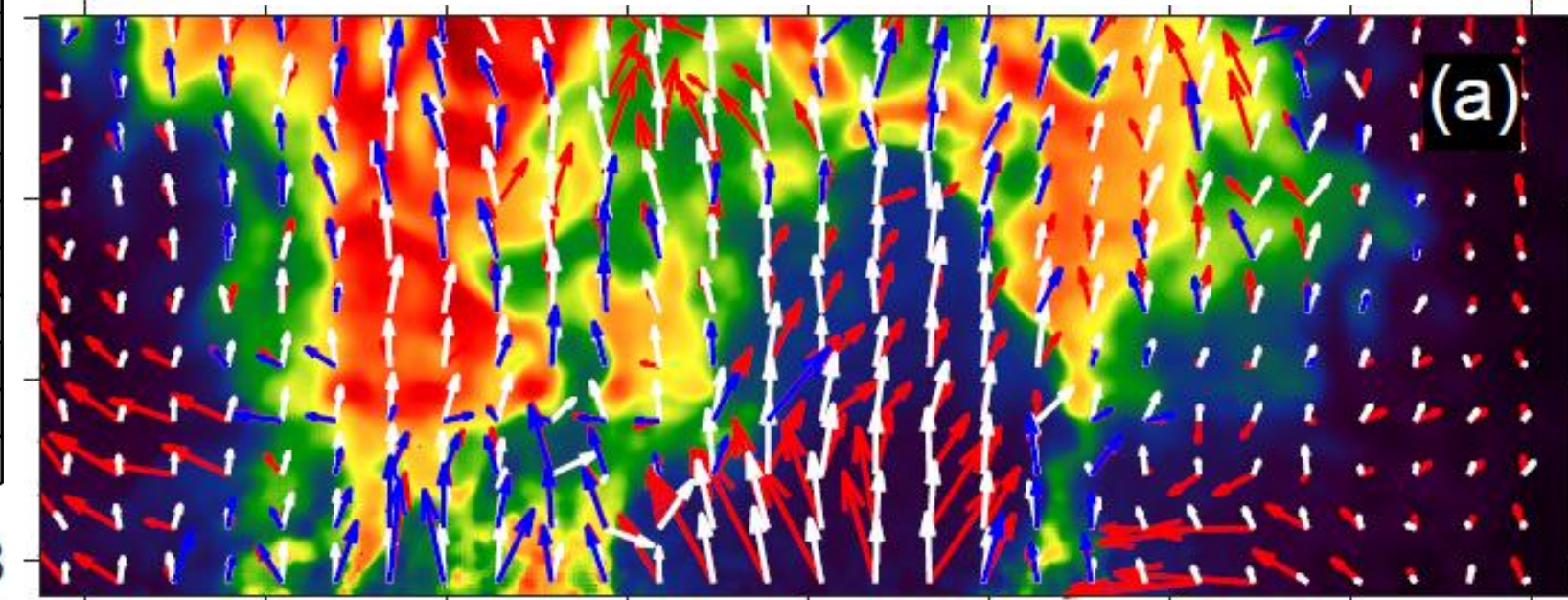
$$\hat{v} = \underset{\beta}{\text{argmin}} I_D(I_0, I_1, \beta) + \lambda J_P(\beta)$$

penalty function

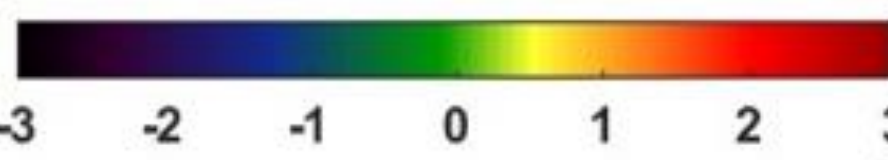
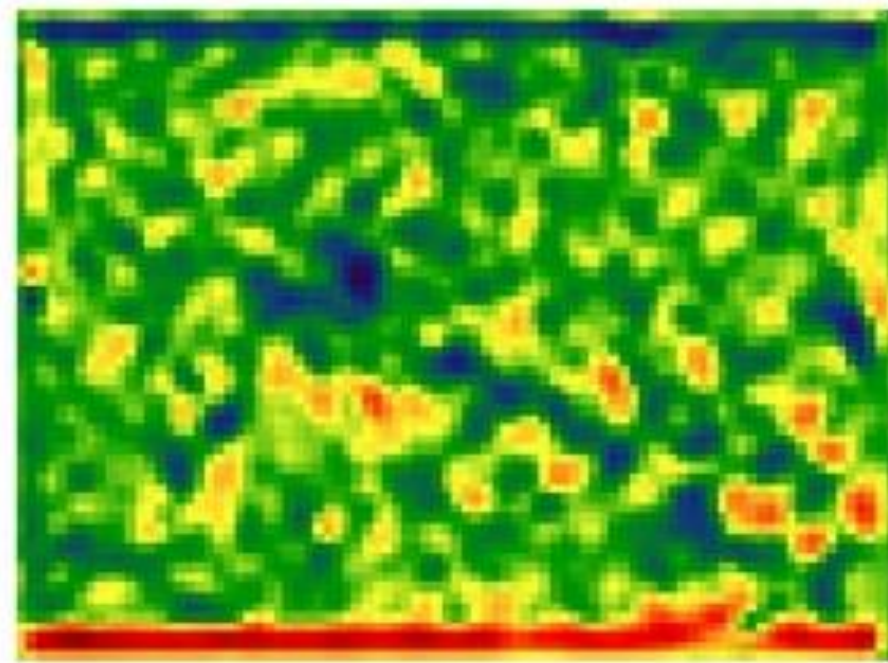
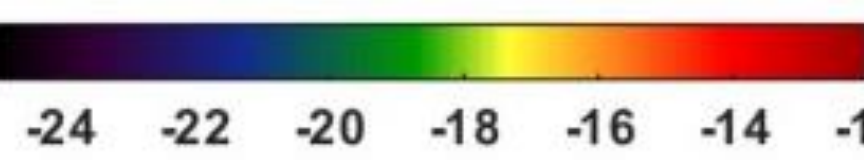
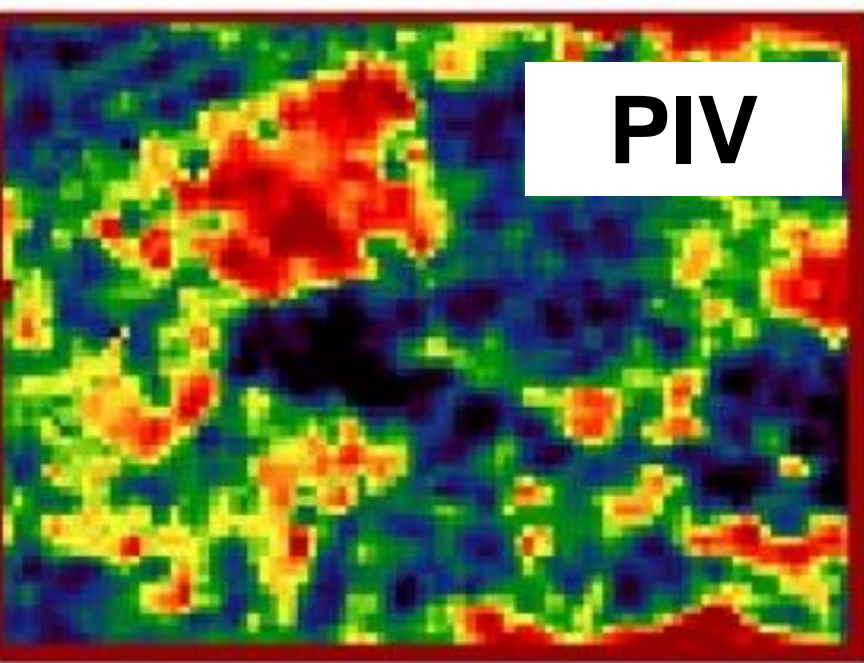
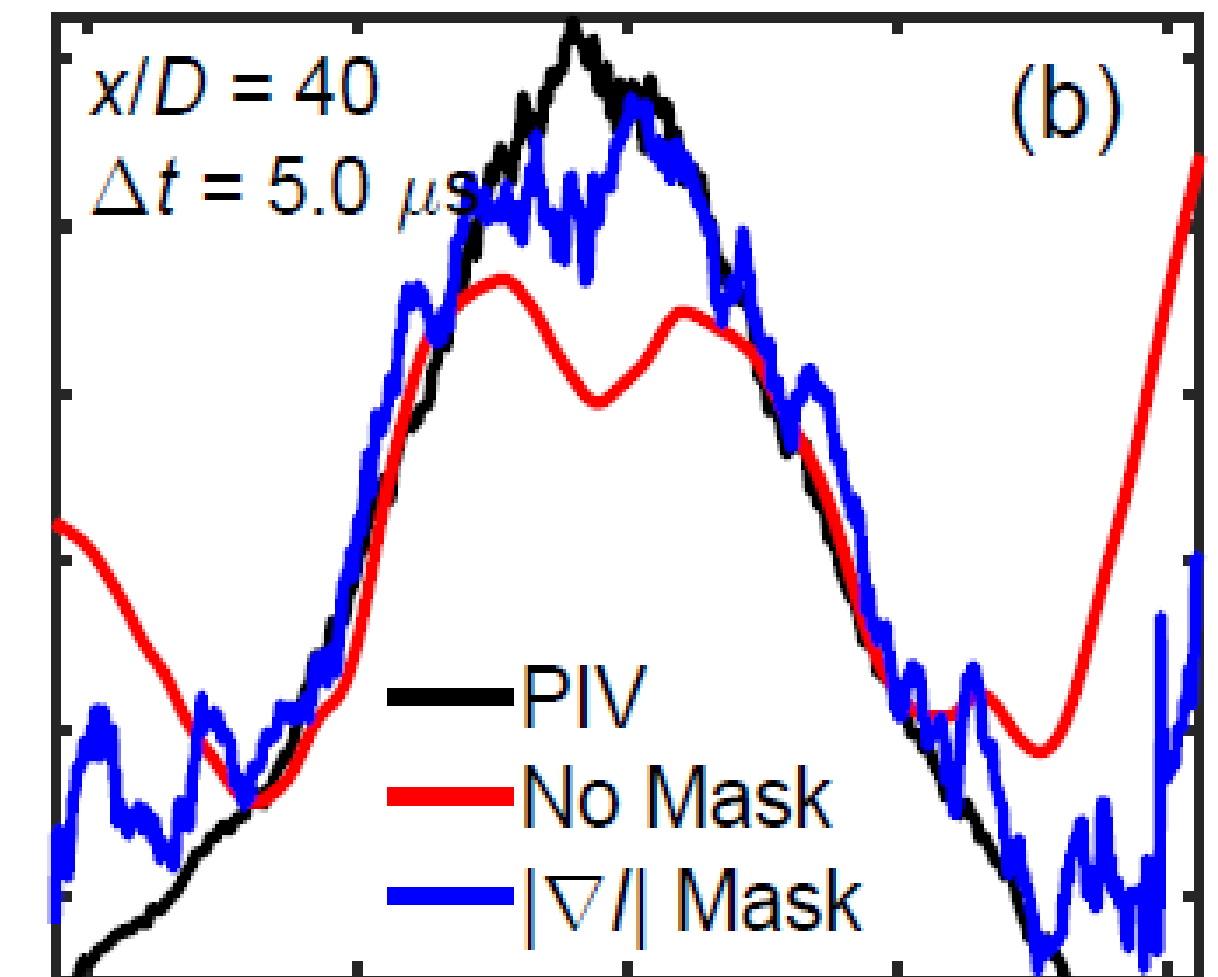
regularization



Dual-Shot OH PLIF + wOFV



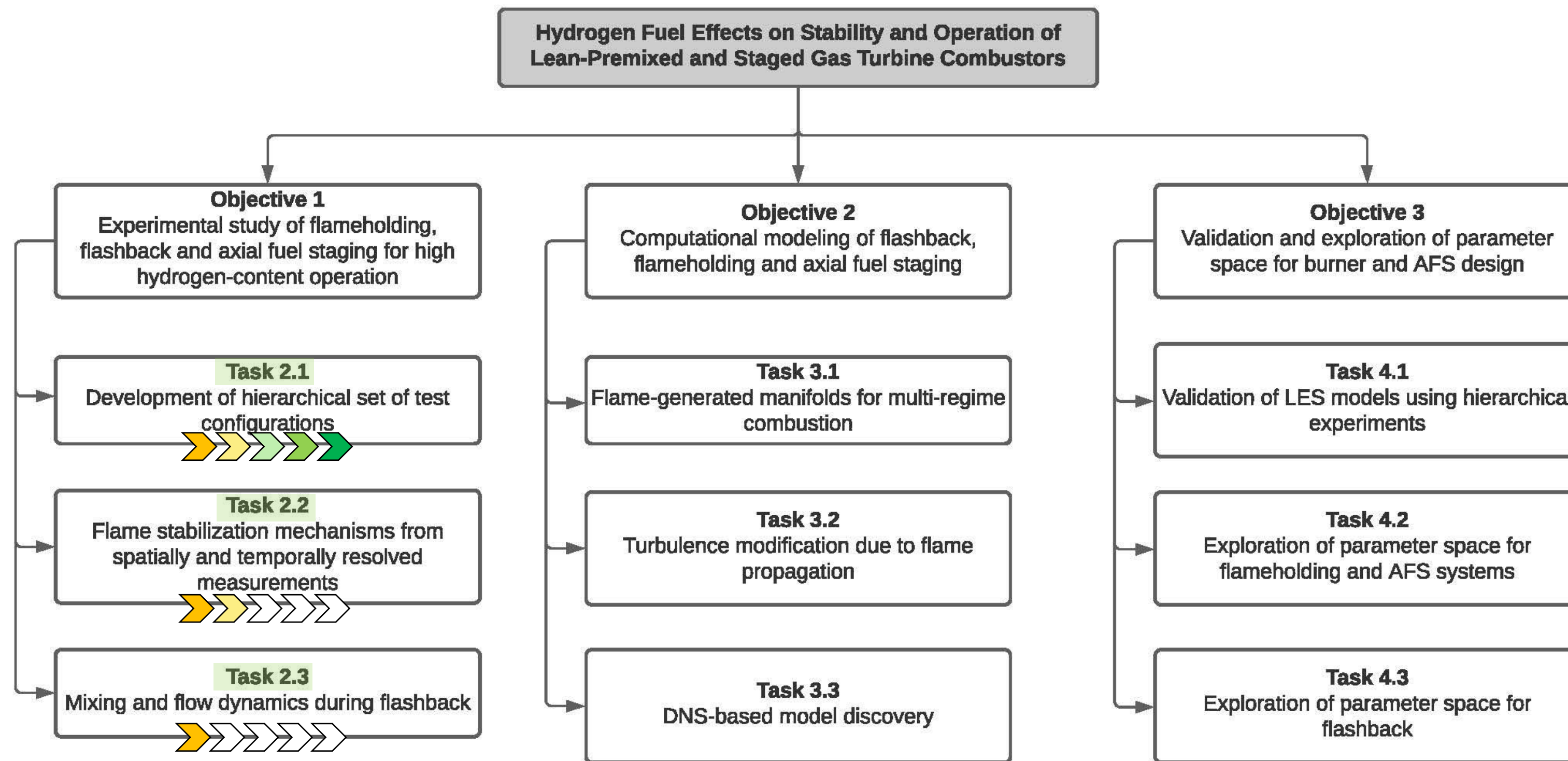
PIV No Mask $|\nabla|$ Mask



Smallest dissipative scales resolved



- Test rig is setup; in the final year of this program, data will be acquired, analyzed, and passed to UM collaborators for LES model assessment (focus is on stabilization and flameholding mechanisms)
- The experimental testbed provides new opportunities for identifying mechanisms underpinning flameholding, stabilization, and flashback when using HHC fuels
- Longer term - testbed scale is ideal for “rapid” parametric evaluation of HHC combustion – fundamental mechanisms



DOE-NETL USTR Program Review Meeting

FE0032076 - Hydrogen Fuel Effects on Stability and Operation of Lean-Premixed and Staged Gas Turbine Combustors

Computational Effort

30 - Oct - 2023

Co-PI: Venkat Raman

Presenter: Vansh Sharma

A.

LES Studies

Focus: core flow physics and flame processes that control combustor operation using hydrogen and hydrogen-containing (HC) fuels

Develop framework for understanding following limit processes:

- Flame-holding
- Flame blowout
- Flashback

B.

DNS Studies

Processes are combination of different phenomena

- Entrainment
- Strain Rate – Extinction with chemistry effects
- Turbulent boundary layer
- Heat transfer effects

C.

Flashback
Studies

A. LES Studies

Understand the flame behavior in a representative geometry - JICF

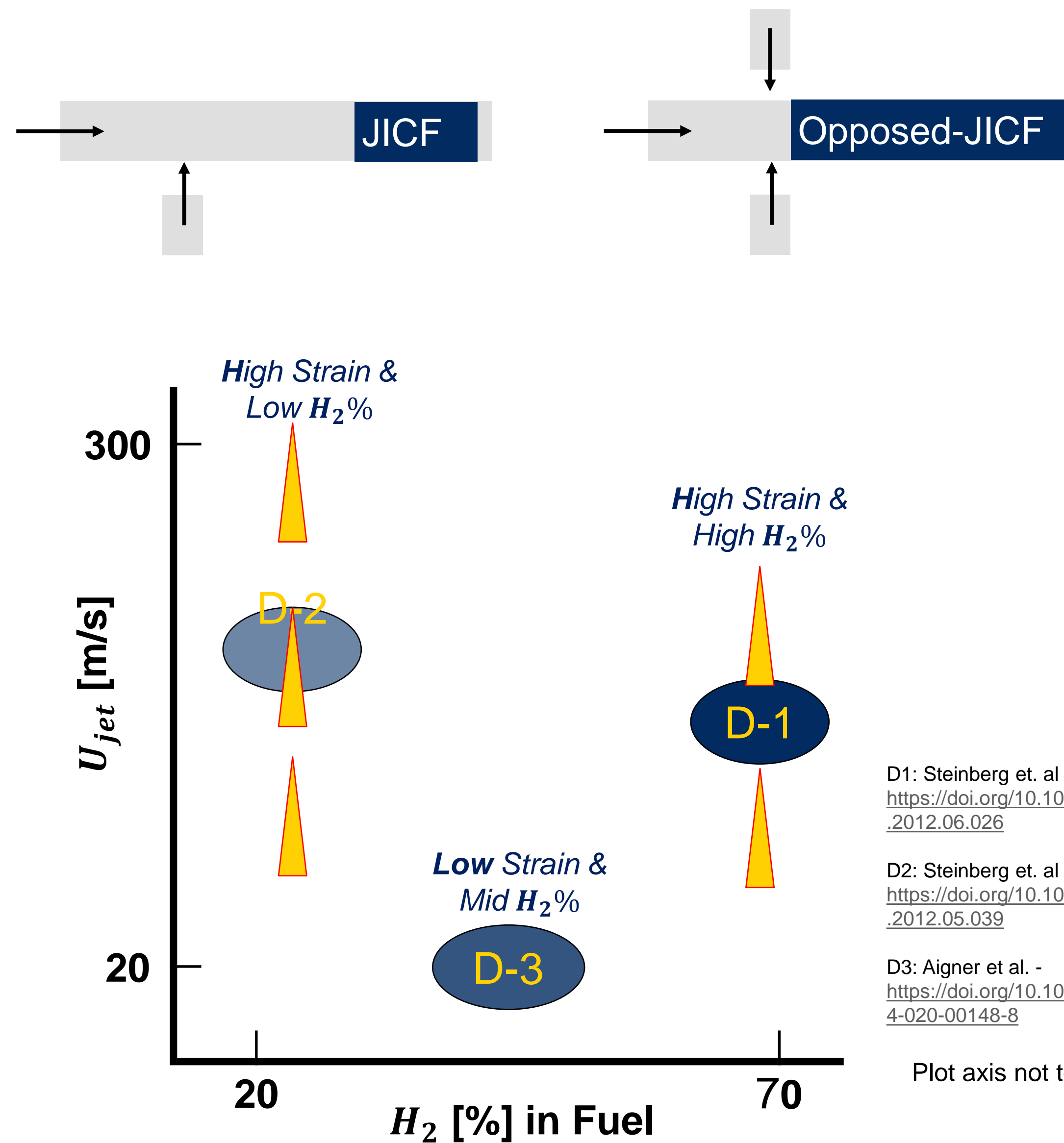
- Flamelet-based combustion modeling

- Model validation via experiments

- Combustion model limits: Non-Premixed vs Premixed Tabulation

Cases from literature [1]-[3]

- Bounds of strain rate vs Hydrogen %
- Flame stabilization and blowout process



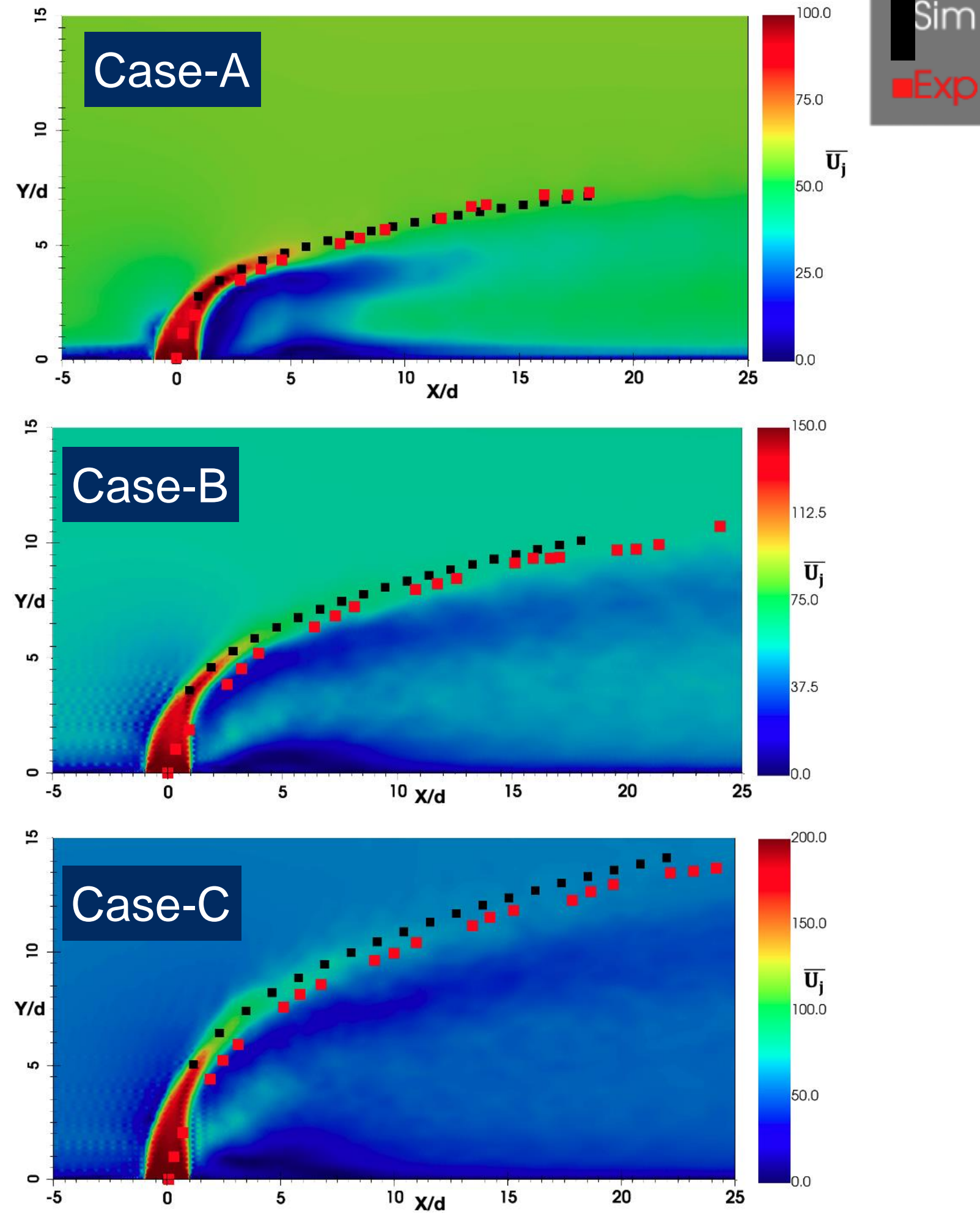
D1: Steinberg et. al - <https://doi.org/10.1016/j.proci.2012.06.026>

D2: Steinberg et. al - <https://doi.org/10.1016/j.proci.2012.05.039>

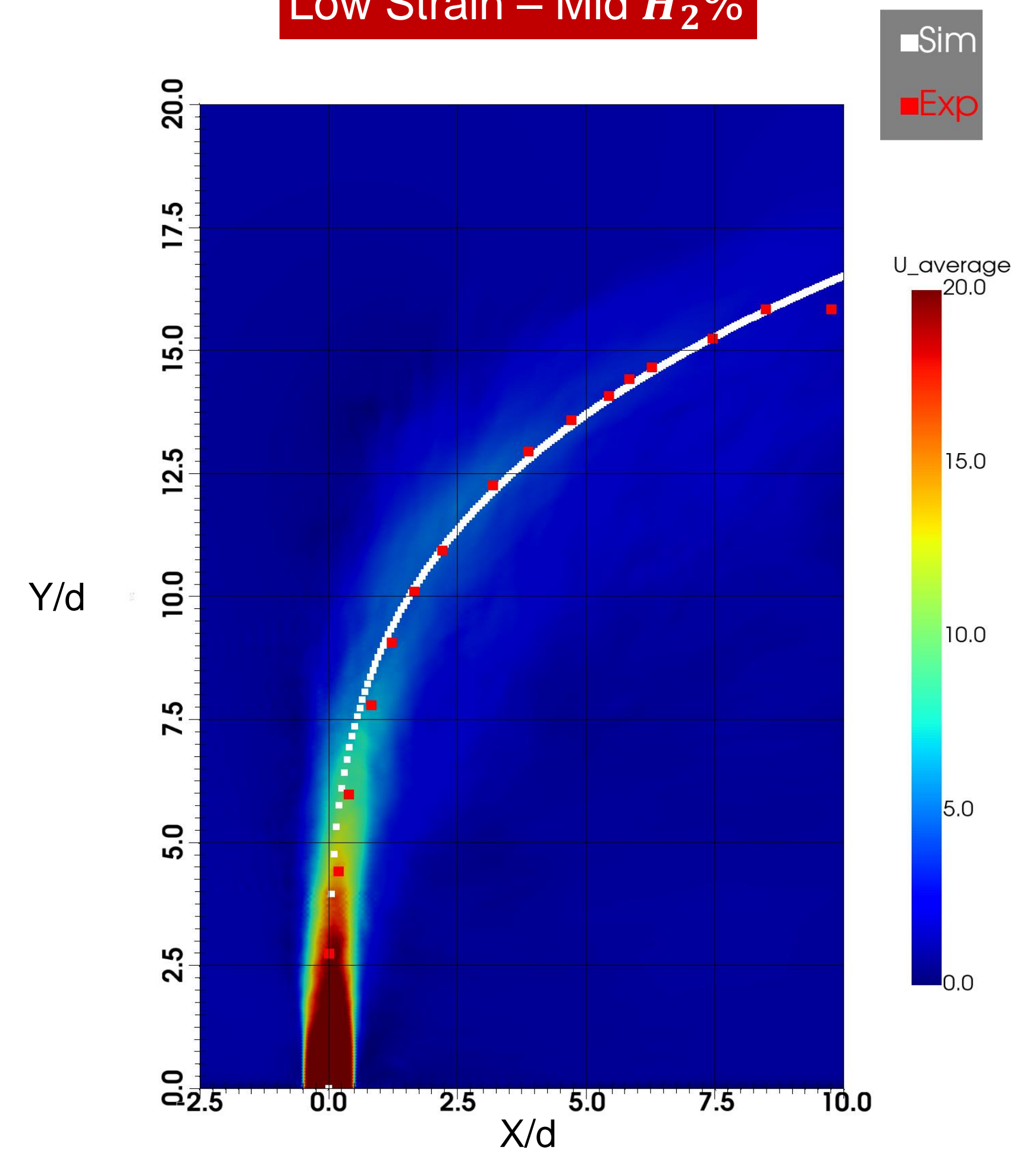
D3: Aigner et al. - <https://doi.org/10.1007/s10494-020-00148-8>

Plot axis not to scale

High Strain – High $H_2\%$



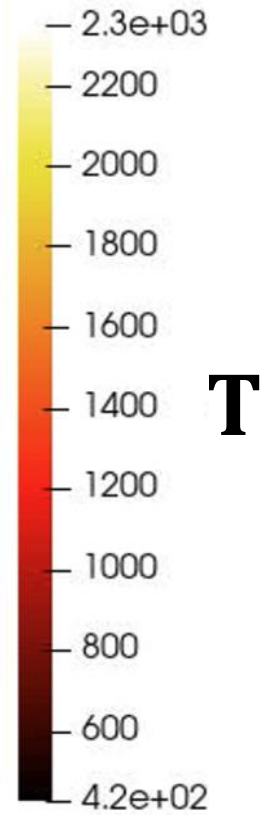
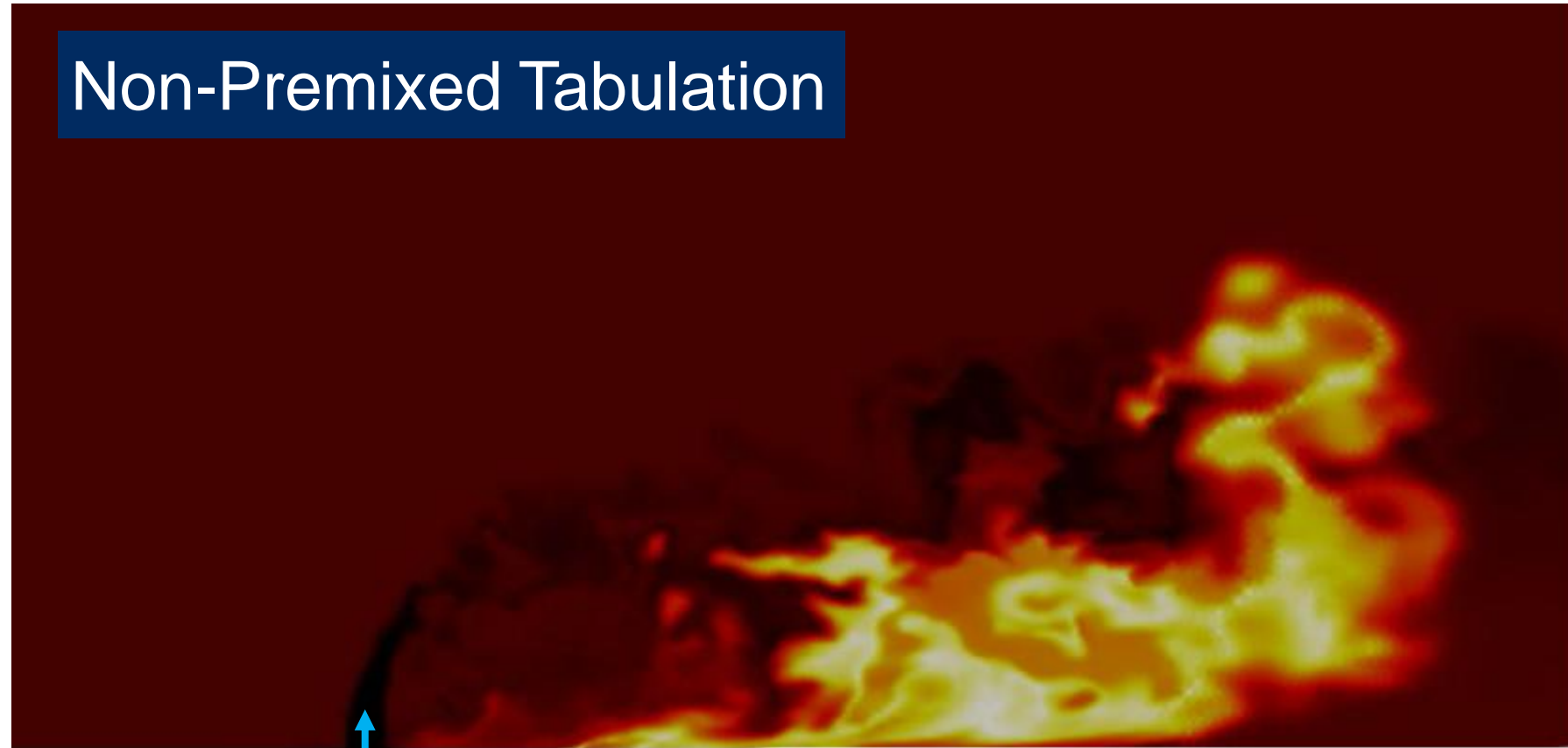
Low Strain – Mid $H_2\%$



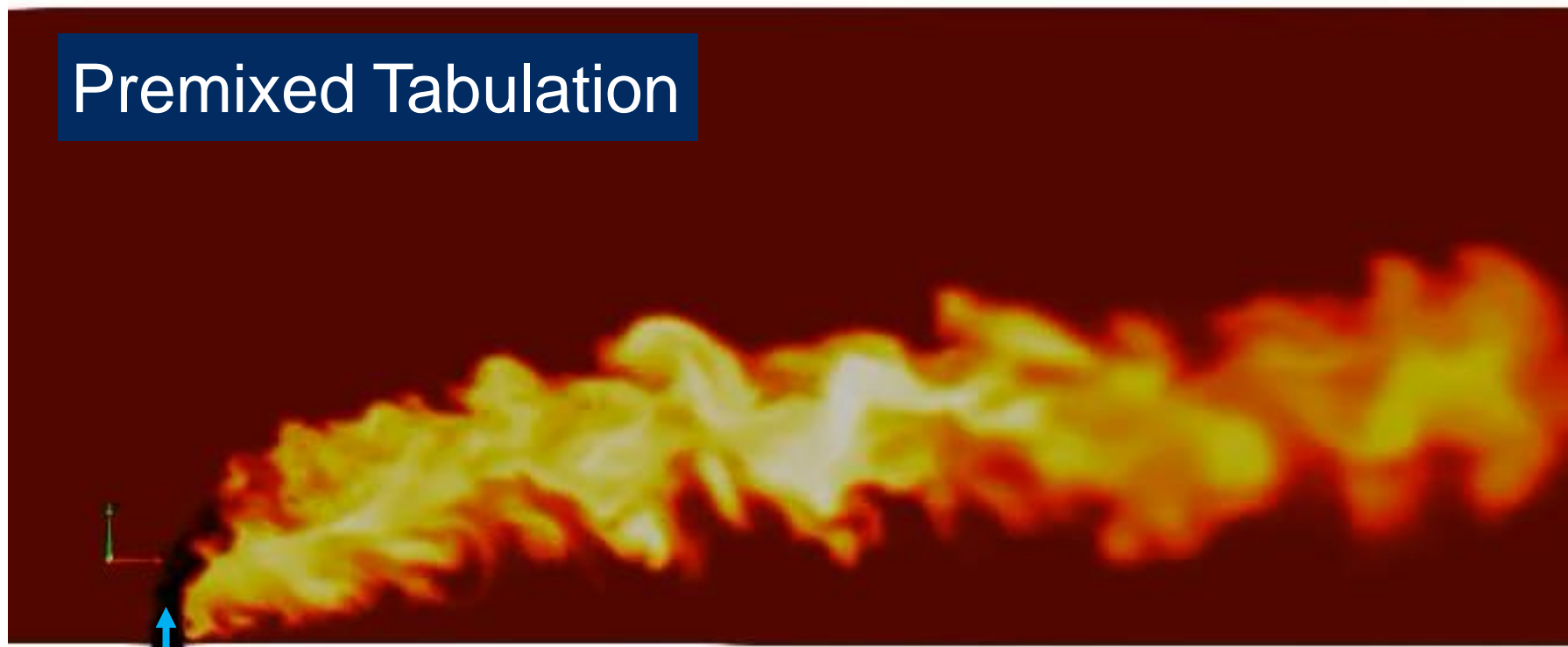
V. Sharma, Y. Tang and V. Raman. Stabilization of Hydrogen-enriched Jet Flames in a Crossflow [accepted to AIAA SCITECH 2024 Forum]

High Strain – High $H_2\%$

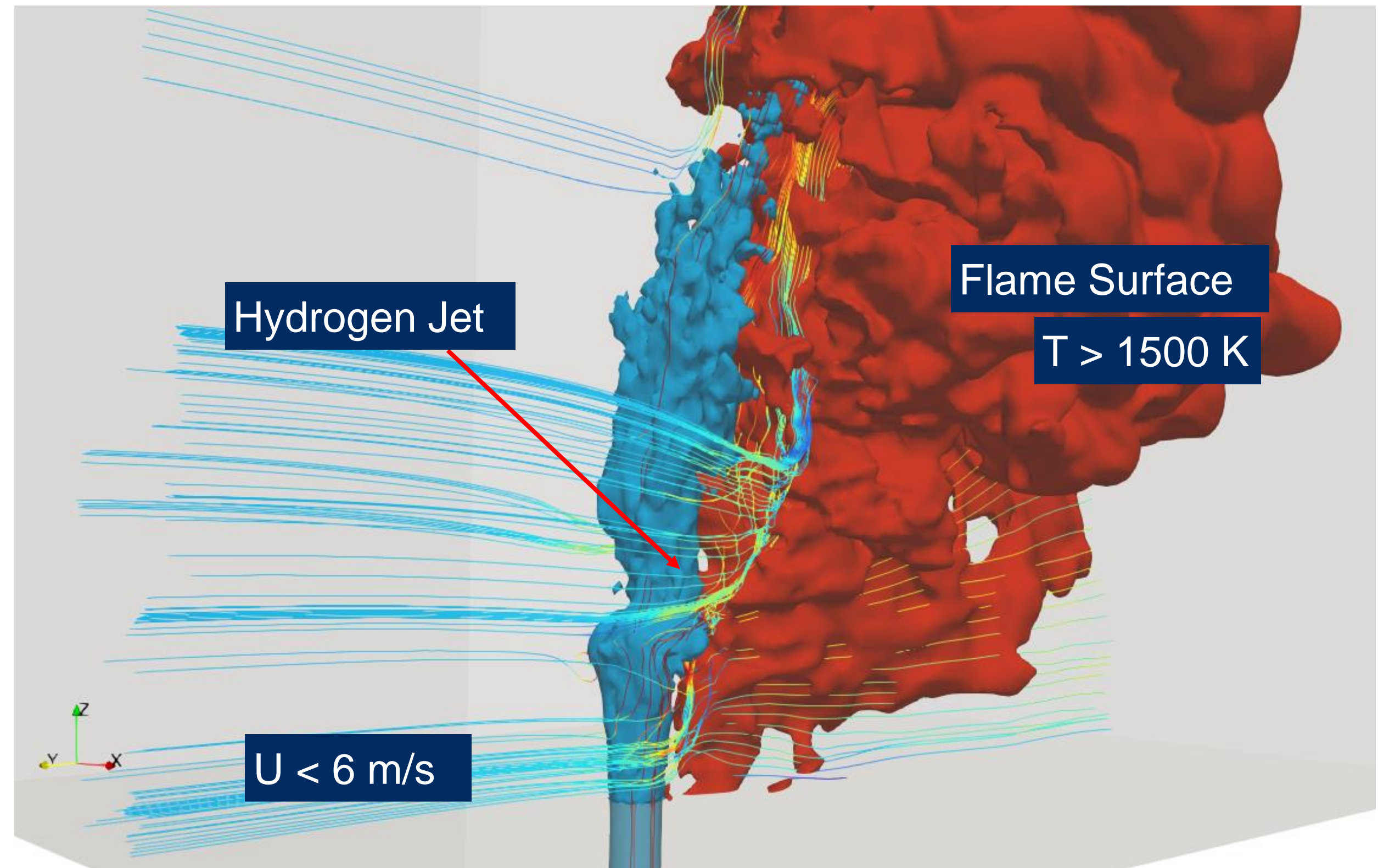
Non-Premixed Tabulation



Premixed Tabulation



Low Strain – Mid $H_2\%$



Hydrogen Jet

Flame Surface

$T > 1500\text{ K}$

$U < 6\text{ m/s}$

V. Sharma, Y. Tang and V. Raman. Stabilization of Hydrogen-enriched Jet Flames in a Crossflow [accepted to AIAA SCITECH 2024 Forum]

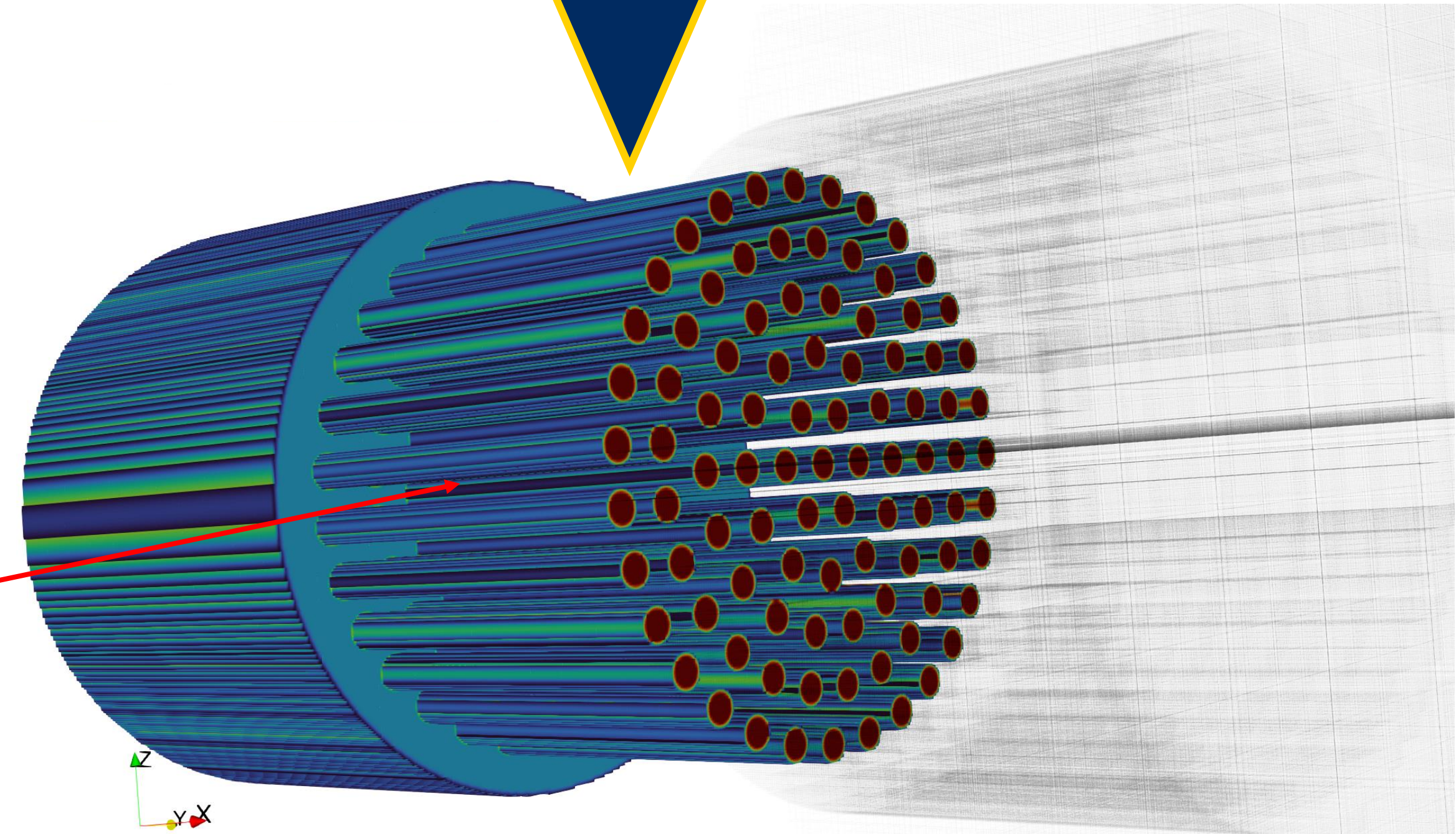
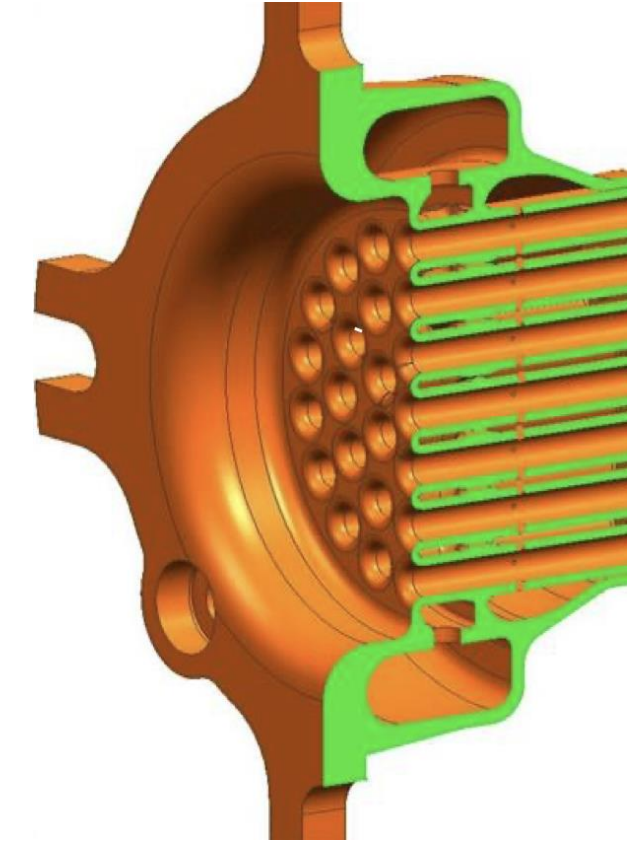
B. DNS Studies

In collaboration with GE [Michael Hughes and Hasan Karim]

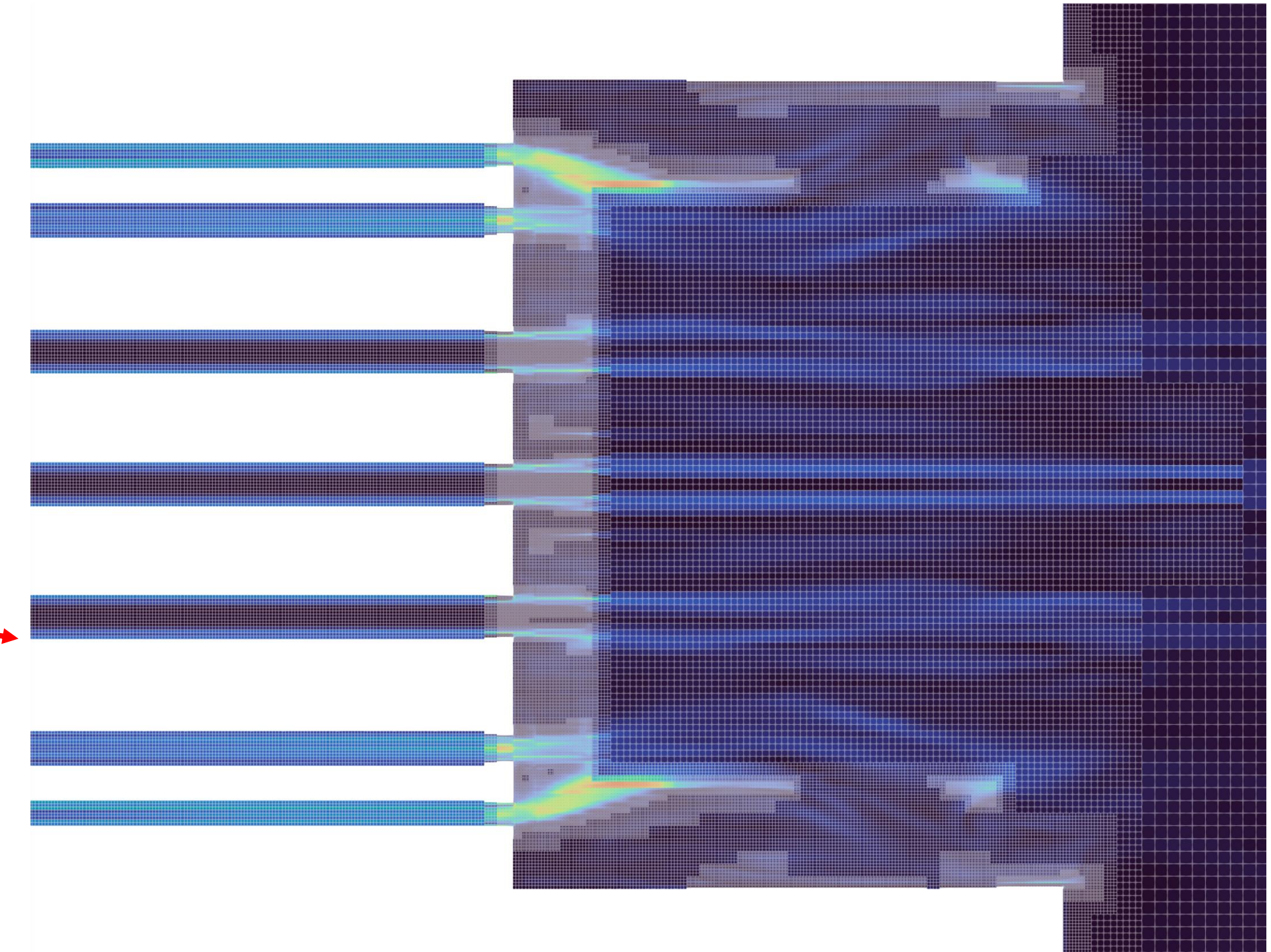
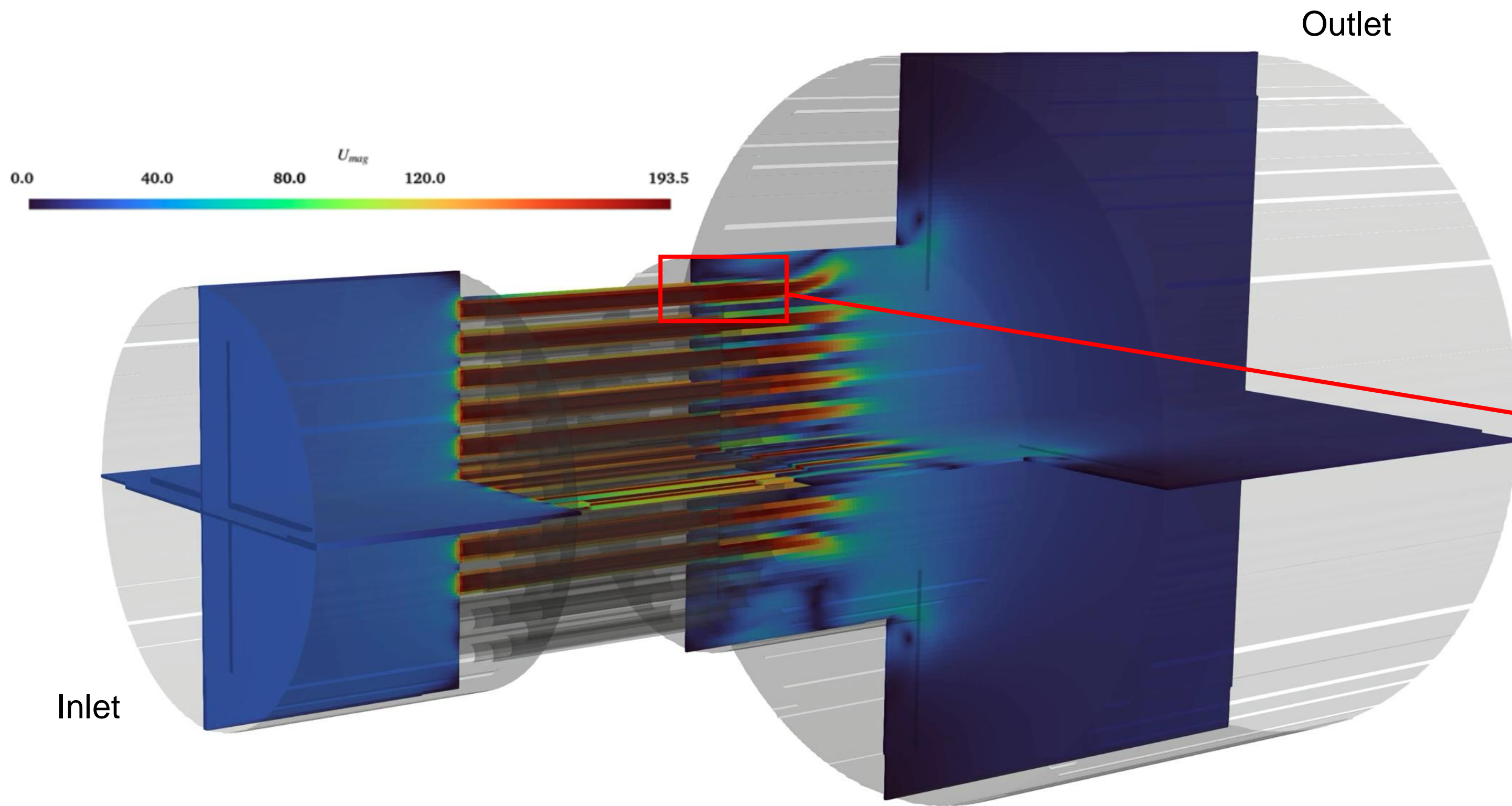
Adaptive Mesh Refinement [AMR] based solver with full chemistry implementation using Cantera and/or in-house Chemistry Lib Solver Capabilities

- AMReX [5] based – Exa-Scale ready
- Mesh refinement + Field Refinement control
- Finite Rate chemistry scalable on GPUs [4]

Multi-Tube Mixer (MTM)



Tubes meshed using Implicit Function
– Faster and Precise Mesh

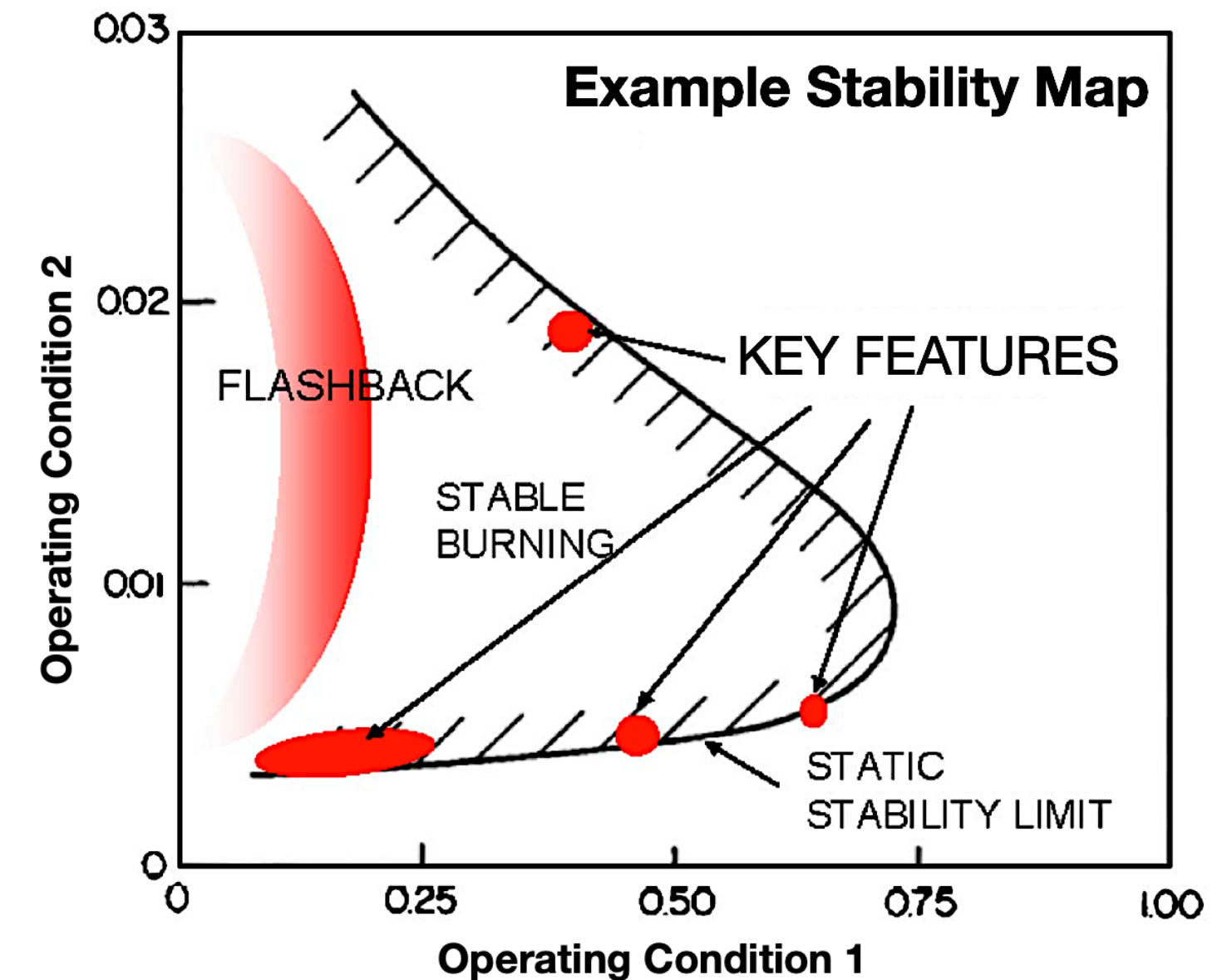
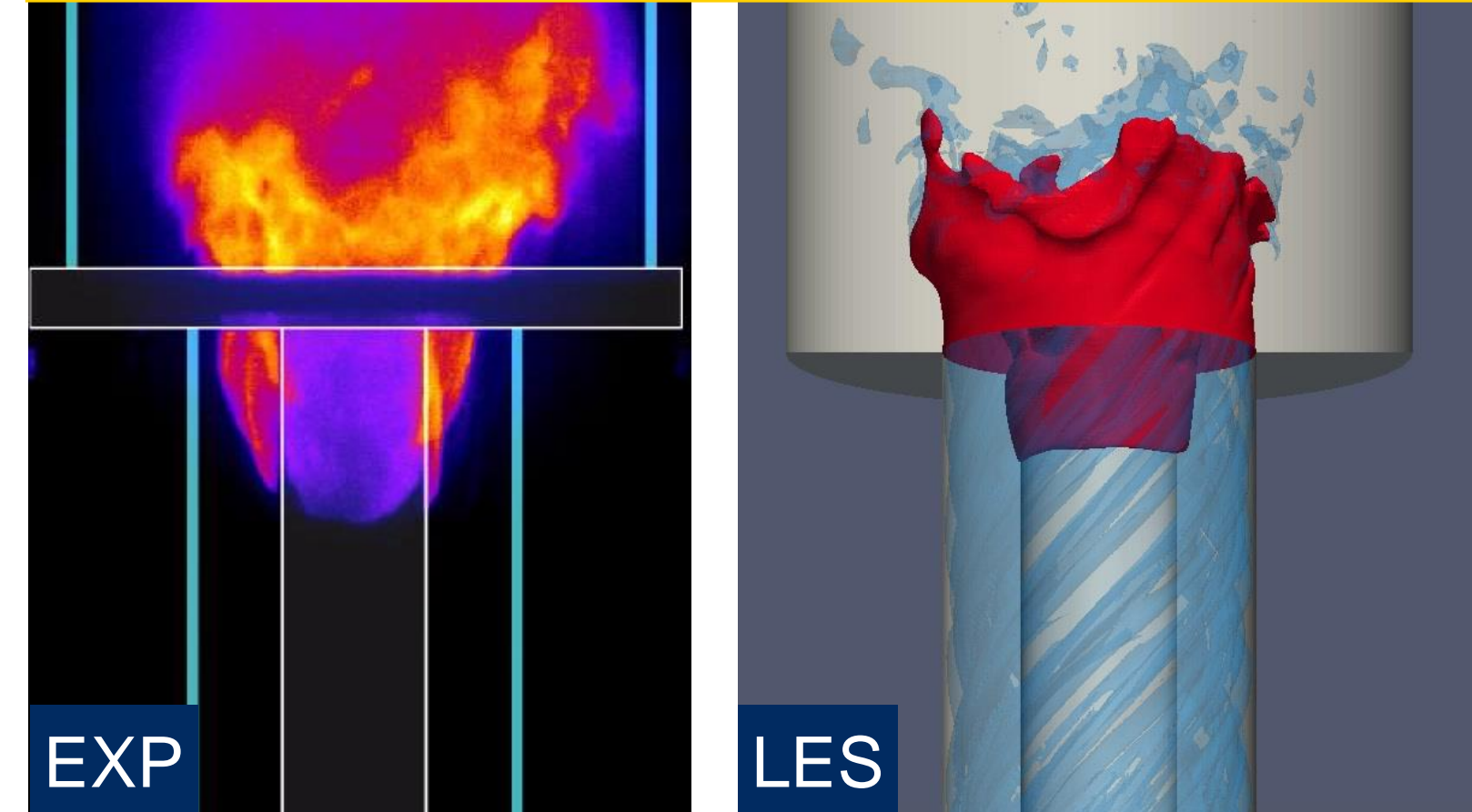


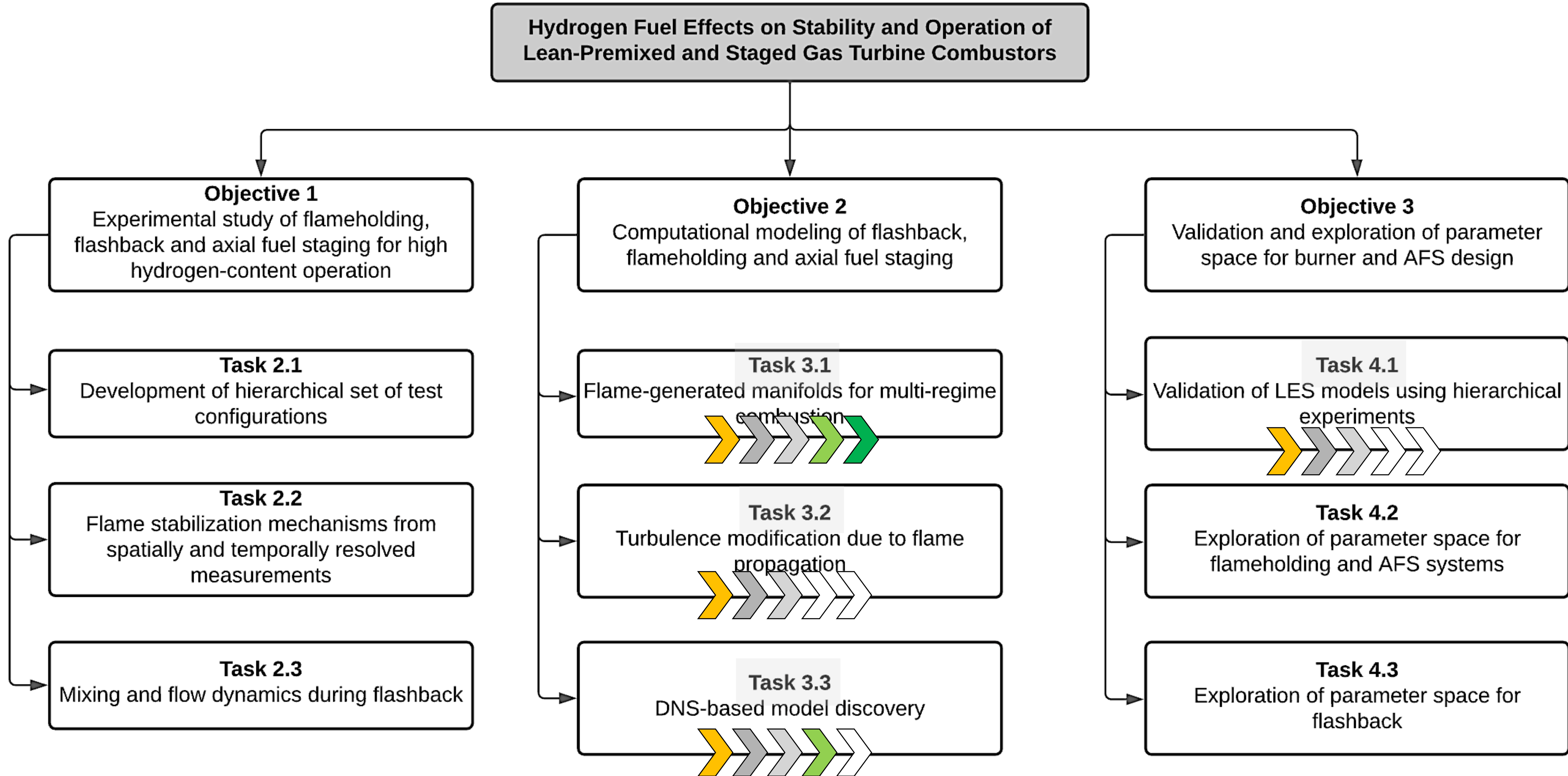
Section View showing tube exit with vorticity refinement

C. Flashback Studies

- Complicated – different unsteady processes involved
- Boundary layer (BL) flashback dominates in H_2 fuels
- Previous work in UTSR project
 - BL Flashback in Swirl combustor
 - Direct dependence on – Turbulent BL, Heat Transfer and Chemistry
- Develop models for flashback using LES and DNS data
 - Open to combustion community: LES Models and DNS data

LES Modeling and Experiments of Flashback in H_2 Rich Gas Turbines: Raman & Clemens





Research publications from the program

- V. Sharma, Y. Tang and V. Raman. “Effects of Pitch Angle and Momentum Ratio on Flame Stabilization in Opposed Jets in Crossflow”. 18th International Conference on Numerical Combustion. May 8-11, 2022, San Diego, CA
- V. Sharma, Y. Tang and V. Raman. “A Computational Study on Effects of Injector Pitch Angle on Flame Stabilization in Opposed Jets in Crossflow”. 12th Mediterranean Combustion Symposium. January 23-26, 2023, Luxor, Egypt
- V. Sharma, Y. Tang and V. Raman. Stabilization of Hydrogen-enriched Jet Flames in a Crossflow [accepted to AIAA SCITECH 2024 Forum]

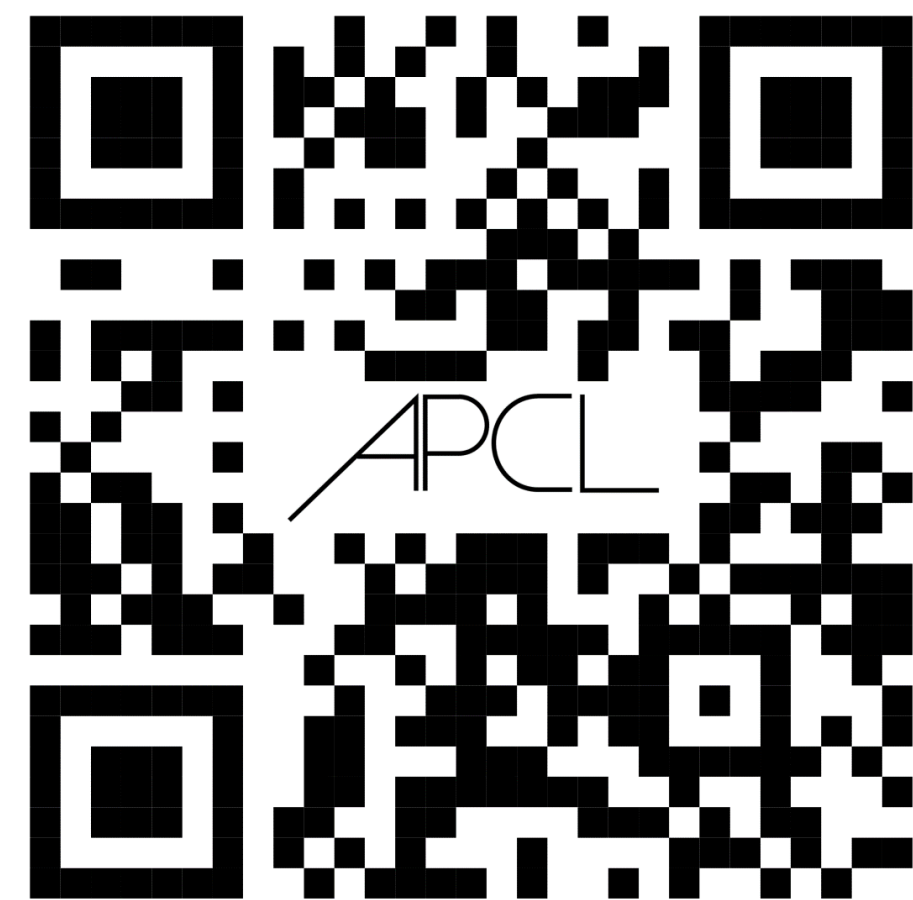
Publications cited:

1. D1: Steinberg, A. M., Sadanandan, R., Dem, C., Kutne, P., and Meier, W., “Structure and stabilization of hydrogen jet flames in cross-flows,” Proceedings of the Combustion Institute, Vol. 34, No. 1, 2013, pp. 1499–1507. <https://doi.org/10.1016/j.proci.2012.06.026>,
2. D2: Fleck, J. L., Griebel, P., Steinberg, A. M., Arndt, C. M., Naumann, C., and Aigner, M., “Autoignition of hydrogen/nitrogen jets in vitiated air crossflows at different pressures,” Proceedings of the Combustion Institute, Vol. 34, No. 2, 2013, pp. 3185–3192. <https://doi.org/10.1016/j.proci.2012.05.039>
3. D3: Saini, P., Chterev, I., Pareja, J., Aigner, M., and Boxx, I., “Effect of Pressure on Hydrogen Enriched Natural Gas Jet Flames in Crossflow,” Flow, turbulence and combustion, Vol. 105, No. 3, 2020, pp. 787–806. <https://doi.org/10.1007/s10494-020-00148-8>
4. Barwey S, Raman V. A Neural Network-Inspired Matrix Formulation of Chemical Kinetics for Acceleration on GPUs. Energies. 2021; 14(9):2710. <https://doi.org/10.3390/en14092710>
5. AMReX: Software Framework for Block Structured AMR: <https://doi.org/10.5281/zenodo.2555438>

Thank You



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Name	Fuel	Composition (v/v)	J	U_j (m/s)	Re_j	U_{cf} (m/s)	Re_{cf}	P (bar)	T_j (K)	T_{cf} (K)
D-1A	H2/N2	70/30	1.96	100	3000	55	44000	1	423	750
D-1B		70/30	4.84	150	4500	55	44000	1	423	750
D-1C		70/30	8.41	200	6000	55	44000	1	423	750
D-2A	H2/N2	27/73	2.90	308	83000	300	450000	10	312	1185
D-2C		27/73	1.10	125	35000	200	300000	10	312	1185
D-3A	CH4/H2	60/40	102.10	19.9	17900	1.5	22000	10	298	465