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High-speed and High-quality Field Welding Repair Based on Advanced Non-destructive Evaluation and Numerical Modeling

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Presentation outline

- Background and Objectives
- Research Status and Accomplishments
- Summary and Conclusions



Creep Strength Enhanced Ferritic (CSEF) Steels

- Owing to its high creep-rupture strength, Grade 91 (9Cr-1MoVNb) steel is one of the most-widely used materials in structural components such as tubing, piping, and headers in the current fleet of fossil plants
- Grade 92 steel, having a higher creep strength than Grade 91 with addition of tungsten (W) and reduction in Molybdenum (Mo), is increasingly used in plant components

100 000 h Creep Rupture Strength at 600 °C



H. Cerjak and E. Letofsky: Sci. Technol. Weld. Join., Vol. 1, pp. 36–42 (1996)

Engineered Base Metal Microstructure



Optical Microscopy Prior austenite grain boundaries

Grade 91



Scanning Electron Microscopy Tempered martensite



Transmission Electron Microscopy Subgrains and precipitates

Grade 92

HFW

41.4

• Tempered martensite

det HV

mag 🖽 spot WD

12.0

5 000 x

 Carbide precipitation along PAGB and martensite laths

H.C. Whitt, Ph.D. Dissertation, The Ohio State University, 2019. R. Johnson, M.S. Thesis, The Ohio State University, 2021.

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Formation of Deleterious Microstructure

- Heat treatment at a temperature close to A1 (e.g., 760 °C or 1400 °C) is essential to obtain the tempered martensite microstructure
- Microstructure deleterious to mechanical properties can form if temperature is not maintained
 - Temperature too high (e.g., between A1 and A3) can lead to formation of ferrite (α)
 - Temperature too much lower than A1 can lead to untempered martensite



Literature Review of Temperbead Welding Techniques and Considerations for Grade 91 Components. EPRI, Palo Alto, CA, October 2012. 1026505.



Industry Needs and Project Objectives

• Technical gaps:

- How to ensure field welding repair onto Grade 91 or 92 worked properly?
- How to optimize welding parameters to reduce formation of deleterious microstructure?

• Specific objectives:

- Developing a non-destructive evaluation (NDE) technique incorporating machine learning which can be used for reliable inspection of detrimental microstructure before and after welding
- Significantly improving the fidelity and predictive capability of computational model for multi-pass, multi-layer welding by incorporating molten pool dynamics and metallurgical transformation kinetics
- Training graduate and undergraduate students on NDE and welding applications related to fossil energy

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Overview of Research Tasks

Task 1.0 – Project Management and Planning	Task 2.0 – Fabrication of Weld Coupons
Task 3.0 – Gleeble Physical Simulation	Task 4.0 – Microstructure and Hardness Characterization
Task 5.0 – Non-Destructive Evaluation	Task 6.0 – Physics-based Models
Task 7.0 – Reporting	





Task 3.0 - Gleeble Physical Simulation for Grade 91 and Grade 92 steels

- Gleeble used to produce weld HAZ microstructures i.e., CGHAZ, FGHAZ, and ICHAZ
- Hardness (HV) survey ongoing for all HAZ microstructures in both tempered and non-tempered conditions

	Sample	CGHAZ	FGHAZ	ICHAZ
	Material	Temp range	Temp range	Temp range
	Grade 91	T (1200°C) > 1150°C	1150°C > T (1100°C) >870°C	1150°C > T(875°C) >870°C
	Grade 92	T (1200°C) >1150°C	1150°C >T (1100°C) >920°C	1150°C >T (940°C) >920°C

Temperature ranges used for Gleeble Simulation

1400



Actual testing in Gleeble

1200 ŝ 1000 800 600 400 200 50 100 150 250 Time (sec) Gr.92 CGHAZ at T = 1200°C 1400 1200 _{ତି} 1000 800 600 400 200

Gr.91 CGHAZ at T = 1200°C



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Gleeble thermal cycles for the **CGHAZ Weld simulation for Grade** 91 and Grade 92.

Time (sec)

300

9

100

50

Task 4.0 - Microstructure and Hardness Characterization



Vickers Hardness survey plot of Grade 91 samples showing the Weld Metal (WM), Heat Affected Zone (HAZ), and Base metal (BM)



Gr. 91 Sample





Vickers Hardness survey plot of Grade 91 samples showing the Weld Metal (WM), Heat Affected Zone (HAZ), and Base metal (BM)

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Task 4.0 - Microstructure and Hardness Characterization

Grade 92 BOP welds showing (top) Sample (bottom) cross section of sample







Vickers Hardness survey plot of Grade 92 BOP weld showing the Weld Metal (WM), Heat Affected Zone (HAZ), and Base metal (BM) for all three heat inputs.



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Task 5.0 - Nondestructive Evaluation

- Micro-resolution Ultrasonic • testing to evaluate weld microstructures
 - Gr. 91 and Gr. 92 Steel weld microstructure
 - CMT, FCAW, and GTAW (varied heat inputs)
- Ultrasonic images correlated ٠ to weld microstructures as a characterization technique
 - Ultrasonic velocity data
 - Peak to Peak amplitude _
 - Hardness measurements
 - Weld macrograph samples





BM



Grade

WM

CGHAZ FGHAZ

Task 5.0 - Nondestructive Evaluation



Straight beam UT





Phased array hand scan



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Micro-resolution ultrasonic imaging system



Task 5.0 - Nondestructive Evaluation

Relationship between Weld Microstructures, Amplitude, and Hardness (Hv) in Grade 91

- Lower amplitude (%) signals are closely related to certain areas of the weld microstructure
- The hardness values slightly varied between the two welds based on heat input



Correlation of weld microstructure to (peak to peak) Amplitude signals ultrasonic images.

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Task 5.1 - Machine Learning via CNN

- Convolutional Neural Networks (CNN) is a subtype of Neural Network for applications in image recognition
- Convolution applies a feature detector (Kernel) to the input image



Input: Gr.91 and Gr. 92 weld NDE C-images

McDermott, J. "Convolutional Neural Networks-Image Classification With Keras." (2020).

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Task 6 - Integrated Molten Pool and Metallurgical Modeling

Molten pool model

Predicted Thermal cycles

Metallurgical model of martensite tempering

Mesh for molten pool model

	Nie V		
5 mm	Substrate —		
	y x	30 mm	

- A main limitation with the existing finite element model is that the bead shapes and sizes must be known beforehand to set up the model. Such information is not always available.
- The molten pool model predicts the bead shapes and sizes by solving mass, momentum and energy conservation equations along with Volume of Fluid (VOF) method to track molten pool free surface.
- To facilitate computational efficiency, the coordinate system is attached to the moving heat source (i.e., Eulerian frame of reference).
- For model development, experimental data of welding onto low alloy steel SA-533 is used.



Model Validation for Single Bead on Plate Weld







	¹ Exp. (mm)	Comp. (mm)	Error
Deposit height	1.45	1.33	8.42%
Depth	1.22	1.25	2.79%
Width	7.00	7.24	3.42%

¹K. Zhang, M.S. Thesis, The Ohio State University, 2016

Bead Formation in Multi-Pass, Multi-Layer Weld



Model Validation for Three-Bead Deposit



- Predicted bead shapes consistent with those observed experimentally
- As the molten pool model does not require the bead shape as an input, it can be readily used to study how welding parameters and bead placement affect the thermal profiles

Calculation of Thermal Cycles

Metallurgical Model for Martensite Tempering

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 Extent of tempering (φ) calculated by non-isothermal Johnson-Mehl-Avrami-Kolmogorov (JMAK) equation:

$$\phi_i = 1 - \exp\left\{-\{k_0 \times \exp\left(-\frac{Q}{RT_i}\right) \times (\Delta t + \tau_i)\}^n\right\} (1 \le i \le m)$$

$$\tau_i = \frac{\sqrt[n]{-\ln[1 - \phi_{i-1}]}}{k_i}$$

• Hardness of tempered martensite (*H*) calculated by

$$\phi = \frac{H_{BM} - H}{H_{BM} - H_{\infty}} \longrightarrow H = H_{BM} - \phi(H_{BM} - H_{\infty})$$

Material parameters extracted from isothermal tempering experiments in Gleeble

1/RT

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Validation of Tempering Model for Single Bead Weld

Variation of Tempering and Hardness for Three-Bead Weld

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Validation of Tempering for Three-Bead Weld

Location	Distance from fusion line	Measured hardness (Hv)	Calculated hardness (Hv)
Probe 1	0.7 mm	308	326
Probe 2	1.2 mm	293	305

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Summary

- 1. Micro-resolution ultrasonic imaging capable of detecting various weld regions such as weld metal and heat-affected zone
- 2. Characterization performed on CMT and FCAW samples are consistent with past characterization studies
- 3. GTAW bead on plate samples indicate that weld process optimization will need to be performed
- 4. Molten pool model capable of simulating multi-layer, multi-pass welding without knowing bead shapes and sizes beforehand
- 5. Extent of tempering and hardness prediction considering thermal cycles and material tempering response

Next steps

- Scan Gleeble samples using micro-resolution ultrasonic imaging to understand ultrasonic beam dynamics in the HAZ regions
- Employ GTAW-hot wire welding parameters on Grade 92 samples based on computational modeling
- Apply the integrated molten pool and metallurgical model for Grade 91 and Grade 92 welds
 - Consideration of fresh ferrite formed in the intercritical HAZ
 - Tempering parameters extracted from Gleeble isothermal tempering experiments

Publications

- A. Aryan, O. C. Onwuama, D. Bourgeois, and W. Zhang. "Hardness Prediction by Incorporating Heat Transfer and Molten Pool Fluid Flow in a Multi-pass, Multi-layer Weld for Onsite Repair of Grade 91 steel." Presentation at American Welding Society Annual Professional Program, Atlanta, United States. Nov. 2022. https://doi.org/10.2172/1898594
- O. C. Onwuama, A. Aryan, J. K. Na, D. Bourgeois, and W. Zhang. "Material Characterization of Grade 91 Steel Welds using, Micro-resolution Ultrasonic Imaging System." Presentation at American Welding Society Annual Professional Program, Atlanta, United States. Nov. 2022. https://doi.org/10.2172/1898549
- O. C. Onwuama, A. Aryan, J. K. Na, D. Bourgeois, and W. Zhang. "Micro-resolution Ultrasonic Image Characterization of Grade 91 Steel Welds", Journal article submitted for peer review in April 2023.

