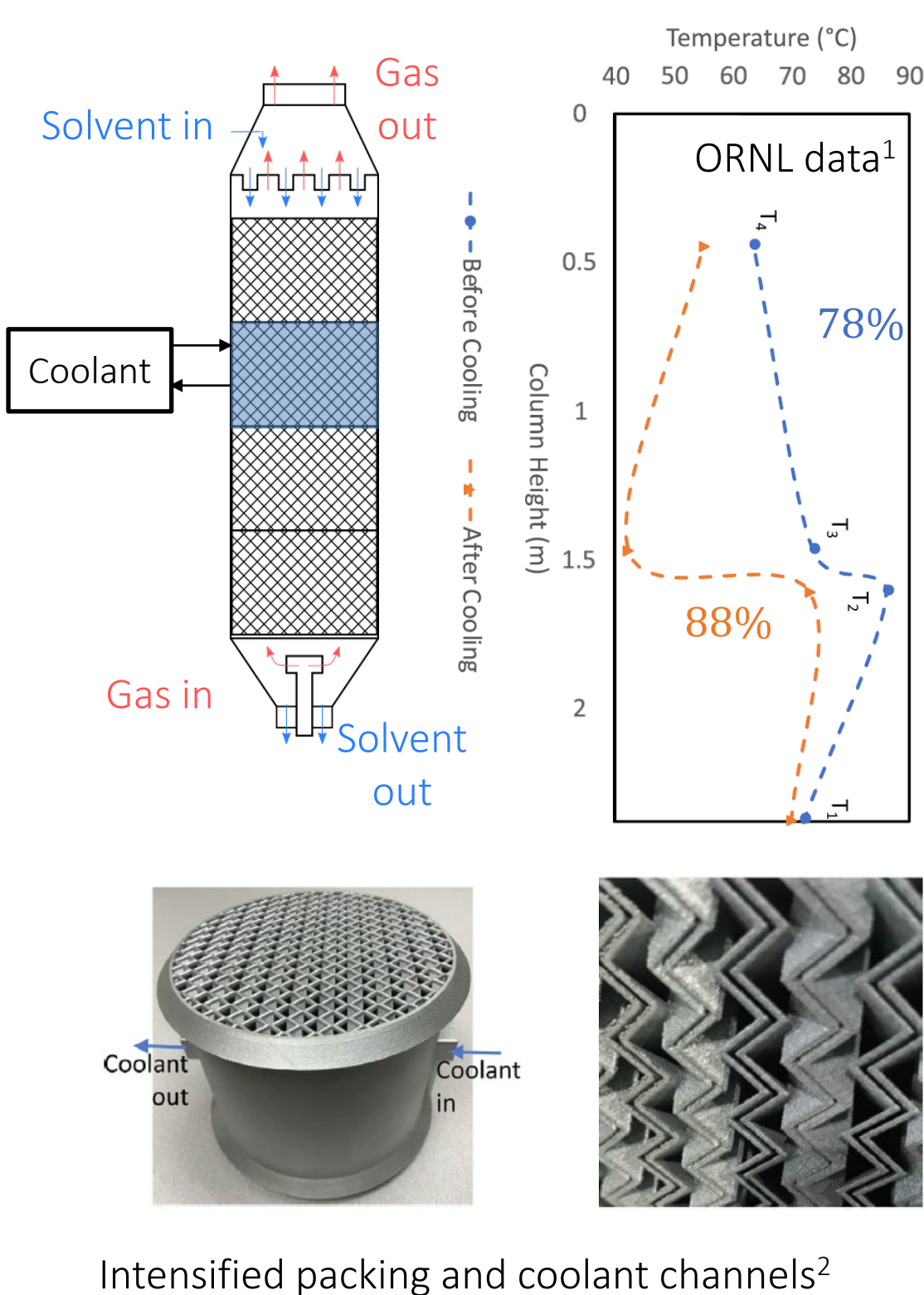


## Motivation: Process Intensification of Packed Columns

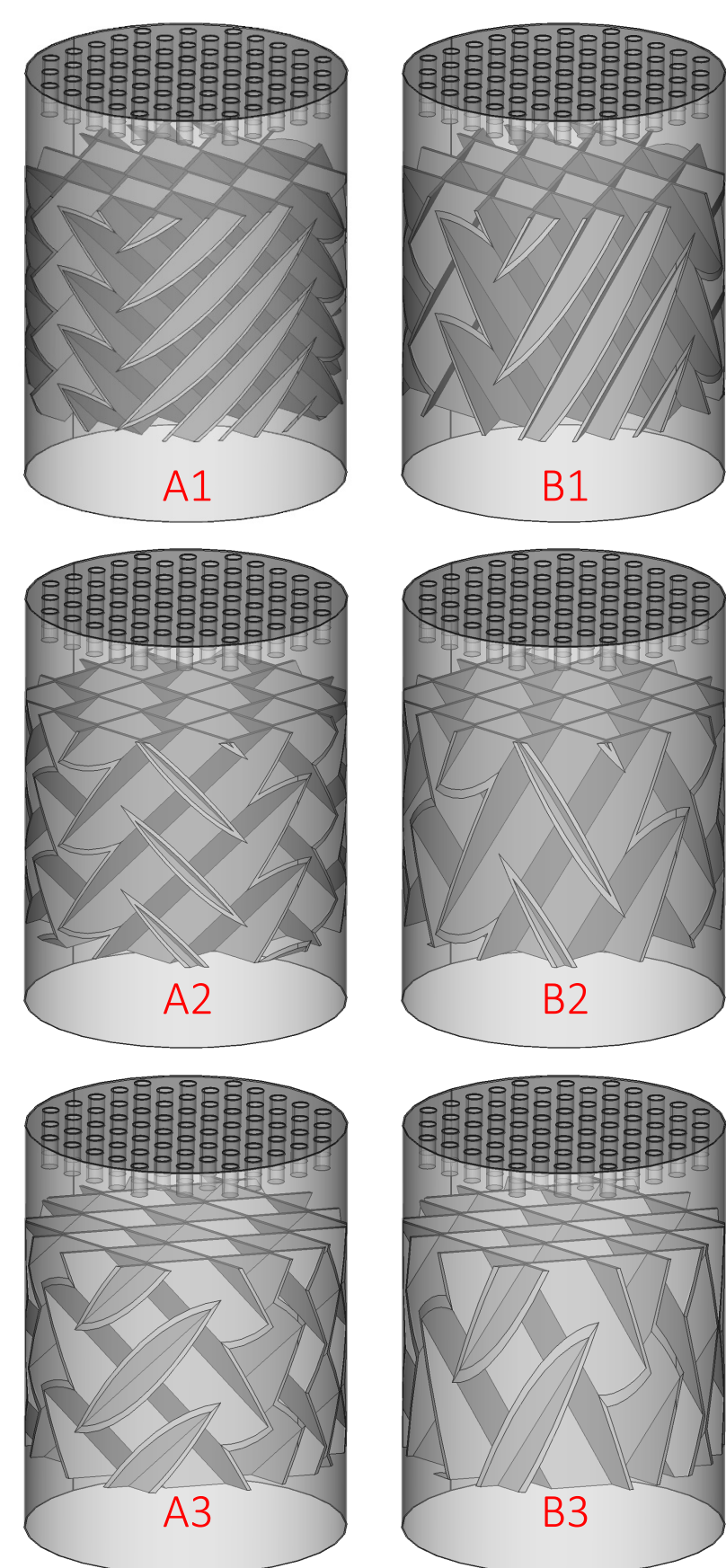
- Temperature rise in the column leads to reduced reactivity and CO<sub>2</sub> absorption.
- Packing geometries with embedded cooling channels can enhance column performance and reduce operational and capital costs.
- Computational Fluid Dynamics (CFD) is the only tool offering direct calculations of wetted area (packing-solvent interface) and interfacial area (solvent-flue gas interface) in the column, as a function of the design.
- CFD is the only tool that can inform process models for the effect of the packing's design on the column's performance, within a process optimization framework.



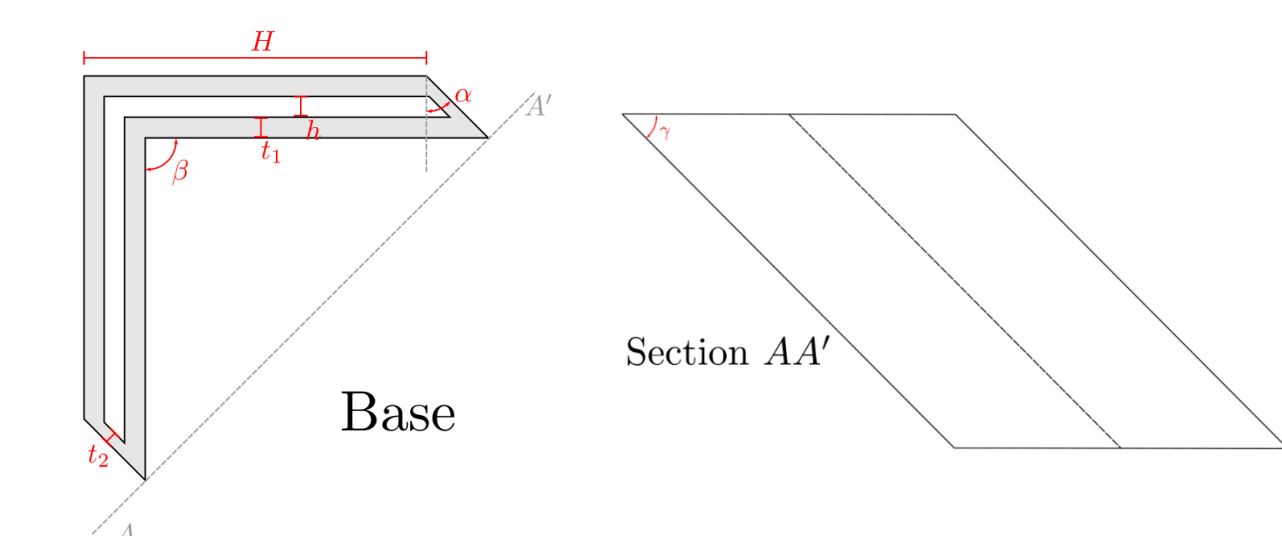
### Longer-term Objective:

- Design structured packing to optimize carbon capture rate for given solvent and operating conditions.
- Develop a computational framework to map the geometrical features of the structured packing to column performance metrics.
- Create a computational tool for process optimization that can incorporate the effect of packing design and embedded cooling through reduced order models acquired from Machine Learning (ML) algorithms.

## Parametric Construction of Alternate Packing Geometries for Optimal Column Performance



- FreeCAD based Python script automatically generates geometry for a user-defined set of parameters.



- Column performance metrics will be evaluated for each geometry using CFD simulations and mapped to the underlying geometrical parameters and operating conditions.

Design	$\beta$	$\gamma$
A1	60°	45°
A2	90°	45°
A3	120°	45°
B1	60°	60°
B2	90°	60°
B3	120°	60°

### References

- Miramontes, Jiang, Love, Lai, Sun, Tsouris "Process intensification of CO<sub>2</sub> absorption using a 3D printed intensified packing device." *AIChE J.* 2020; 66:e16285.
- Miramontes, Love, Lai, Sun, Tsouris "Additively Manufactured Packed Bed Device for Process Intensification of CO<sub>2</sub> Absorption and Other Chemical Processes." *Chemical Engineering Journal*, 388, p. 124092.
- Plaza, J.M., Van Wagener, D. and Rochelle, G.T., "Modeling CO<sub>2</sub> capture with aqueous monoethanolamine." *Energy Procedia*, 1(1), pp.1171-1178.

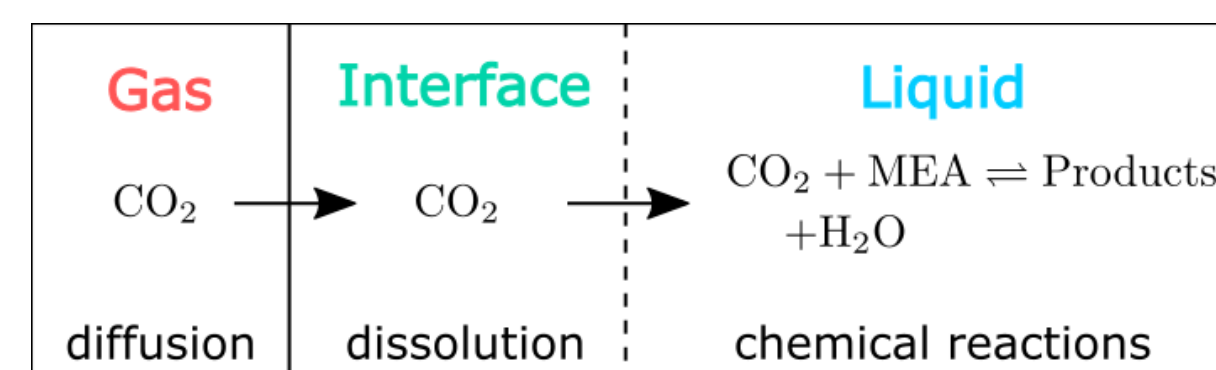
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## Mass Transfer and Thermochemical Model

### Mass Transfer model:

- Interface assumed at equilibrium
- Henry's law:  $\frac{c_l}{c_g} = He$
- Reactions considered within the bulk liquid.



Properties and models incorporated from IDAES: Instantaneous apparent/true species conversions

### Thermochemical properties:

- Ideal gas property models for the gas phase
- MEA solvent properties extracted from the IDAES package
- Solvent reaction kinetics modeled using a two-reaction mechanism<sup>3</sup>:  
 $2\text{MEA} + \text{CO}_2 \rightleftharpoons \text{MEACOO}^- + \text{MEA}^+$   
 $\text{MEA} + \text{H}_2\text{O} + \text{CO}_2 \rightleftharpoons \text{MEA}^+ + \text{HCO}_3^-$
- Liquid & vapor phase properties:
  - Mixture density
  - Mixture viscosity
  - Mixture thermal conductivity
  - Mixture specific heat
  - Species diffusivities
- Surface tension (temperature & composition dependent)
- Reaction kinetics

## Numerical Setup

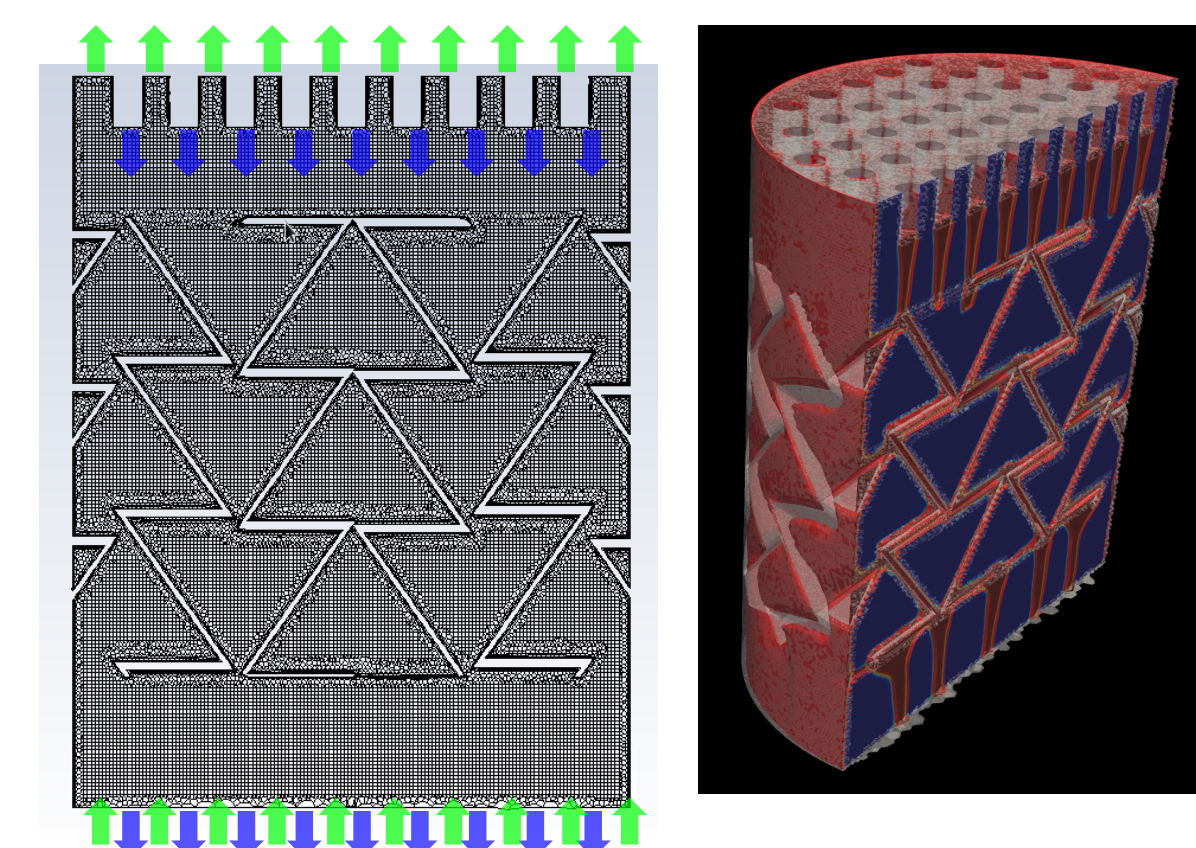
### Numerical solver and algorithm:

- Multiphase flow solver: ANSYS Fluent
- Interface tracking: Geometric Volume of Fluid (VOF) method
- Explicit reaction rate source terms

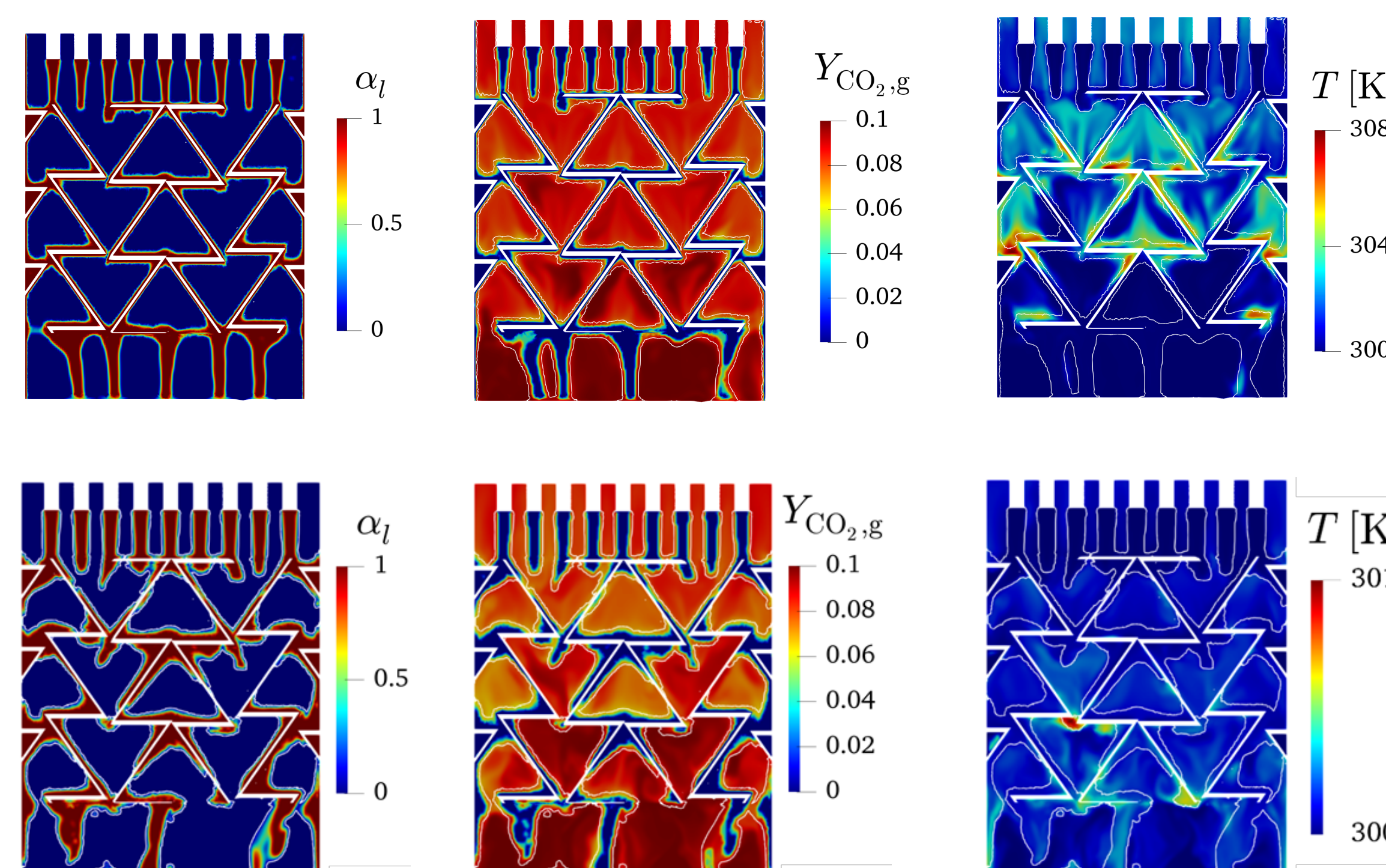
### Simulation conditions:

- Solvent: 30% MEA, 70% H<sub>2</sub>O ( $Ka \approx 1017$ )
- Flue gas: 10% CO<sub>2</sub>, 1.5% H<sub>2</sub>O, 88.5% N<sub>2</sub>
- Constant static contact angle of 40°

Liquid inflow velocity	$T_{in} = 300 \text{ K}$	$T_{in} = 343 \text{ K}$
0.1 m/s (Low)	Case 1A	Case 1B
0.3 m/s (High)	Case 2A	Case 2B

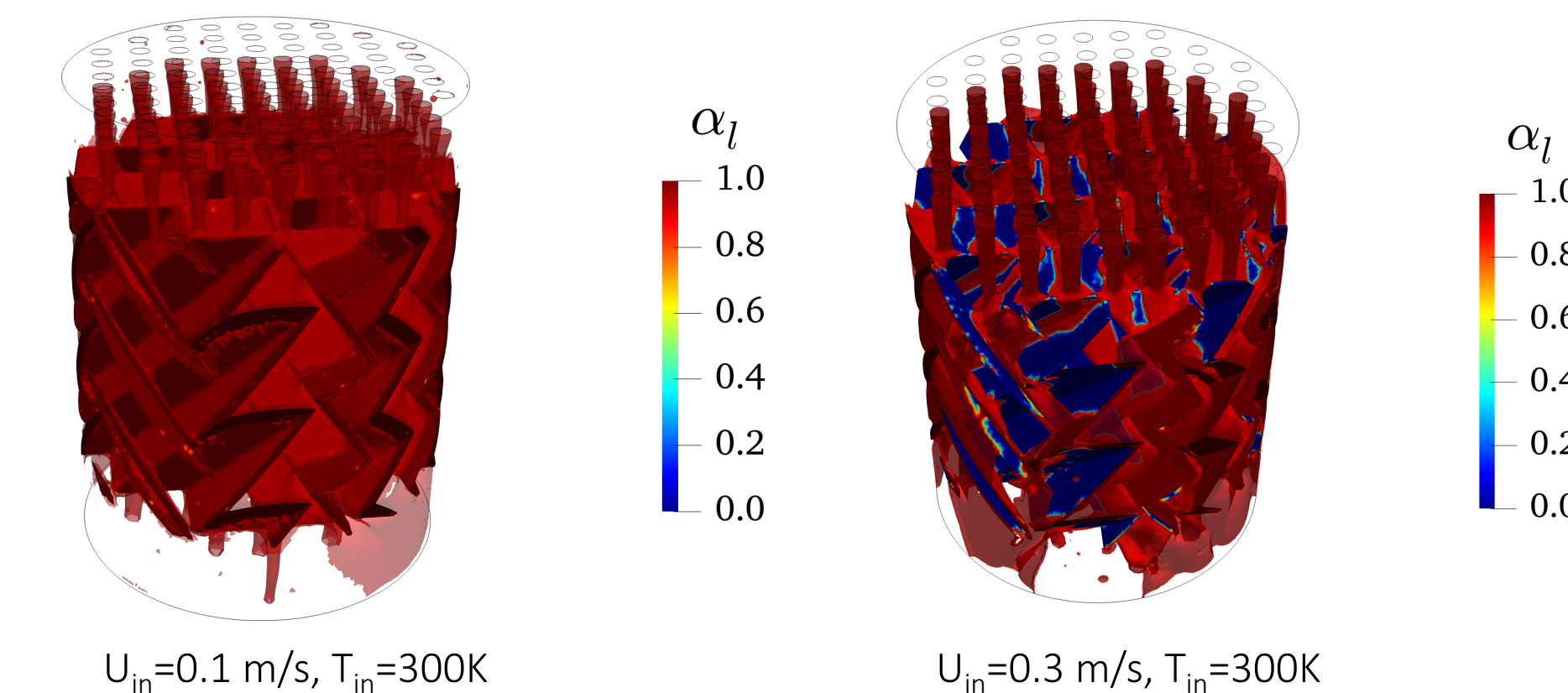


## Preliminary Results



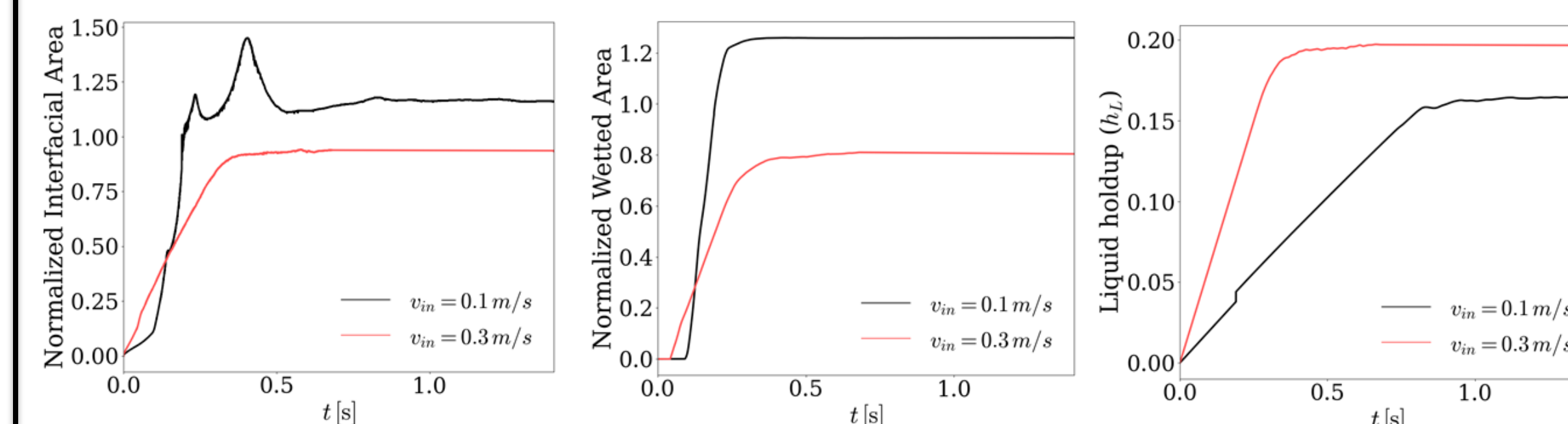
Distribution of liquid void fraction, CO<sub>2</sub> mass fraction and temperature in the column for liquid inflow velocity of  $U_{in} = 0.1 \text{ m/s}$  and  $U_{in} = 0.3 \text{ m/s}$  and temperature,  $T = 300 \text{ K}$ .

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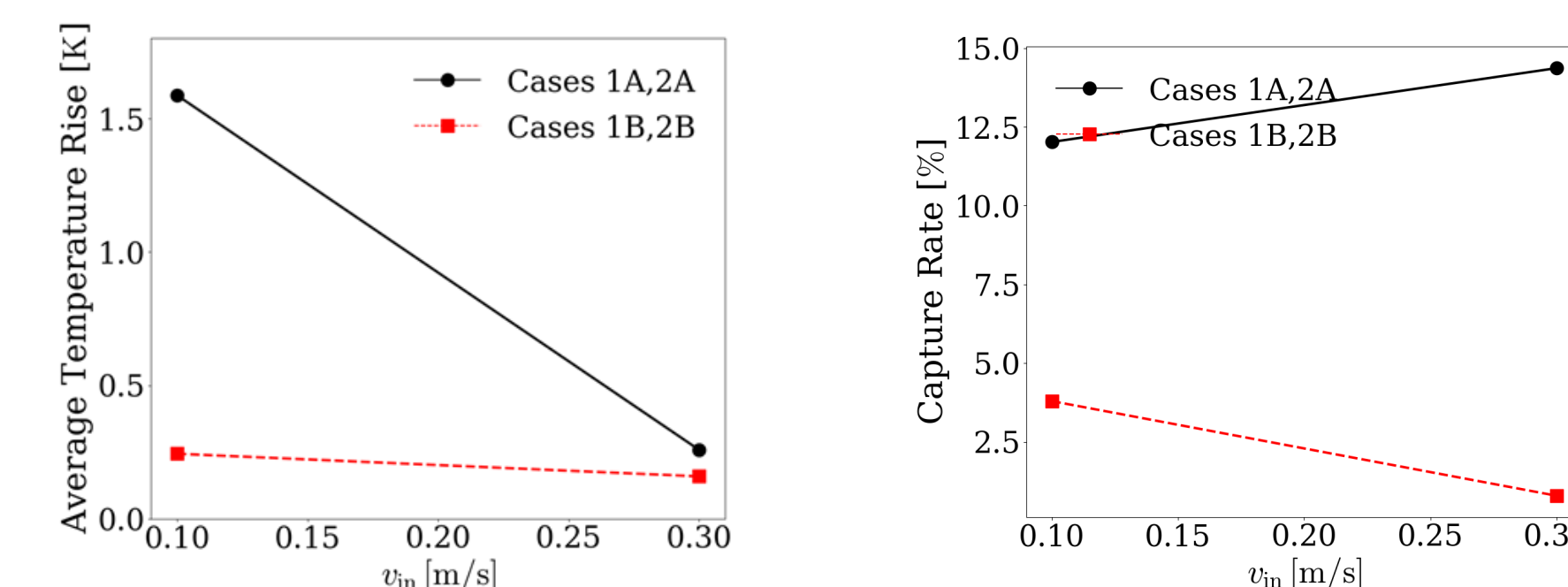


Distribution of the liquid void fraction  $\alpha_l$  over the packing surface for Cases 1A ( $U_{in}=0.1 \text{ m/s}$ ,  $T=300\text{K}$ ) and 2A ( $U_{in}=0.3 \text{ m/s}$ ,  $T=300\text{K}$ ).

## Column Performance Metrics



Normalized interfacial area ( $A_i/A_p$ ) is  $\approx 26\%$  higher for case 1A at steady state. Normalized wetted area ( $A_w/A_p$ ) is  $\approx 57\%$  higher for Case 1A at steady state. Liquid holdup is  $\approx 17\%$  higher for Case 2A at steady state.



Temperature rise is higher for case 1 (A and B) due to the higher  $A_i$  and flow residence time ( $\tau_r$ ). Capture rate is higher for case 2A relative to 1A due to a lower temperature rise and  $\tau_r$ .

Key quantities that impact the column performance: interfacial and wetted areas, liquid holdup, average temperature rise, and capture rate for different liquid loads.

## Summary & Conclusions

- First ever implementation of IDAES reaction dynamics and thermodynamics for an absorption CFD column.
- Unique, coupled multiphysics approach covering, mass, momentum and heat transfer.
- Locally and thermally dependent material properties.
- CFD simulations were performed to model CO<sub>2</sub> absorption in a three-dimensional column for four different solvent inflow conditions.
- Trends in interfacial and wetted areas, and predicted rate of CO<sub>2</sub> absorption are found to be generally consistent with observations.
- Capture rate is higher in packed column at lower temperature ( $T = 300 \text{ K}$ ) compared with that at  $T = 343 \text{ K}$ .
- Three-dimensional CFD modeling framework is shown to be a potential tool for predicting column performance trends in optimizing contactor designs. CFD predictions will further guide in improving existing process modeling frameworks for absorption columns.