

Fog+Froth-Based Post-Combustion CO₂ Capture in Fossil Fuel Power Plants DE-FE0031733

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<http://uknow.uky.edu/research/unique-public-private-research-consortium-established-caer-co2-capture-pioneers>

***2023 Carbon Management Research Project Review Meeting
August 28-September 1, 2023***

Project Objective

Reduce CO₂ capture capital and operating costs by reducing the absorber size

Performance Dates: 5/1/2019-12/31/2023

BP1

5/1/2019-1/31/2021

- Test Plan, TMP
- Absorber Fabrication and Testing
- Absorber Integration into Existing UK Bench CO₂ Capture Unit
- Parametric Testing

BP2

2/1/2021-12/31/2023

- Long-term testing
- SPDT, TEA, EH&S, TGA
- Low Absorber Bottom T Performance Evaluation

Project Team and Funding

Project Participant	Scope of Work
University of Kentucky (UK)	<ul style="list-style-type: none"> • Project Lead • Nozzle selection, compact absorber design, fabrication and integration with existing facilities • Parametric and long-term study, data analysis, reporting and project management
Industrial Climate Solutions, Inc. (ICSI)	<ul style="list-style-type: none"> • Frothing generation design and section fabrication
NexantECA	<ul style="list-style-type: none"> • Techno-economic analysis (TEA)
ALL4	<ul style="list-style-type: none"> • Environmental, Health and Safety (EH&S) assessment

	DOE-NETL	Cost Share	Total
Total	\$2,947,404	\$738,023	\$3,685,427
Percent Share	80%	20%	100%

Executive Summary

On Track to Meet Deliverables and Success Criteria

- Achieved over 2300 total hours of operation
- Absorber bottom T of 27 °C demonstrated
- TEA on low absorber bottom T case complete:
 - Net Power Output of 686 MWe, 5% increase from 2019 B12B
 - LCOE of 95.6 \$/MWh (ex. T&S), 9% reduction from B12B
 - BESS of \$36.7/tonne CO₂, 20% reduction from B12B

Previous Findings:

- 2.3 mol C/kg rich loading demonstrated, on par with traditional absorber performance with >2X absorption height
- Statistical analysis of long-term campaign data show residence time is limiting factor for CO₂ absorption and no performance change with increasing solvent degradation
- Solvent emissions after absorber consistent with small pilot data, supporting <1 ppm after water wash



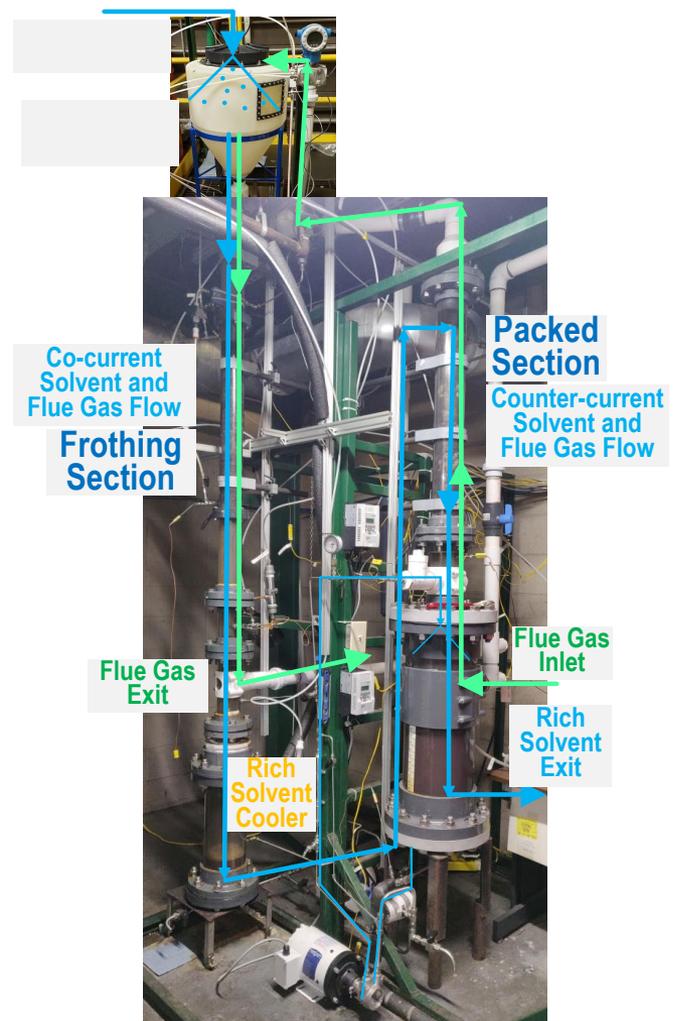
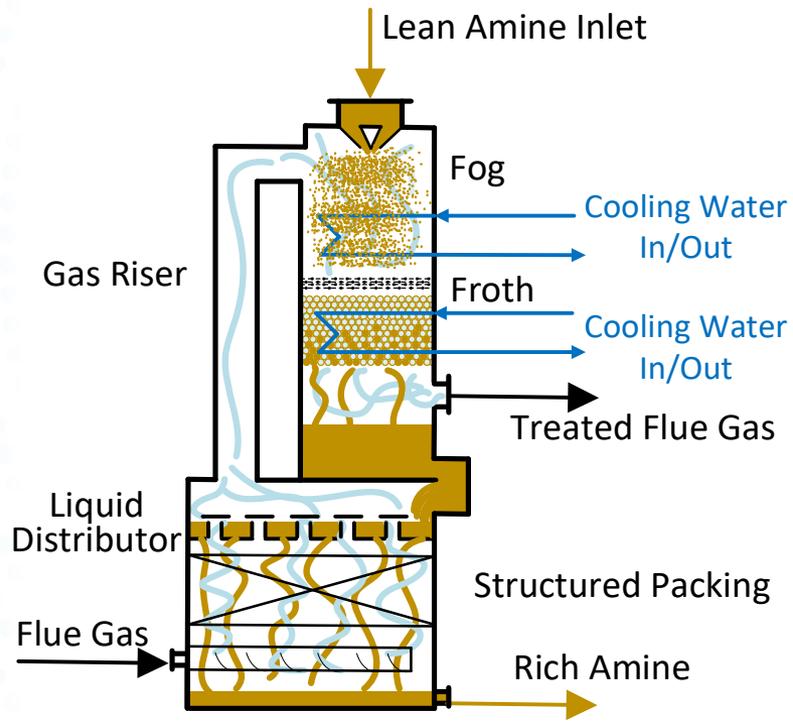
Technology Background

High Liquid-Gas Contact Surface Area
 Low CO₂ Diffusion Resistance

Reduced Absorption Height Requirement
 Lower CAPX and OPEX

Low Absorber Bottom T

Advantageous VLE For Higher Rich Loading
 Lower Regeneration Energy Requirement



CO₂ Capture Direct Costs

Equipment	45%
Columns	50%
Heat Exchangers	25%
Pumps	10%
Instrumentation and Control	5%
Balance of Plant	10%
Civil	20%
Installation	20%
Engineering Fee	10%
Insurance and Others	5%
	100%

Increased A – Replace Packing with Fog and/or Froth

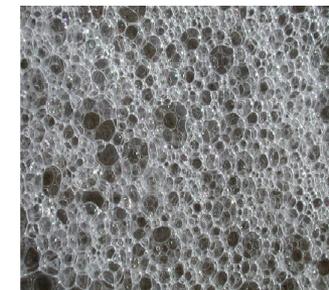
With a fog, the surface area is increased by 5 to 7 times that of 250Y structured packing.

Liquid-Gas Contact Surface Area at L/G=3.5 mass/mass					
Uniform Droplet Size (μm)	30	40	50	75	100
Liquid-Gas Contact Surface Area (m^2/m^3)	3119	2339	1871	1247	936
Improvement over 250Y Structured Packing	12.5X	9.4X	7.5X	5.0X	3.7X



With a froth, the surface area is increased by >4 times that of 250Y structured packing.

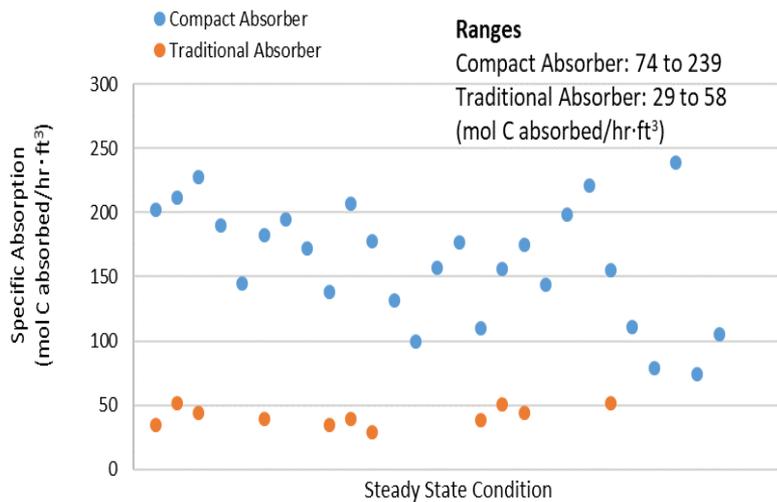
Liquid-Gas Contact Surface Area at L/G=3.5 mass/mass				
Uniform Bubble Size (mm)	3	4	5	8
Liquid-Gas Contact Surface Area (m^2/m^3)	2000	1500	1200	750
Improvement over 250Y Structured Packing	8X	6X	3X	3X



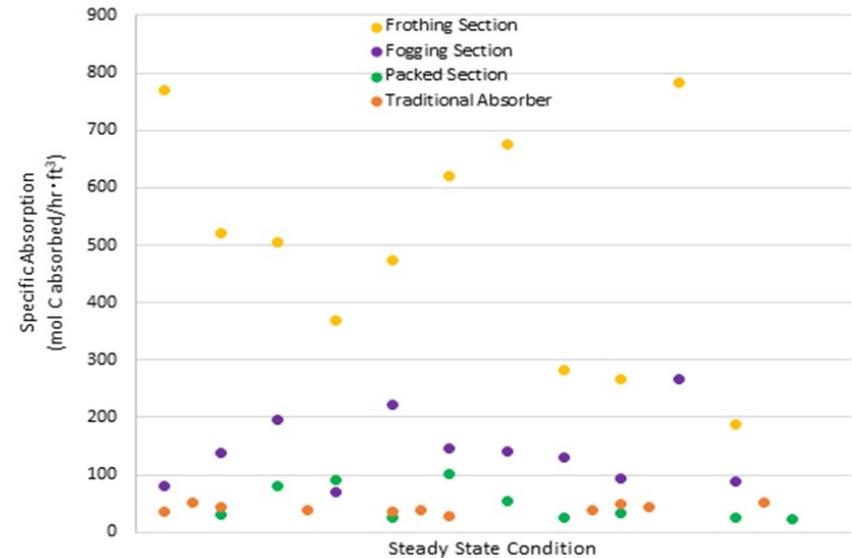
Increased k'_g – Replace Packing with Fog and/or Froth

Specific absorption 2.6 to 4.1X higher than in the traditional absorber, depending on the operating parameters.

Specific Absorption in the Compact Absorber Parametric Campaign Compared with that in a Traditional Absorber

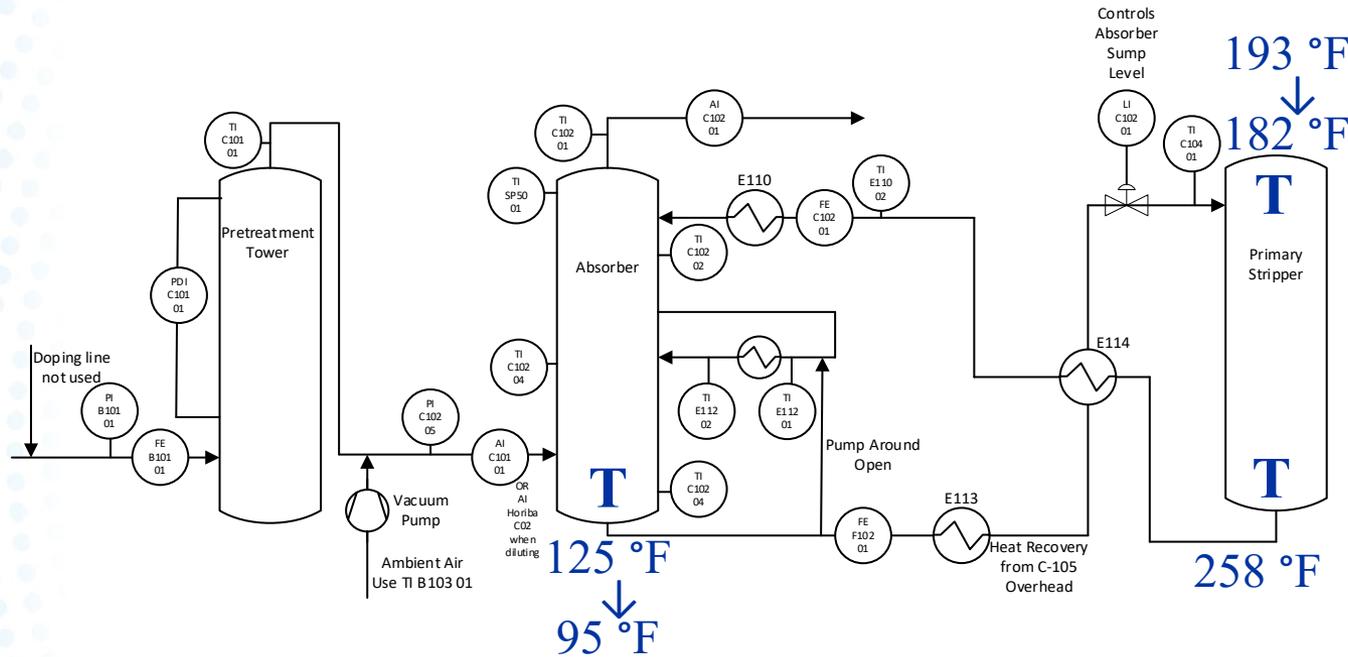


Specific Absorption in Each Section of the Compact Absorber Compared with that in a Traditional Absorber



Lower Absorber Bottom Temperature

Lower Absorber Bottom T → Lower Stripper Top T → Increased Stripper Bottom to Top ΔT → Decreased Regeneration Energy



UK Small Pilot Evaluations with 14 & 4 vol% CO₂ Flue Gas by Dilution with Air

2022 Advanced Solvent Campaign Inlet CO ₂ Concentration	Flue Gas Flow (acfm)	Lean Flow (lb/h)	Lean Absorber Inlet Temp. (°F)	Absorber Bottom Temp. (°F)	Stripper Bottom Temp. (°F)	Stripper Top Temp. (°F)	Stripper Bottom to Top Δ Temp. (°F)	% Capture	Heat Duty (KJ/kg CO ₂)
14 vol%	1300	10999	104	123	258	193	65	98	2631
4 vol%	550	4013	92	96	258	182	76	98	1767

Solvent Regeneration Process Requirements

Carrier gas flow and CO₂ desorption

$$Q_{stripper} = Q_{desorption} + Q_{sensible} + Q_{latent}$$

For 1 mole/s CO₂ at one condition of a selected solvent

$$Q_{sensible} = \frac{1}{\Delta\alpha} \cdot C_p \cdot \Delta T$$

$$Q_{latent} = \Delta U_{vapor} + P \cdot \Delta V$$

Where ΔU_{vapor} is the change in internal energy of the vapor, $E_{bottom\ T} - E_{rich\ inlet\ T}$

$$E_T = E_{CO_2}(T, P_{CO_2}) + E_{H_2O}$$

Rich Inlet T
Rich Loading

Bottom T
Lean Loading

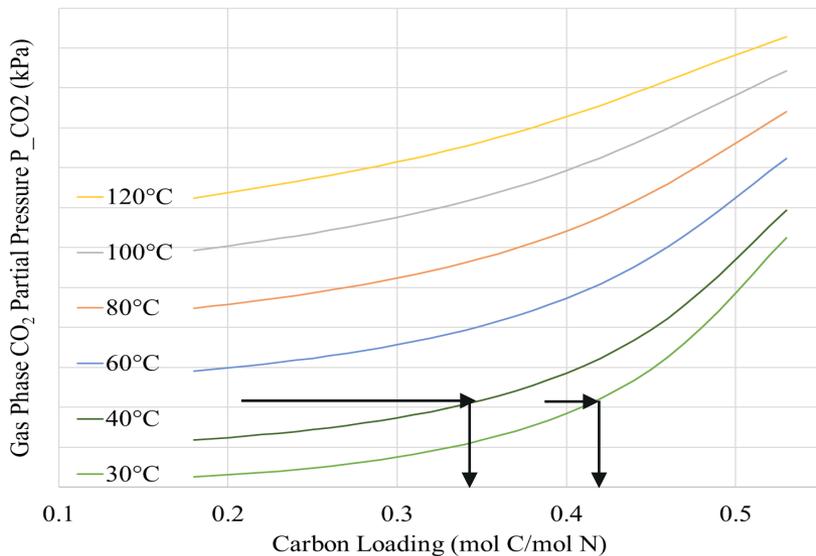


Lower Absorber Bottom Temperature

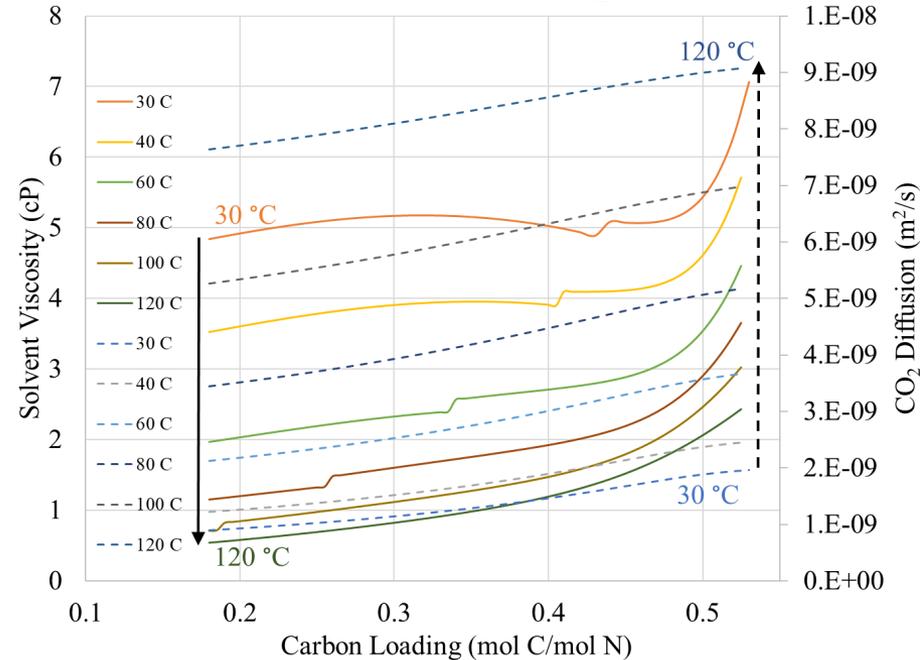
Lower Absorber Bottom T →
 Higher Achievable Rich
 Loading

Lower Absorber Bottom T →
 Increased Viscosity → Increased
 CO₂ Diffusion Resistance →
 Decreased CO₂ Diffusion

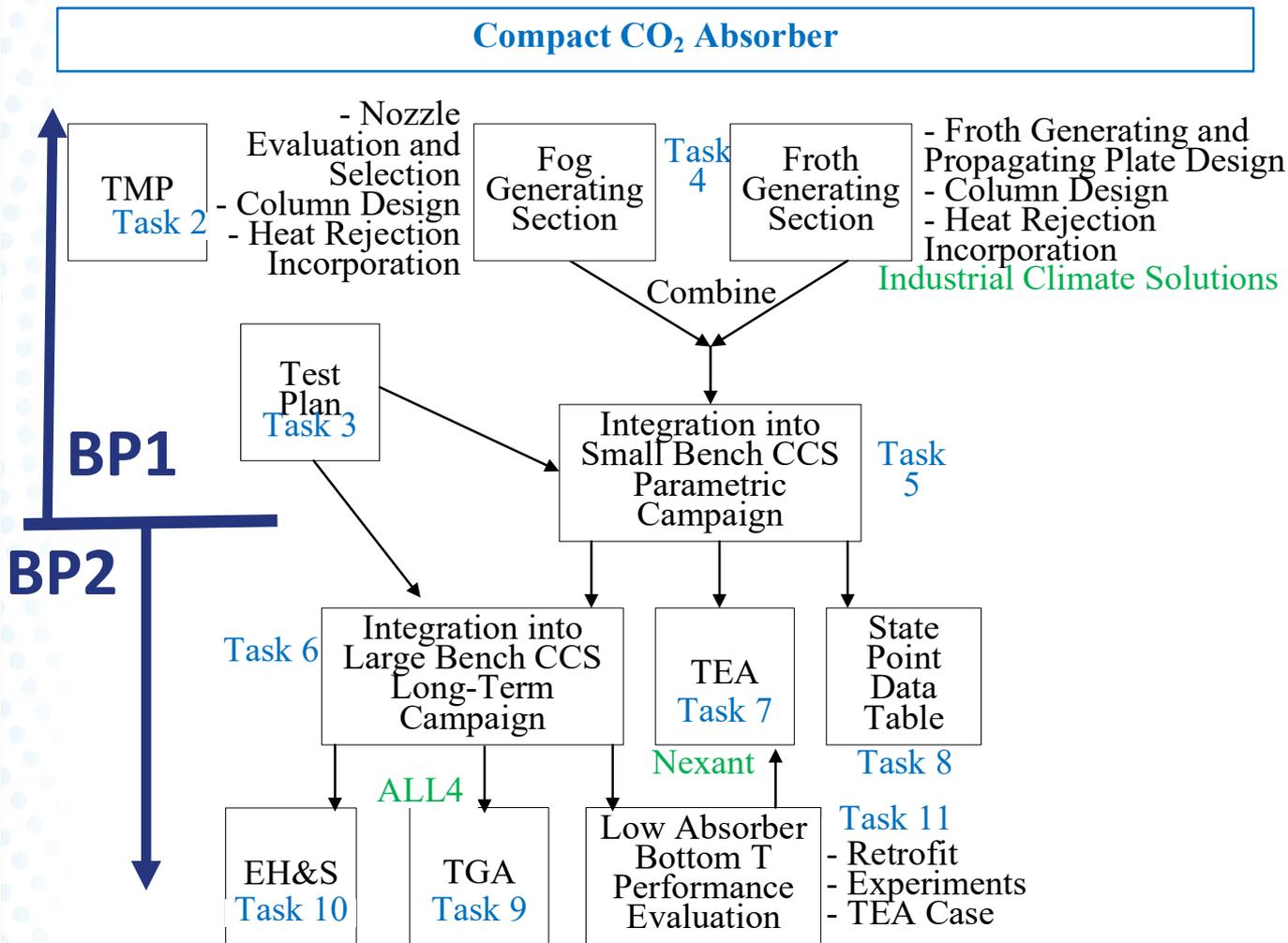
UK Solvent
Vapor-Liquid Equilibrium



UK Solvent
Viscosity and CO₂ Diffusion



Technical Approach



Design, Fabricate and Research a Compact Absorber

Atomizing Nozzle Selection

Froth Screen Design

In-Situ Heat Rejection

UK's Bench Post-combustion CO₂ Capture Facilities

Evaluation

Parametric Campaign

Long Term Campaign

TEA

EH&S

State Point Data Table

TMP

TGA

Cold Absorber Bottom T Evaluation

Additional TEA Case

Project Milestones

	Milestone Title/Description	Planned Completion Date	Actual Completion Date
1	PMP Updated	5/31/2019	5/31/2019
2	Project Kickoff Meeting	7/31/2019	5/14/2019
3	Technology Management Plan (TMP) Updated	7/31/2019	7/25/2019
4	Test Plans Completed	8/31/2019	9/15/2019
5	Fog Section of Unit Constructed and Tested	9/30/2019	8/2/2019
6	Froth Section of Unit Constructed and Tested	9/30/2019	1/31/2020
7	Compact Absorber Constructed and Integrated into Small Bench Process	4/30/2020	6/30/2020
8	Parametric Test Campaign Complete	1/31/2021	1/31/2021
9	Long-term Test Campaign Complete	6/30/2022	3/9/2022
10	Techno-economic Analysis (TEA) Complete	8/31/2022	9/7/2022
11	State Point Data Table Updated	4/30/2021	3/31/2021
12	Technology Gap Analysis (TGA) Complete	5/30/2023	7/31/2023
13	Environmental, Health and Safety (EH&S) Assessment Complete	10/31/2022	9/30/2022
14	Existing bench unit modified and achieves an absorber bottom temperature of $\leq 95^{\circ}\text{F}$ at 2-20% CO_2 inlet concentration.)	3/31/2023	2/28/2023
15	Test plan approved by NETL that covers 80-95 °F absorber bottom temperatures and 2-20 vol% inlet CO_2 concentrations	4/30/2023	2/28/2023
16	Complete ~200 hours experiments between 2 to 8 vol% inlet CO_2 concentrations at 80-95 °F absorber bottom temperatures	6/30/2023	6/28/2023
17	Complete ~200 hours experiments between 8 to 14 vol% inlet CO_2 concentrations at 80-95 °F absorber bottom temperatures	8/31/2023	5/18/2023
18	Complete ~200 hours of experiments between 14 to 20 vol% inlet CO_2 concentrations at 80-95 °F absorber bottom temperatures	10/31/2023	
19	Additional TEA Case Complete and TEA Revised	12/31/2023	

Project Success Criteria

BP1

1. Atomizing nozzles compared, selected and tested ✓
2. Froth plates compared, selected and tested ✓
3. Functioning fogging+frothing-based compact absorber with liquid/gas contact area increased by at least 5 times over structured packing ✓
4. Mass transfer enhancement by at least 4 times ✓
5. Fog droplet size of 10-50 μm ✓
6. Froth bubble size of 3-5 mm with liquid film thickness of $<10 \mu\text{m}$ ✓
7. Open section of hybrid absorber captures 60-70% of the CO_2 and packed section captures 20-30% of the CO_2 ✓

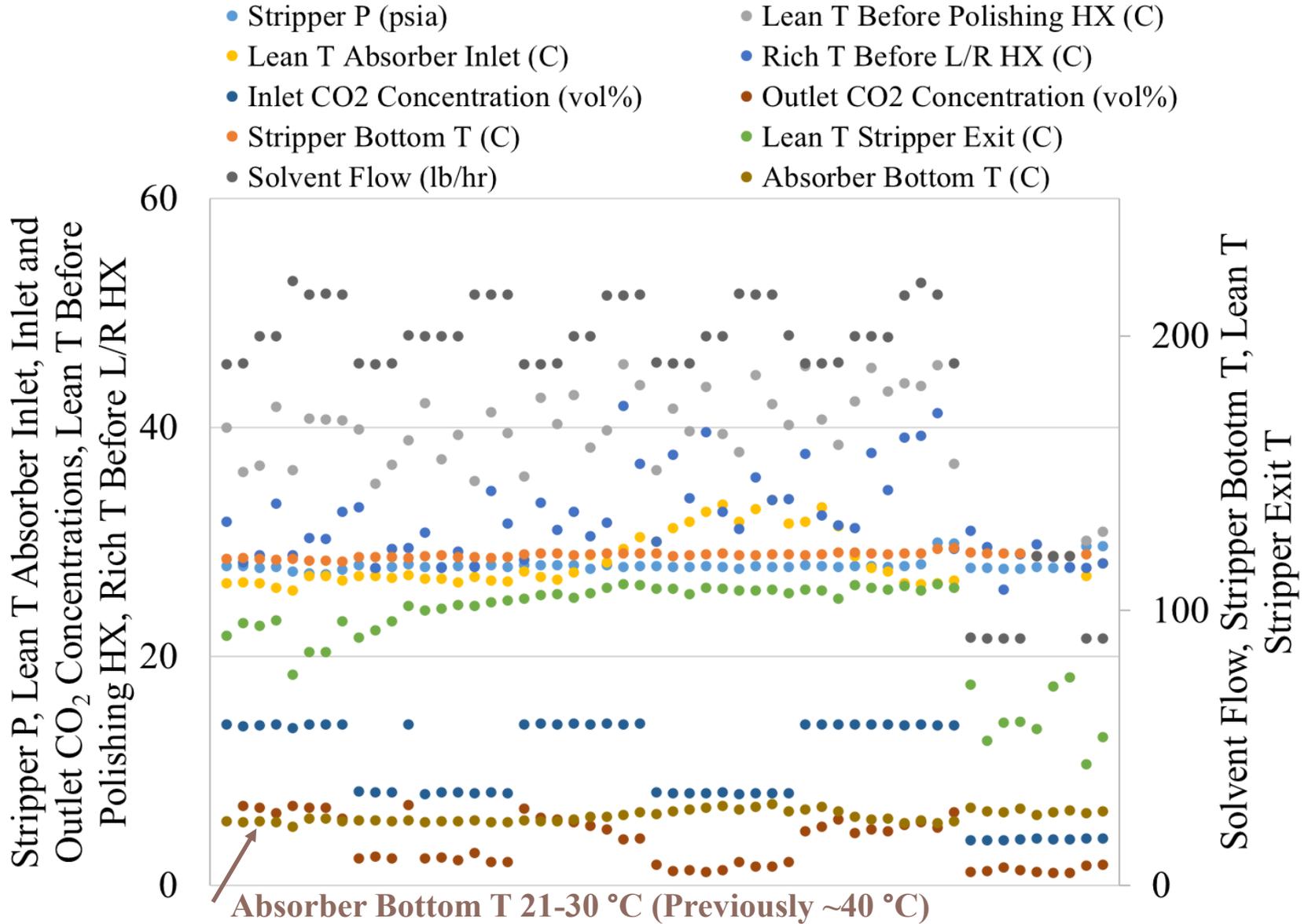
BP2

8. Long term verification of fogging+frothing-based compact absorber functionality with solvent degradation, based on ~1000 run hours on the UK CAER bench CCS with at least the same baseline capture efficiency and regeneration energy ✓
9. TEA shows the following:
 - A) capital cost savings of $\geq 10\%$ and cost of CO_2 capture reduction of $\geq 15\%$ compared to DOE RC B12B, B) an absorber column that is ~70% shorter for the same CO_2 removal duty with ~50% electricity savings for the flue gas booster fan due to the shorter column and packing height, ✓
 - C) when the UK CAER advanced solvent is used (with a heat of desorption ~20% less than 30 wt% MEA), a specific reboiler duty (energy consumption) of 900 Btu/lb (2.1 GJ/tonne) CO_2 captured can be reached by reducing the primary stripper exhaust $\text{H}_2\text{O}/\text{CO}_2$ ratio to 0.25, and ✓
 - D) ~50% reduction in the CCS capital cost ✓
10. EH&S assessment shows no impediment to technology development ✓
11. When evaluated with varied absorber bottom temperatures, the compact absorber performance at least matches the baseline capture efficiency and rich solvent loading with reduced regeneration energy. ✓

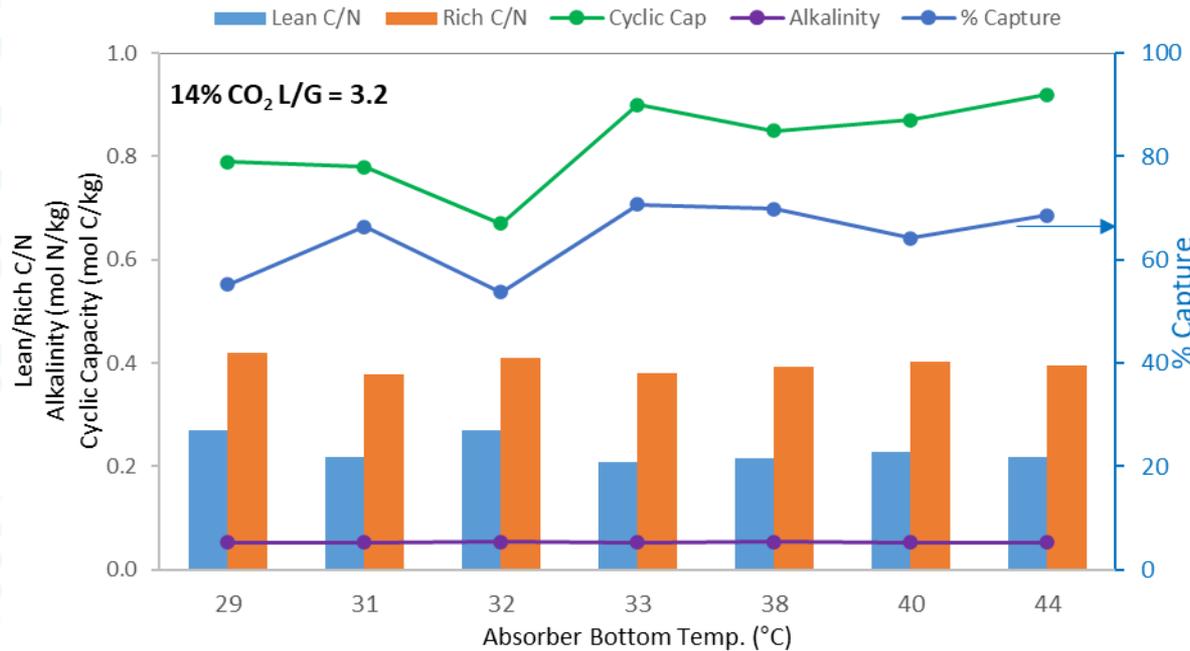
Project Risks and Mitigation Strategies

Environmental Impact	<ul style="list-style-type: none">• An alternative solvent will be used or a system modification will be made, depending on the environmental problem identified.
Low Mass Transfer in Fogging and Froth Section	<ul style="list-style-type: none">• Alternate nozzle/plate configuration may be used• Fixture installation to enhance gas/liquid interface will be considered• Solvent properties may be modified for fine mist•
Froth Stability and Bubble Size	<ul style="list-style-type: none">• Froth generating plate will be modified• Alternate liquid distributor will be considered• Solvent physical properties will be adjusted and tuned
Impact of In-situ Heat Exchanger on Fog and Froth	<ul style="list-style-type: none">• Heat exchanger design will be modified• Heat exchanger location will be adjusted
Impact of Solvent Degradation on Fog and Froth	<ul style="list-style-type: none">• Alternate nozzle configuration will be used• Froth generation plate will be modified• Degradation inhibitors may be added to the solvent

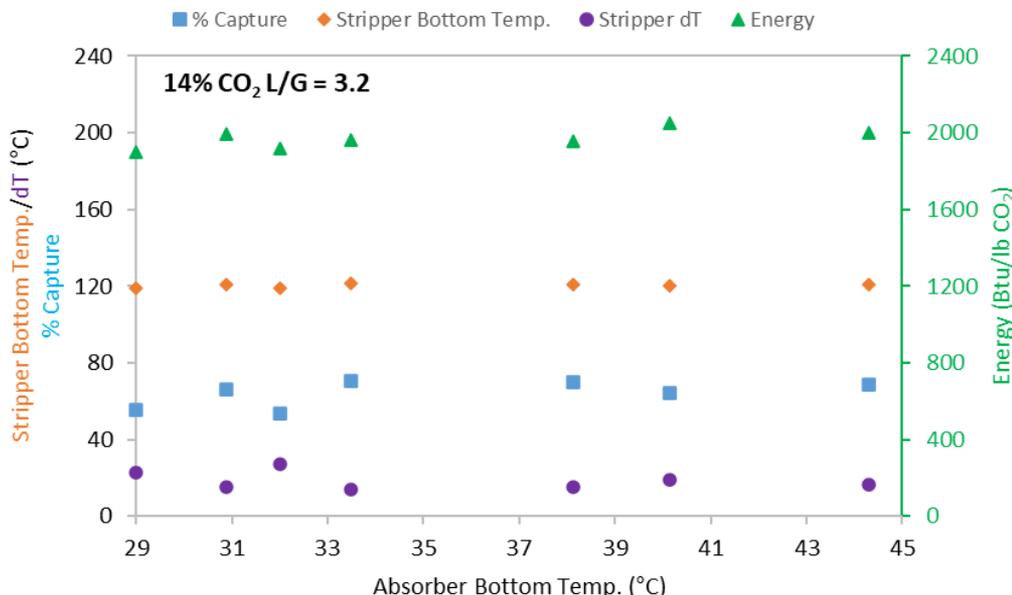
Low Absorber Bottom T Achieved



Bench Scale Performance Maintained

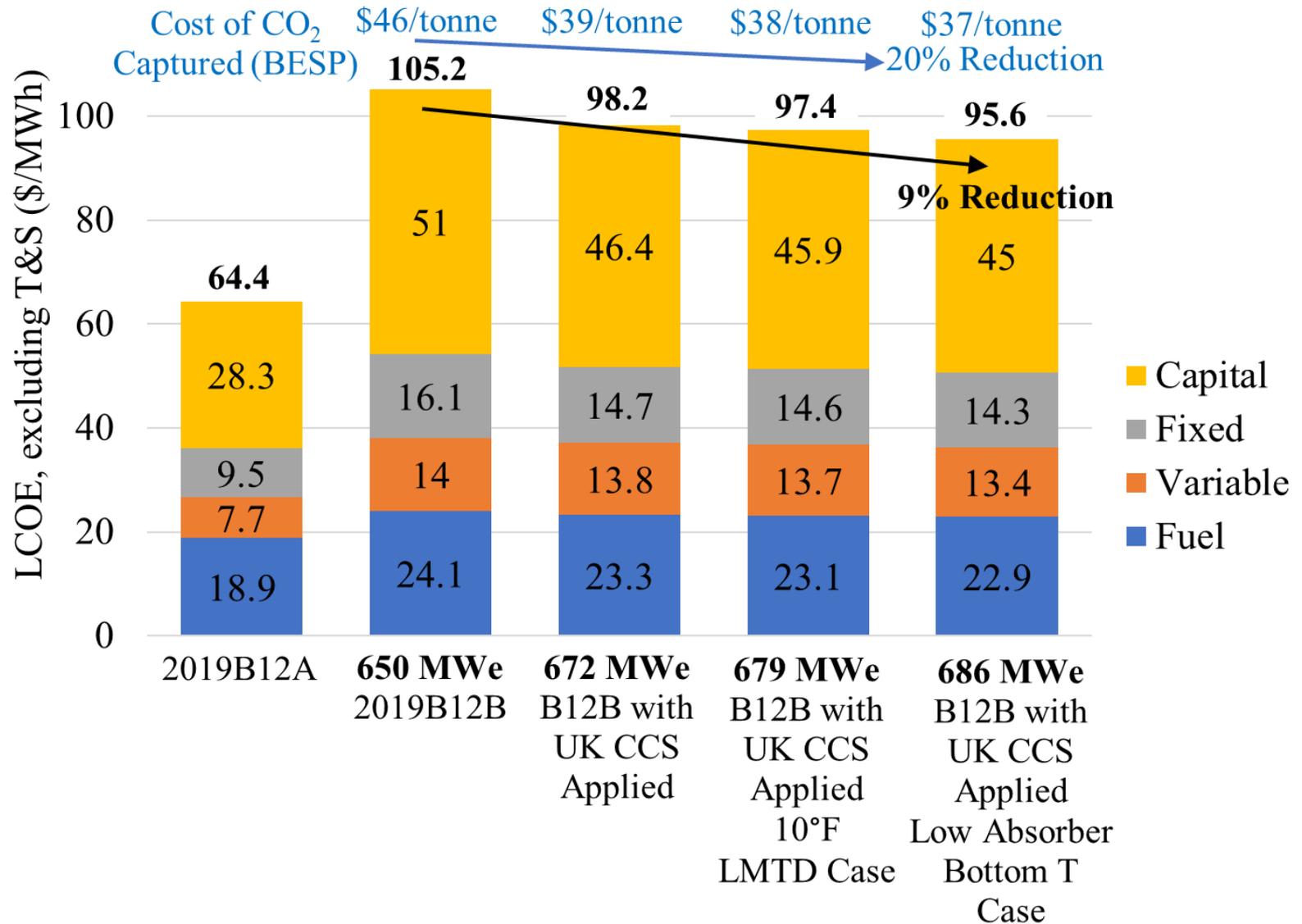


**11 °C Lower
 Absorber Bottom T
 → Same Rich
 Loading and Cyclic
 Capacity
 Because 4" ID
 Absorber is More
 Sensitive to
 Viscosity Increase**



**11 °C Lower
 Absorber Bottom T
 → Same Stripper
 Top T and Bottom to
 Top ΔT
 Because L/R
 Exchanger is
 Oversized at Bench
 Scale**

TEA Case with Low Absorber Bottom T



Next Step:

Maintain

Inlet Free Amine Flux: Inlet CO₂ Flux
to Demonstrate Higher Rich Loading
and Reduced Regeneration Energy

Synergy Opportunities

Solvent spray to be applied at large pilot, engineering scale demonstrations, NGCC FEED and CO₂ removal.

Low absorber bottom temperature to be applied at low CO₂ concentration point sources.

Collaborating with PPL Corporation, Nucor Steel, Vitro Glass, WY ITC.

Lesson Learned

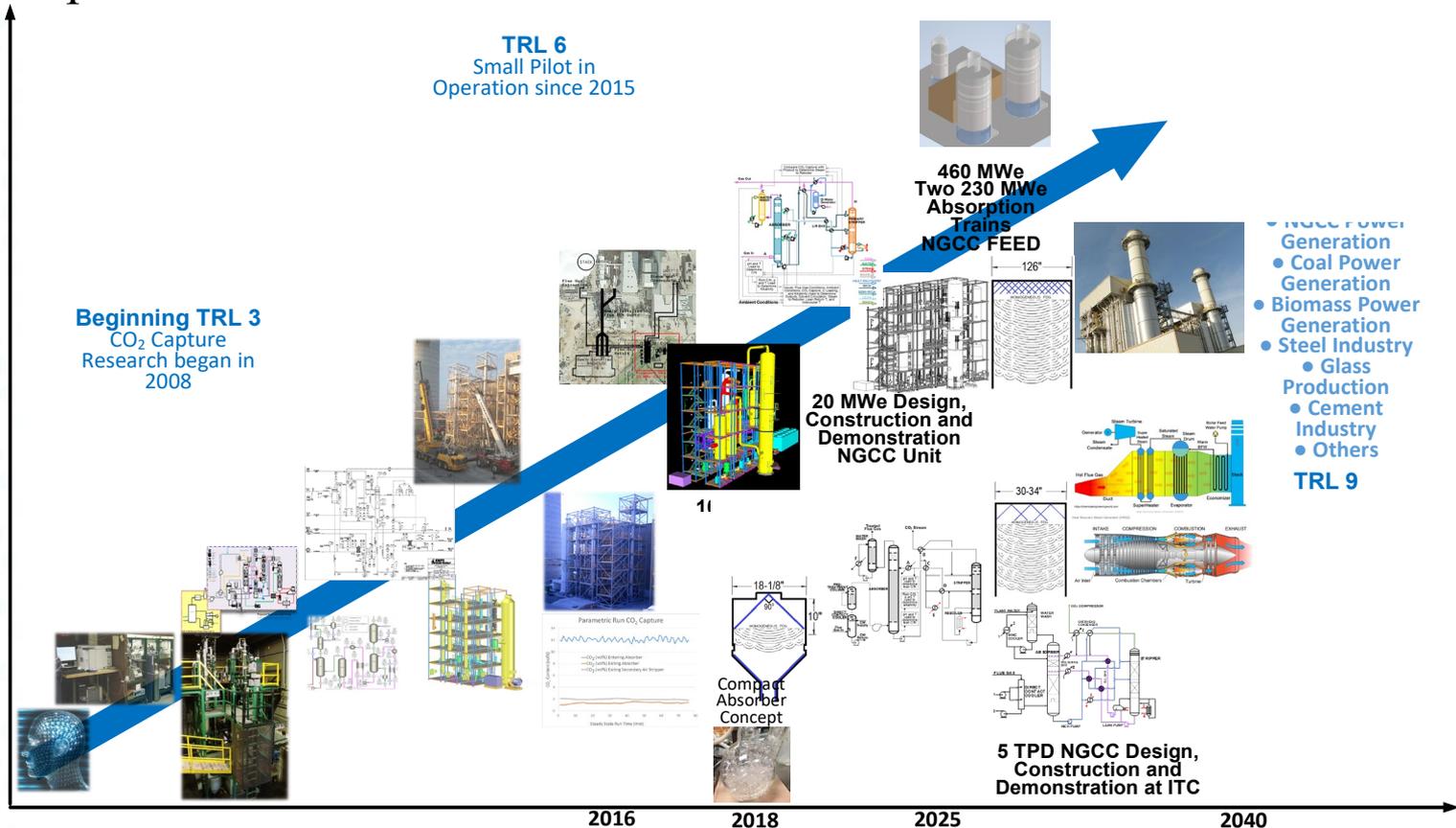
1. Advancing through the TRLs in small steps is necessary. Results differ at the lab, bench and pilot scales and the fundamental reasons must be understood.
2. 4” ID column is very sensitive to wall effects and solvent physical properties.

Development & Commercialization

Develop: Counter-current Solvent Spray and Nozzle Array Design for Large Scale Application

Demonstrate: Engineering Scale and Large Pilot, NGCC and Industrial Applications

Incorporate: Solvent Spray and Cold Absorber Bottom T into Suite of UK CO₂ Capture Processes for Reduced CAPX and OPEX



Acknowledgements

U.S.DOE NETL: Carl Laird, Greg O'Neil, José Figueroa, Dan Hancu and Lynn Brickett

Industrial Climate Solutions (Baker Hughes): Bill Hargrove and Richard Adamson

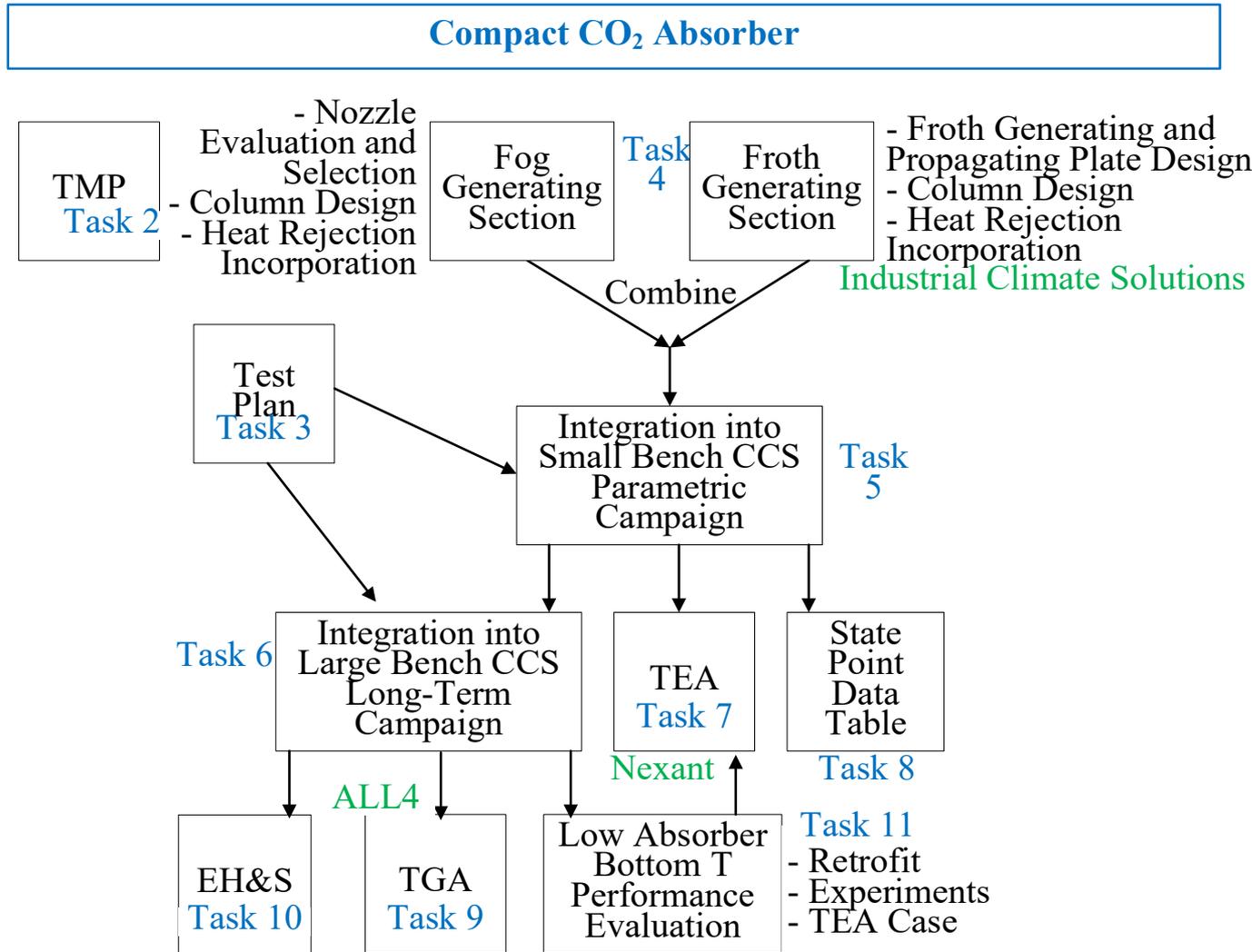
NexantECA: Alexander Zoelle, Nicholas Knez, Gabrielle Farrell, and Babul Patel

ALL4: Karen Thompson

UK: Reynolds Frimpong, Aaron Smith, Marshall Marcum, Len Goodpaster, Lisa Richburg, and Kunlei Liu



Appendix: Organizational Chart



Appendix: Gantt Chart

