

Computational Guidance for RTI Test Campaign

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Lawrence Livermore







CCSI² – Modeling, Optimization and Technical Risk Reduction



Presentation Overview

- Overview of CCSI² Modeling Capabilities
- CCSI²-RTI Collaboration
 - SDoE work for TCM pilot campaign
 - Process modeling
 - Transition to new project for modeling of GEN2NAS
- Summary and Future Work



FOQUS – Framework for Optimization, Quantification of Uncertainty, and Surrogates



CCSI² Capabilities – Uncertainty Quantification (UQ) and **Stochastic Modeling**



- Quantification of risk associated with scaleup
- Robust design and optimization
- Reduction of epistemic uncertainty through ٠ data collection (Bayesian inference)

Bayesian Inference





Sequential Design of Experiments (SDoE)

- **Design of experiments (DOE)** is a powerful tool for accelerating learning by targeting maximally useful input combinations to match experiment goals
- <u>Sequential design of experiments (SDoE)</u> allows for incorporation of information from an experiment as it is being run, by updating selection criteria based on new information
- Specific algorithms can be tailored to match experimental goals. Options available in the CCSI Toolset include:
 - Uniform Space Filling (USF)
 - Non-Uniform Space Filling (NUSF)
 - Input-Response Space Filling (IRSF)
 - Robust Optimality-Based Design of Experiments (ODoE)
- Recommended to run experiments in phases to take advantage of SDoE capabilities and customize test designs to meet expected project outcomes



Detailed discussion on SDoE:



Technical Risk Reduction: Sequential Design of Experiments and Uncertainty Quantification (Abby Nachtsheim – LANL) Thursday (8/31/2023) @ 9:30 AM during Point Source Carbon Capture Breakout Session

Highlights of CCSI² – RTI Collaboration

- Collaboration initiated in 2019 with early CCSI² work focused on computational support for modeling RTI's non-aqueous solvent (NAS) system and evaluating model performance against small pilot data
- Development of tools for amine emissions and aerosol formation
- Contributed sequential design of experiments (SDoE) capabilities to design a portion of the test campaign for NAS at TCM in 2022
- SLB forms partnership with RTI to support and accelerate industrialization of RTI solvent systems
 - CCSI² met with SLB and RTI (March 2023) to develop strategy for future work and demonstrate capabilities of CCSI² Computational Toolset
- Current work focused on refining process models of NAS and transition into new project in support of new project for next-generation solvent system



TCM Test Campaign for RTI NAS Solvent

- Leveraged SDoE to guide NAS test campaign at TCM → focused on demonstrating high levels of CO₂ capture with low solvent emissions and regeneration energy requirement
- CCSI² team contributed separate designed experiments for gas-fired combined heat and power (CHP) [3.7 vol% CO₂] and residual fluidized catalytic cracker (RFCC) [13.5 vol% CO₂] flue gas sources
- Each designed experiment includes a series of test matrices with 12-22 proposed operating conditions for flexibility in design size

<u>Design factors</u>: CO₂ Capture: 85 – 95% Absorber L/G Ratio: 2.5 – 6.5 kg/kg Stripper Pressure: 0.9 – 3.2 barg



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SDoE Results – Data Collection at TCM

Data sets generated for SDoE demonstrate good coverage of operation space:

Carbon Capture Simulation for Industry Impact



CCSI² Process Modeling Support – Current Work Goals

- Evaluate quality of fit to pilot data of current version of process model
 - Coal-based flue gas (analysis in progress)
 - Natural gas-based flue gas (analysis forthcoming)
- Identify needs for refinement of individual sub-models through re-calibration and/or parametric UQ
- Leverage CCSI² Toolset to determine best practices for solving robustness issues associated with these models
 - Ensure modeling framework is sufficiently robust in order to extend to new solvent formulations



Preliminary Process Modeling Results - Absorber

- Initial efforts to model absorber have revealed computational challenges that must be addressed in order to successfully execute future scope
 - Incorporation of solvent intercooling and kinetic models have strong effect on model robustness
 - Plan to explore options for leveraging FOQUS tool to improve model performance
- CO₂ capture percentage generally overpredicted (~6% on average)
 - Performance of absorber highly sensitive to thermodynamic models in comparison to aqueous systems (MEA, CESAR1)
 - Uncertainty in model inputs (e.g., CO₂ loading, intercooler duty, solvent temperature) could potentially have an impact



Preliminary Process Modeling Results - Stripper

- Modeled stripper section as stand-alone process with CO₂ capture level constrained based on experimental data
- Stripper inlet temperature fixed to experimental value by adjusting lean/rich heat exchanger
- Compared experimental and model predictions of specific reboiler duty (SRD):



Identify bias in which the model consistently underpredicts heat of absorption by 20% - can attribute in part to heat of absorption calculation



Preliminary Process Modeling Results - Stripper

 $Q_{reb} = Q_{sensible} + Q_{CO_2 Desorption} + Q_{H_2 o Evaporation}$

Potential sources of discrepancy:

- Thermodynamic model (VLE, heat of absorption, heat capacity)
- Uncertainty in boundary conditions (lean/rich CO₂ loading, temperature, pressure)

Heat of absorption calculation:

- For water-lean solvent, term associated with H₂O evaporation should be negligible
- For thermodynamic consistency in e-NRTL model, calculations of differential heat of absorption expected to be consistent with Gibbs-Helmholtz equation

Differential Heat of Absorption:

Gibbs-Helmholtz Equation:



Preliminary Process Modeling Results - Stripper



- Heat of absorption not directly defined in Aspen Plus as physical property. Two options for including in thermodynamic model regression:
 - Differential heat of absorption requires user subroutine
 - Gibbs-Helmholtz equation use temperature perturbation on CO₂ partial pressure (*method* used in this work)
- With internally consistent thermodynamic framework, these methods should produce comparable results
- Magnitude of differential heat of absorption underpredicted – directionally consistent with bias in SRD prediction
- This discrepancy is not unique to this system additional analysis is ongoing for multiple solvent systems

GEN2NAS Project

- RTI awarded new project (FE032218) to advance their non-aqueous capture technology with new solvent formulation
- Planned CCSI² contributions (EY23 EY24):
 - Computational modeling to quantify effect of solvent properties (e.g., viscosity, thermodynamics) on equipment performance
 - Implement UQ work for assessment of risk associated with scale-up of process models
 - Explore use of SDoE strategies to aid in data collection for model and sub-model validation
- For more details on this project:
 - GEN2NAS Solvents for CO₂ Capture from NGCC Plants (FE0032218)
 (Jak Tanthana RTI) Wednesday (8/30/2023) @ 11:30 AM during Point Source Carbon Capture Breakout Session



Summary and Conclusions

- Collaboration with RTI has demonstrated successful application of CCSI² Toolset for development and refinement of process models of novel CO₂ capture processes
 - SDoE methods improve quality of data collection \rightarrow essential for quantifying and reducing risk for process scale-up
- These tools and methodologies can be customized to support different technologies and test campaign goals
- Work is ongoing to finalize process models of first-generation NAS system, which will be leveraged to support development of models for new solvent formulation (GEN2NAS)



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For more information

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Backup Slides



Heat of Absorption Calculation Inconsistency – Other Models



MEA model distributed with Aspen Tech software (ENRTL-RK thermodynamic method)



PZ model distributed with Aspen Tech software (ENRTL-RK thermodynamic method)



MEA model developed by CCSI team – Akaike information criterion (AIC) used to regress parameters to fit thermodynamic data - *does not include electrolyte pair parameters*

(ELECNRTL thermodynamic method)

Differential Heat of Absorption

Gibbs-Helmholtz Equation

