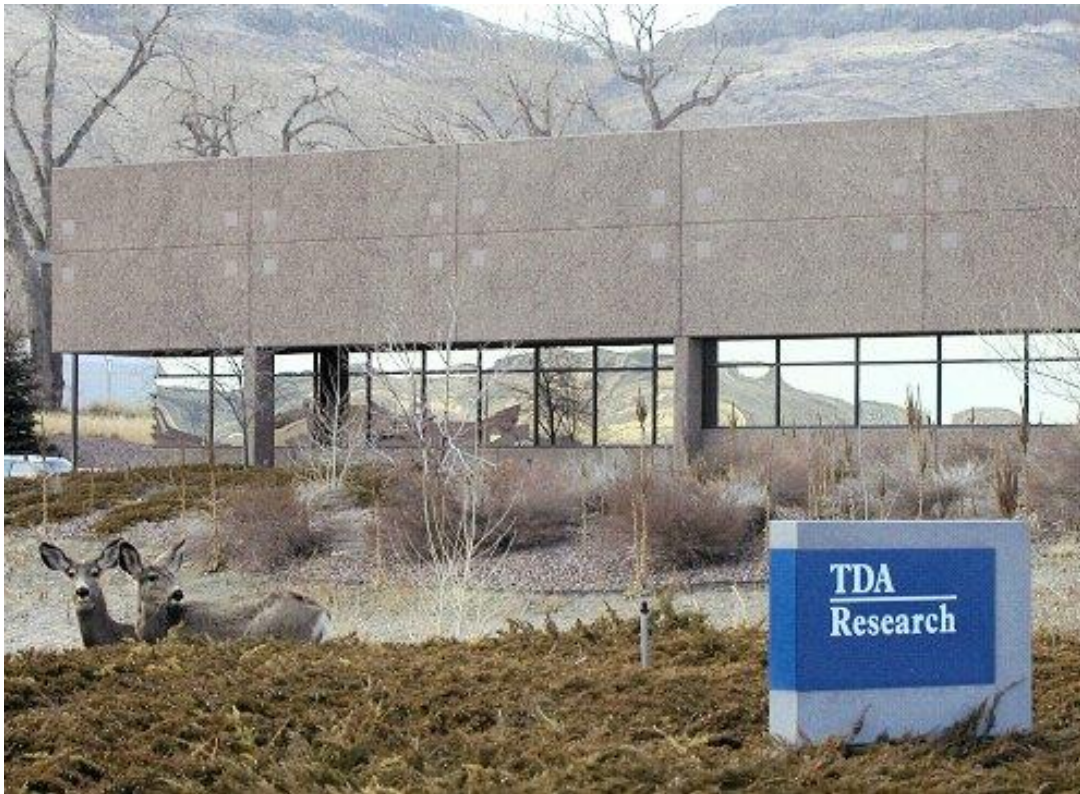


Membrane-Sorbent Hybrid System for Post-Combustion Carbon Capture (DE-FE00031603)



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TDA Research, Inc.

August 28, 2023

Project Objectives and Project Team



- Design and construct a $\approx 1 \text{ MW}_e$ scale membrane-sorbent hybrid system for post-combustion carbon capture
- Hybrid process combines a polymer membrane and a low-temperature physical adsorbent to remove the CO_2 from flue gas
 - Membrane has been developed by MTR
 - Adsorbent has been developed by TDA for post-combustion capture

Main Project Tasks

- | | |
|-----|--|
| BY1 | <ul style="list-style-type: none">✓ Design of the Test Unit✓ Initial Design Review✓ Preliminary Techno-economic analysis |
| BY2 | <ul style="list-style-type: none">✓ Fabrication of the Test Unit✓ Site Preparation, Installation and Shakedown Tests |
| BY3 | <ul style="list-style-type: none">✓ Field Tests (ongoing; 6–12 months duration)✓ High Fidelity Techno-economic Analysis |

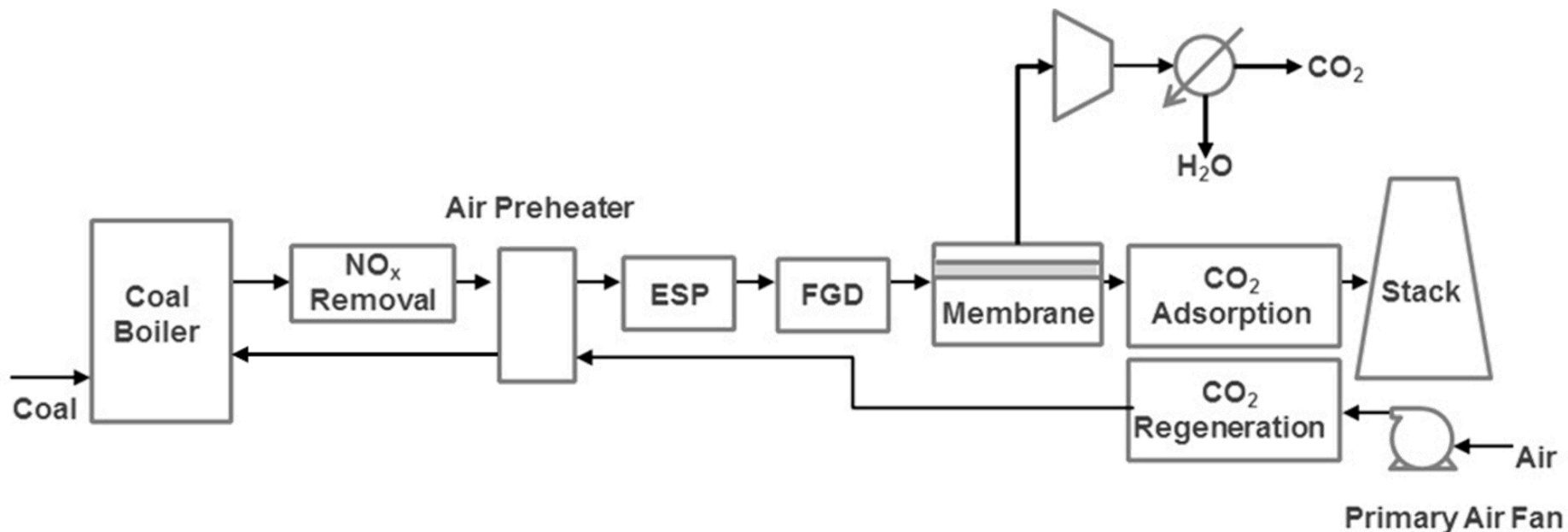
Project Duration

- Start Date = August 18, 2018
- End Date = August 14, 2023

Budget

- Project Cost = \$11,498,524
- DOE Share = \$9,198,799
- TDA & its partners = \$2,299,725

Hybrid Membrane Sorbent Process



- **Membrane operates at $\approx 50^{\circ}\text{C}$ under mild vacuum (≈ 0.2 atm), removes ≈ 55 – 60% of CO₂ and almost all water**
 - TDA's sorbent removes remaining CO₂ in the membrane effluent (retentate) ensuring 90+% carbon capture
 - The boiler feed air is used as a sweep gas to facilitate sorbent regeneration
 - CO₂ circulation to the boiler air intake increases the CO₂ concentration in the flue gas, providing a higher driving force for the membrane

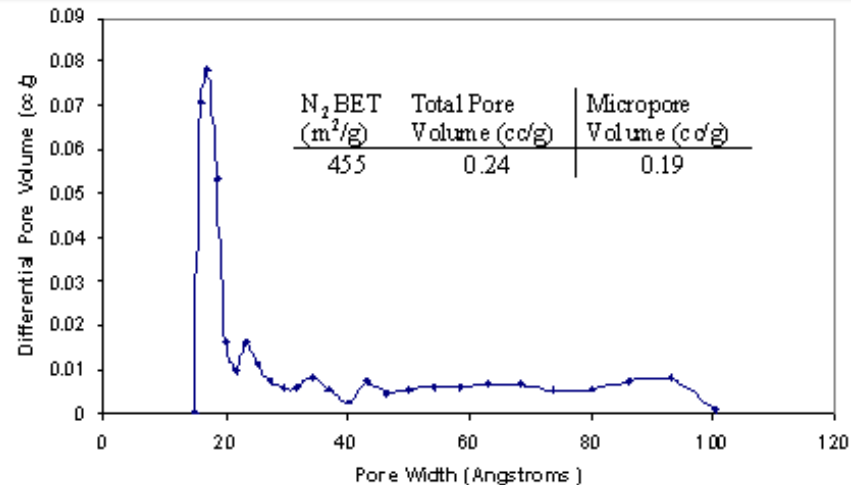
TDA Sorbent

- TDA developed a mesoporous carbon sorbent modified with surface functional groups that remove CO₂ via strong physical adsorption
 - CO₂-surface interaction is strong enough to allow operation at low partial pressures
 - Because CO₂ is not bonded, the energy input for regeneration is low
- Heat of CO₂ adsorption is **4–5 kcal/mol**



US Patent 9,120,079, Dietz, Alptekin, Jayaraman "High Capacity Carbon Dioxide Sorbent", US 6,297,293; 6,737,445; 7,167,354

Sorbent optimization and production scale-up was completed in a separate DOE project (DE-0013105)

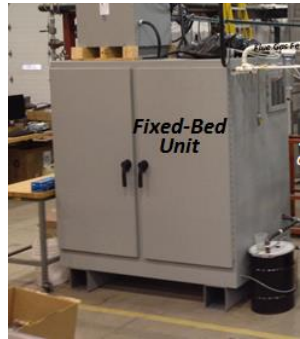


Sorbent operation in a VSA system was successfully demonstrated with actual flue gas (DE-0013105)



Technology Maturation

**0.5–1 kW
Sorbent
Only Tests**



**Gas Technology
Institute (GTI)
Tests with pilot coal
combustor**

0.5–1 kW Hybrid Tests



**Western Research Institute/
Thermosolv**



50 kW Hybrid Tests

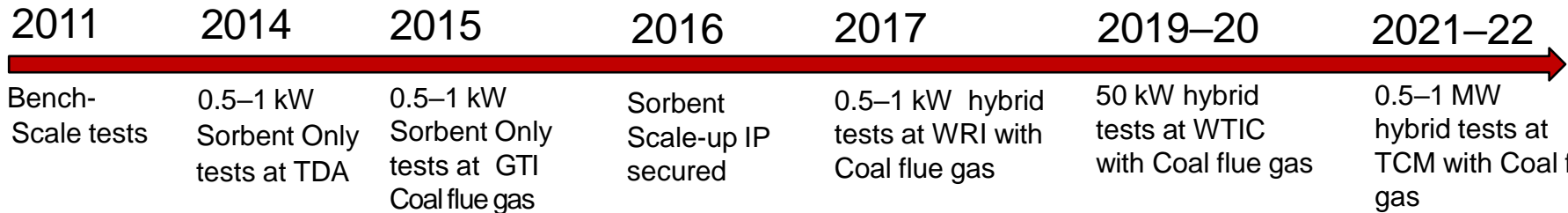


**Wyoming Integrated Test
Center (WITC) Basin Electric's
Dry Fork Station Gillette, WY**

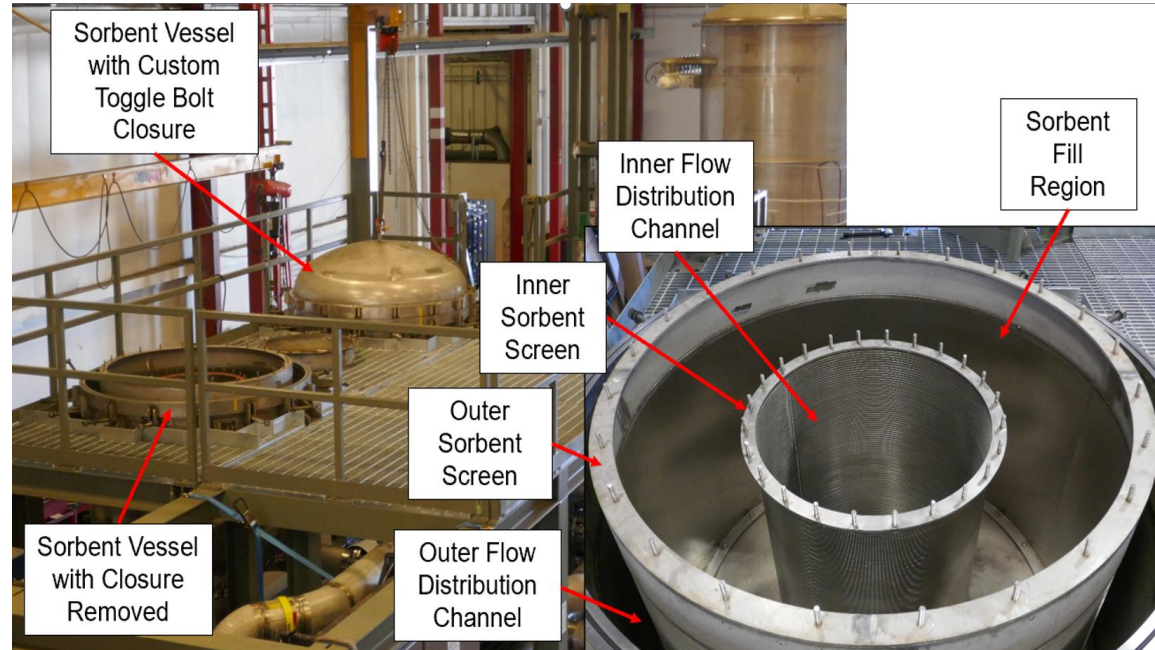
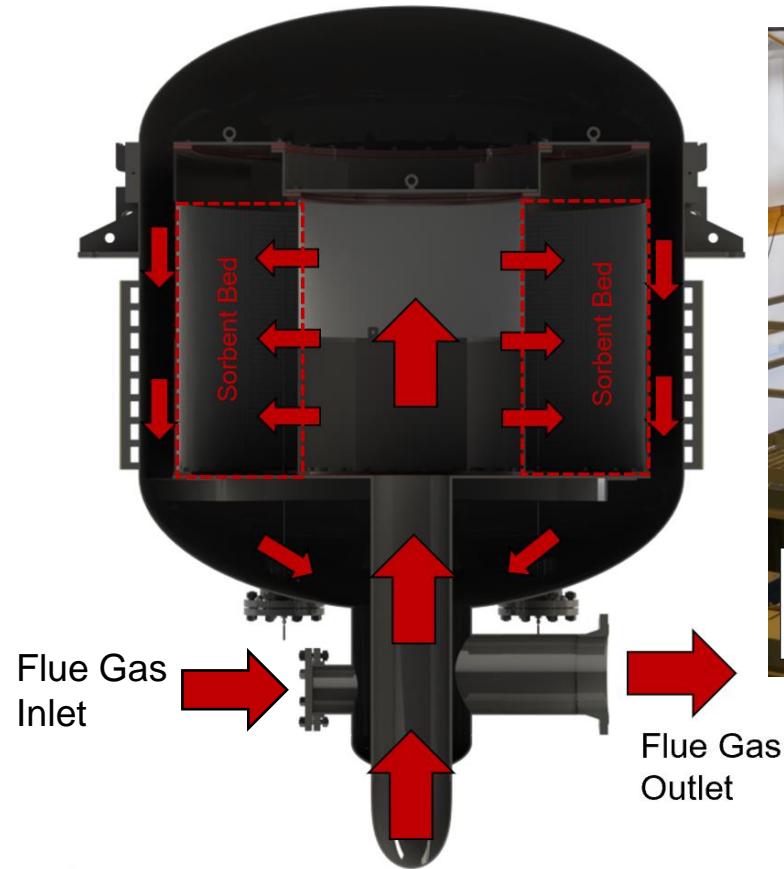
0.5–1 MW Hybrid Tests



**Technology Centre Mongstad
(TCM) Norway**

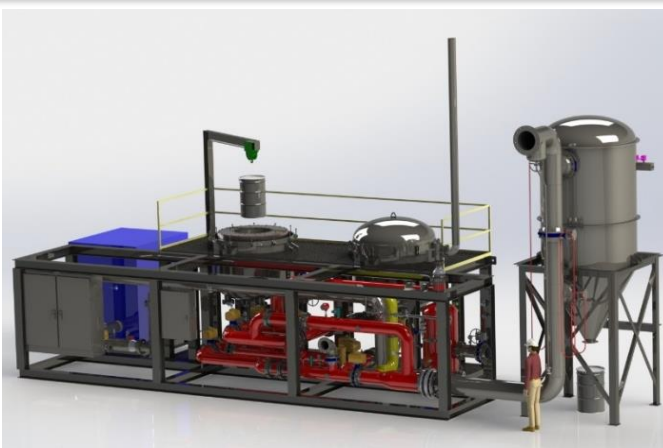


TDA Radial Flow Reactor Concept



- Sorbent is loaded in annular section of the vessel
- The flow is in radial direction
- Higher cross-sectional area and lower bed depth minimize the dP through the bed

Project Focus



TDA's Sorbent System



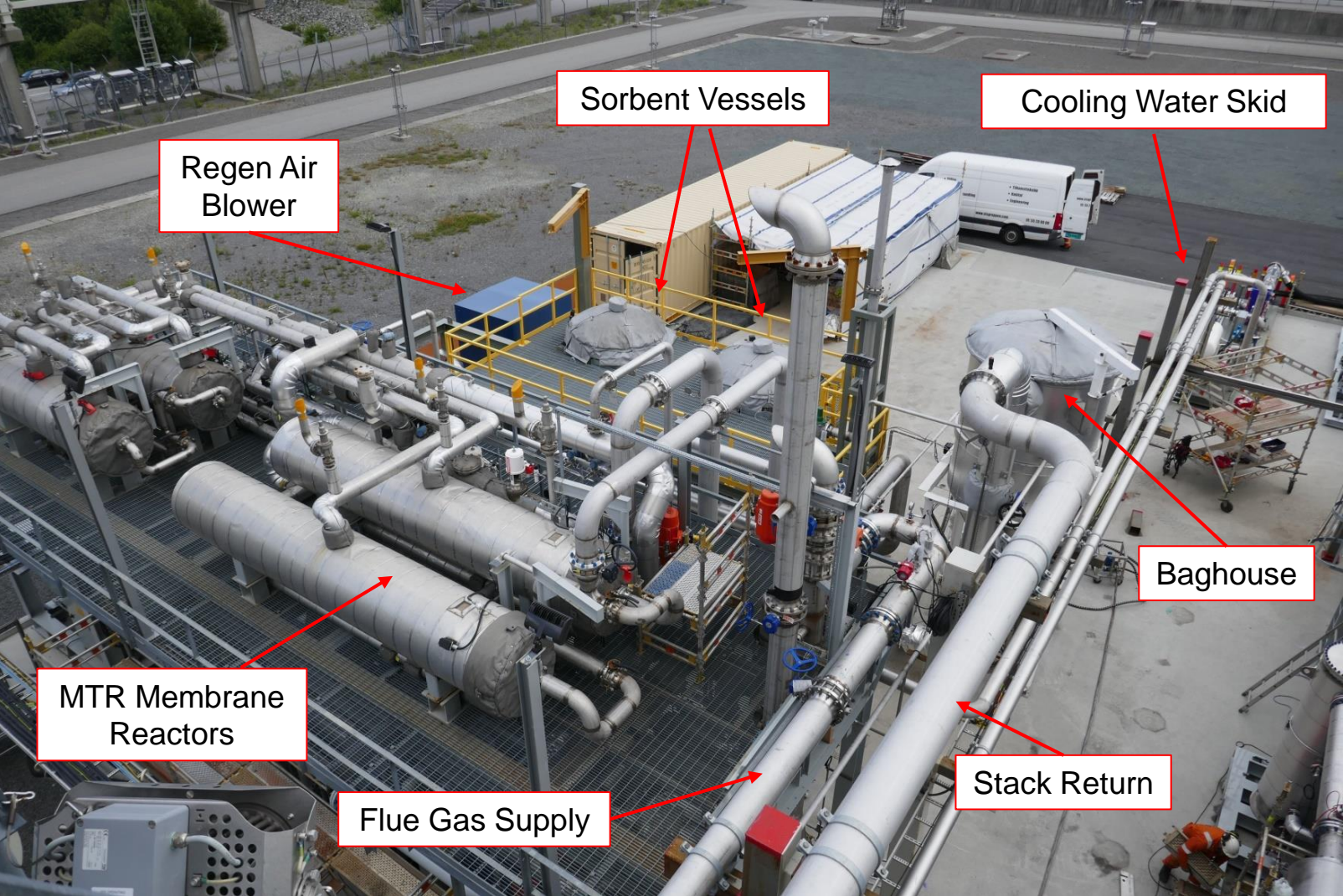
Existing MTR Membrane Module



TCM Mongstad, Norway

- ✓ **Demonstrate sorbent performance**
 - ✓ CO₂ removal efficiency
 - ✓ CO₂ uptake capacity
- ✓ **Demonstrate the mechanical stability of the sorbent**
- ✓ **Demonstrate sorbent life**
- ✓ **Demonstrate effective operation of the radial flow reactors**
 - ✓ Low pressure drop and modular operation
 - Uniform flow distribution
- ✓ **Development/Validation of Design Models (CFD and Adsorption Models)**
- ✓ **Cycle optimization**
- ✓ **Optimization of the Hybrid System Operation**

Hybrid Membrane System Overview



Sorbent Vessels

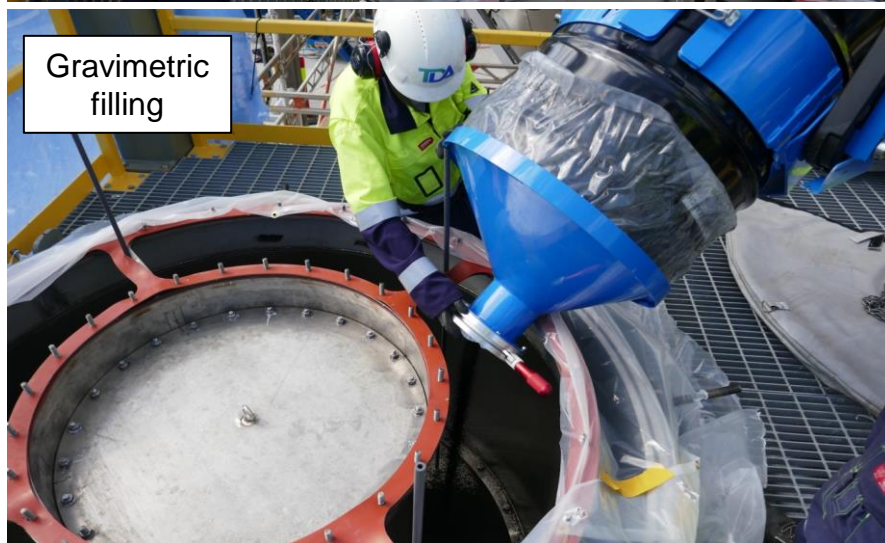


Baghouse

Sorbent Vessel #1

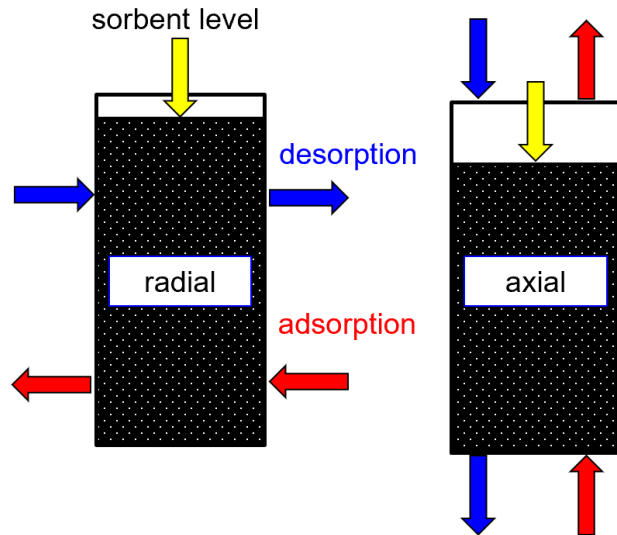
Sorbent Vessel #2

Sorbent Loading into the Vessels



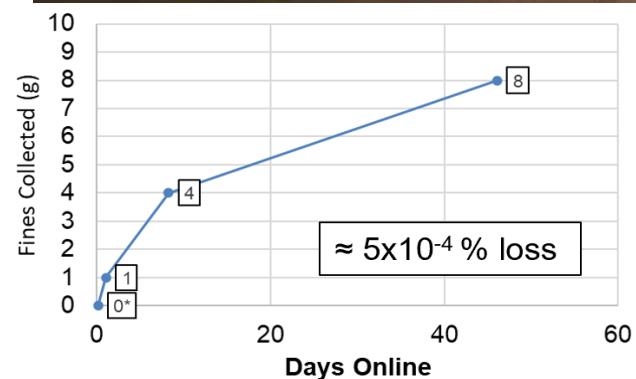
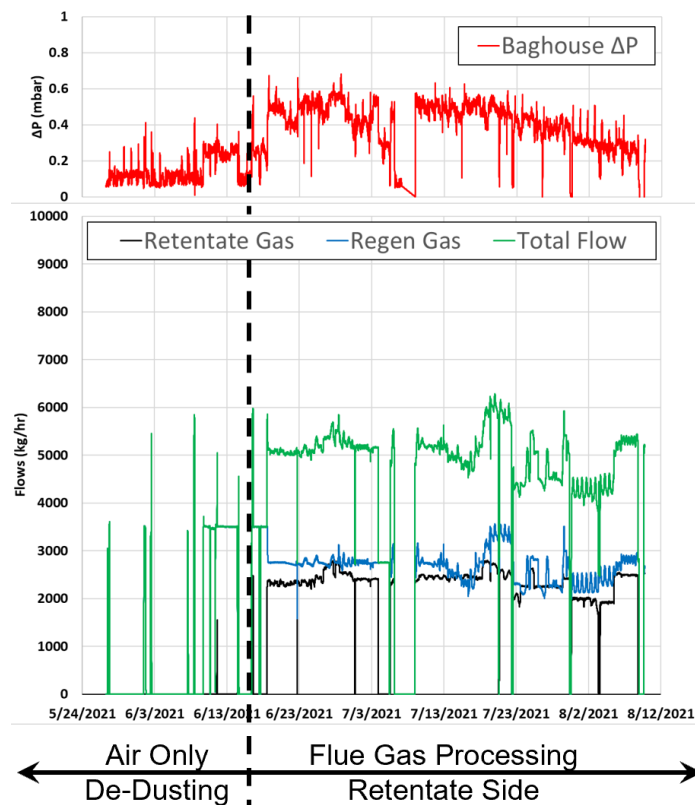
Sorbent Settling and Retainment

- Sorbent settling is not desirable as it generates a void at the top of the bed and cause flow by-pass
- System internals and loading procedures ensured effective pre-settlement
- Top of the sorbent bed is sealed with custom gaskets
- After a short run, the beds were topped off (<2% of total sorbent mass)



- Amount of dust generated was surprisingly low (much lower than we observed in axial beds)
- Sorbent retention was excellent; total fines collected in the baghouse over the first month of operation was $\leq 0.0006\%$ wt. of the initial load

Measurement of Sorbent Dusting



- **Baghouse pressure drop was low and stable over time; consistent with a low rate of fines collection**
- **Total volume of dust collected in baghouse to date is ≈ 8 g; very low in comparison to the sorbent inventory of ≈ 1.7 tonne**
The collected particulate also included fabrication debris

Field Test Summary

Time online (taking flue gas):

- 4,001 hours[†] (≈ 167 days)
- Availability 80.5%

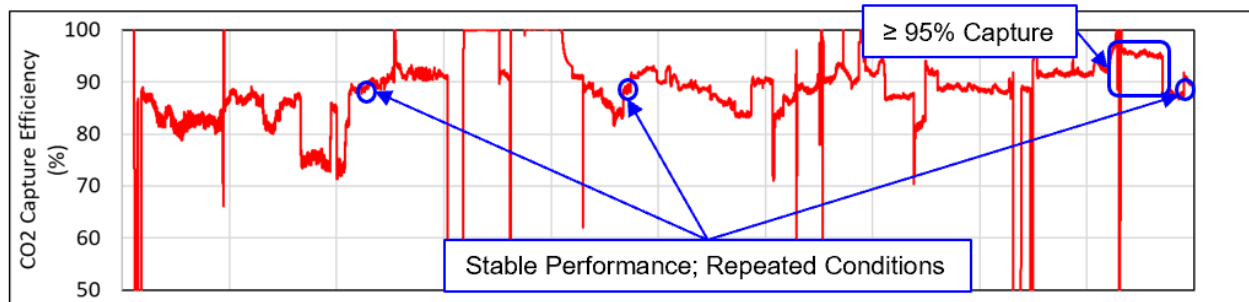
RFCC flue gas CO₂:

- 1,889 tonne received[†]
- 1,645 tonne captured
- 87.1% net capture efficiency (w/ upsets)
- 161,182 sorbent cycles

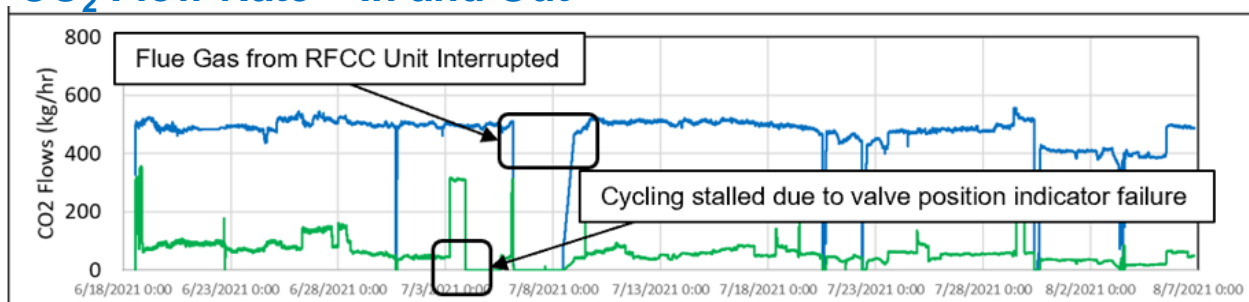
CO₂ Capture Breakdown

| | < 90% | > 90% | > 95% |
|---------------------|-------|-------|-------|
| hours | 2,212 | 1,789 | 307 |
| days | 92 | 75 | 13 |
| Percent of run time | 55.3% | 44.7% | 7.7% |

CO₂ Capture Efficiency

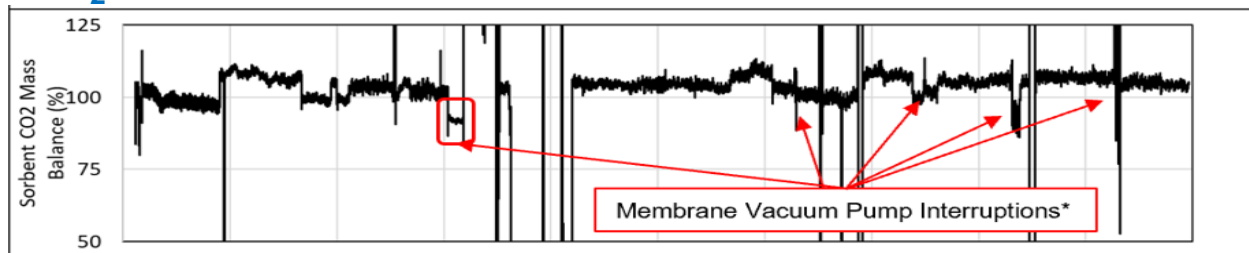


CO₂ Flow Rate – In and Out



* - Membrane vacuum pump interruptions increase CO₂ load to the sorbent sub-system by 50–100%

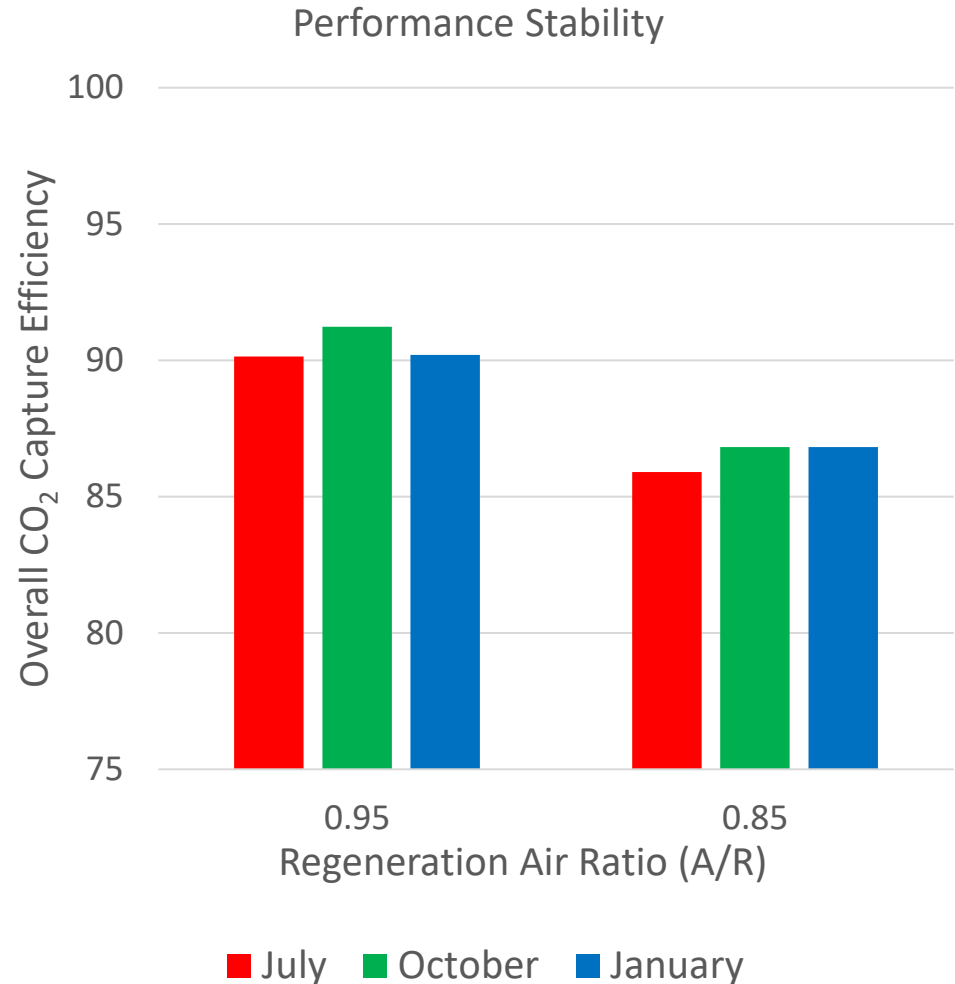
CO₂ Mass Balance



† - includes 70 hours (≈3 days) and 7.2 tonne of CO₂ from CHP flue gas testing at the end of the campaign

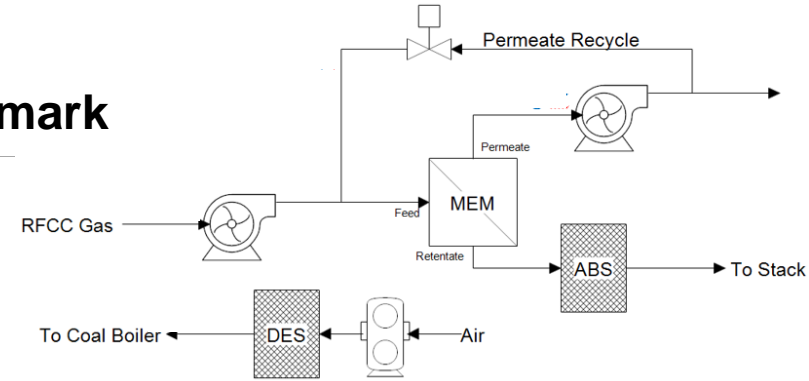
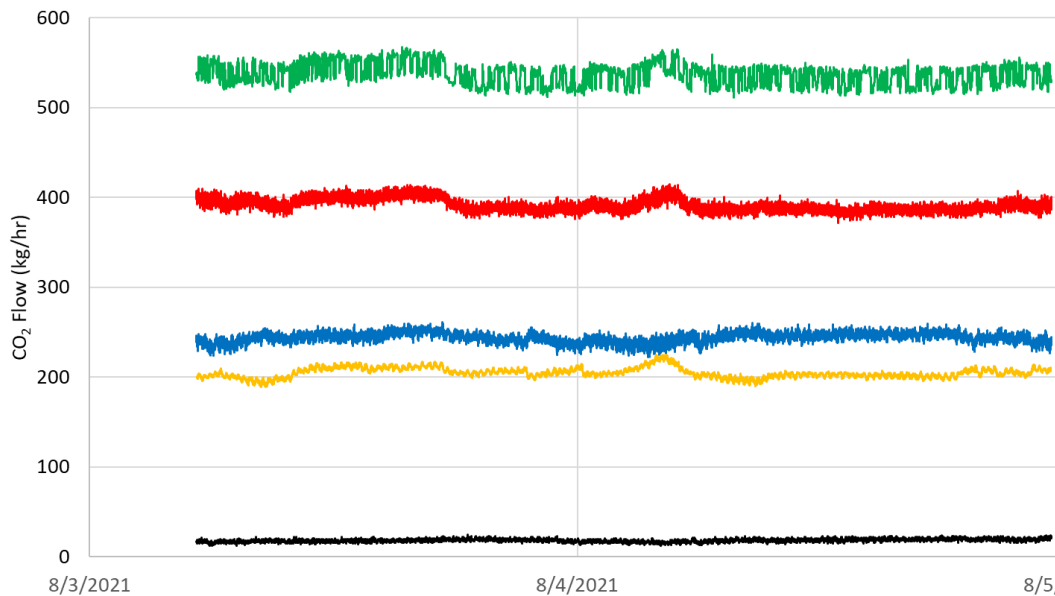
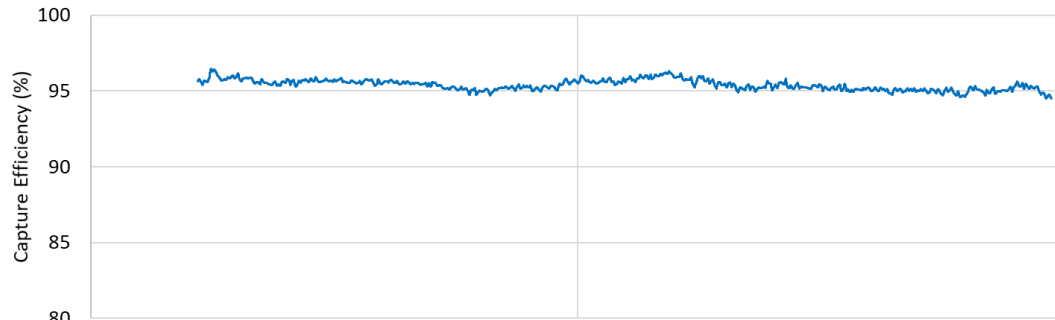
Performance Stability

- **Performance stability is checked periodically under several baseline conditions**
 - Overall CO₂ capture efficiency of the system was measured over a range of regeneration air/retentate flow (A/R) ratios
 - The chart compares two A/R ratios in three different months (summer/fall/winter) during the test program
- **No measurable change in system performance was observed through eight months of testing**



High CO₂ Capture Efficiency (≥95%)

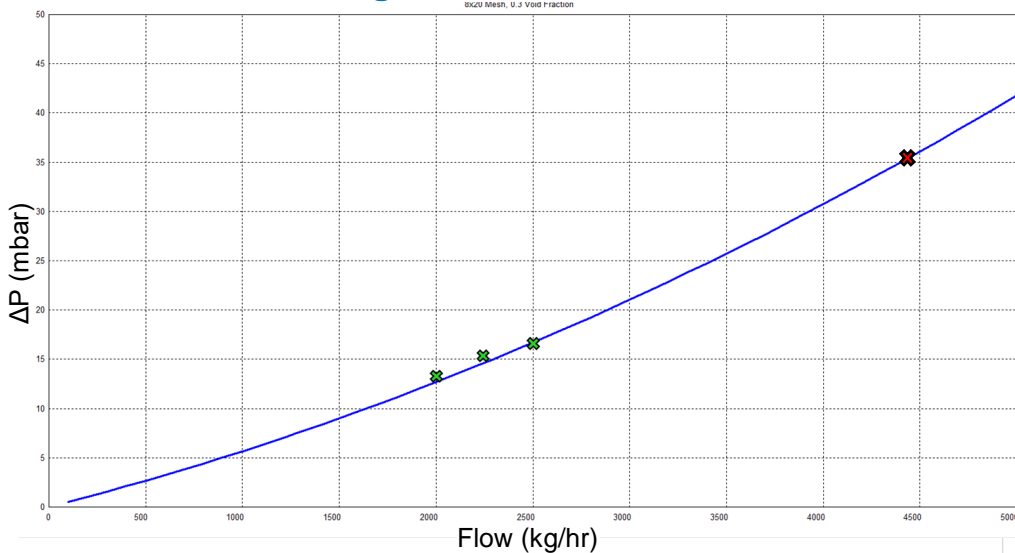
- **95% CO₂ removal efficiency was demonstrated in several 48-hour tests**
- **Data below are from 38 days total run time mark**



- ← Membrane Feed (includes recycled permeate)
- ← Flue Gas Inlet (Hybrid System Inlet)
- ← Retentate (Sorbent Inlet)
- ← Permeate Product (excludes recycled CO₂)
- ← CO₂ Slip (stack)

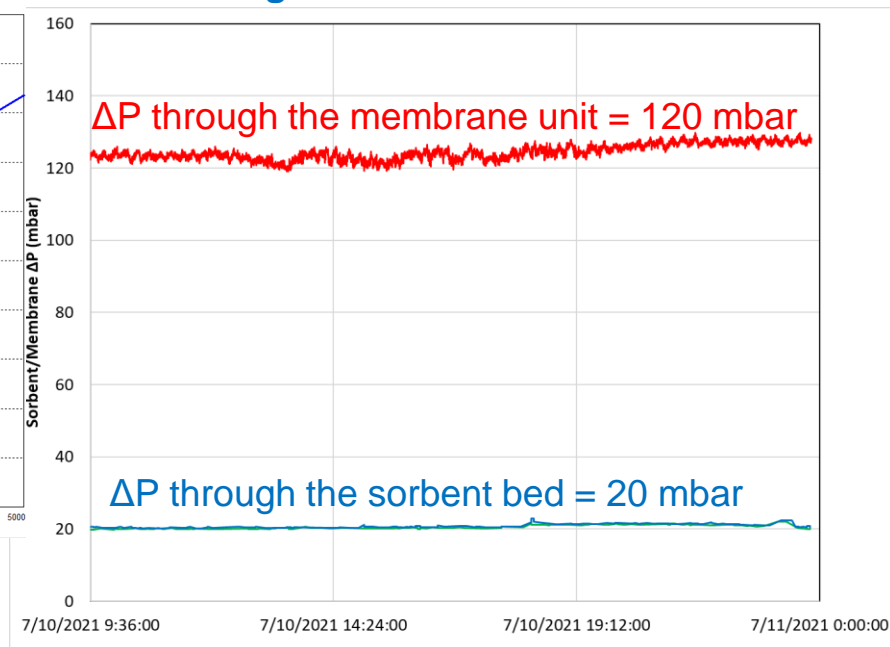
Pressure Drop Measurements

ΔP through the Bed vs. Flow Rate



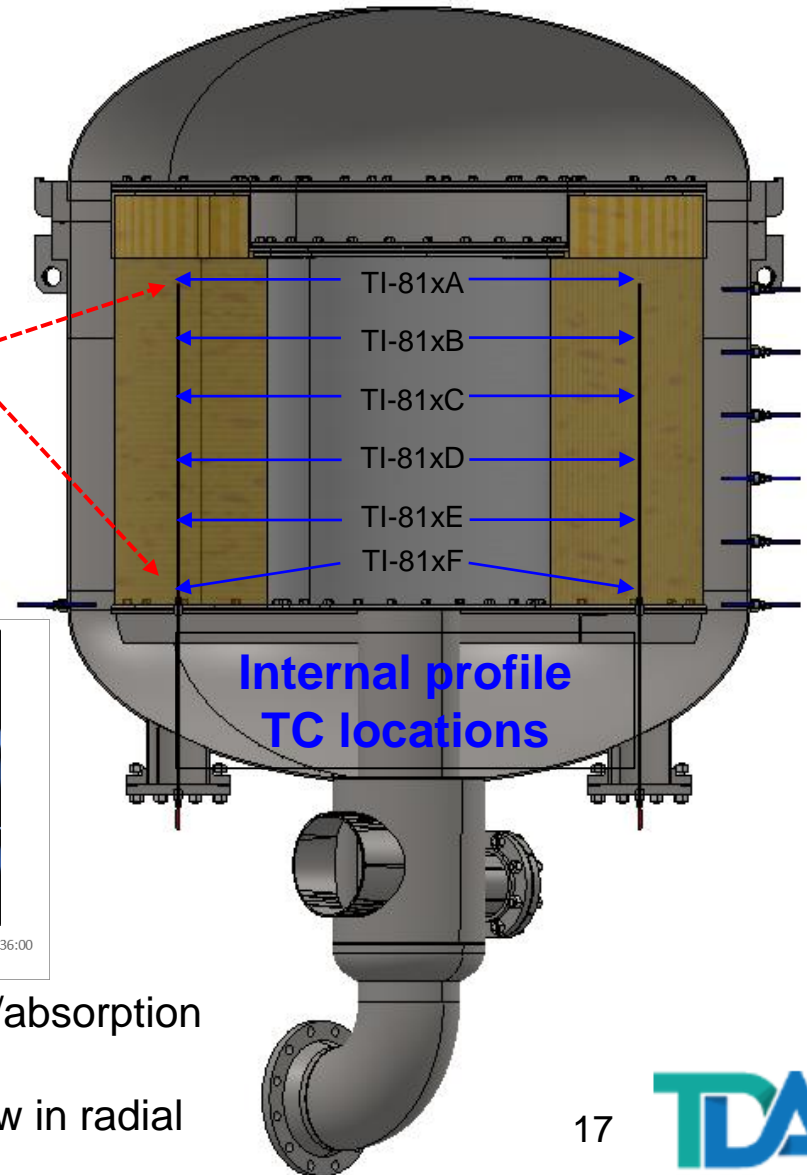
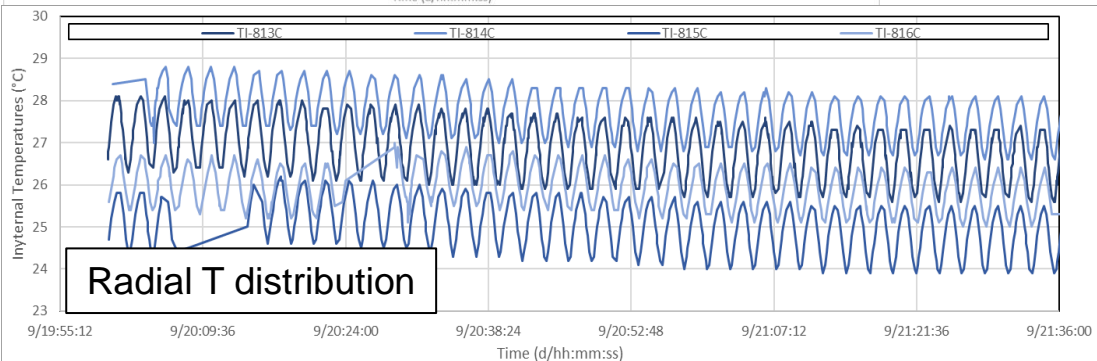
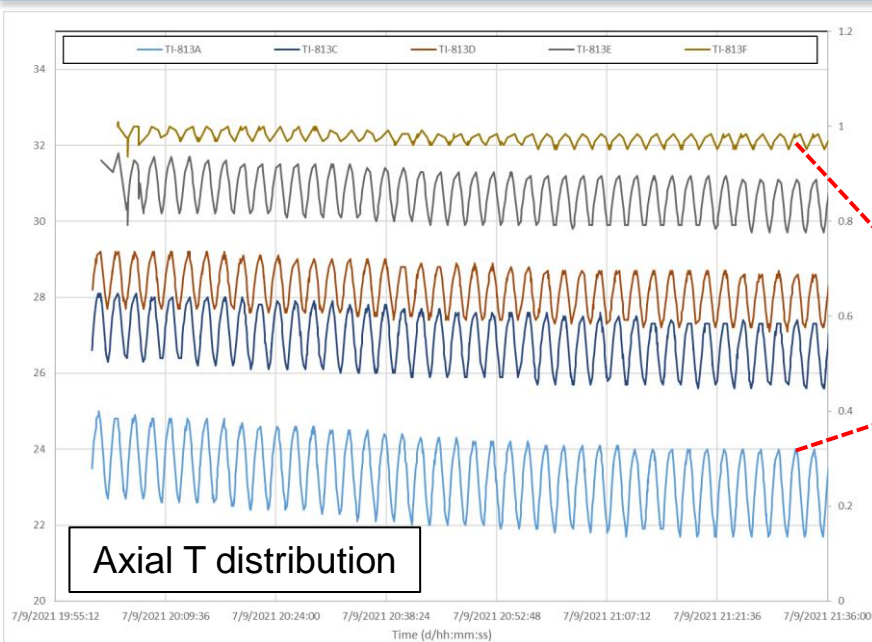
- ✕ Experimental pressure drop vs. flow data from TCM
- ✕ Highest possible flow through the system

ΔP through the membrane and sorbent



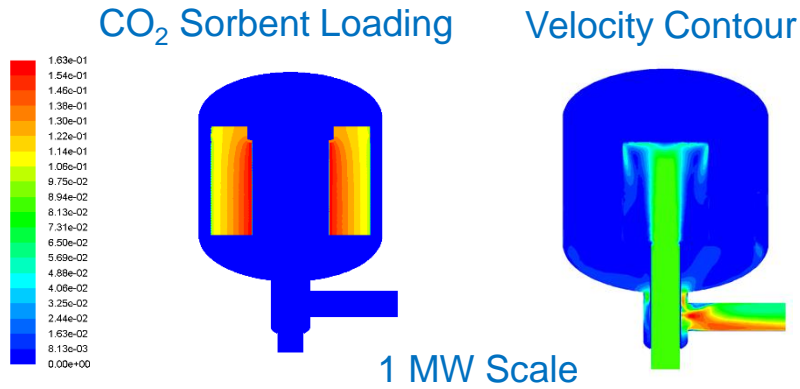
- TDA's radial sorbent bed design achieved a very low pressure drop
- At the 2000–2500 kg/hr flue gas flow, the total ΔP was measured as <20 mbar
- Actual measured ΔP s agree well with the model results
- The membrane unit treating the same flue gas flow and rejecting the same amount CO_2 generated ≈ 120 mbar pressure drop (Stage 1 membrane)

Temperature Distribution in the Bed

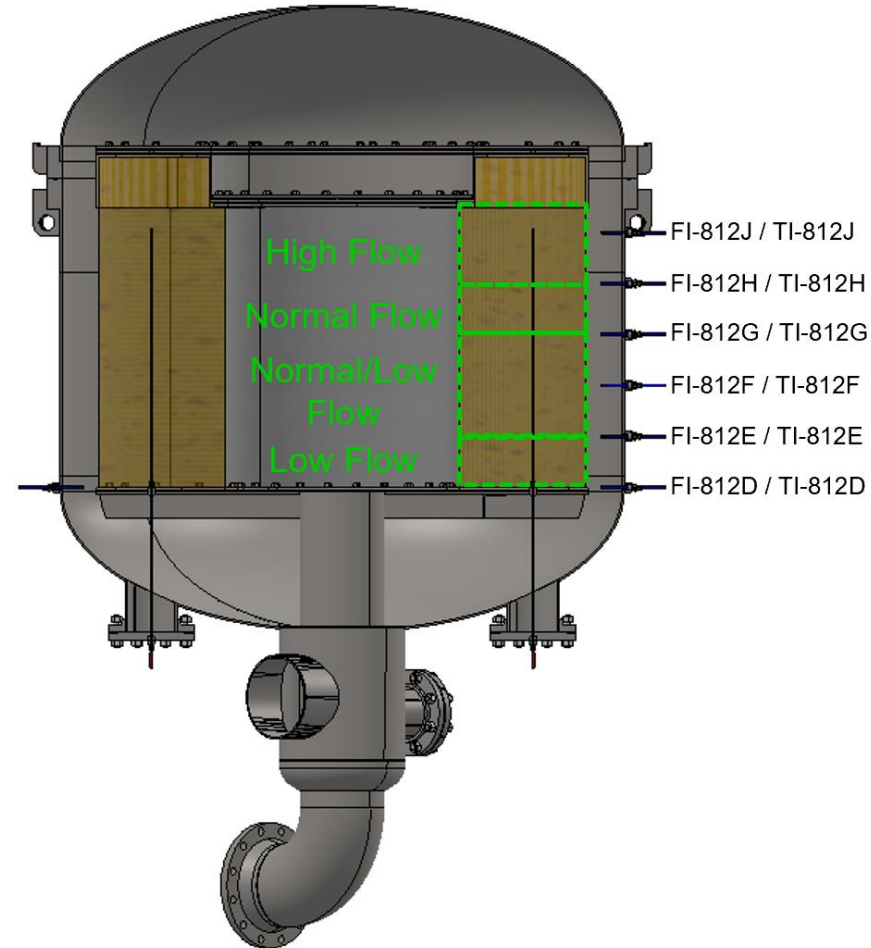
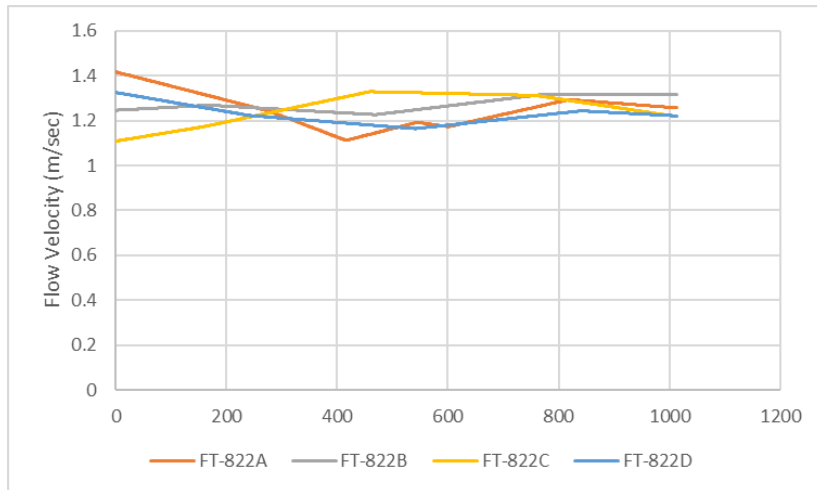


- Axial T distribution/cyclic ΔT indicates higher flows/absorption near the top
- Radial T distribution/cyclic ΔT indicates uniform flow in radial direction

Flow Distribution in the Bed



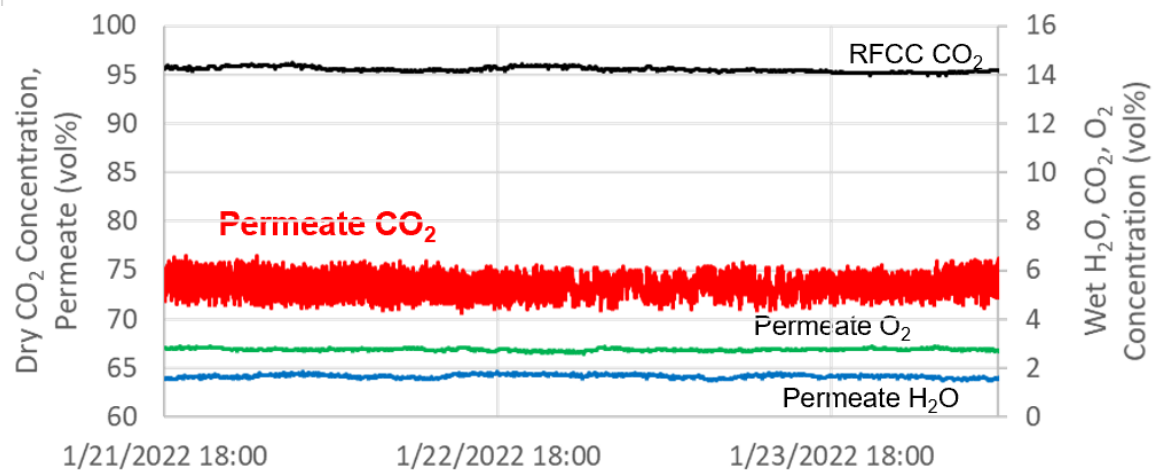
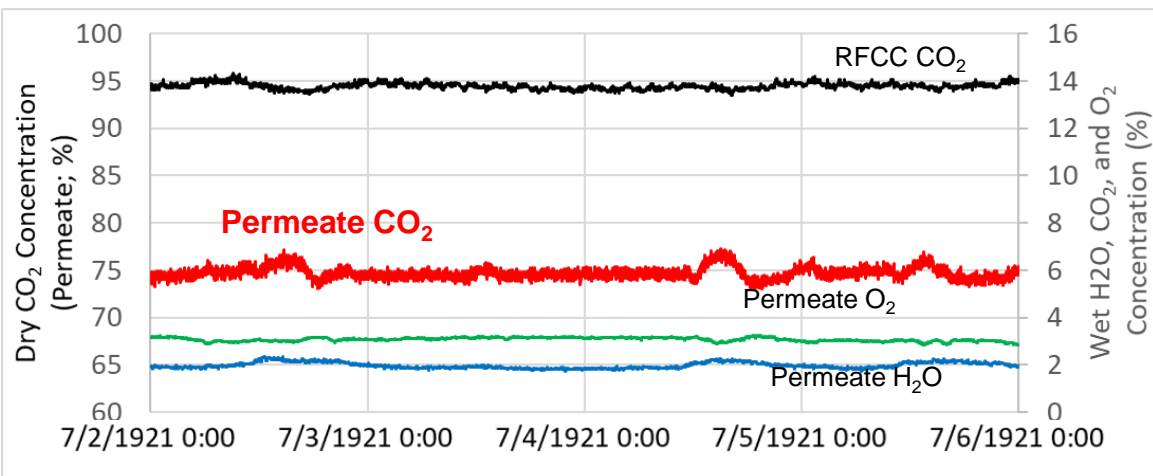
Radial Flow Distribution (Measured)



- Radial flow velocity measurements show uniformity within $\pm 2\%$
- Axial flow velocity measurements indicate a flow imbalance towards top of the bed

Membrane Performance

- Hybrid system was fitted with MTR's Gen-1 Polaris membranes
- Stable performance with $\approx 78\text{--}80\%$ vol. CO_2 purity (dry basis)



Membrane modules being loaded with new membranes prior to shipment

Reactor Vessel Design

Sorbent System - Hybrid

| | Stage I | Stage II |
|-------|---------|----------|
| Bed 1 | | |
| Bed 2 | | |
| 60s | 30s | 30s |

Adsorption - Flue gas flow

Desorption - Air Purge flow

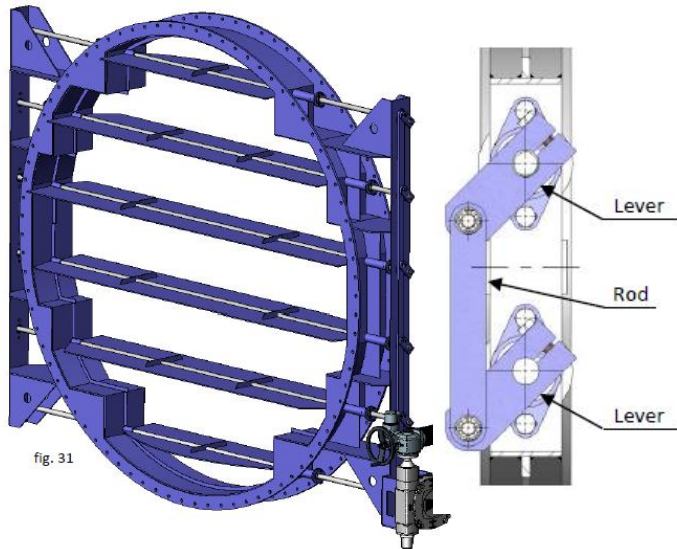
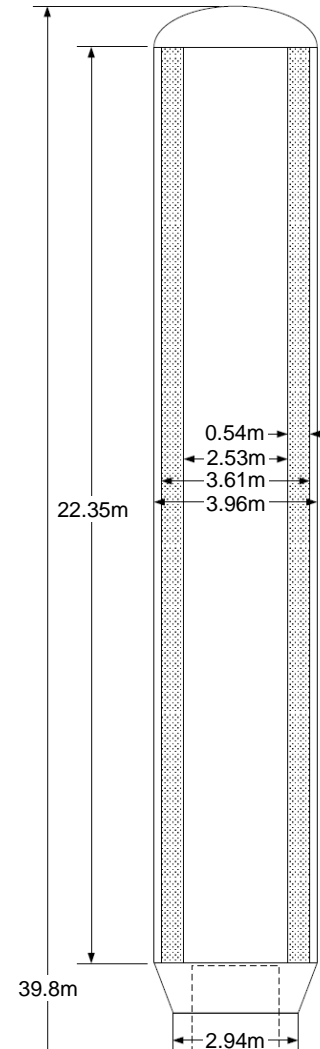


fig. 31

$\Delta P=50$ mbar

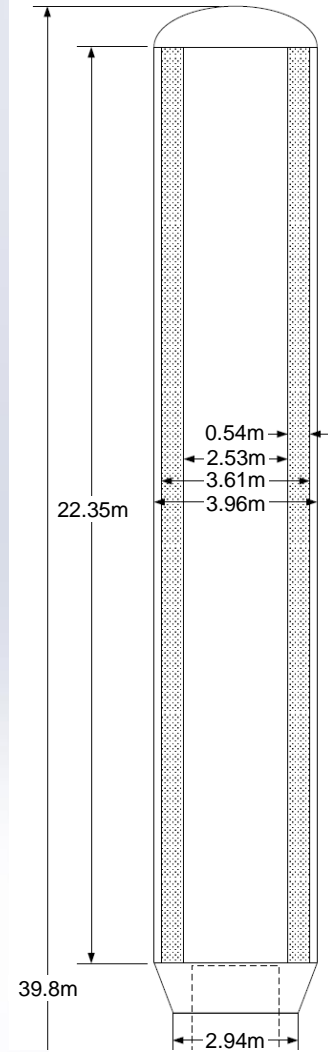
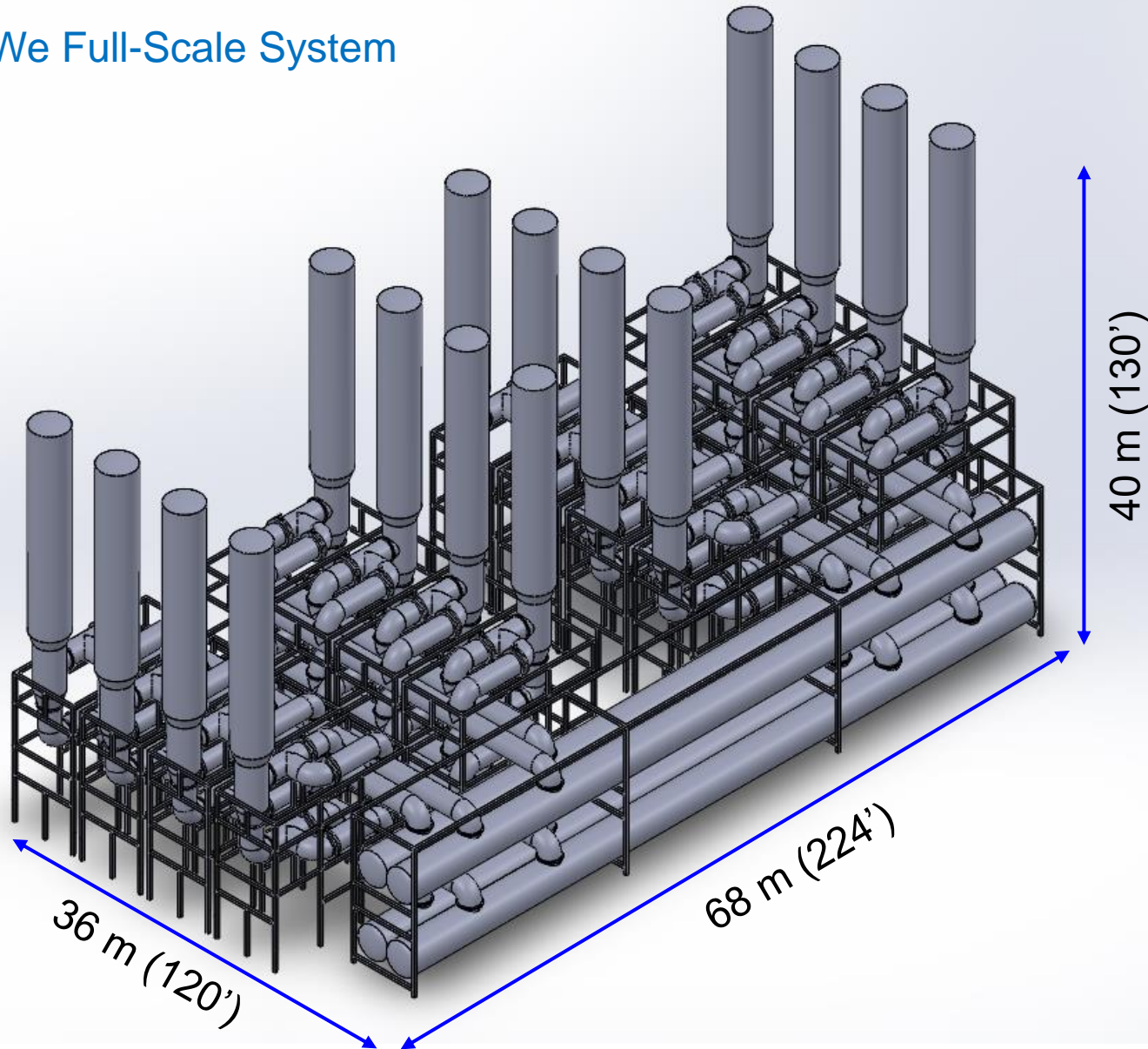
| | |
|-----------------------|---------------------------|
| Module Size: | 68.75 MW |
| No. of Trains: | 8 |
| Beds/Train: | 2 |
| Total Beds: | 16 |
| Flue Gas Flow: | 74.5 m ³ /s |
| CO ₂ Flow: | 1.22 tonne/min |
| Capacity: | 1.8% Wt. |
| Cycle Time: | 1 min |
| Sorbent Inventory: | 67.8 tonne/m ³ |
| Sorbent Density: | 0.59 tonne/m ³ |
| Bed Volume: | 116.4 m ³ |
| Bed Area: | 12.3 m ² |

- Sixteen (16) radial beds
- SA516-70 carbon steel;
0.5" thickness
- 13 ft OD x 73¹/₃ ft T/T

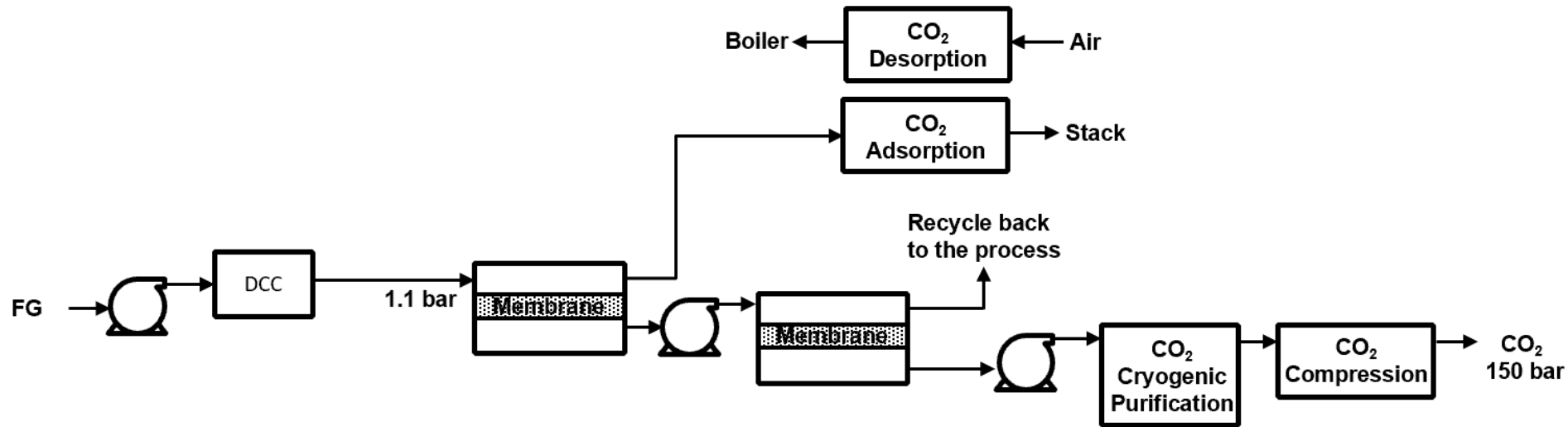


3-D Layout of the Hybrid Sorbent System

550 MWe Full-Scale System



Baseline Hybrid Process PFD



- A two-stage membrane process is utilized to recover the CO₂ at the desired purity
- A cryogenic purification system is used to ensure that the O₂ (<10 ppm) and other impurity levels in the CO₂ meets pipeline specifications
- In addition to the baseline study, other cases were also studied including one which does not require re-circulation of the CO₂ into the boiler

Final TEA - Rev. 4 \$2018 Basis

| Capture Technology | No Capture | Amine | Membrane-Sorbent Hybrid BP3 | Membrane-Sorbent Hybrid Retrofit |
|---|-------------|----------------|-----------------------------|----------------------------------|
| Case Studies | B12A | B12B | Baseline Case | No re-circ to boiler |
| Gross Power, MWe | 685 | 770 | 905 | 902 |
| CO ₂ Capture/Removal, MWe | - | 30 | 129 | 126 |
| CO ₂ Purification, MWe | - | - | 23 | 23 |
| CO ₂ Compression, MWe | - | 44 | 56 | 55 |
| Balance of Plant, MWe | 35 | 46 | 47 | 48 |
| Total Auxiliaries, MWe | 35 | 120 | 255 | 252 |
| Net Power, MWe | 650 | 650 | 650 | 650 |
| Net Plant Efficiency, % HHV | 40.3 | 31.5 | 30.0 | 30.6 |
| Carbon Capture, % | 0 | 90 | 90 | 90 |
| Coal Feed Rate, kg/h | 214,112 | 273,628 | 287,191 | 281,990 |
| Carbon Capture System (CCS) CAPEX \$1,000s | - | 738,606 | 351,305 | 346,060 |
| FG Cleanup + CCS CAPEX inc. Compression | 120,427 | 970,432 | 506,415 | 537,729 |
| LCOE, \$/MWh | 64.4 | 105.2 | 101.2 | 99.4 |
| LCOE inc. T&S, \$/MWh | | 114.2 | 110.6 | 108.7 |
| Breakeven CO2 Sales Price, \$/tonne | | 45.7 | 39.1 | 38.0 |
| Breakeven CO2 Emissions Penalty, \$/tonne | | 73.5 | 68.5 | 65.4 |

- TDA's membrane sorbent hybrid system has a net plant efficiency of 30.0% compared to and a cost of capture of \$39.1/tonne CO₂
 - 14.4% lower capture cost than the reference amine system on Rev. 4 Basis
- A stand-alone hybrid without any recirculation to the boiler was also simulated
 - \$38/tonne CO₂ capture cost; 16.8% lower than reference amine cost

Acknowledgments

- **DOE/NETL Project Manager, Andy O’Palko**
- **MTR Team, Thomas Hofmann, Jay Kniep, Tim Merkel, Erik Westling**
- **GTI Team, Chuck Shistla**
- **UCI, Ashok Rao**
- **TCM Team, Sundus Akhter, Magnus Aronsson, Kjetil Hantveit, Karstein Mangersnes, Blair McMaster, Stein Olav Nesse, Monica Iren Eidsheim Solend, Roger Solheim, Magne Andreas Tresvik**