

Design of a 1 MW Direct Fired Oxy-Fuel Combustor for sCO₂ Power Cycles



SOUTHWEST RESEARCH INSTITUTE



Current Agenda:

- **Project Review**
 - Project Goals
 - Test Rig Overview
- **Design Review**
 - Combustor Design - CFD & Analysis Review
 - Light-off Conditions Cycle Modeling
- **Facility Status Update**

Project Objectives & Status

- Design a 1 MW thermal oxy-fuel combustor capable of generating 1200°C outlet temperature
- Manufacture combustor, assemble test loop, and commission oxy-fuel combustor
- Evaluate and characterize combustor performance using temperature, pressure, and optical access for advanced diagnostics
 - Demonstrate closed-loop operability including light-off, combustion stability, and water separation
 - Achieve continuous operation of oxy-combustor design at full-scale pressure and temperature conditions
 - Validate oxy-combustion models for heat transfer, mixing, and critical reactions

COMPLETE

IN PROCESS, 70% COMPLETE
COMPLETION DATE: May 2023

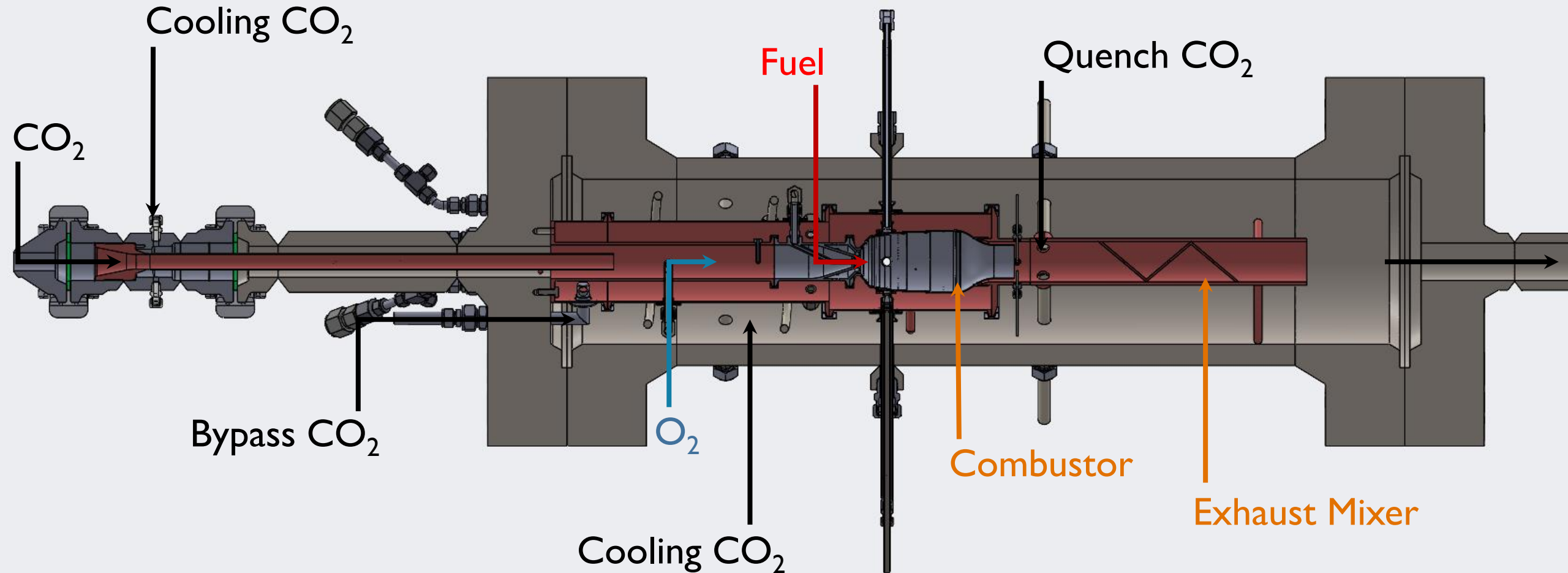
COMPLETION DATE: December 2023

Combustor Test Rig

Overview

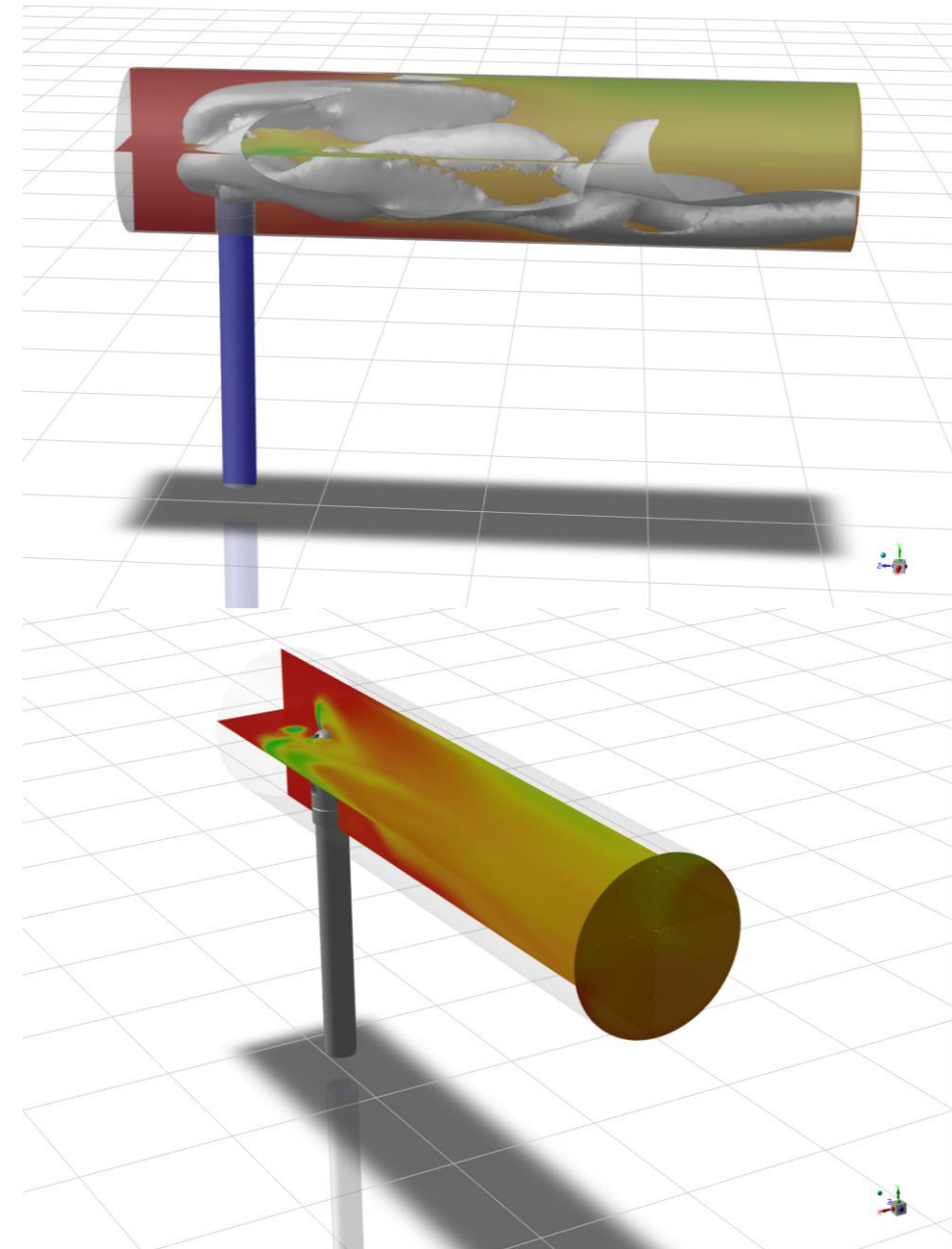
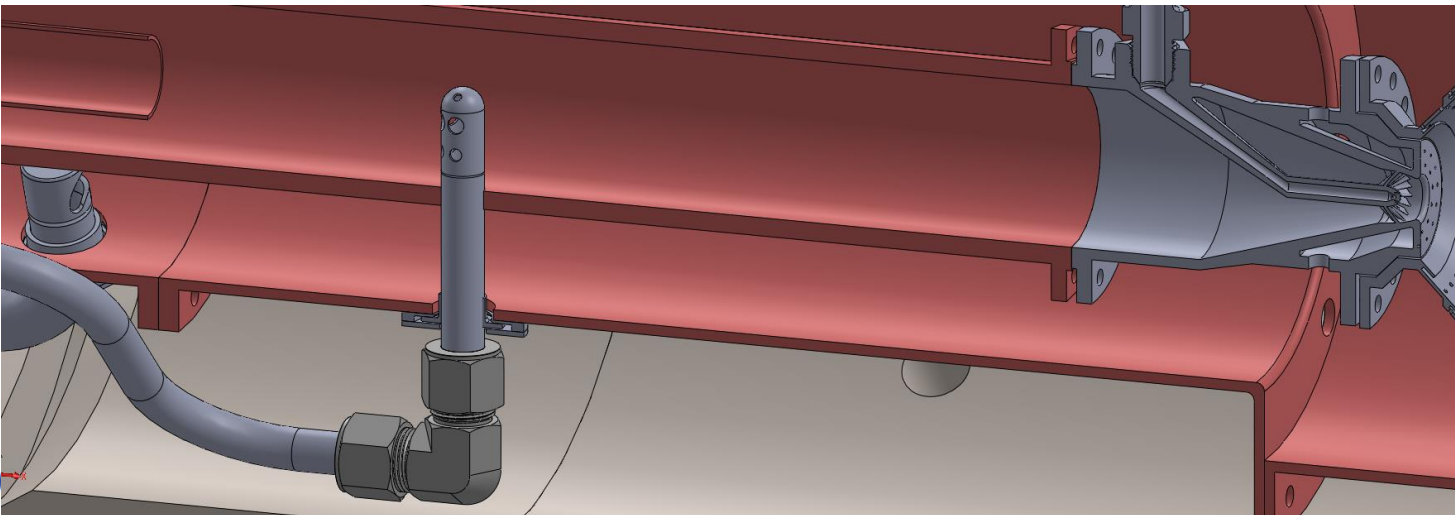


Combustor Schematic

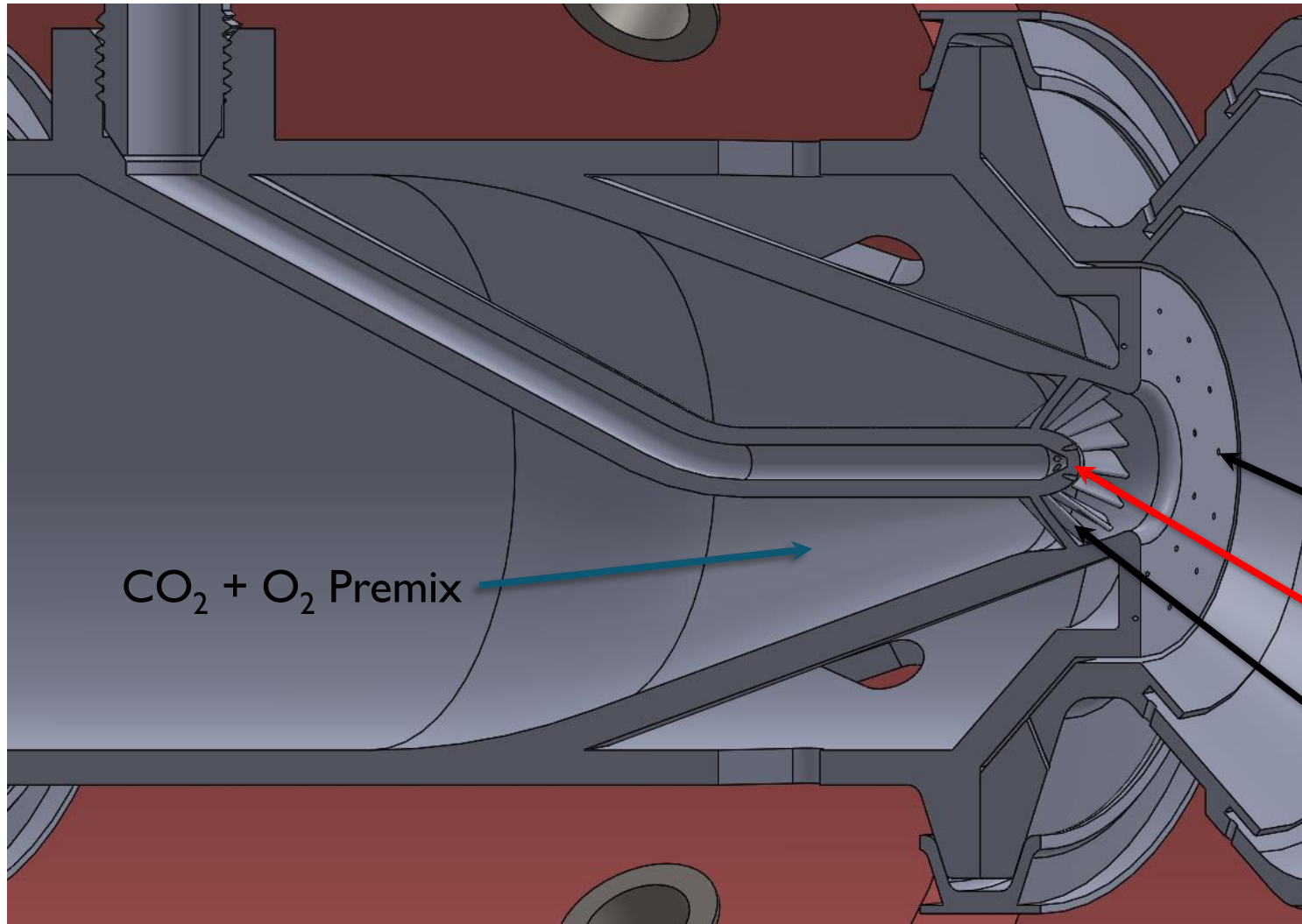


Oxygen System

- Guidance from personnel at NASA Stennis and White Sands, review from project partner Air Liquide
- LOX tank with cryogenic pump and ambient vaporizer
- Oxygen injection upstream of fuel injector



Fuel Injector



- Additively manufactured Haynes 282
- Swirl angle of inlet vanes chosen after literature review and CFD simulations

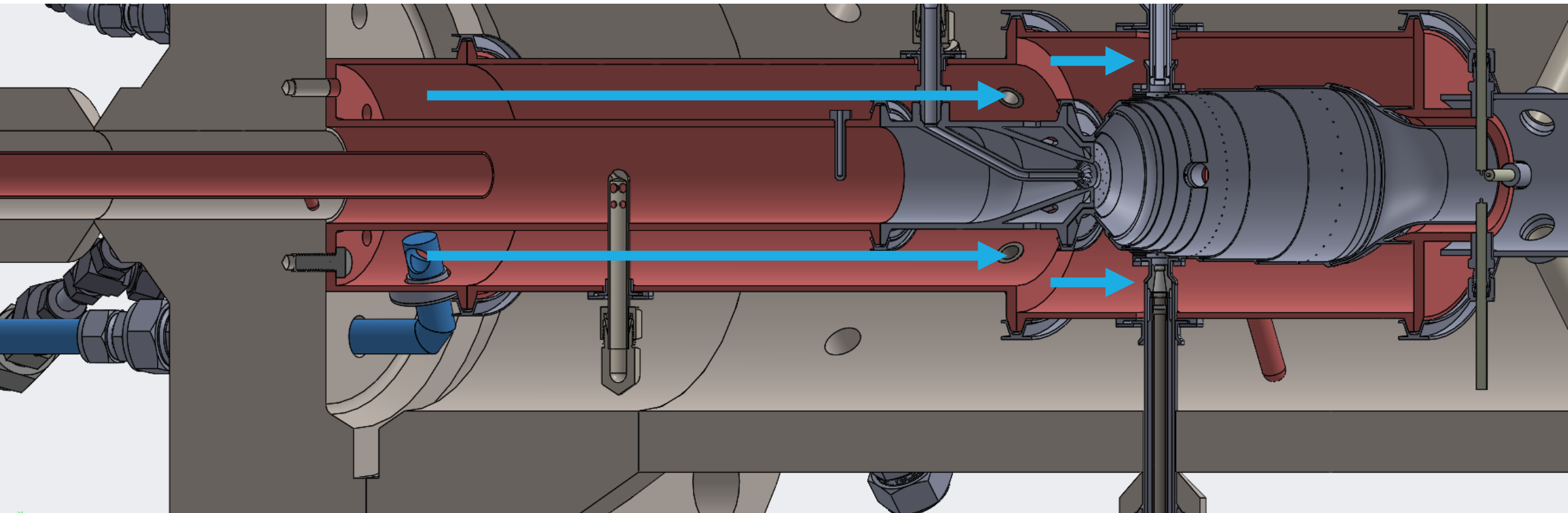
CO₂ Face Cooling

Methane Fuel Injection Point

Swirling Vanes

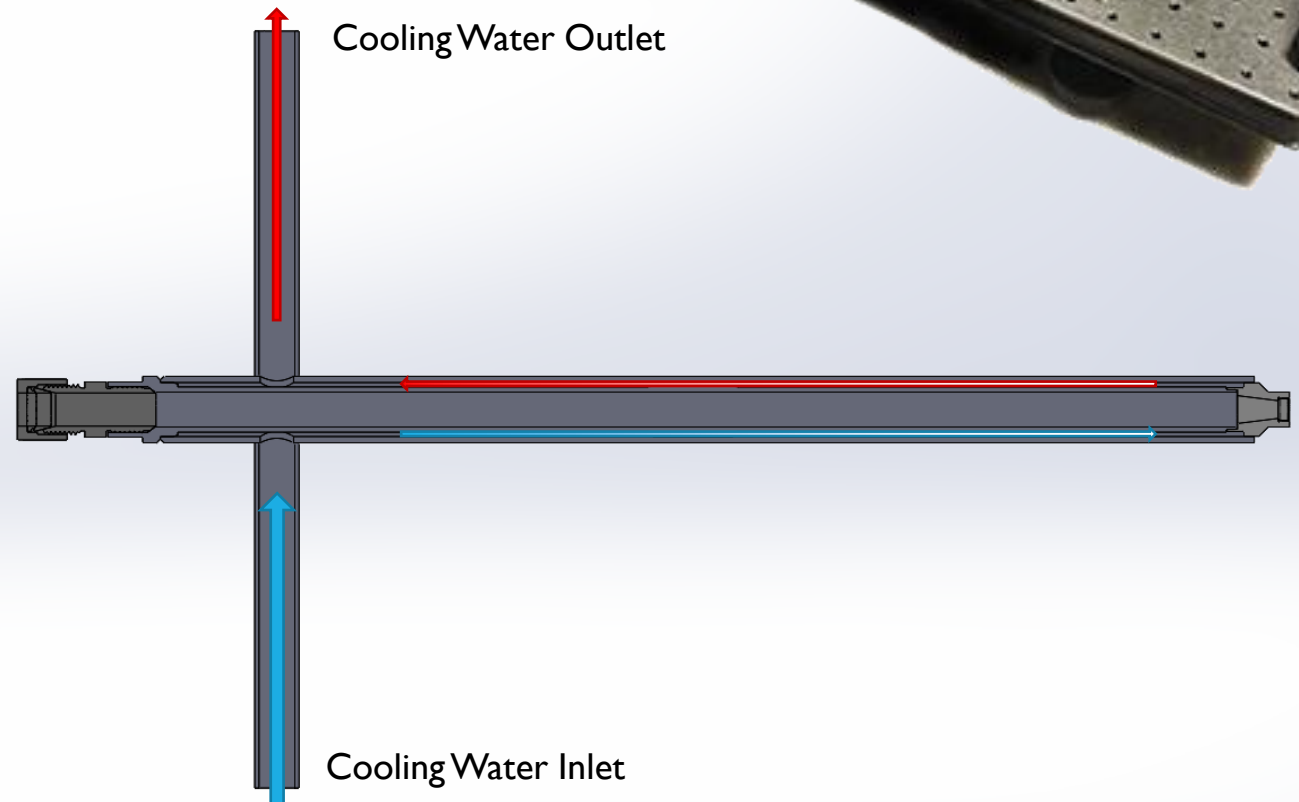
Combustor Cooling

CO₂ bypass gas enters annulus from a dedicated line (highlighted in blue) with flow control, allowing remote manipulation of combustor liner temperatures

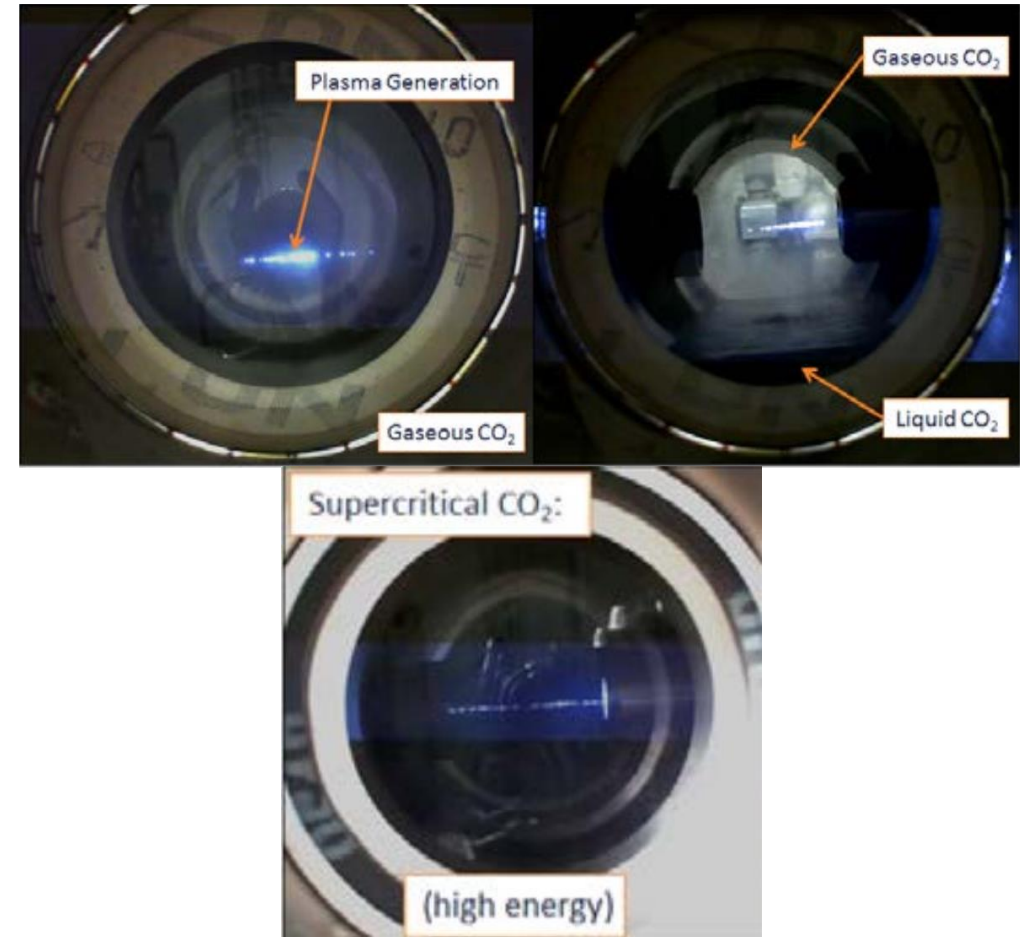
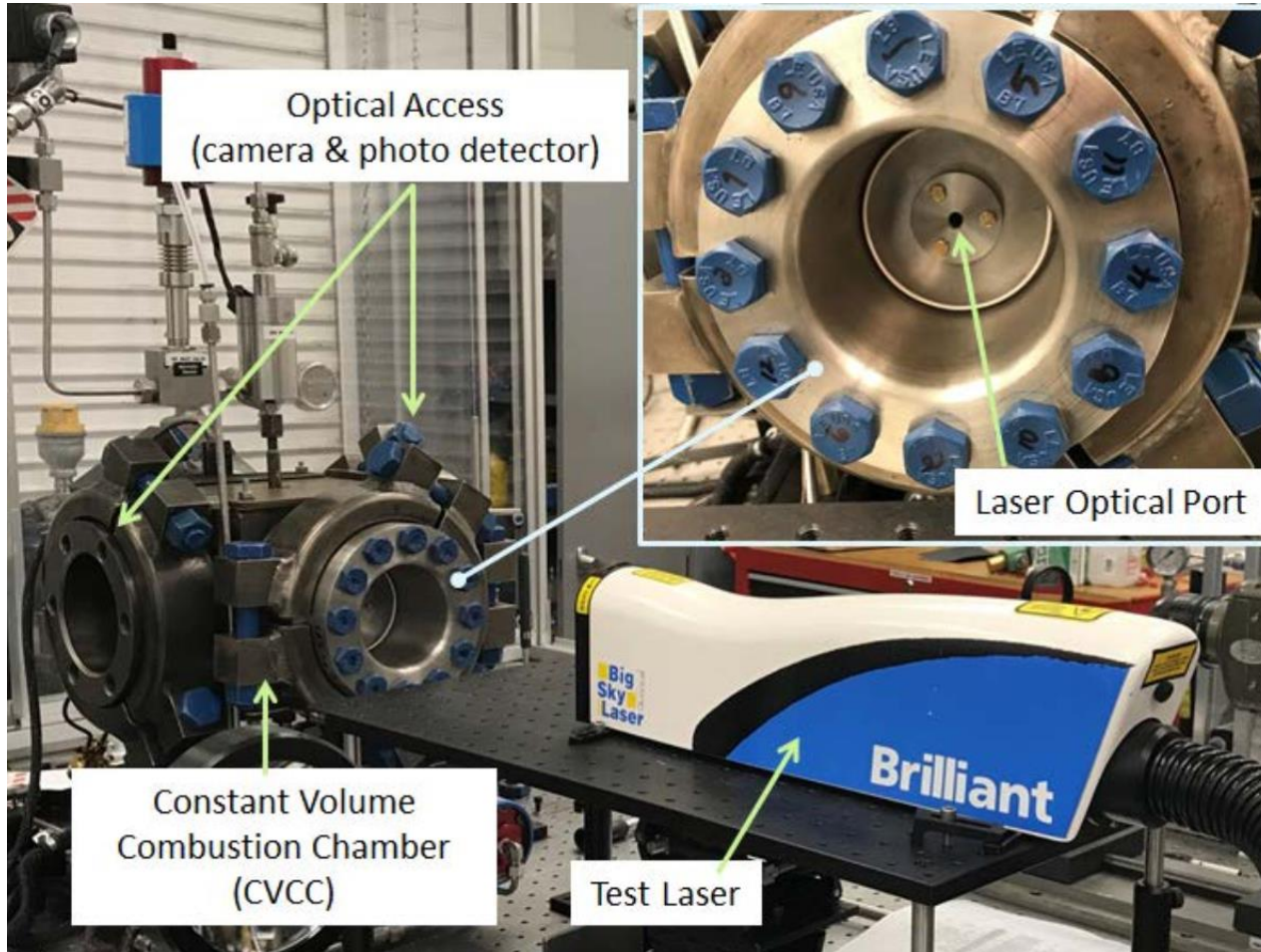


Laser Ignition System

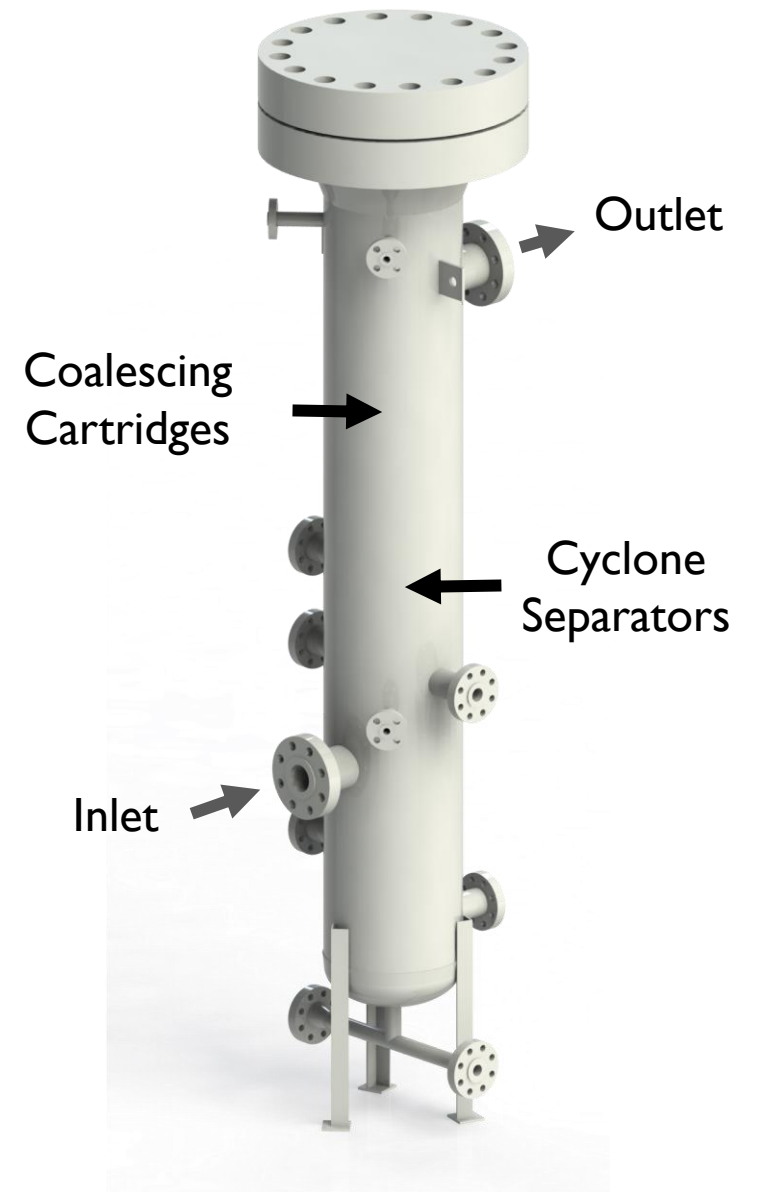
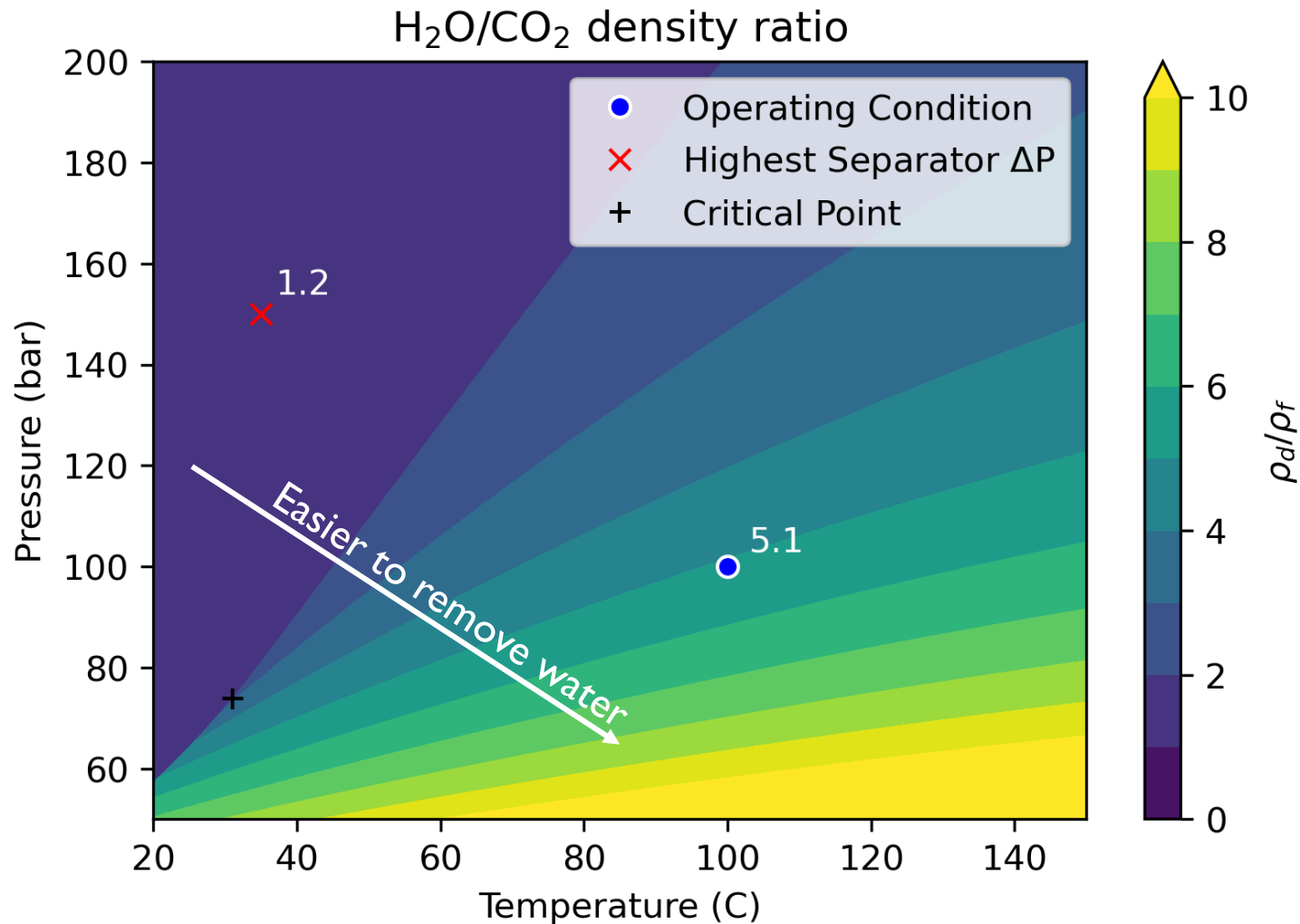
- Class 4 Quantel Qsmart Twins
 - 380mJ @ 532nm, 10Hz
- Water cooled probe allows access to the combustor and keeps focal lens temperature low



Previous Laser Ignition Tests

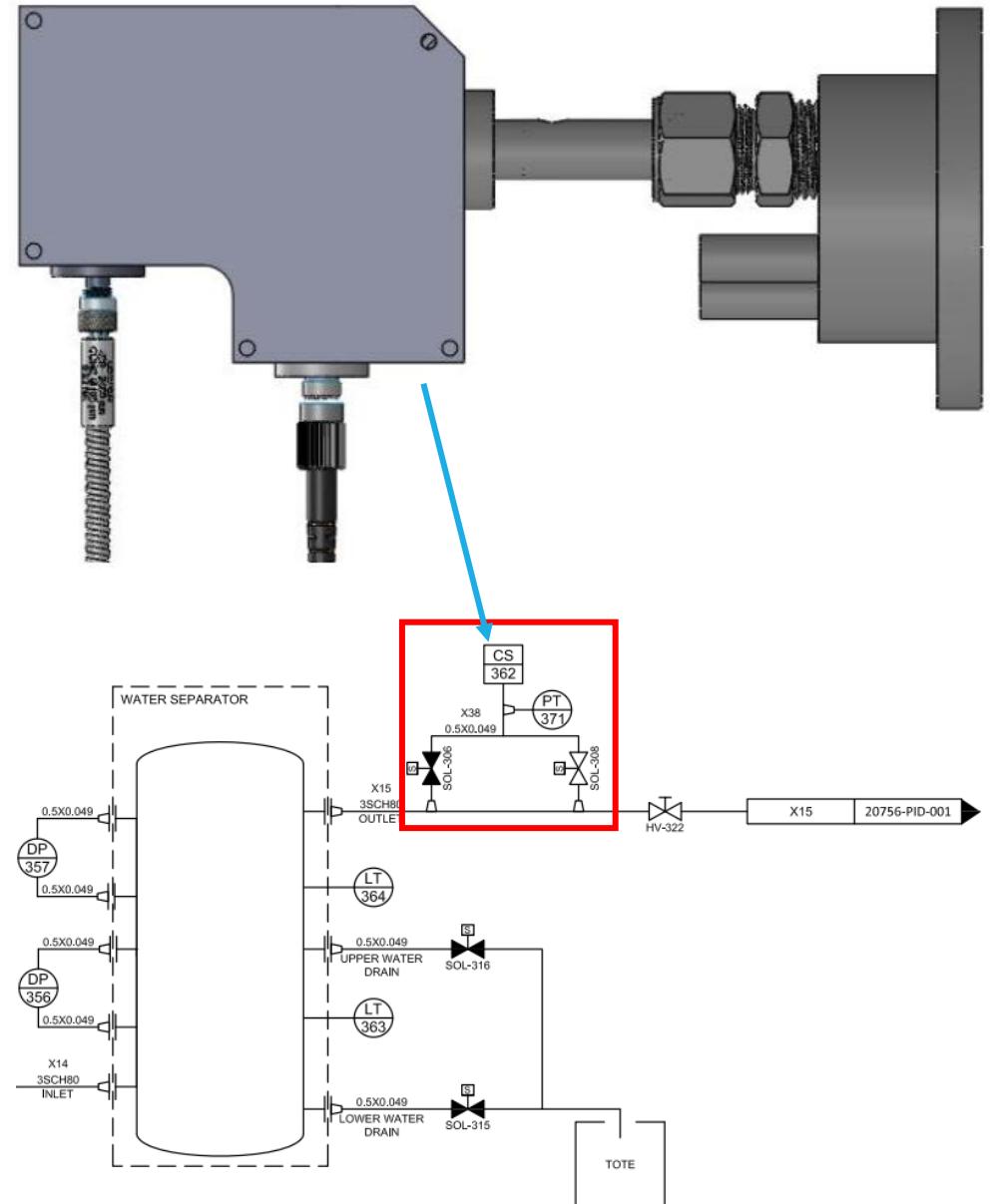


Water Separator



Constituent Sensor

- Working with Sporian Microsystems to develop a constituent sensor to detect H_2O in the test loop using Raman spectroscopy.
- Highly accurate detection of H_2O in flowing sCO_2 confirmed at SwRI testing in March 2022.
- Alternatives exist, including Supercritical Fluid Chromatography (CFS) and Fourier Transfer Infrared (FTIR), and high-pressure oxygen sensors. FTIR is available on-site but limited to low pressure and O_2 .



Combustor Modeling

Design Details



Chemical Kinetics

Georgia Tech and University of Central Florida each created combustion mechanisms for the sCO₂ oxy-combustion system. Georgia Tech’s model was ultimately selected on the balance of speed and accuracy.

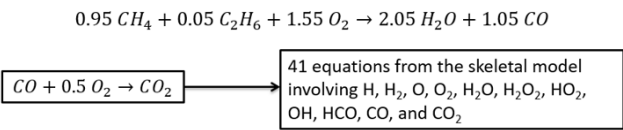


Figure 1-2. The Conversion of the 6-Species Kinetic Model to a 13-Species Kinetic Model

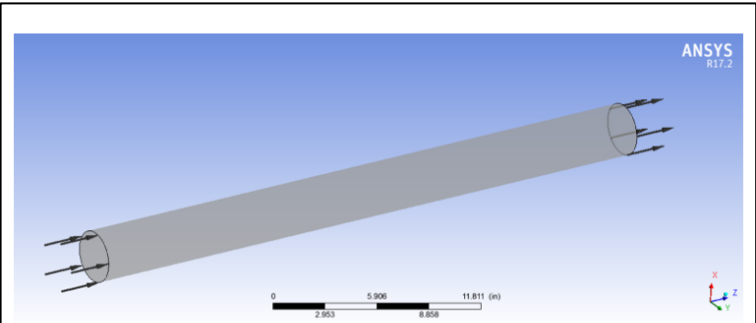


Figure 1-3. Simplified Premixed Reaction Chamber

Table 1-1. Premixed Chamber Inlet Species Mass Fractions

Component	Inlet Mass Fraction
C ₂ H ₆	0.00113
CH ₄	0.01148
O ₂	0.05003
CO ₂	0.93738

Table 1-2. Computational Comparison between the 6-Species and 13-Species Simulations

Elements	Species	Equations	Processors	Time (s)	Time Factor
2.32E+06	6	2	15	3,852	1
2.32E+06	13	42	15	7,675	2.0
1.34E+06	6	2	15	2,081	1
1.34E+06	13	42	15	4,388	2.1

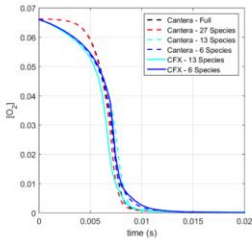


Figure 1-6. Predicted Mole Fraction O₂ Versus Time Results

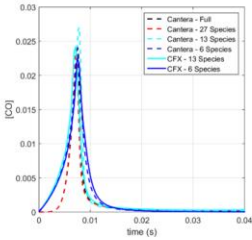


Figure 1-7. Predicted Mole Fraction CO Versus Time Results

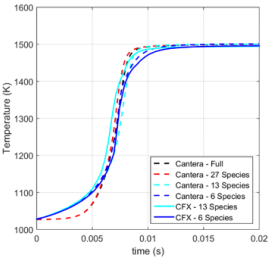


Figure 1-4. Predicted Temperature Versus Time Results

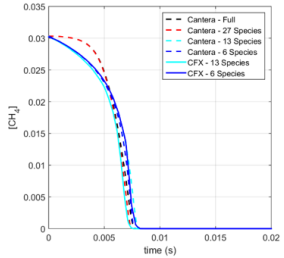


Figure 1-5. Predicted Mole Fraction CH₄ Versus Time Results

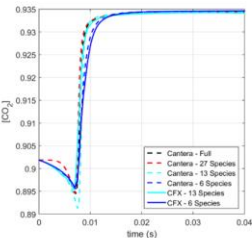


Figure 1-8. Predicted Mole Fraction CO₂ Versus Time Results

Grid Sensitivity

- The chemical kinetic simulations also explored grid dependence.
- A 13 species mechanism was used.
- Grid size requirements are dependent in part on turbulence models.
- Additional grid refinement was performed when switching from steady to unsteady flow simulations.

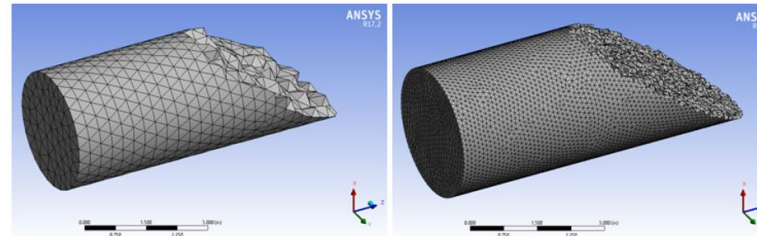


Figure 1-9. Examples of Coarse (left) and Fine (right) Meshing Results for Premixed Chamber

Table 1-3. Mesh Statistics for Premixed Chamber

Elements	Element Multiplication Factor
0.05E+06	1.0
0.40E+06	8.0
0.85E+06	17.0
1.30E+06	26.0
2.30E+06	46.0
1.34E+06	26.8
6.17E+06	122.0

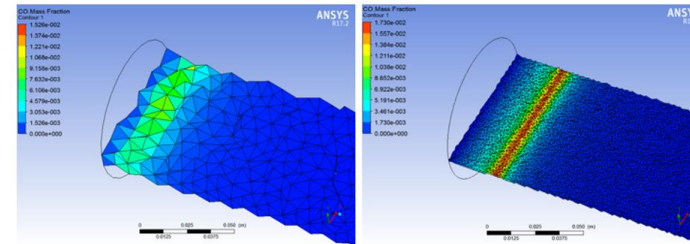


Figure 1-13. CO Mass Fractions Contoured to Show the Grid Resolution of the Combustion Reaction. Coarse Grid (left) and Fine Grid (right)

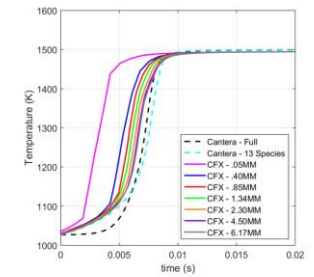


Figure 1-10. Predicted Temperature Versus Time Results for Various Resolutions

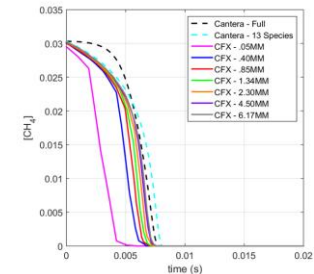


Figure 1-11. Predicted Mole Fraction of CH₄ Versus Time Results for Various Resolutions

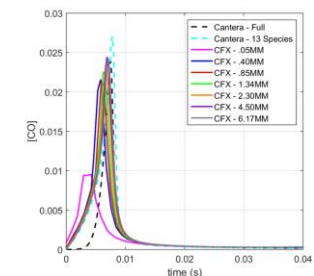
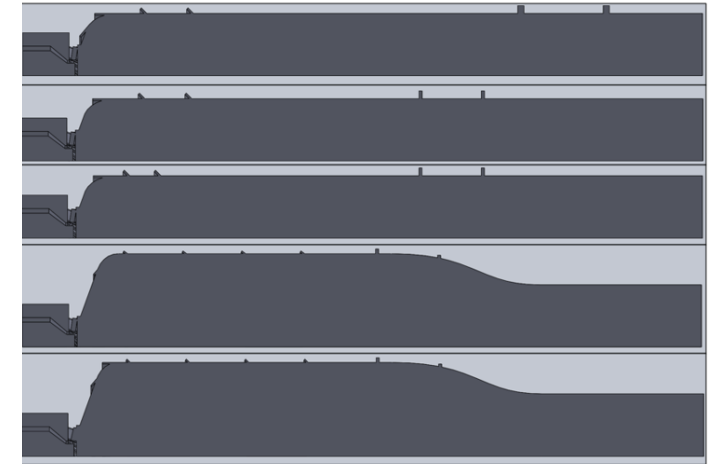
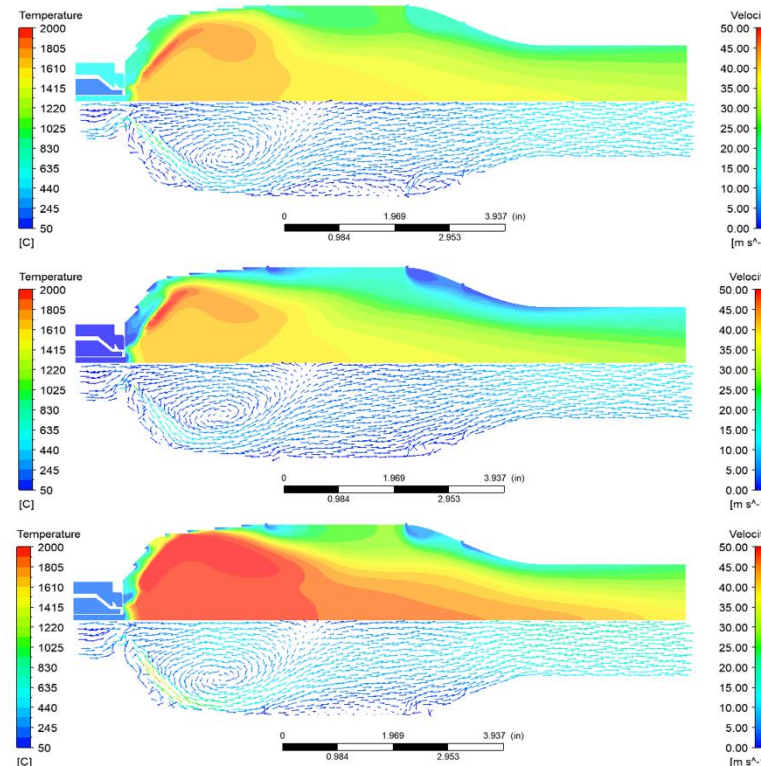
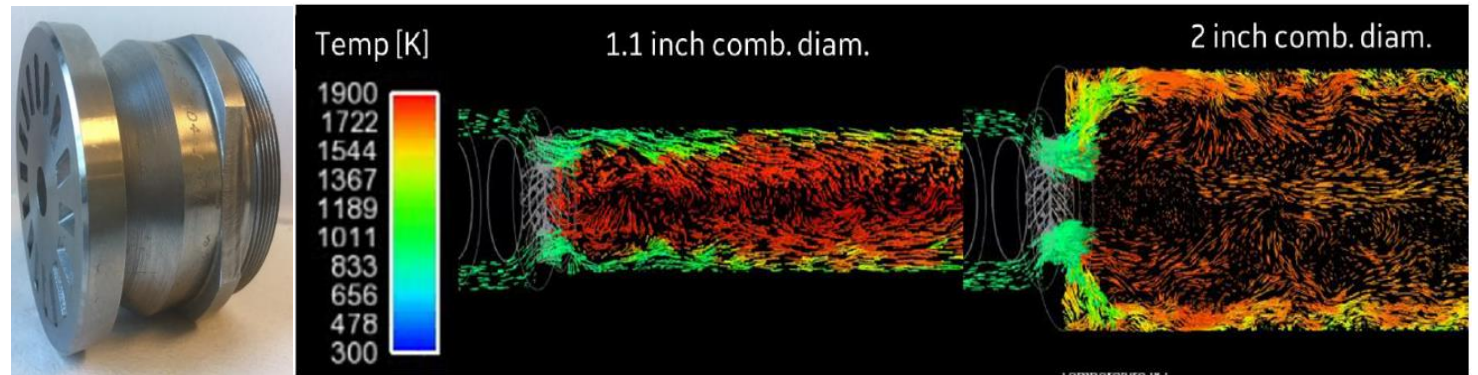


Figure 1-12. Predicted Mole Fraction of CO Versus Time Results for Various Resolutions

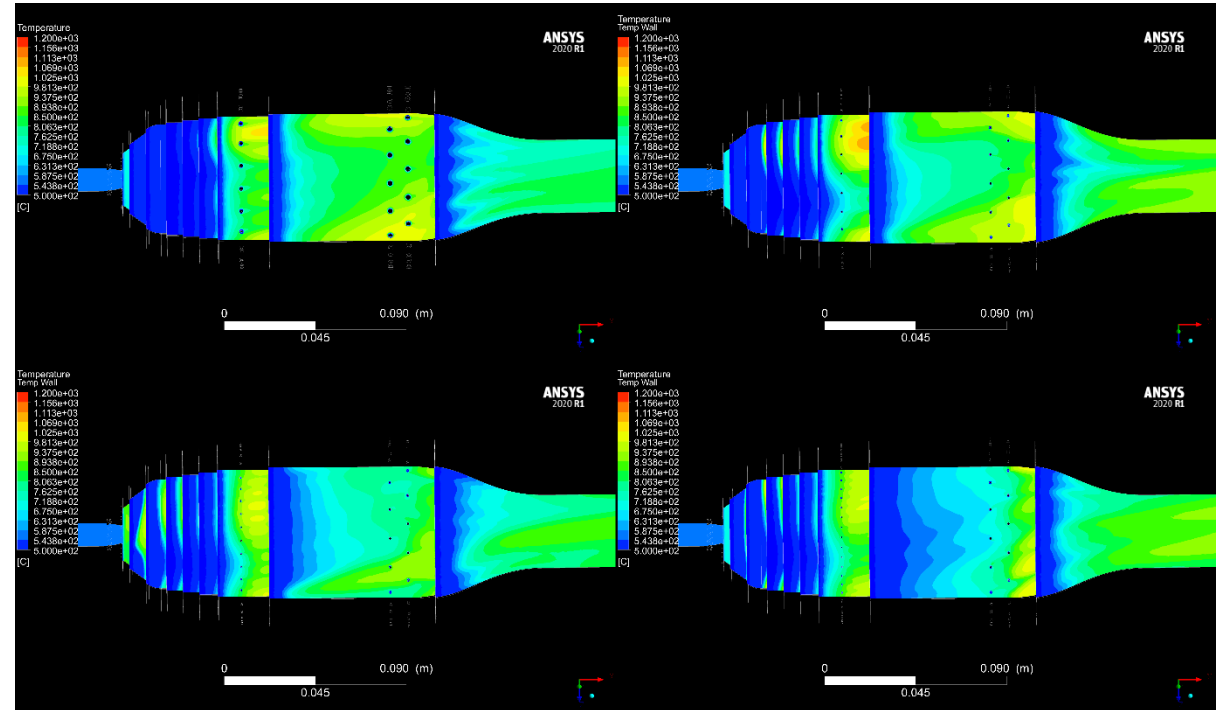
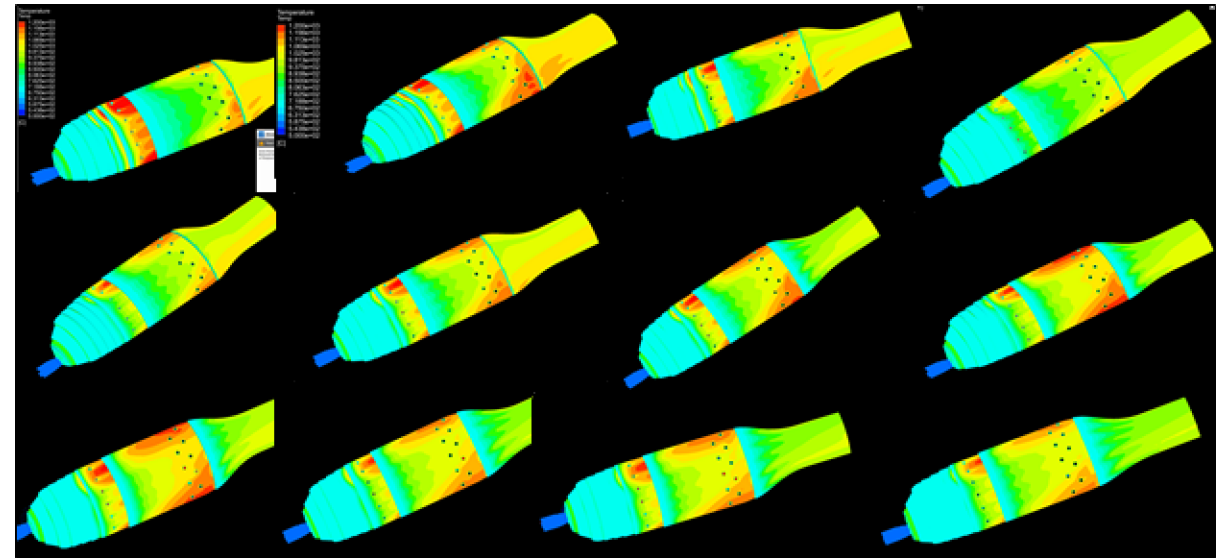
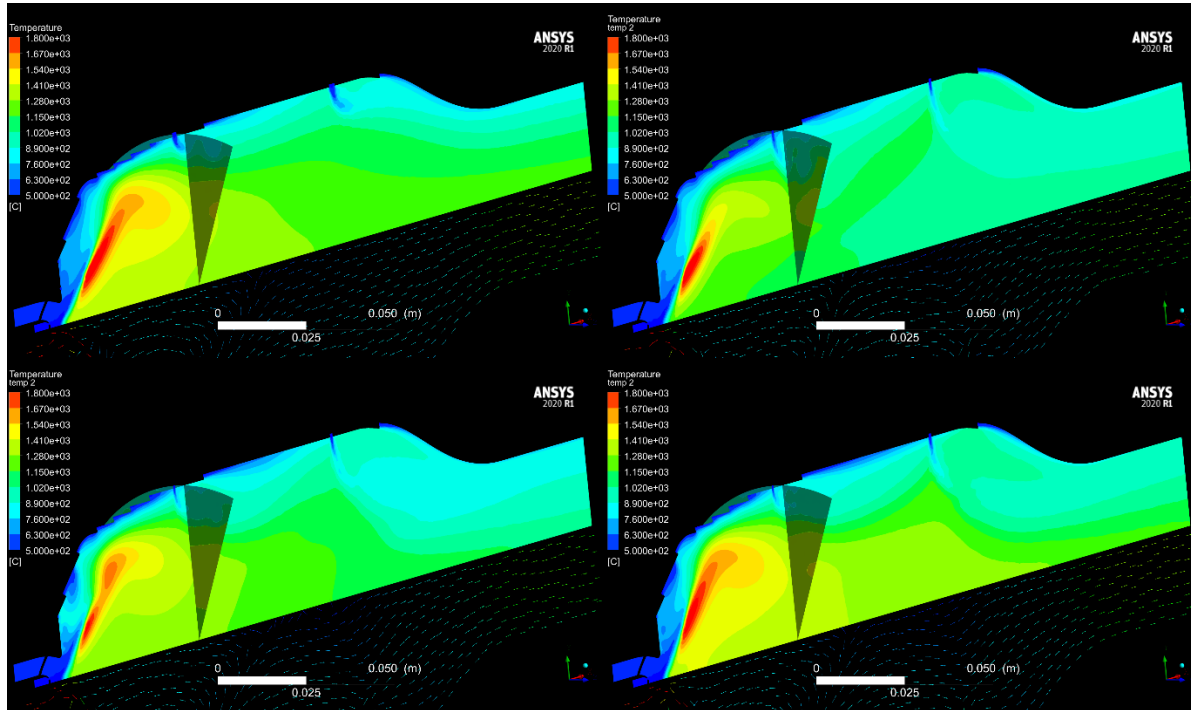
Flow Field

- Combustor design adapted from an older GE approach, but has changed significantly.
- Flame stability relies on swirl and cooling hole recirculation control.
- Light-off simulations have not yet been conducted at **low temperatures and pressures using real gas effects**



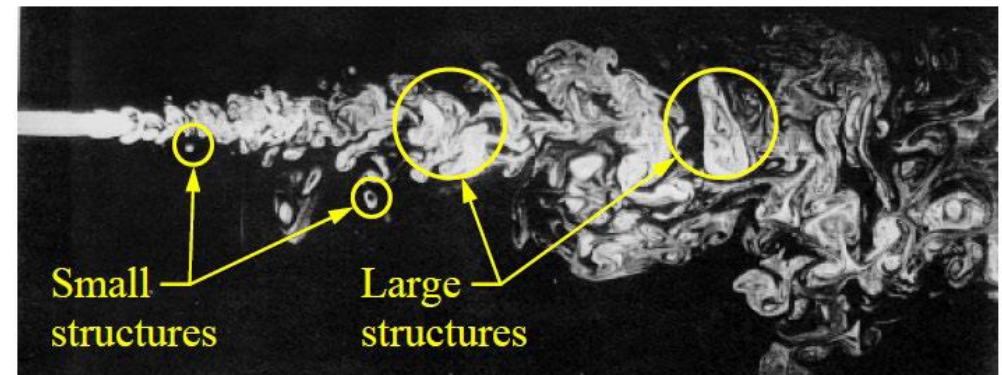
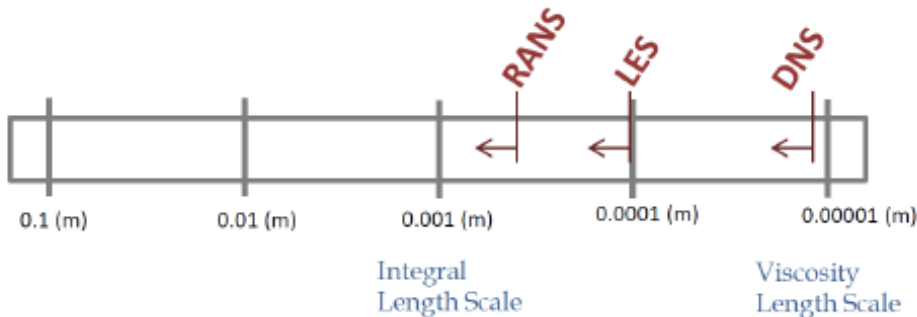
Design and Optimization

Preliminary approaches explored the design space using low-cost, low-fidelity steady RANS simulations.



Turbulence Modeling

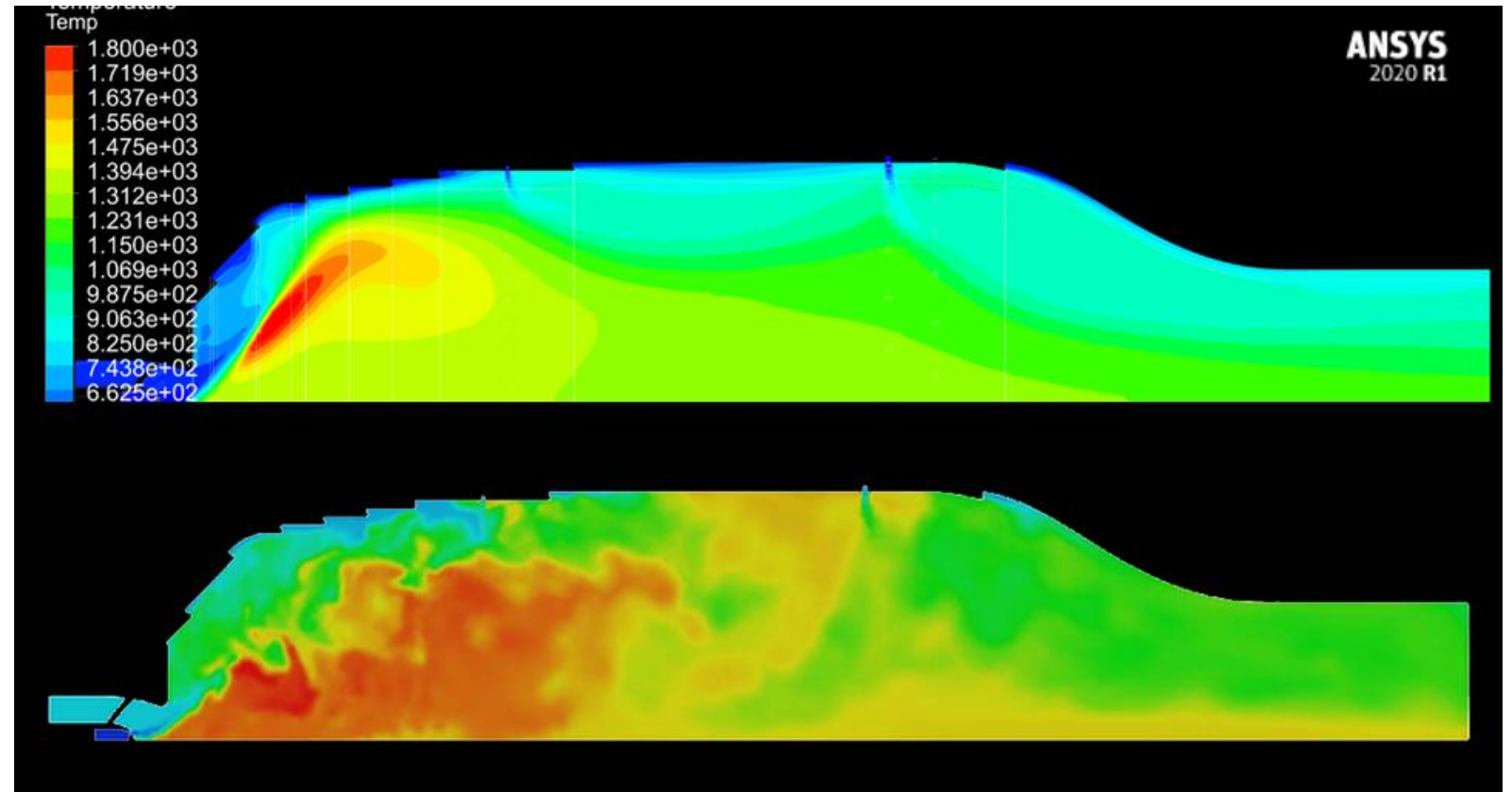
- Two approaches over the design cycle
 - **Steady Reynolds-Averaged Navier-Stokes (RANS):** This model is used to account for mixing by introducing turbulent diffusion coefficients for momentum, energy, and species
 - **Unsteady Detached Eddy Simulations (DES):** Resolves the large length scale like LES and models the small, near-wall length scale like RANS
- Turbulence Chemical Interactions not yet modeled, only assuming laminar flame speeds, currently investigating this liability.



CONVERGECFD

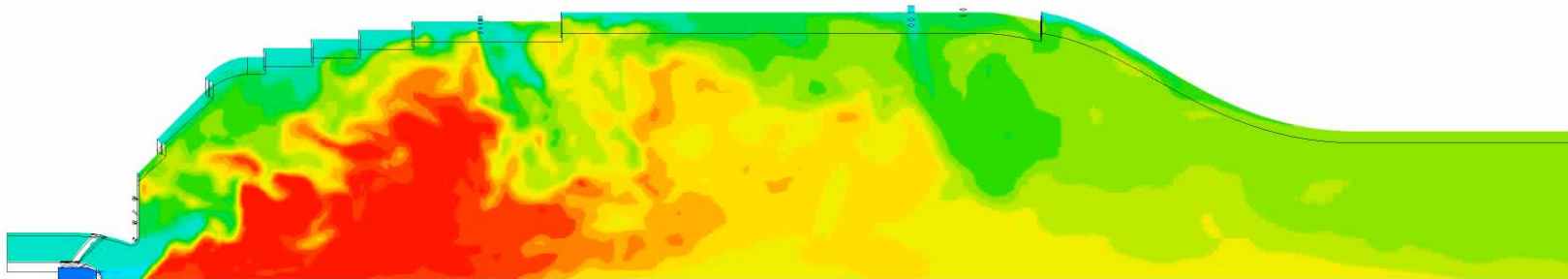
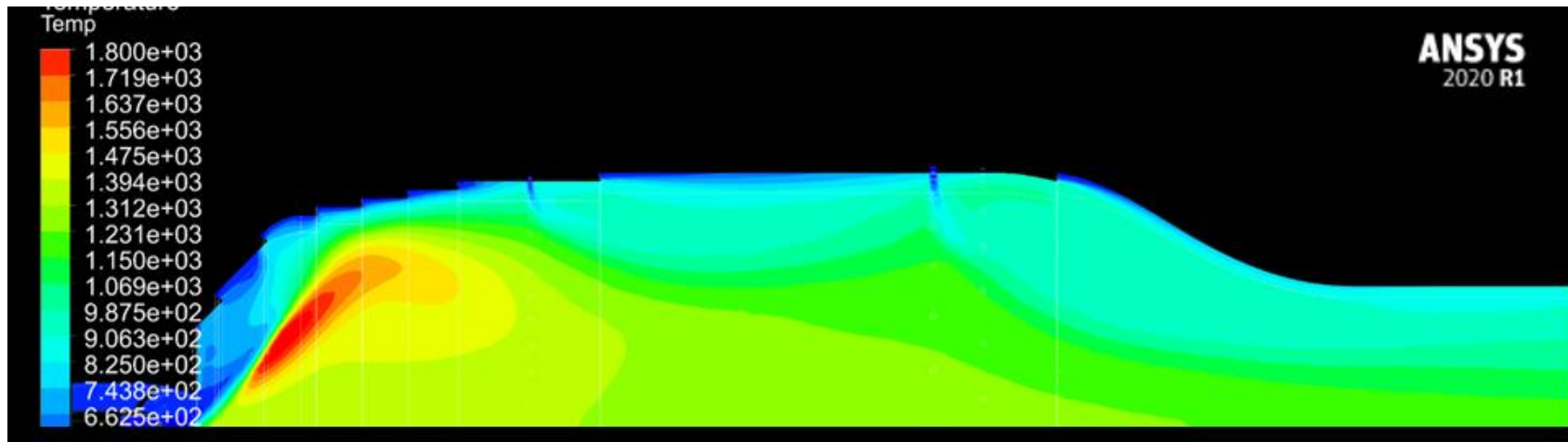
Steady vs. Unsteady Modeling

Steady RANS Simulation

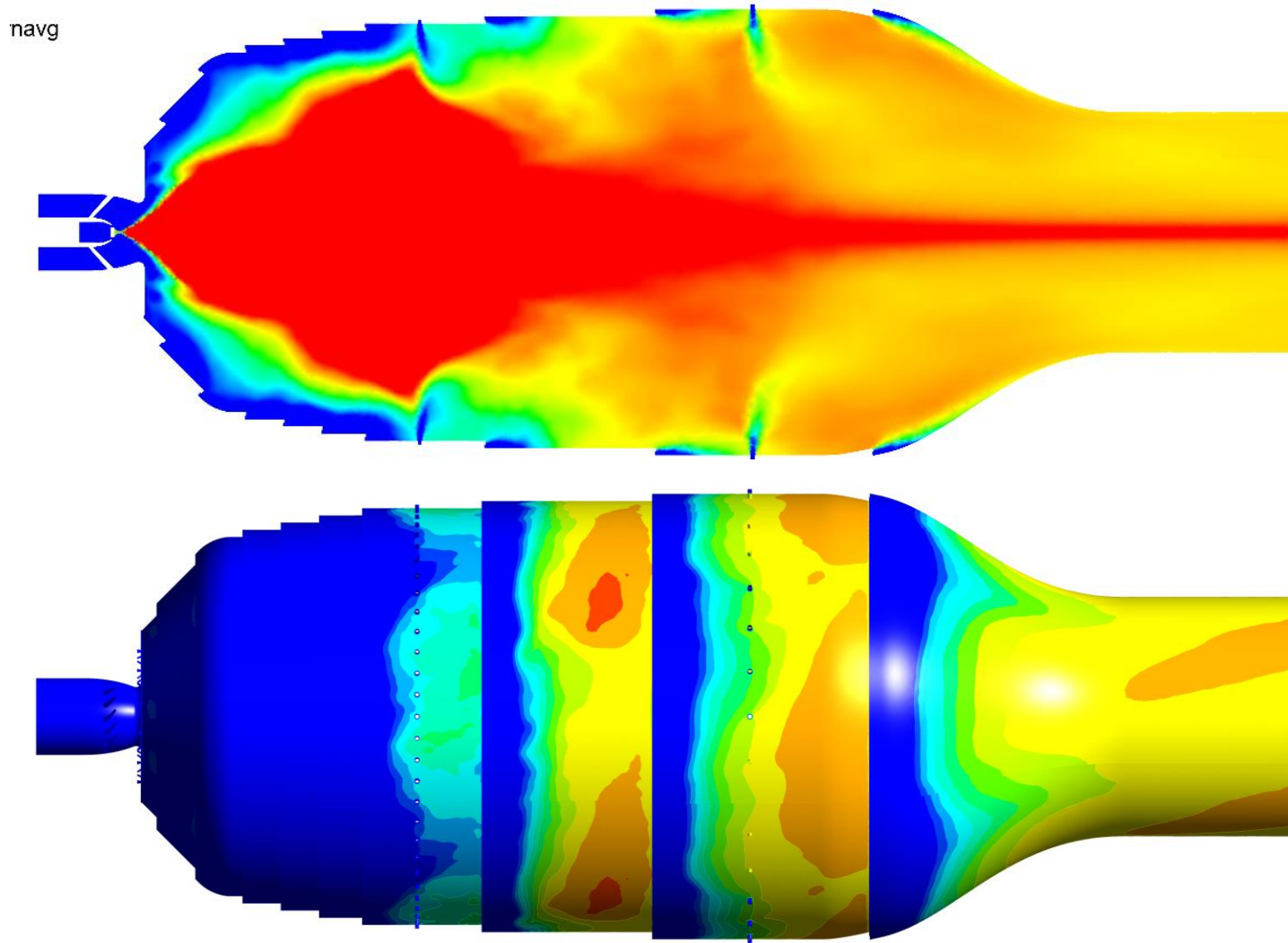


Unsteady DDES Simulation
(~5-10x cost per run)

Unsteady Combustion Simulations



Time-averaged DES results



Light-Off Conditions

Literature Review & Cycle Modeling

Light-Off: Open Loop

Nominal Targets	1	2	3	4	5	6	7	8	9
Substance	CO2	CO2	CO2	CO2	O ₂	CO2	Methane	CO2	CO2
Function	Main Loop Inlet	Inlet Thermal Cooling	Instrumentation Quench	Combustor Cooling	Oxidizer	Casing Cooling	Fuel	Exhaust Quench	Loop Exit
Pressure [psi]	247	270	270	270	300	270	300	270	240
Temp [°C]	149	90	90	90	50	90	50	90	405
Flowrate [lbm/s]	0.041	0	0	0.209	0.00765	0	0.00189	0	0.260

43 kW combustion

		Temperature [C]	Pressure [Bar]	Enthalpy [kJ/kg]	State	Fluid	CO2			
						CO2	CO2;H2O .9925;.0075 mass			
State 1	Compressor Inlet	33.00	15.60	499.08	Superheated gas					
State 2	Compressor Outlet	38.00	17.60	501.99	Superheated gas	Compressor Flow Rate [kg/s]	Compressor Flow Rate [lb/s]			
State 3	Recycle valve inlet	38.00	17.60	501.99	Superheated gas	1.81	4			
State 4	Recycle Valve outlet	36.29	15.88	501.99	Superheated gas		71.2			
State 5	Quench line	38.00	17.60	501.99	Superheated gas	Loop Flow Rate [kg/s]				
State 6	Recuperator HP Inlet	38.00	17.60	501.99	Superheated gas	1.81				
State 7	Recuperator HP Outlet	#[PHFLSH error 2]	17.50	#VALUE!	#VALUE!					
State 8	Cool line	38.00	17.50	502.09	Superheated gas	Percentage of compressor recyl	Percentage of HP Flow through recuperator	Percentage of Flow through heater		
State 9	Heater Inlet	38.00	17.50	502.09	Superheated gas	94%	6%	1% quench flow		
State 10	Heater Outlet	149.37	17.25	611.31	Superheated gas	3.75	0.25	0.041	0 lb/s	
State 11	Combustor Inlet	149.37	17.25	611.31	Superheated gas					
State 12	Combustor Outlet	407.02	17.23	885.26	Superheated gas	Cooler Duty Required [kW]	Recup HP outlet Temp [C]	Combustor Main Inlet [C]		
State 13	Throttle Valve Inlet	407.02	17.23	885.26	Superheated gas	4.96	#[PHFLSH error 248] Single-phase it	149.37		
State 14	Throttle Valve Outlet	407.02	17.23	885.26	Superheated gas					
State 15	Recuperator LP Inlet	407.02	17.23	885.26	Superheated gas					
State 16	Recuperator LP Outlet	#[PHFLSH error 2]	15.13	#VALUE!	#VALUE!	Energy added by heater [kW]				
State 17	Separator Inlet	#[PHFLSH error 2]	15.13	#VALUE!	#VALUE!	2.03				
State 18	Separator outlet	#VALUE!	85.00	#VALUE!	#VALUE!					
State 19	Cooler Inlet	36.29	15.88	501.99	Superheated gas					
State 20	Cooler Outlet	33.00	15.60	499.08	Superheated gas					
						Manual Inputs				
						Critical Outputs				

States in yellow are not active open loop

Swap to Closed Loop

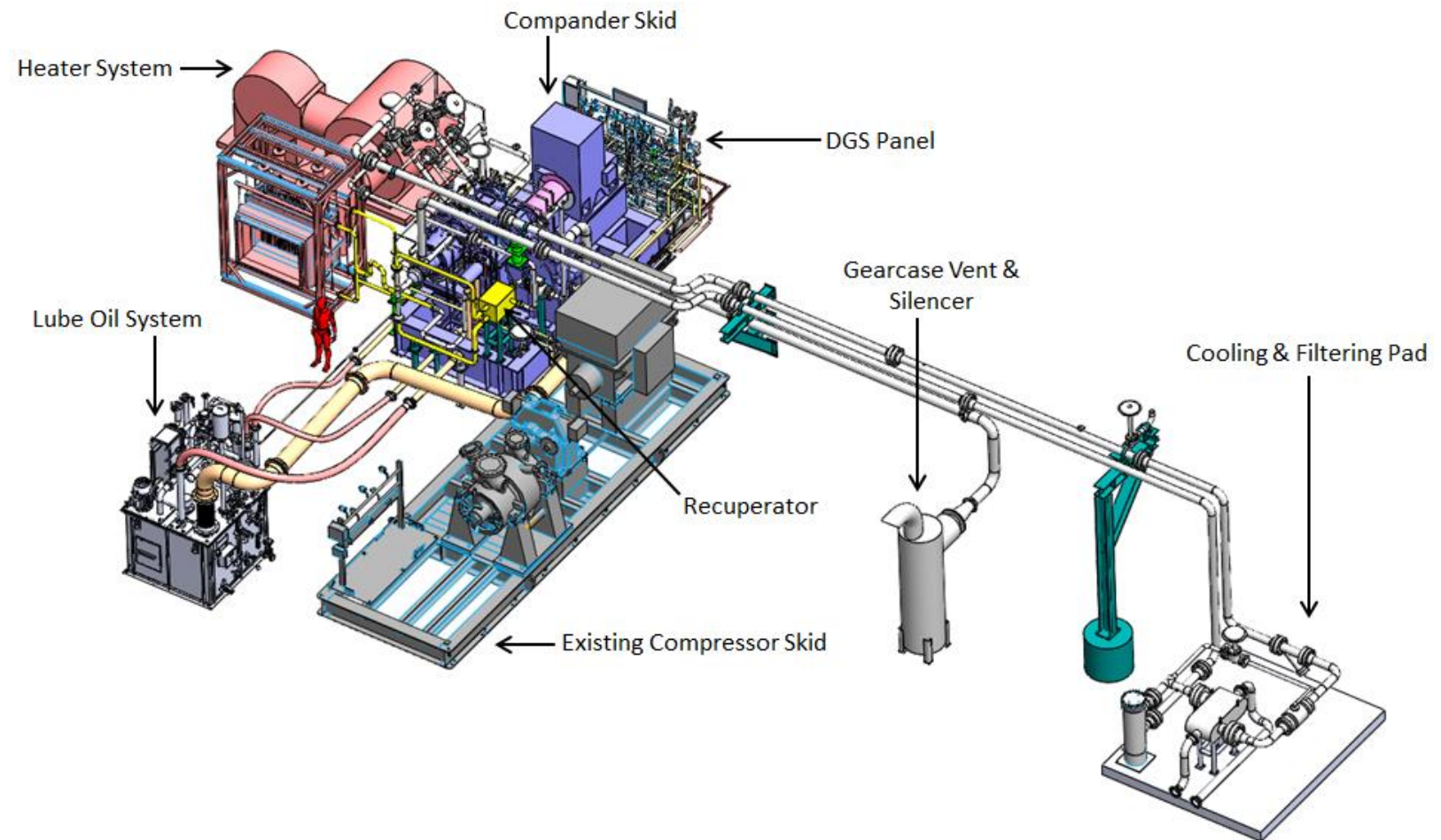
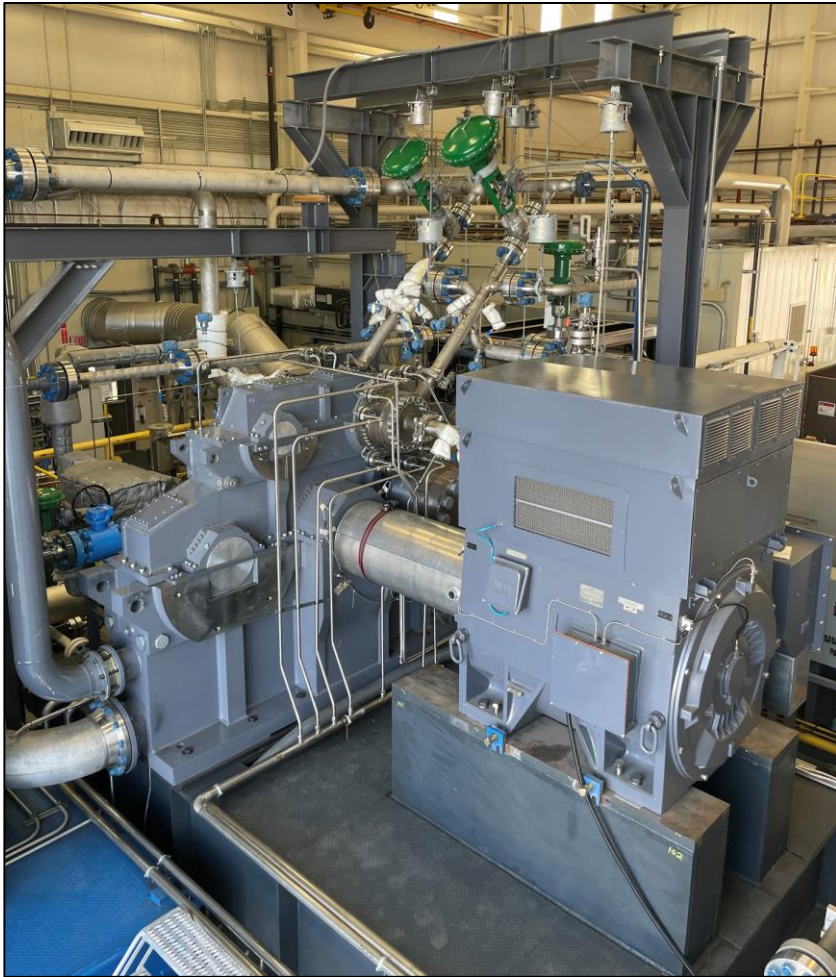
Nominal Targets	1	2	3	4	5	6	7	8	9
Substance	CO2	CO2	CO2	CO2	O ₂	CO2	Methane	CO2	CO2
Function	Main Loop Inlet	Inlet Thermal Cooling	Instrumentation Quench	Combustor Cooling	Oxidizer	Casing Cooling	Fuel	Exhaust Quench	Loop Exit
Pressure [psi]	247	270	270	270	300	270	300	270	240
Temp [°C]	149	117	38	117	50	117	50	38	127
Flowrate [lbm/s]	0.041	0	0.05	0.209	0.00765	.75	0.00189	0.95	2.010

		Temperature [C]	Pressure [Bar]	Enthalpy [kJ/kg]	State	Fluid	CO2			
						CO2	CO2;H2O .9925;.0075 mass			
State 1	Compressor Inlet	33.00	15.60	499.08	Superheated gas					
State 2	Compressor Outlet	38.00	17.60	501.99	Superheated gas	Compressor Flow Rate [kg/s]	Compressor Flow Rate [lb/s]			
State 3	Recycle valve inlet	38.00	17.60	501.99	Superheated gas	1.81	4			
State 4	Recycle Valve outlet	36.29	15.88	501.99	Superheated gas		42.5/71.2			
State 5	Quench line	38.00	17.60	501.99	Superheated gas	Loop Flow Rate [kg/s]				
State 6	Recuperator HP Inlet	38.00	17.60	501.99	Superheated gas	1.81				
State 7	Recuperator HP Outlet	117.01	17.50	579.17	Superheated gas					
State 8	Cool line	117.01	17.50	579.17	Superheated gas	Percentage of compressor recycle	Percentage of HP Flow through recup	Percentage of Flow through heater		
State 9	Heater Inlet	117.01	17.50	579.17	Superheated gas	50%	25%	1%	quench flow	
State 10	Heater Outlet	150.15	17.25	612.09	Superheated gas	2	1	0.041	1 lb/s	
State 11	Combustor Inlet	150.15	17.25	612.09	Superheated gas					
State 12	Combustor Outlet	126.50	17.23	588.65	Superheated gas	Cooler Duty Required [kW]	Recup HP outlet Temp [C]	Combustor Main Inlet [C]		
State 13	Throttle Valve Inlet	126.50	17.23	588.65	Superheated gas	51.80	117.01	150.15		
State 14	Throttle Valve Outlet	125.97	16.23	588.65	Superheated gas					
State 15	Recuperator LP Inlet	125.97	16.23	588.65	Superheated gas					
State 16	Recuperator LP Outlet	86.50	16.13	550.25	Superheated gas	Energy added by heater [kW]				
State 17	Seperator Inlet	86.50	16.13	550.25	Superheated gas	0.61				
State 18	Seperator outlet	86.74	15.88	550.64	Superheated gas					
State 19	Cooler Inlet	62.88	15.88	527.63	Superheated gas					
State 20	Cooler Outlet	33.00	15.60	499.08	Superheated gas					
						Manual Inputs				
						Critical Outputs				
inputs displayed				kg/s						
Heater eff	3%		Recup HP flow	0.45						
Heater flame temp	1050.00		Recup LP flow	0.91	<-- Separator ~ 8					
Recup load	35									

Facility Status

Procurement & Fabrication

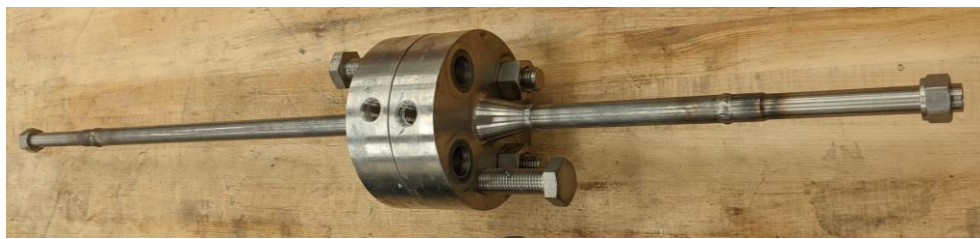
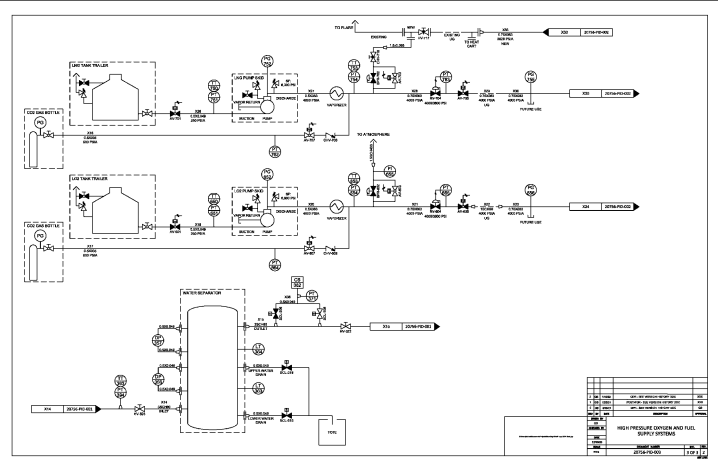
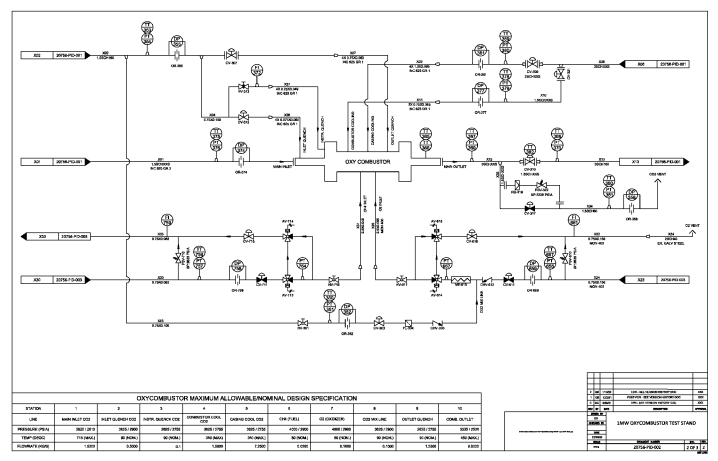
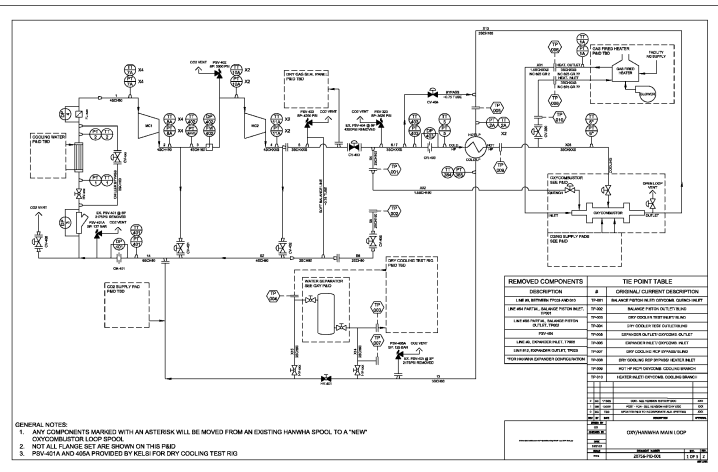
Fully Commissioned sCO₂ Compressor Loop



Flow Control Hardware

Purchased Components:

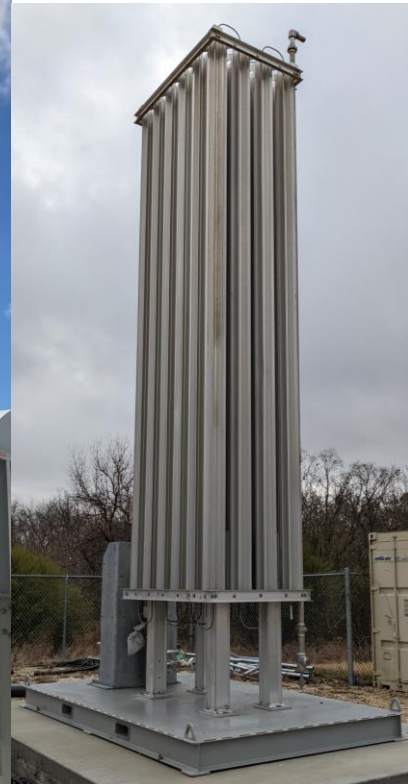
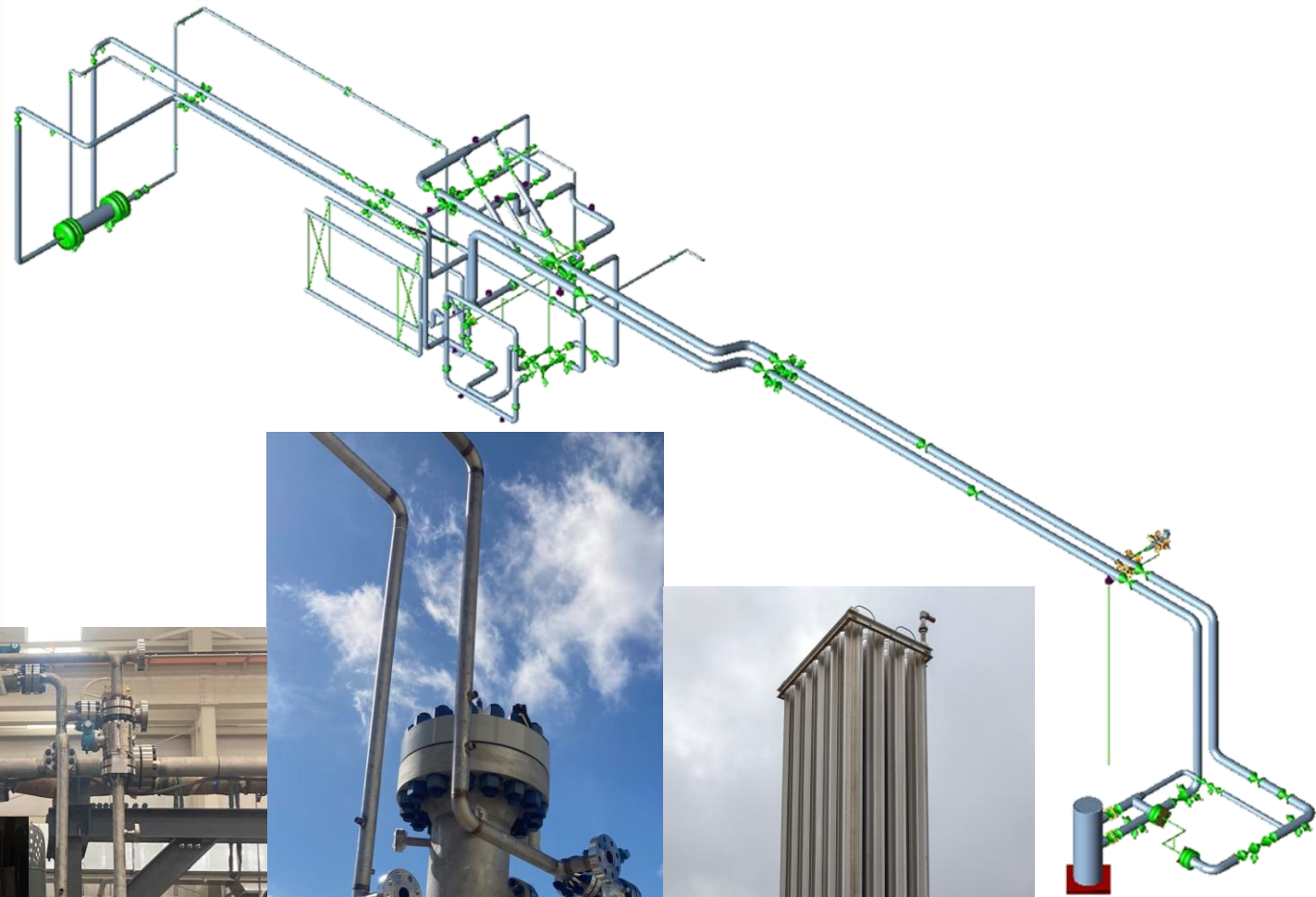
- Control Valves
- Actuated Valves
- Hand Valves
- Check Valves
- Orifice Flow Meters
- Pressure Regulators
- Pressure Safety Valves



Piping & Supply Lines

Completed Components:

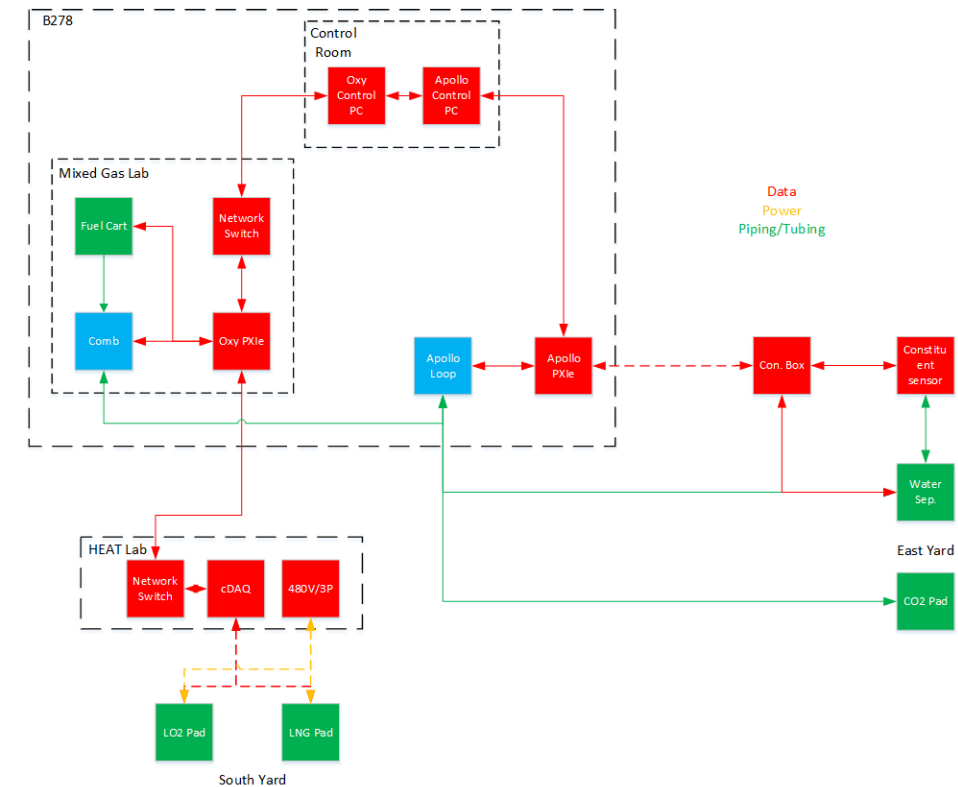
- Heater outlet to Combustor Inlet
- Fuel and Oxygen supply pads
- Fuel supply and vent lines
- Water Separator



DAQ & Instrumentation

Purchased Components:

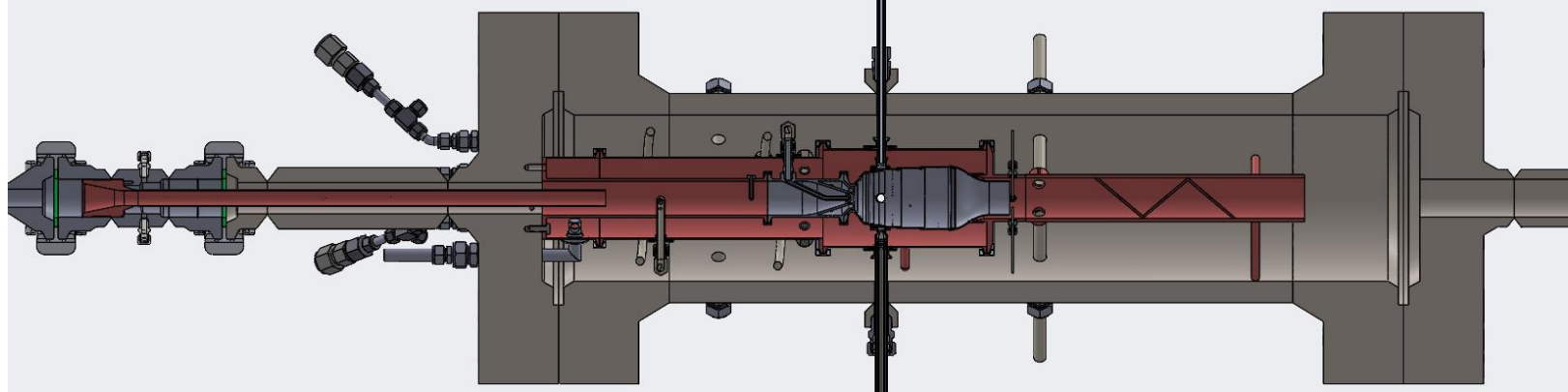
- PXIe chassis
- cDAQ
- Voltage Cards
- Amperage Cards



Combustor

Completed Components:

- Inlet spool
- Inlet flange
- Thermal lining tubes
- Primary flow inlet
- Fuel injector
- Combustor liner
- Exhaust mixer
- Pass-through grommets
- Casing and Exit flanges
- Thread-o-lets
- Compression fittings
- Optical probes
- Laser-ignition probe



Questions

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