

Aluminization Coatings and Glass Seals for a High Temperature Hydrogen Reactor

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PNNL is operated by Battelle for the U.S. Department of Energy





Background & Project Objective

- Our industrial partner is developing innovative electrolyzer technology for use in high temperature processes (e.g., steel plants) utilizing tubular cells.
- A critical challenge they are facing is creating stable, hermetic seals between the tubular cells (CTE ~ 12.8 $\times 10^{-6}$ /°C) and Inconel 617 manifolds (CTE ~ 15.8 x10⁻⁶/°C)
- Partnered to evaluate PNNL's sealing and coating IP (US Patent Numbers) 10,577,694, 10,378,094, and 9,481,923) to overcome this challenge and demonstrate hermetic sealing in a full-scale reactor test.



Reactive Air Aluminization (RAA) Coating Deposition



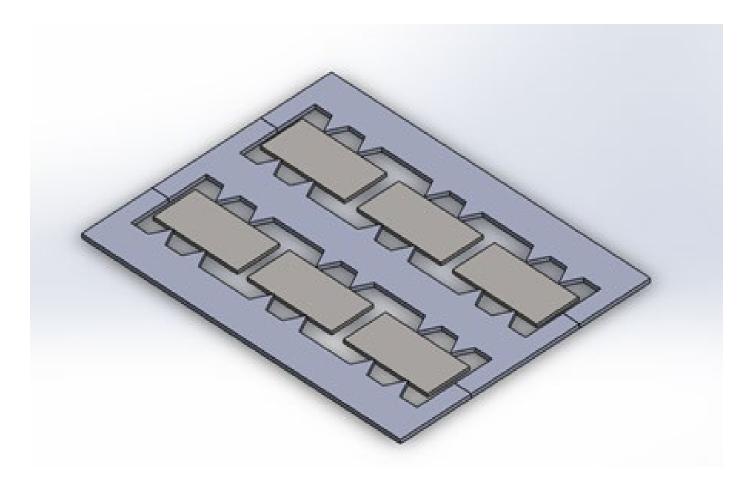
RAA coating applied with ultrasonic spray coater



Spray Coating Challenges

Issue: Inconel 617 is not magnetic, and therefore not magnetically held down.

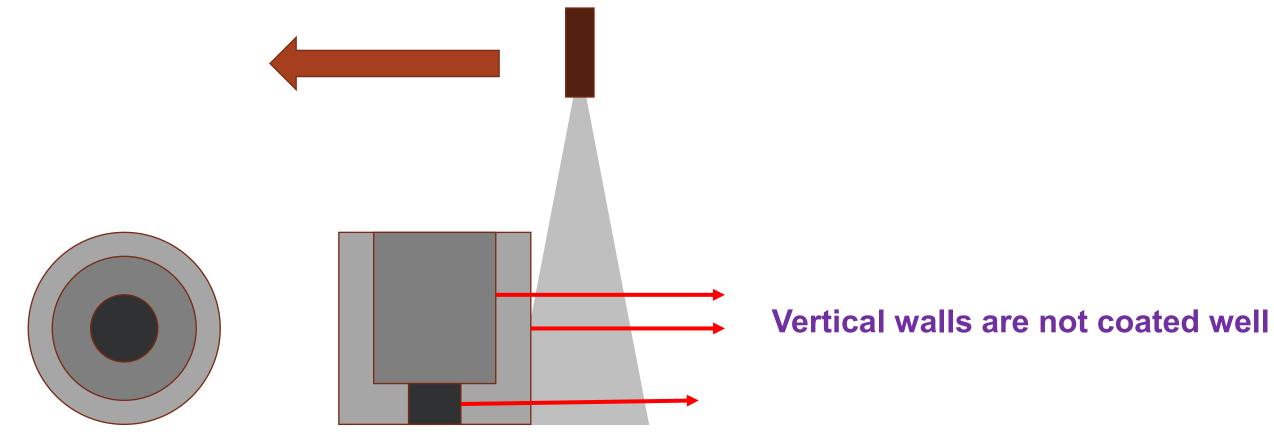
Solution: Designed a magnetic fixture to hold coupons down without shielding.





Spray Coating Challenges

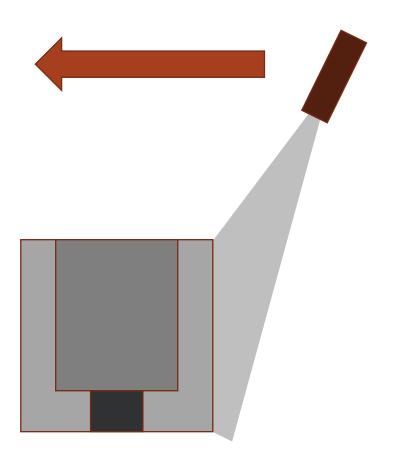
Issue: Spray coater works best for surfaces that are largely perpendicular to spray direction, but our parts are shaped like:





Solution to Spray Coating Challenge #2

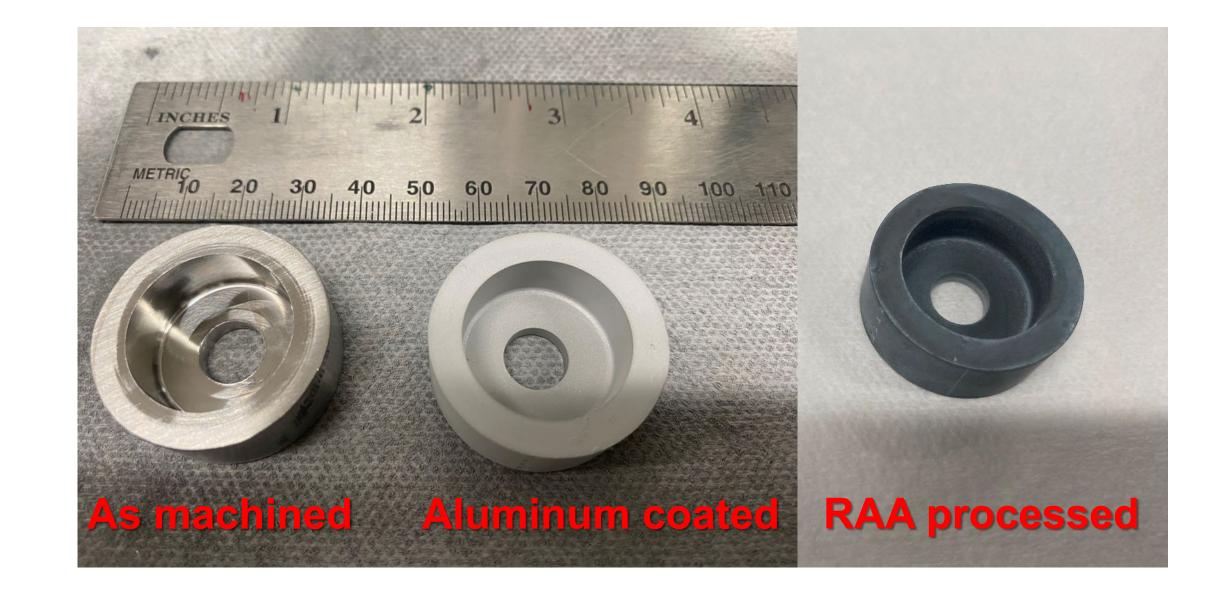
Working with the vendor, we were able to solve some calibration issues related to the rarely implemented tilted head configuration







Resulting Parts



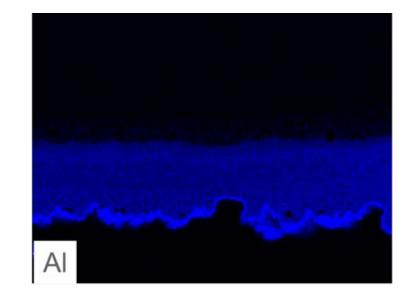


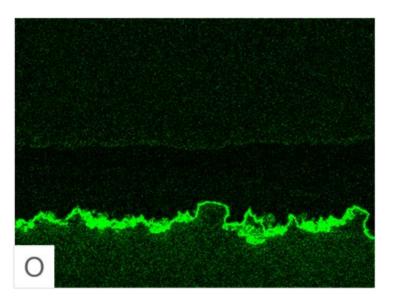
RAA Coating Microstructure on Inconel 617

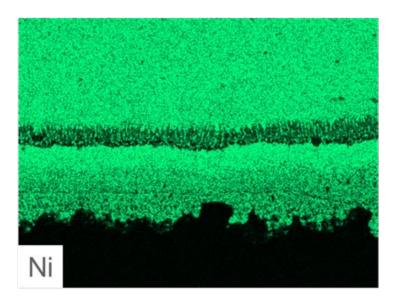
RAA-6

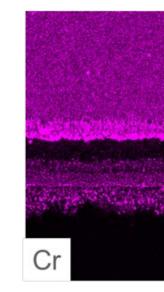
The reaction band is composed of Ni, Cr, Co, Fe and Mo.

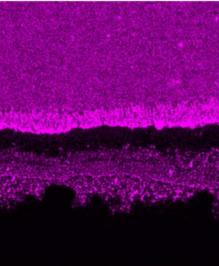








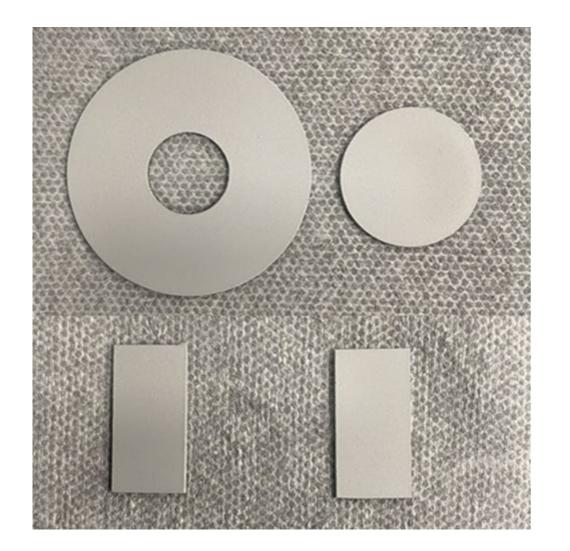


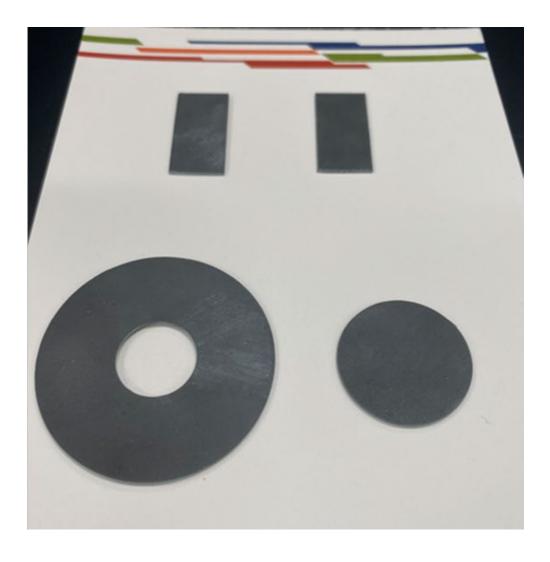




RAA Coatings will be Pop-gun Rupture Tested

Pop-Gun washer & disc pair is RAA processed









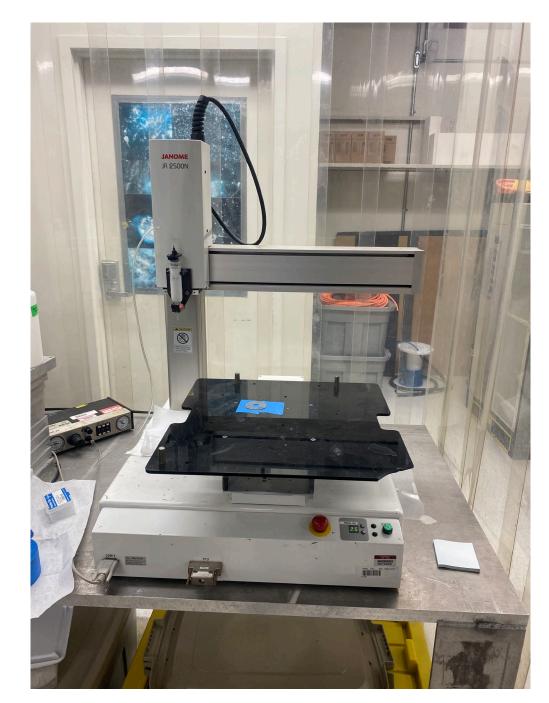
Glass sealant applied via Robotic Dispenser





G18-20%LSCF -17% binder

G18-4%YSZ -17% binder

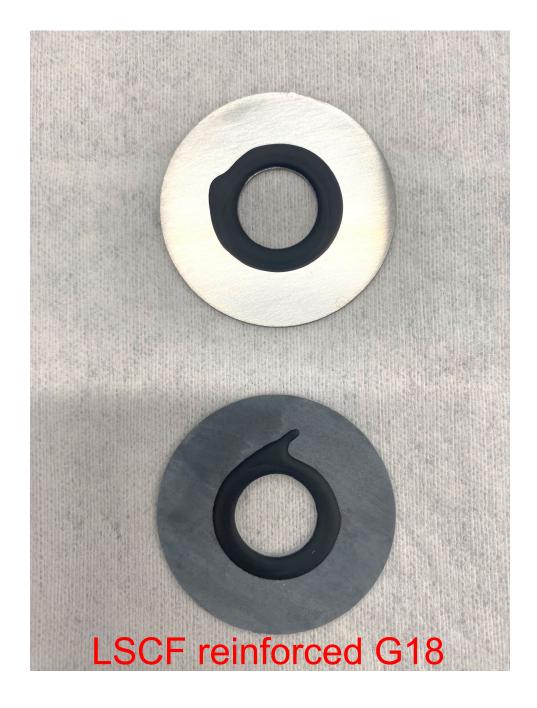


20psi condition ~0.67g of G18+YSZ ~0.8g of G18+LSCF



Simple 2x2 test matrix











Glass sealing discs to washers







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Test samples sealing in the furnace

Pop-gun tests are currently underway



Objective and Tasks for Glass Seal Development

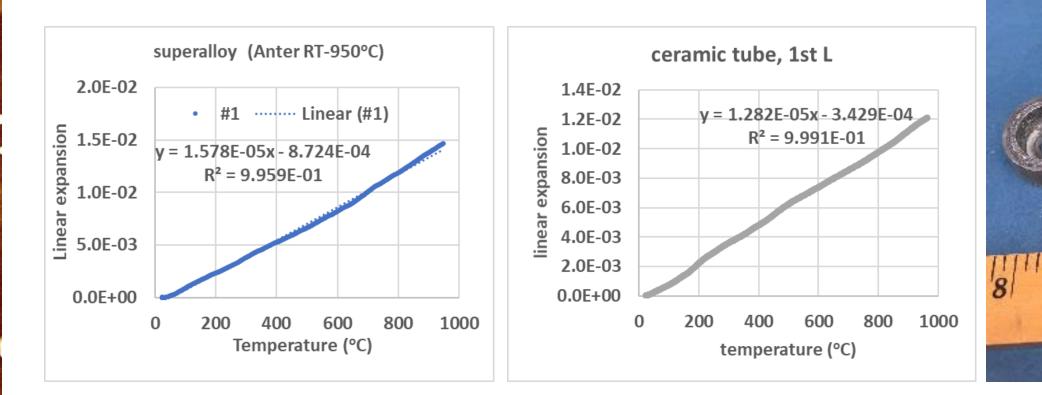
Objective: To develop glass sealant for client's tubular cells in electrolysis application at high temperature (900°C) and high steam (> 90% H₂O)

- Glass Formulation and Thermal Property Characterization: plain glass and composite glass approach, as-made and crystallized state
- Ageing Effect on Thermal Properties and Wetting Study: aged in air and reducing/humid environment at 900°C
- Bonding Strength and Interfacial Reaction Study: tensile testing on YSZ; cup sealing leak test, and interfacial characterization
- Validation of Candidate Glass and Aluminization Coating in a minitube reactor under dual environment



Mating Materials and Configuration for Glass Development

- Superalloy cup manifold & ceramic tubular cell
- Operating condition: 900°C with >90-95%H₂O
- Very large CTE mismatch (~3x10⁻⁶/°C) between superalloy (15.8x10⁻⁶/°C) & tube 12.8 x10⁻⁶/°C
- Targeting ~14x10⁻⁶/°C for sealant CTE



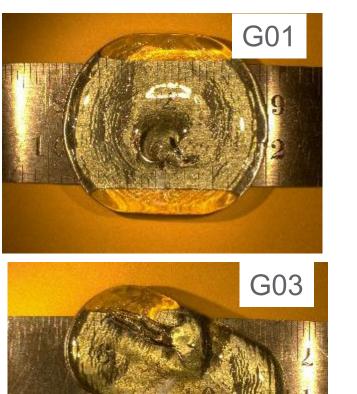


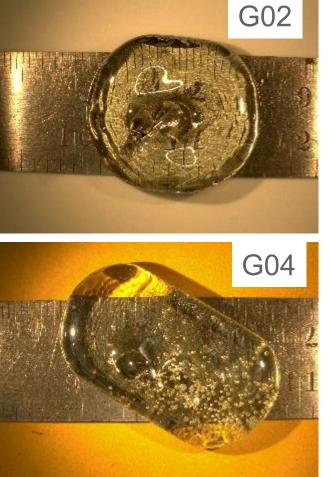




Glass formulation and thermal property characterization: plain glass approach

mole%	SiO2	B2O3	Al2O3	BaCO3	SrCO3	Y2O3	La2O3	
G01	39.0	10.0	9.0	33.0	9.0	0.0	0.0	tr
G02	39.0	10.0	9.0	36.0	6.0	0.0	0.0	tr
G03	39.0	10.0	9.0	39.0	3.0	0.0	0.0	tr
G04	39.0	10.0	9.0	42.0	0.0	0.0	0.0	tr
G05	39.0	10.0	0.0	33.0	9.0	9.0	0.0	
G06	39.0	10.0	0.0	33.0	9.0	0.0	9.0	tr





- All glasses except G05 were homogeneous and transparent in as-made state.
- Among all glasses only G04 showed a desirable CTE of ~14.2x10⁻⁶/°C after firing (930-950°C/2h); however, the wetting behavior was not promising.

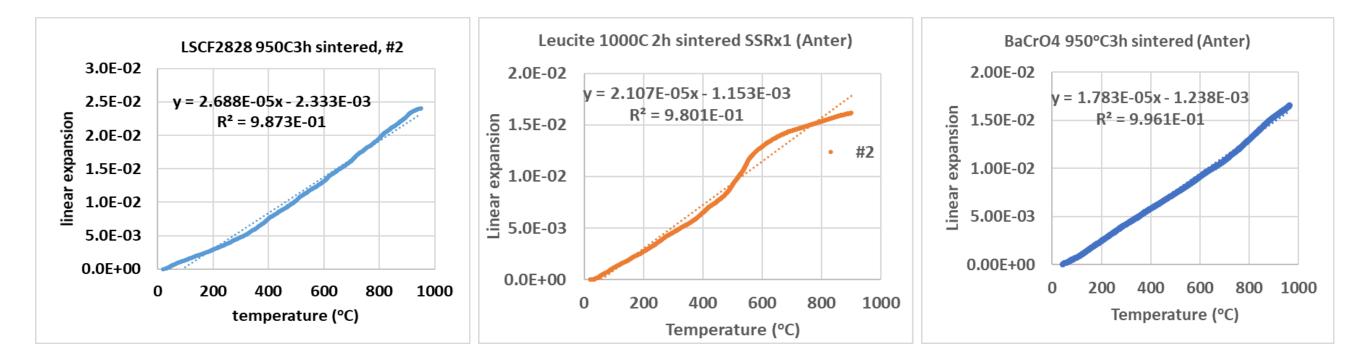


as-made ransparent ransparent ransparent ransparent opaque ransparent



Glass formulation and thermal property characterization: composite glass approach

- Identified 3 high CTE ceramic phases: LSCF2828, Leucite (KAISiO₄), and BaCrO₄ to add to the matrix G18 glass (Ba-Ca-Al-B-Si) - and YSZ fibers for reinforcement
- Potential issues: chemical compatibility, volatility, electrical conductivity, thermal stability in red./H2O, commercial availability
- CTE tailorable by rule of mixtures: $\alpha_{comp} = (\alpha_1 K_1 V 1 + \alpha_2 K_2 V_2)/(K_1 V_1 + K_2 V_2)$





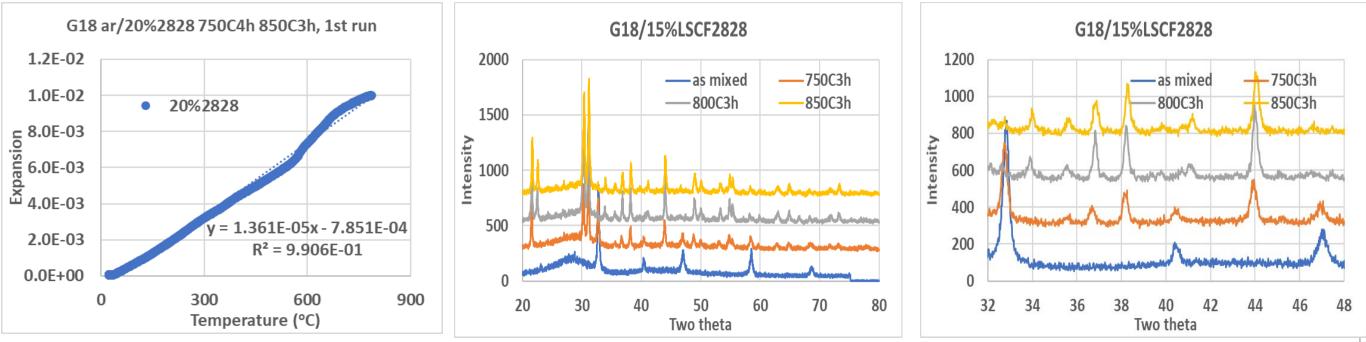


Dissolution of LSCF2828 in G18 glass

- G18 glass highly reactive with LSCF2828 (sub-micron sized mixed conductor active phase)
- CTE of G18/LSCF2828 composite was much lower than model prediction, consistent with XRD results indicating G18 reacted with/dissolved LSCF2828

CTE prediction of composite by rule of mixture

Vf	CTE (G18/2828)	CTE (G18/leucite)	CTE (G18/BaCrO4)
0.00	12.5	12.5	12.5
0.05	14.2	13.0	12.7
0.10	15.6	13.4	12.8
0.15	16.9	13.9	13.0
0.20	18.0	14.4	13.2
0.25	19.0	14.8	13.4
0.30	19.9	15.2	13.6

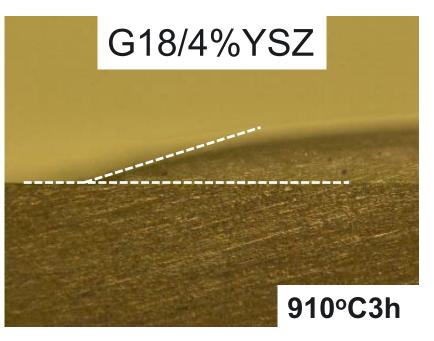


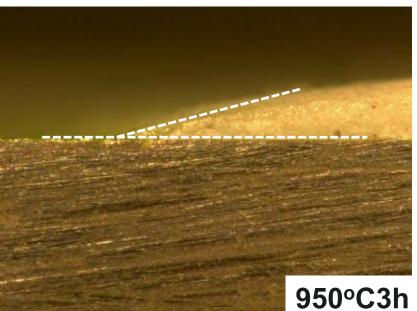


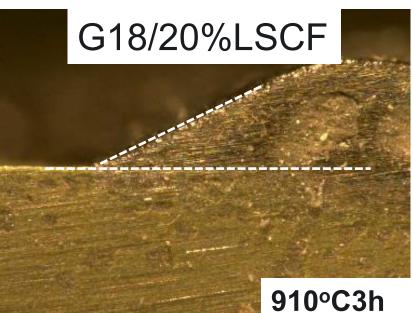
Wetting behavior on YSZ

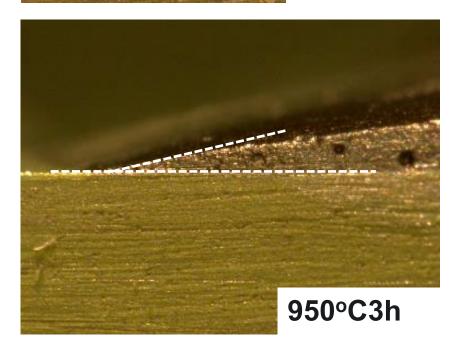
Pacific Northwest

Good wetting observed for both G18/4%YSZ and G18/20%LSCF2828 composite glasses on YSZ layer with wide working temperature range





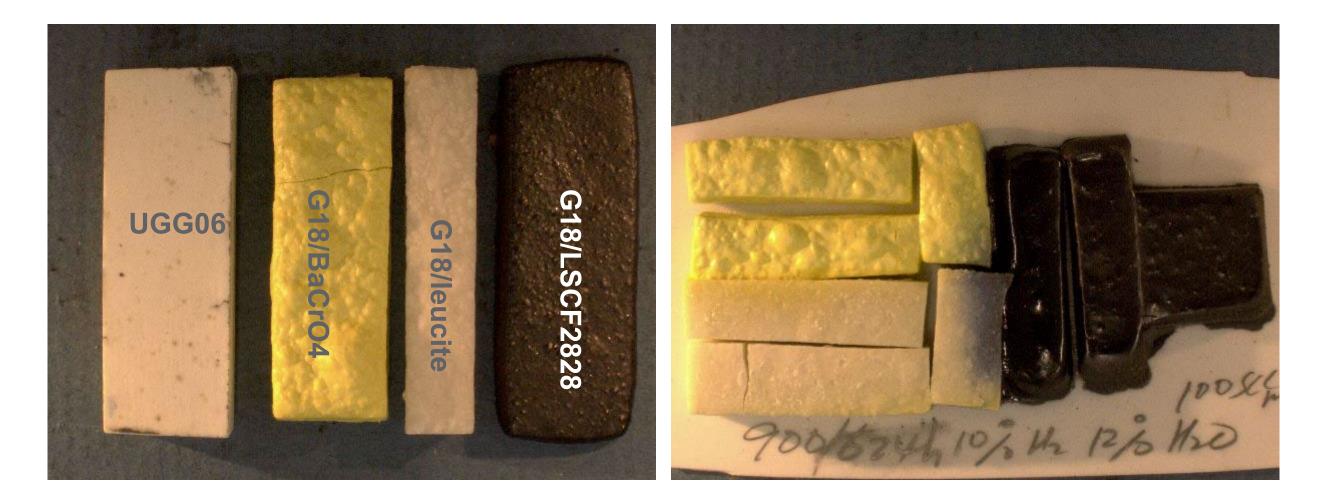






Isothermal ageing of composite glass in air and reducing environment

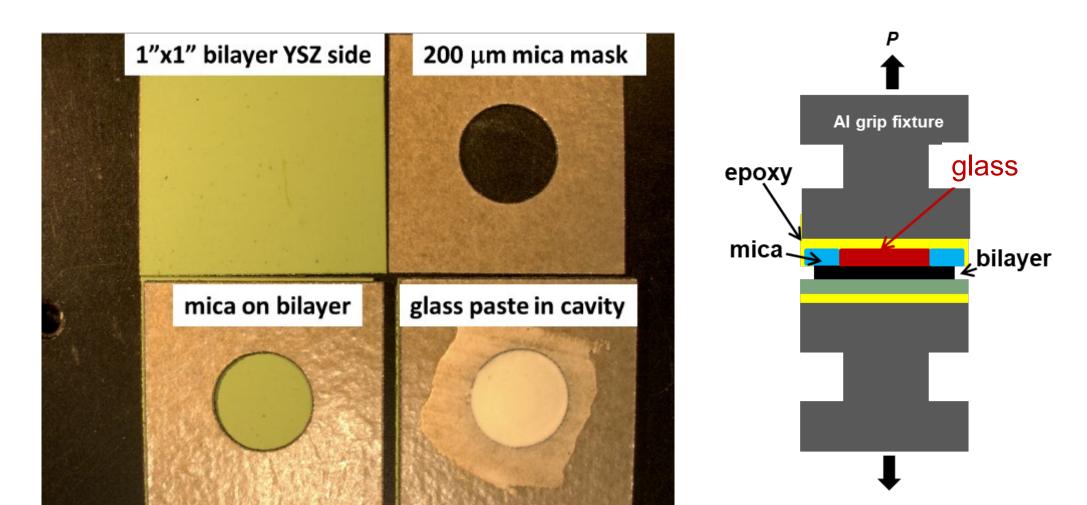
- G18/20%LSCF2828, G18/20%leucite, G18/20%BaCrO₄
- Aged at 900°C 500h in air or 10%H₂/10%H₂O
- Microscopy of samples aged in air or reducing environment showed no distinct difference, suggesting good thermal/environmental stability





Seal bond strength: sample preparation

- Candidate composite glass made as paste using organic binders
- 200-micron thick mica mask (with a central hole) glued onto 1"x1" bilayer on YSZ side
- Apply glass paste to central cavity and smooth with razor blade
- After drying fire to 950°C 3h in air, then epoxy glued to AI fixture and tensile tested
- 8 samples for as-fired, 8 samples for air aged+10 TC, 8 samples for red. aged+10 TC







Pacific

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No substantial bond strength reduction after 900°C/500h ageing + 10 thermal cycles in air or Northwest reducing environment

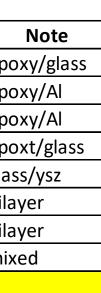
As-fired

	MPa		MPa	
as-fired	20%2828	Note	4%YSZ	Note
1	9.68	epoxy/Al	9.64	epoxy/Al
2	9.59	epoxy/Al	10.82	epoxy/Al
4	9.65	epoxy/Al	7.87	epoxy/Al
5	8.72	epoxy/Al	10.52	epoxy/Al
6	8.17	epoxy/Al	8.93	epoxy/Al
7	9.96	epoxy/Al	11.01	epoxy/Al
8	8.02	epoxy/Al, l	9.84	epoxy/Al
3	2.80	bilayer	6.15	bilayer
avg	9.29	avg	9.80	
std	0.69	std	1.12	

	MPa		MPa	
air aged	20%2828	Note	4%YSZ	
1	4.97	epoxy/Al	7.08	ер
2	3.30	epoxy/Al	6.18	ер
5	7.28	epoxy/Al	7.58	ер
6	6.05	epoxy/Al	6.58	ер
8	8.53	in bilayer	9.46	gla
7	3.73	in bilayer	4.43	bil
3	3.06	in bilayer	5.83	bil
4	3.31	in bilayer	5.09	mi
avg	6.02	avg	7.37	
std	2.03	std	1.28	

	MPa		MPa	
red. aged	20%2828	Note	4%YSZ	
1	8.17	epoxy/Al	7.65	ep
2	7.37	epoxy/glas	8.01	mi
5	9.18	mixed	10.21	ер
6	5.92	epoxy/Al	11.29	ер
8	7.37	mixed	7.14	ер
4	8.00	in bilayer	7.78	mi
7	4.06	in bilayer	5.11	ер
3	4.71	in bilayer	9.18	bila
avg	7.67	avg	8.30	
std	1.08	std	1.92	

- G18/YSZ showed slightly higher strength, likely due to strong fiber reinforcement.
- Small reduction in bond strength after • ageing is likely attributed to crystallized microstructure from as-fired state.



Aged in air

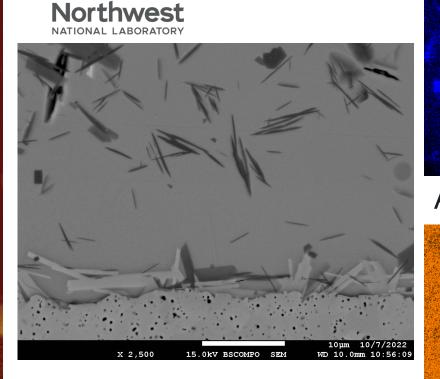
Note oxy/glass ixed bil/epo oxy/Al oxt/Al oxt/Al ixed bil/epo oxy/Al ayer

Aged in $10\% H_{2}$ 20%H₂O

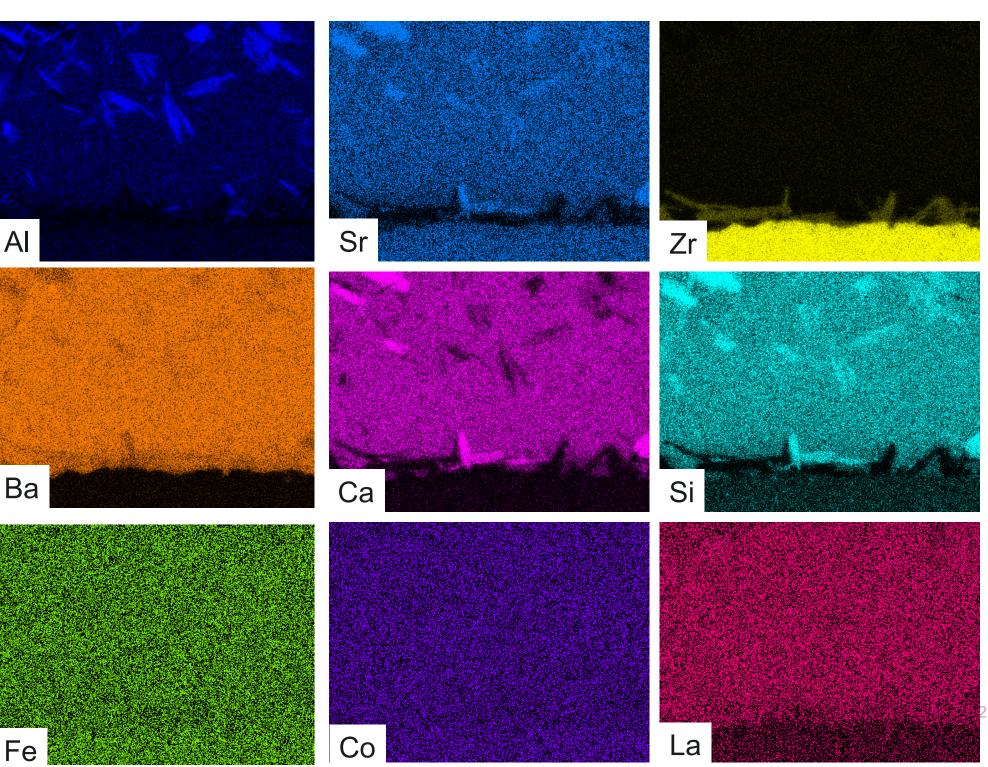


Pacific

EDS of as-fired YSZ/glass (G18/20%LSCF2828)



- Some discrete crystal formed ٠ along interface: Sr-Ca-silicate, BaZrO₃.
- Al-Ca-silicate and Sr-Ca-• silicate in matrix.
- LSCF appeared well dissolved • within glass matrix, no crystalline phase identified along interface.

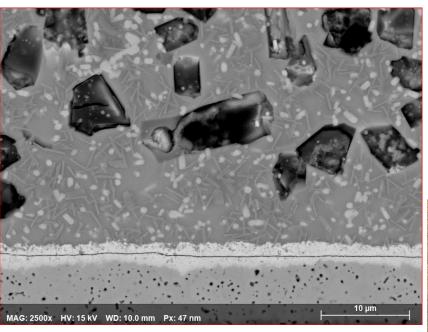




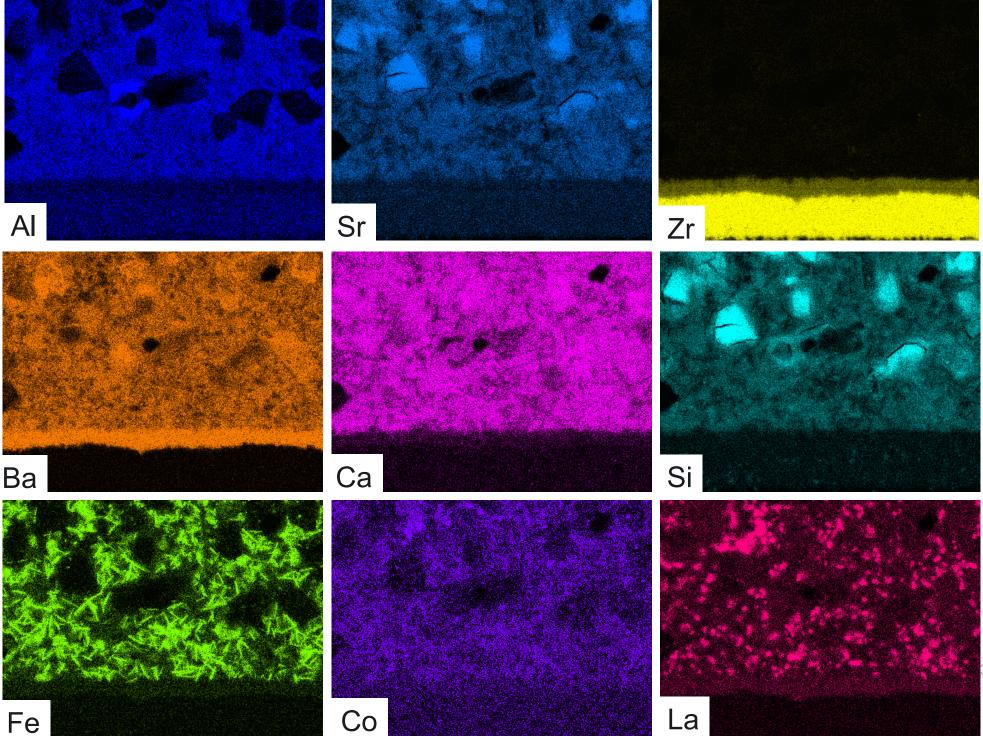


Northwest

EDS of air-aged (900°C/500h) YSZ/glass



- Dense layer, ~3 μm BaZrO₃ formed at interface.
- Interfacial BaZrO₃ cracked during metallography.
- Uniformly distributed La- or Fe-۲ enriched precipitates.
- **Microstructural evolution** resulted in some irregular voids, likely due to redissolution.

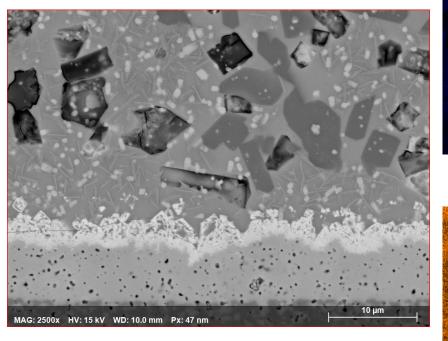




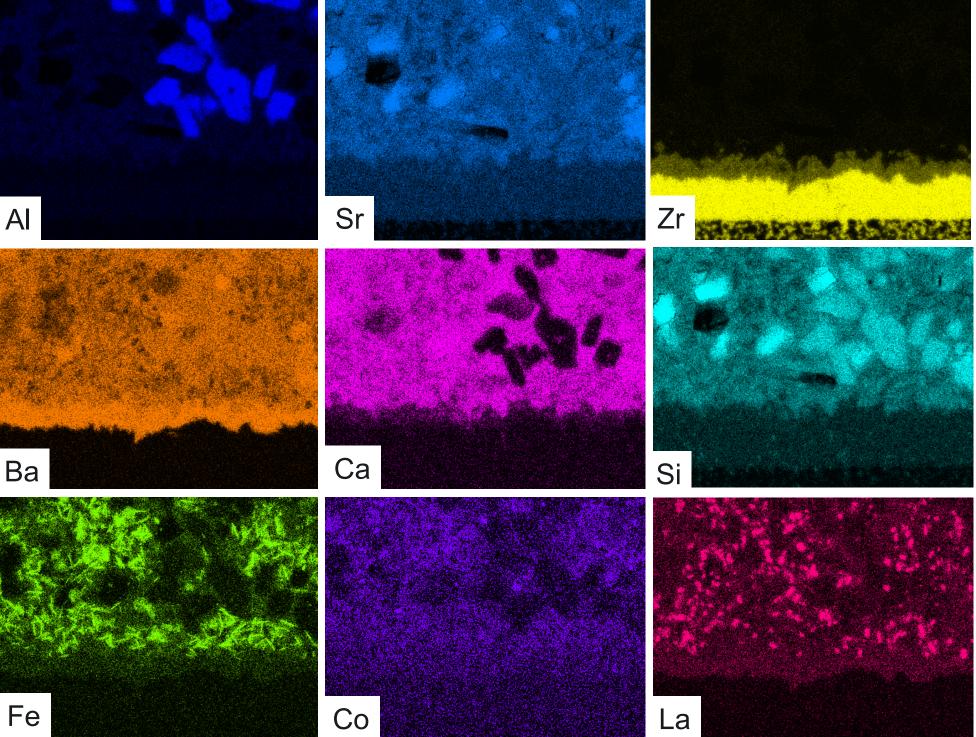


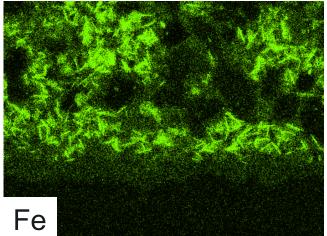
EDS of reducing-aged (900°C/500h) YSZ/glass

Pacific Northwest



- Dense layer, ~2 μ m BaZrO₃ formed at interface.
- Uniformly distributed La- or ٠ **Fe-enriched precipitates**
- **Microstructural evolution** • resulted in some irregular voids, likely due to redissolution.
- No distinct difference from ageing in air.



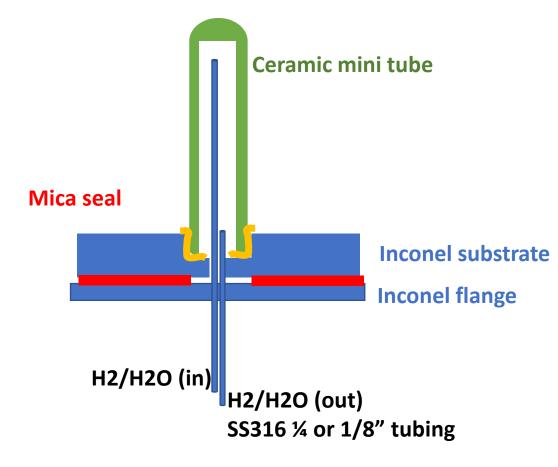






Validation with mini-tube reactor

- Objective is to test glass seal integrity in dual environment at 900°C for ~300-500h followed by ~10 thermal cycles
- Tests underway for both G18/YSZ and G18/LSCF composite glasses









Summary and Conclusions

- Formulated 6 glasses 5 showed good glass behavior, one crystallized upon casting.
- CTE of as-made plain glasses were lower than the targeted values crystallized G04 glass has the closest match; however, its sealing behavior was undesirable due to rapid crystallization.
- 3 high CTE ceramic phases were identified to form composites with G18 matrix glass.
- Chemical compatibility was assessed for high CTE ceramic phases with G18. BaCrO₄ was the least reactive, while leucite and LSCF reacted readily with G18 glass melt.
- Composite G18/20%LSCF2828 and G18/4%YSZ(f) were chosen for dual atmosphere testing. Both glasses showed good wetting on YSZ over a wide temperature range for sealing.
- Interfacial EDS analysis of G18/LSCF on YSZ showed BaZrO3 formation which grows over time at • 900°C to form a dense and continuous layer. No distinct microstructure difference between ageing in air or reducing/humid environment.
- Tensile testing showed strong bonding of candidate composite glasses to YSZ while YSZ fiberreinforcement resulted in a slightly greater strength, due to higher elasticity and toughness. Bond strength showed a small reduction after 900°C/500h ageing in air or reducing environment.
- Composite glass validation testing in a mini-tube reactor under dual environment is underway.



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- Pacific Northwest National Laboratory is operated by Battelle Memorial Institute for the U.S. Dept. of Energy



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Thank you

