

Paulsson, Inc. (PI)

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Development of an Optical Based Single Well Seismic System (OSWS) for Improved CCUS, UGS+H2, EGS & EEOR Characterization and Subsurface Monitoring (SC0018613)

DOE 2022 Resource Sustainability Project Review Meeting October 25, 2022





Single Well Seismic Project – DE-SC0018613



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Survey and Monitoring Markets (>\$2T) for Single Well Seismic Technology and Fiber Optic Seismic Vector Sensors (FOSVS)

- Carbon Capture Usage and Storage (CCUS)
 - >14,000 wells to be drilled before 2050
- Underground Gas Storage (UGS: NG, NG+H2, H2)
 - >\$750 Billion market by 2026
- Enhanced Geothermal Systems (EGS)
 - EGS Potential: 2,300GW = 2X Current Electric Produc.
- Cleaner Enhanced Oil & Gas Recovery (CEOR)
 - We currently leave 65% behind in known location
- Nuclear Energy generate and store Green H2
- Wind Energy Installations (WEI OWCal) store Green H2



Single Well Seismic Presentation

- Optical Sensors
 - Optical Accelerometers: DE-FE0024360
- Borehole Seismic Sources: DE-SC0018613
- Applications & Examples



Strengths of

Fiber Optic Seismic Vector Sensors (FOSVS)

- Long term stability: 30-year MTBF by the Navy
- Very large bandwidth: 5 Hz 14,000 Hz
- Extremely sensitive: 100X a geophone
- Outstanding Vector Fidelity: (80 dB)
- Very High Temperature Tolerant: >320°C (700°C)

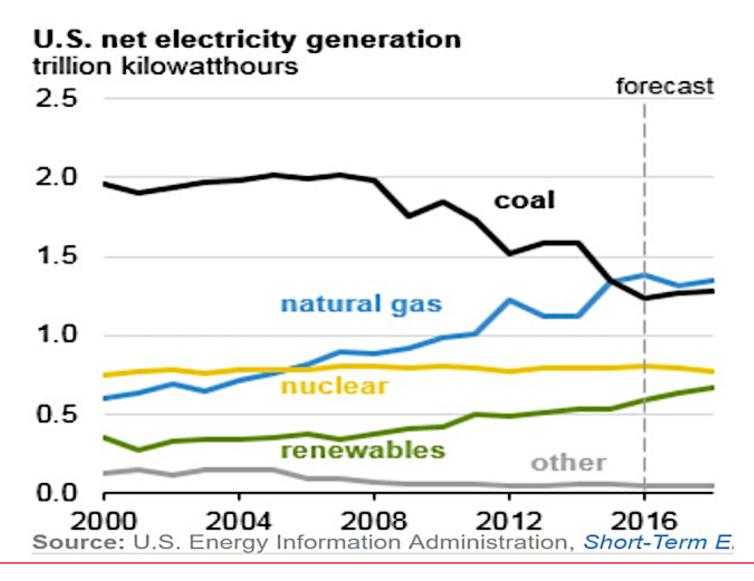
Intrinsically Safe and Very Robust



CCUS is ESSENTIAL to Maintain the USA Oil Production! Current UOG Recovery is 5-8% of OOIP at a cost of \$120 Billion for the 20,000 wells drilled/year. Effective and Monitored CCUS will Double Our Oil **Production & Maintaining our Energy Independence!** U.S. crude oil production (Jan 2005-Nov 2017) eia million barrels per day 12 10 8 tight formation production 6 4 other production 2 n 2005 2008 2009 2010 2011 2012 2013 2014 2015 2016 2017 2007 2006Source: U.S. Energy Information Administration, Petroleum Supply Monthly and Tight Oil Production Estimates by Play



Natural Gas Is Critical For Electricity Generation





High Resolution is Critical Effective CCUS

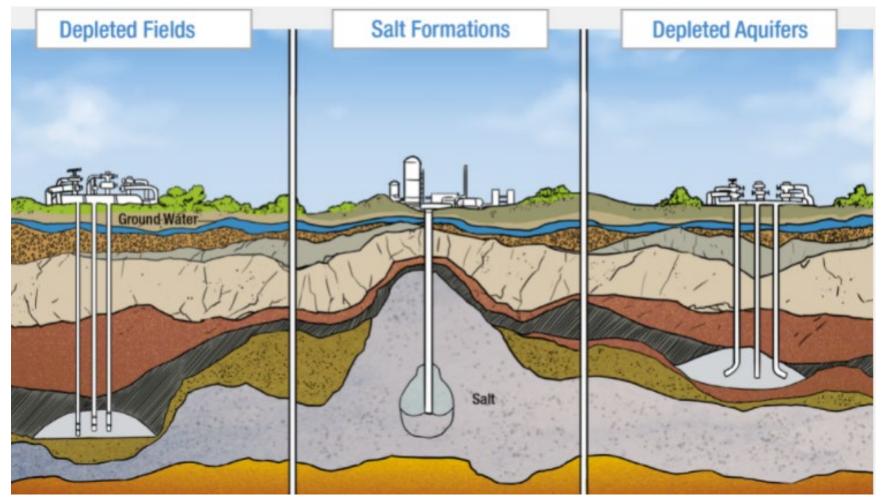
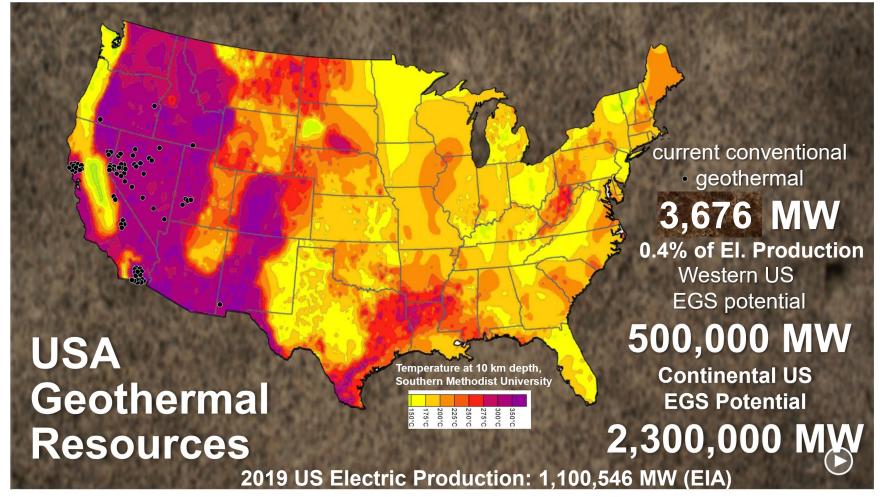


Figure from API showing three applications for improved imaging and monitoring for CCS and UGS applications. From <u>https://energyinfrastructure.org/energy-101/natural-gas-storage</u>.

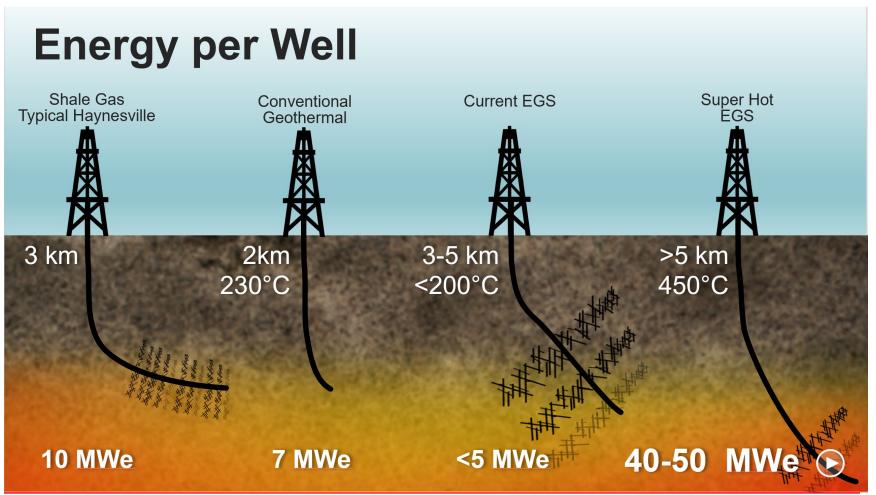


Geothermal Energy has huge potential but current deployment only "Scratches the Surface" - Enhanced Geothermal System (EGS) potential is 625 X Current Production (4GW) or 2,300GW (New Offshore Wind California 1st step is 4GW)





Geothermal Energy Development Requires High Resolution Imaging and Monitoring of the EGS Power Generation to make it Effective!





To Produce Clean Electric Power X **Effective Enhanced Oil & Gas (EEOG)** we must **Develop High-Resolution Subsurface Imaging & Monitoring**



Borehole Seismic Source Technologies

- Fluid Coupled Borehole Sources All couple-in <5% of the source energy into seismic waves. >95% of the Energy Generate Tube waves.
 - Airgun: Powerful but Destructive to the Cement
 - Sparker: Non-Destructive but not enough Power
 - Piezo Electric: Non-Destructive but not enough Power
 - Dynamite: Powerful but Destructive to the Cement
 - Fluid Coupled Vibrators: Narrow Band & Highly Resonant
 - All Generate STRONG TUBE WAVES!!
- <u>Clamped Borehole Sources</u> Couple in >95% of the source energy into seismic waves.
 - Hydraulic Vibrators: Powerful + Broadband but Complex
 - Piezo Electric & Magneto Strictive Vibrators: Non-Destructive, Broad Band, 3C
 - NO TUBE WAVES



Single Well Seismic Technology

- Borehole Vibratory Source Under Development:

 Magneto Strictive Actuator
 3C Source Technology
 >250°C (>482°F) capable
 Operate in Vertical and Horizontal Boreholes
- Borehole Seismic Receivers Developed and Fielded

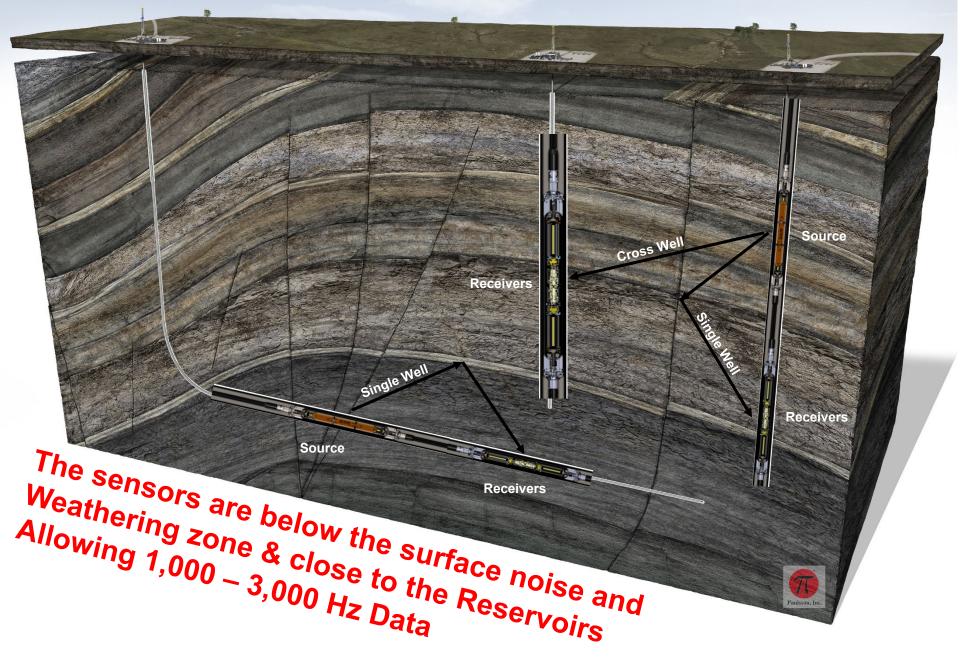
 All Optical Vector 3C Clamped Receivers
 Combined with large aperture Rayleigh DAS
 Tested at 320°C (608°F) for a week!
 Operate in Vertical and Horizontal Boreholes



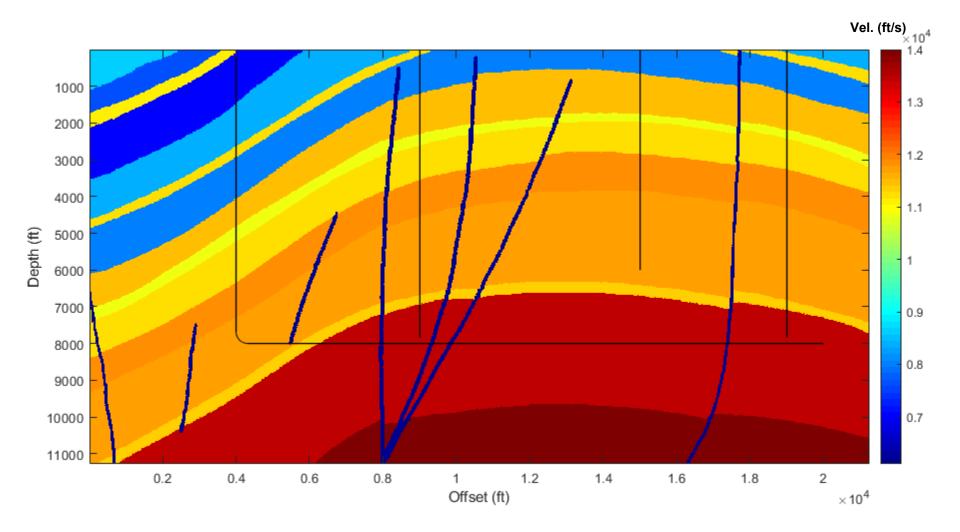
Single Well Seismic Modeling



Single Well Seismic Imaging of Faults and Geology

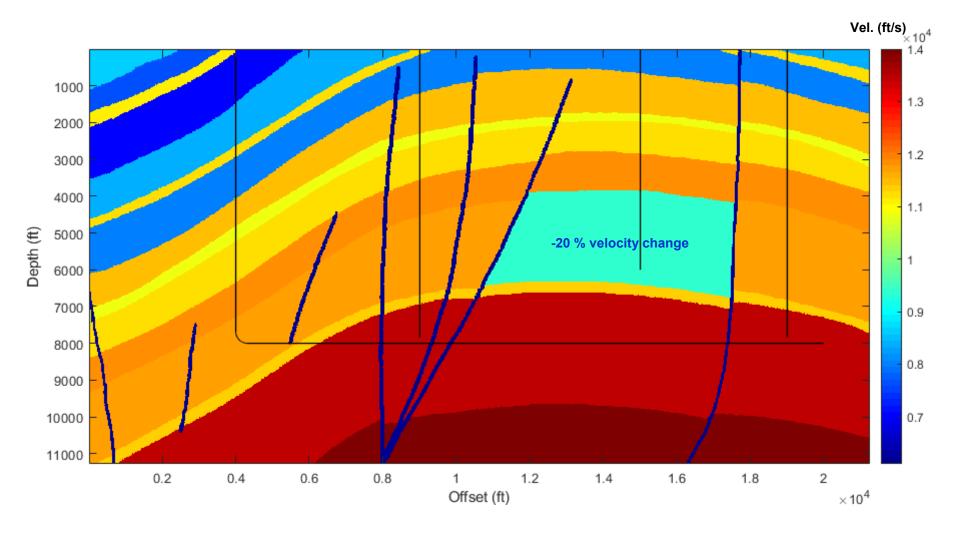


Initial Velocity Model before Fluid Injection



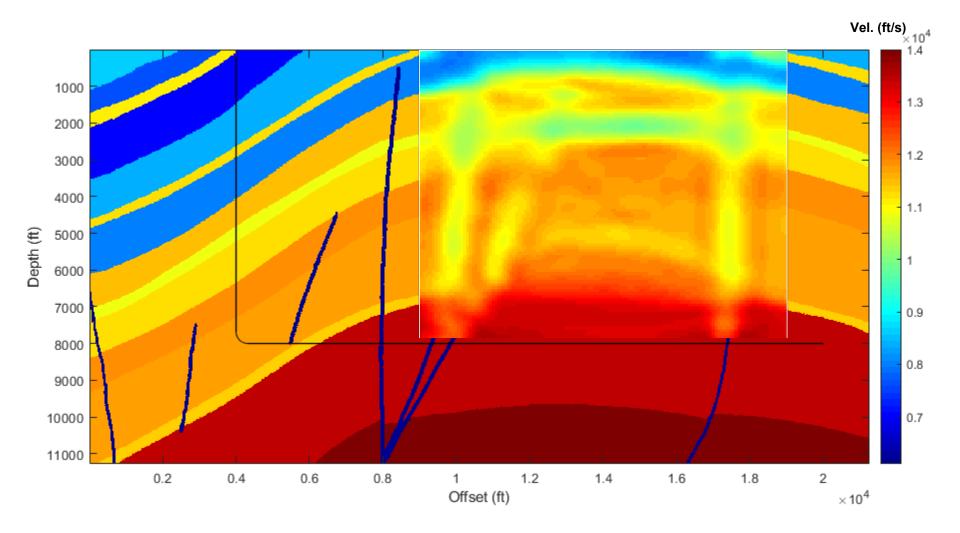


Velocity Model after Fluid Injection



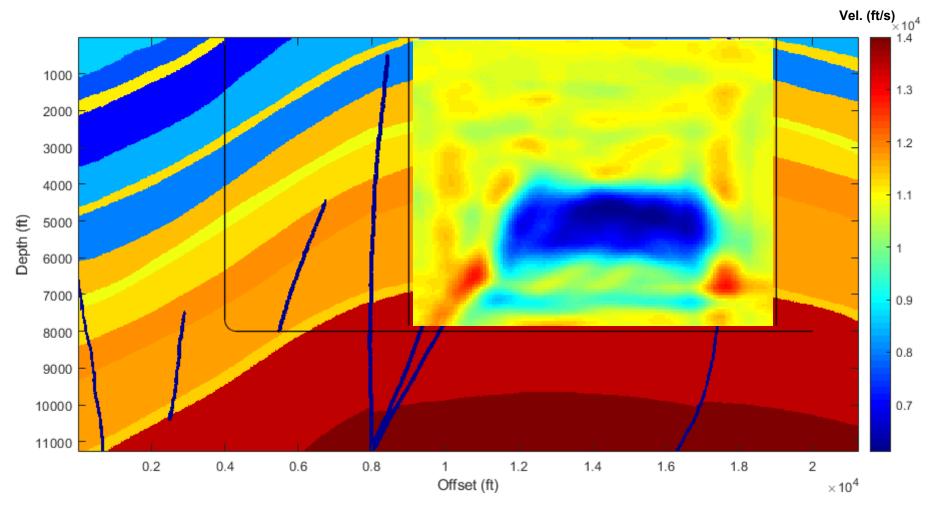


Initial Tomogram before Fluid Injection



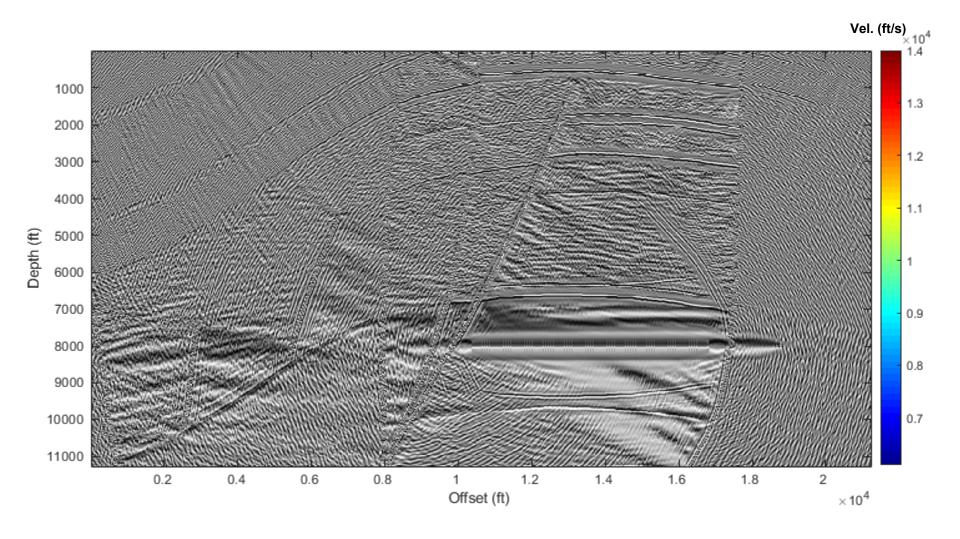


Time-Lapse Tomogram Change from Initial to after Fluid Injection



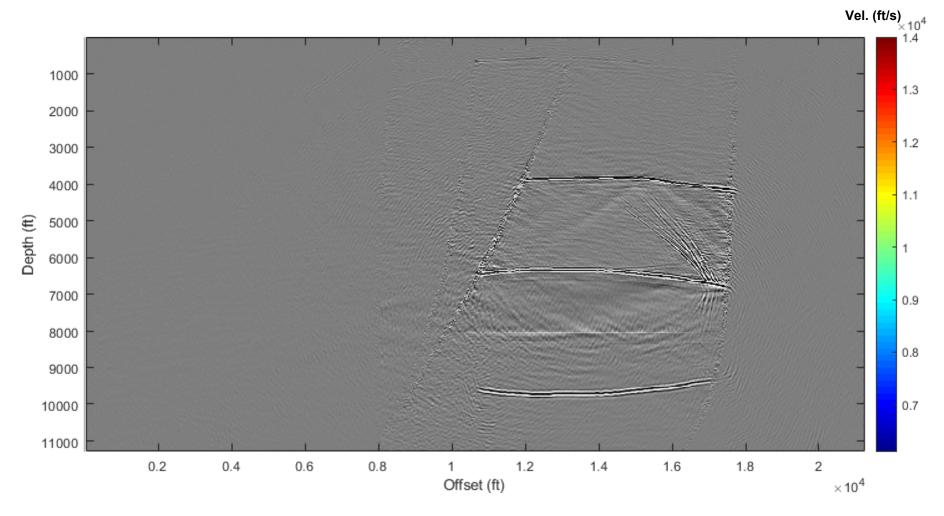


Initial Reverse Time Migration (RTM) before Fluid Injection





Time-Lapse RTM Change from Initial to Fluid Injection

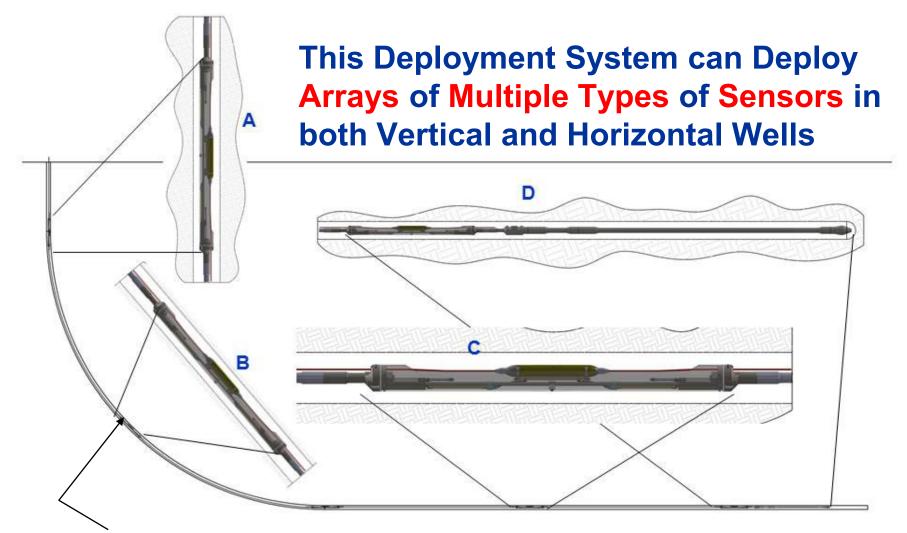




A Single Well Seismic System has two main components: **1. Receivers** 2. Sources



Drill Pipe Deployed System – Housing and Clamping



Clamping system operates by increasing the pressure inside the drill pipe and manifolds using the borehole fluid as the pressurized medium



Fiber Optic Seismic Sensor Deployment System (4th) Battelle, Michigan June 2016 – Also for Single Well



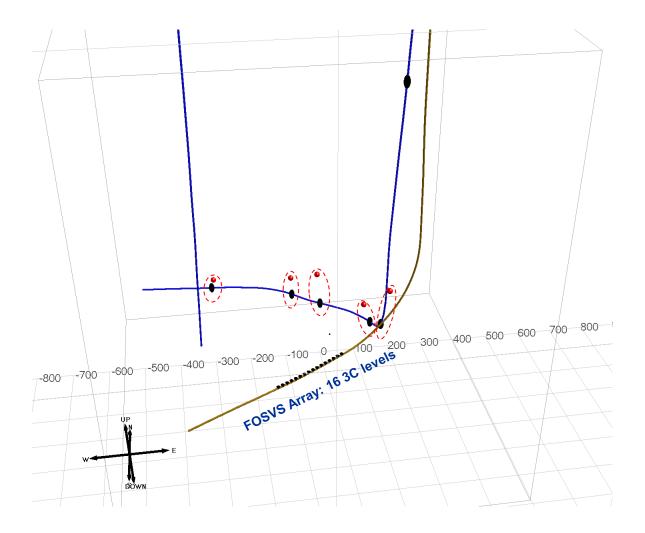
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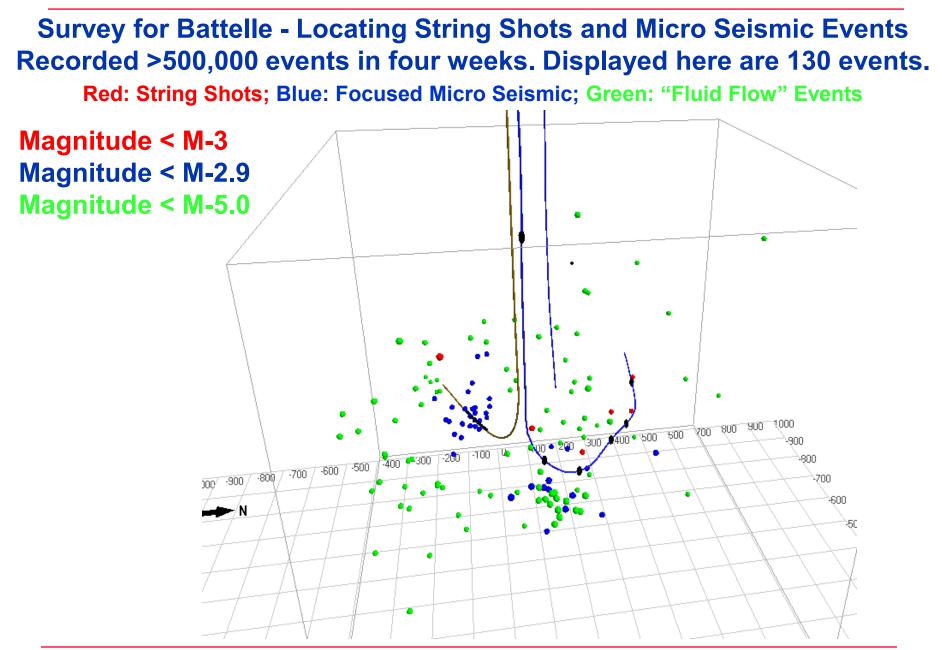
Monitor Fluid Injection: Field Data Recorded with Fiber Optic Seismic Vector Sensor (FOSVS)™ System



Results from Locating 0.5 gram String Shots During a Survey Recorded for Battelle in June 2016

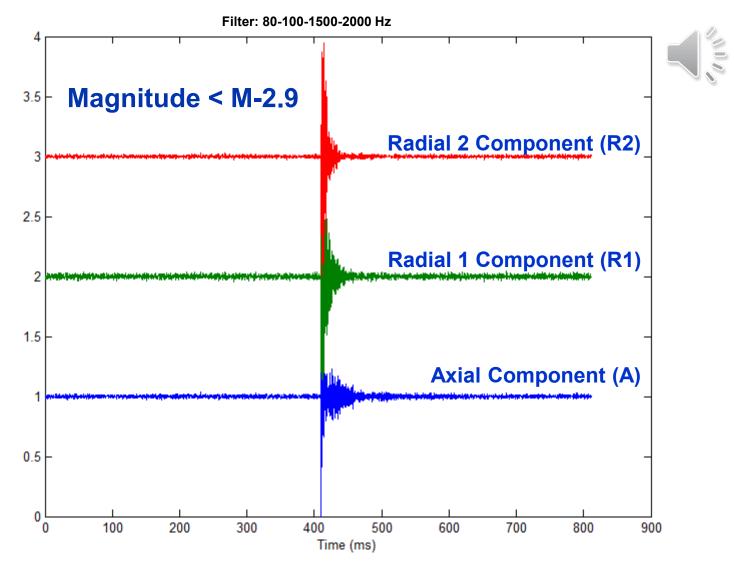






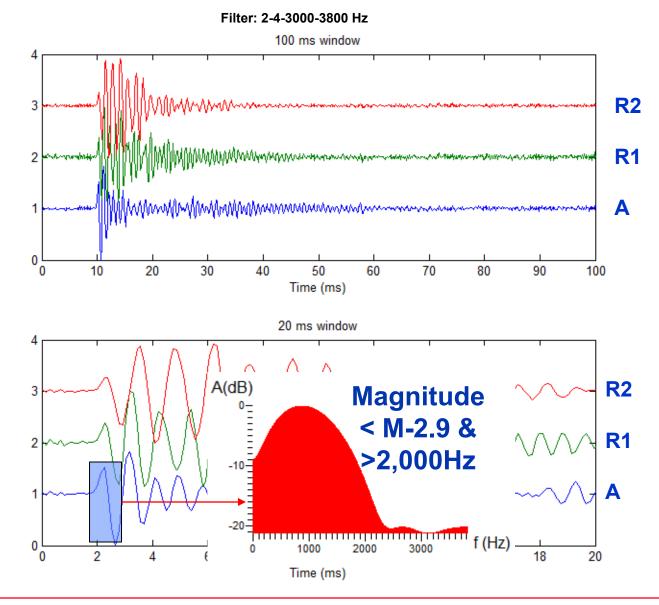


Sound of A Focused MS in 3C, Survey for Battelle, June 2016



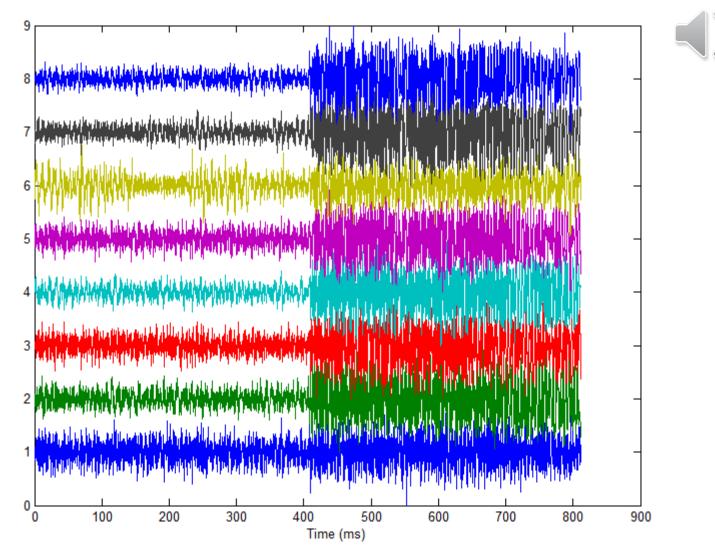


Zoomed-In Focused MS in 3C- Filter: 2-4-3000-3800 Hz



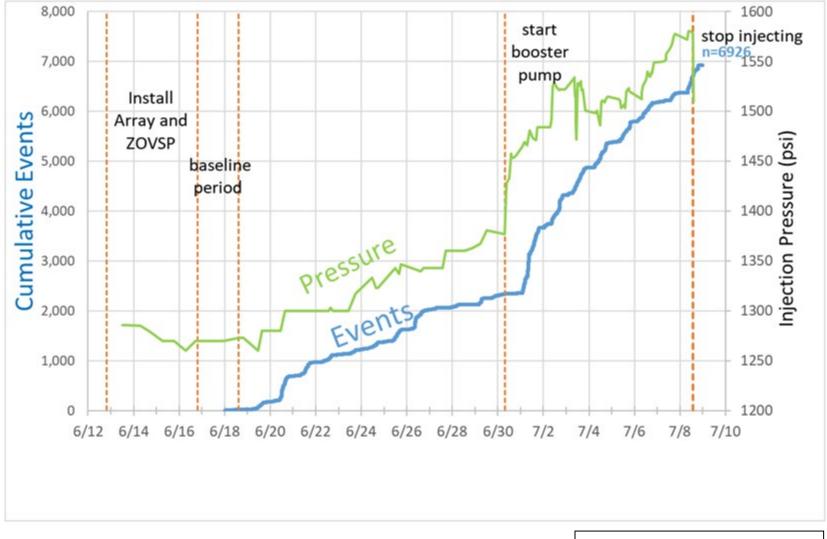


Sound of A Long Duration Event (~M-5.0) –Fluid Flow

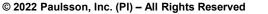




Micro Seismic Events as Function of Injected Fluid Pressure

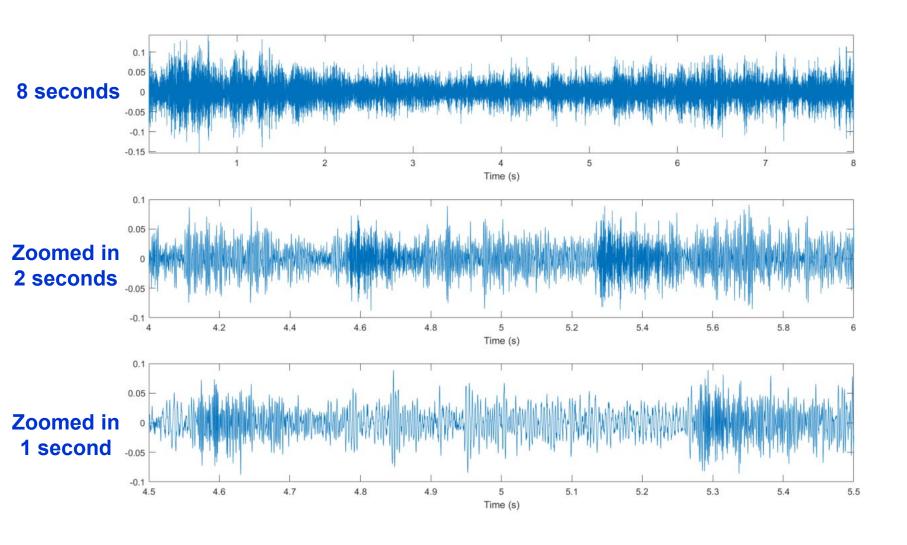


Courtesy Mark Kelley, Battelle, 2019





We looked for Analogs: Cardiac Blood Flow



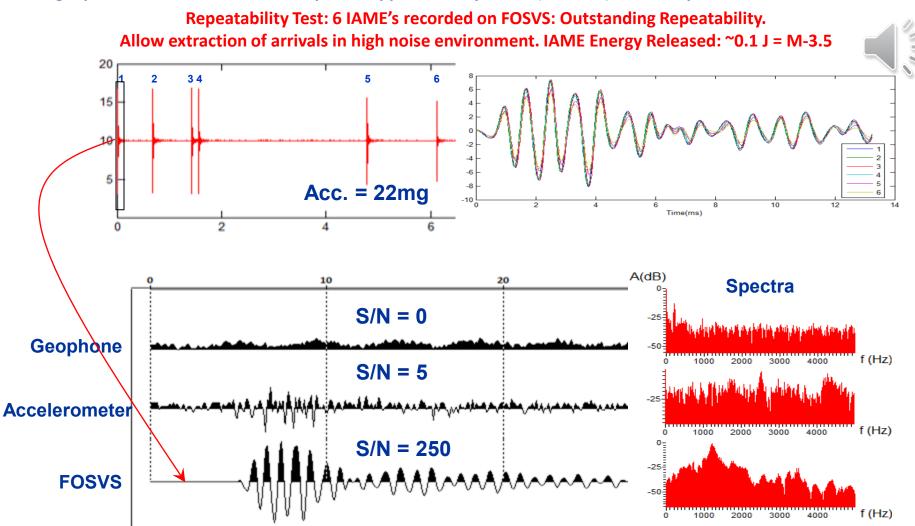


Laboratory Test of Fiber Optic Seismic Vector Sensors



Test of Fiber Optic Seismic Vector Sensors (FOSVS) & IAME

Pressure cell and sensor plate placed on a metal plate sitting on a foam mat on a metal table. Fiber sensor, geophone and accelerometer are placed approximately 20 cm (8 inches) from the pressure vessel with IAMEs





Can You Hear a Pin Drop? Test Object: OD: 0.011", 2" long, 24.8 mg

Pin Dropped 1 cm: 20% of the Pin Length

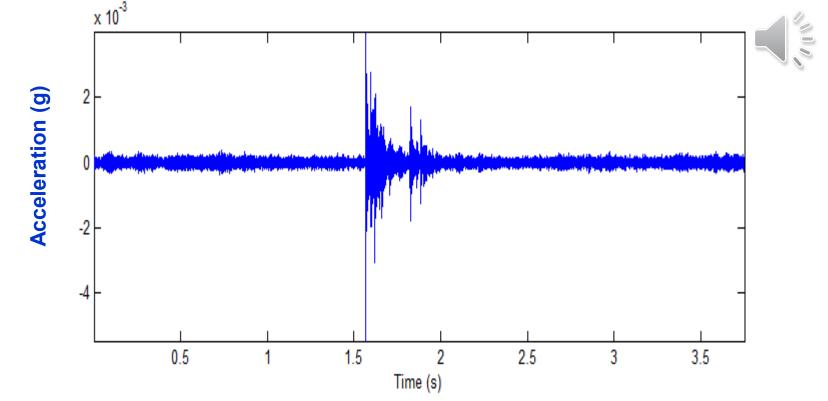




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FOSVS Test: OD: 0.011", 24.8 mg Pin Drop 1 cm:

2.5 µJ kinetic energy (M-7) for 1st of 8 hits of Pin

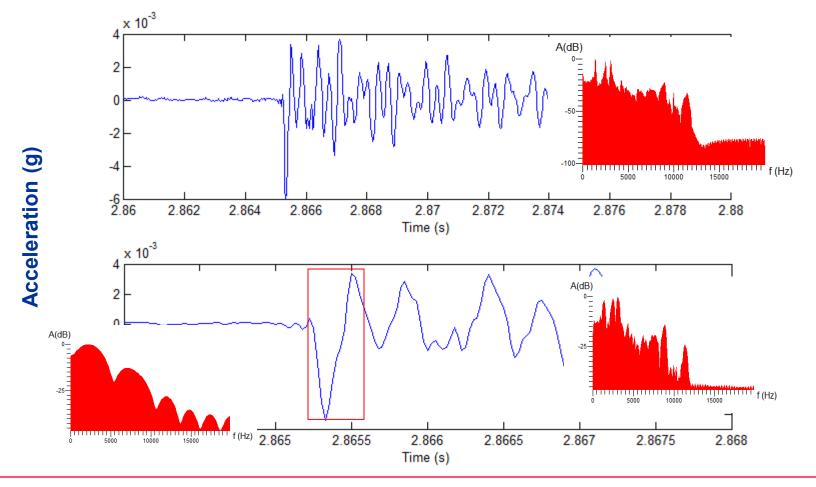


The FOSVS recorded ~17 bounces of the pin = <<M-7



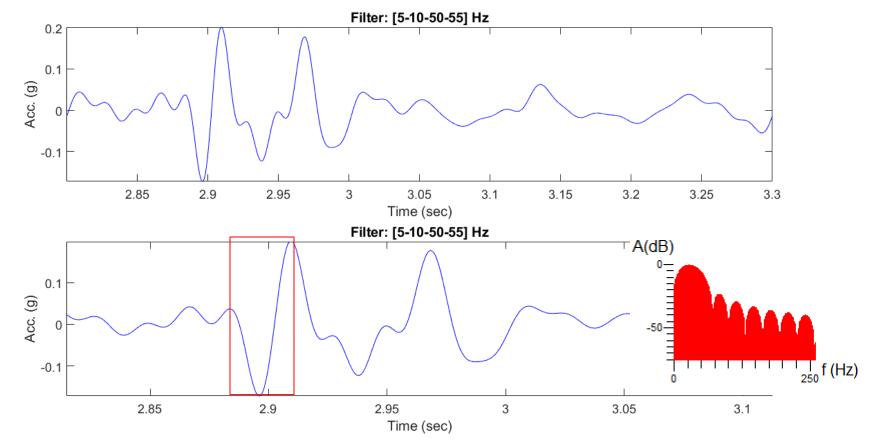
FOSVS Test: OD: 0.011", 24.8 mg Pin Drop 1 cm:

2.5 µJ kinetic energy (M-7) for 1st of 8 hits of Pin



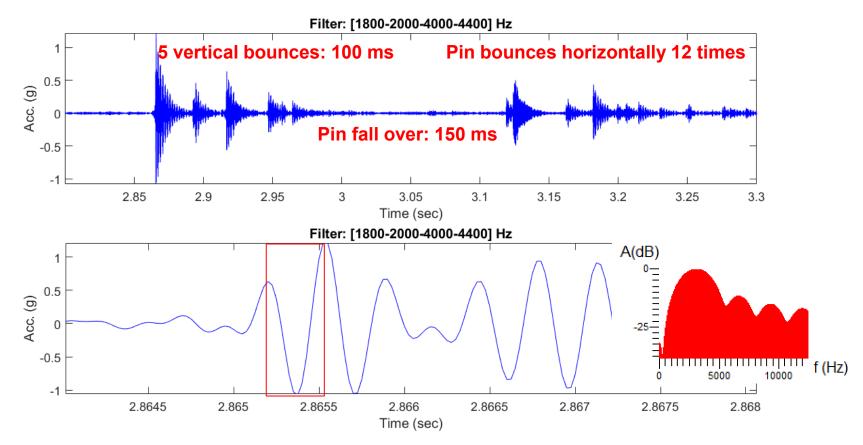


FOSVS Test: OD: 0.011", 24.8 mg Pin Drop 1 cm: 2.5 μJ kinetic energy (M-7) on primary drop Ormsby Filter: 5-10-50-55 Hz (LOW FREQUENCY)



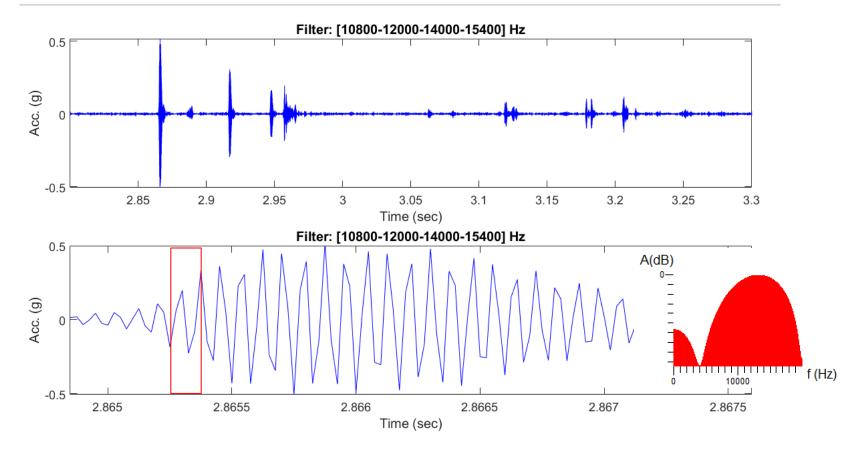


FOSVS Test: OD: 0.011", 24.8 mg Pin Drop 1 cm: 2.5 μJ kinetic energy (Primary: M-7, Bounces: M-8) Ormsby Filter: 1,800-2,000-4,000-4,400 Hz





FOSVS Test: OD: 0.011", 24.8 mg Pin Drop 1 cm: 2.5 µJ kinetic energy (Primary: M-7, Bounces: M-8) Ormsby Filter: 10.8-12-14-15.4 kHz (HIGH FREQ.)





Downhole Seismic Source for Single Well Seismic Tool

DE-SC0018613



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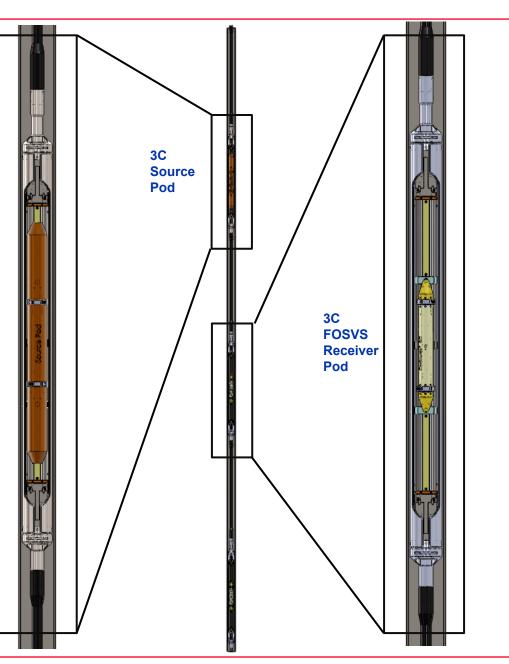
- By placing the Receivers in the borehole, we get 2 – 10 the resolution compared with surface seismic!
- By placing both the source and the receivers we should get much better than 10 times (20-30) the resolution!



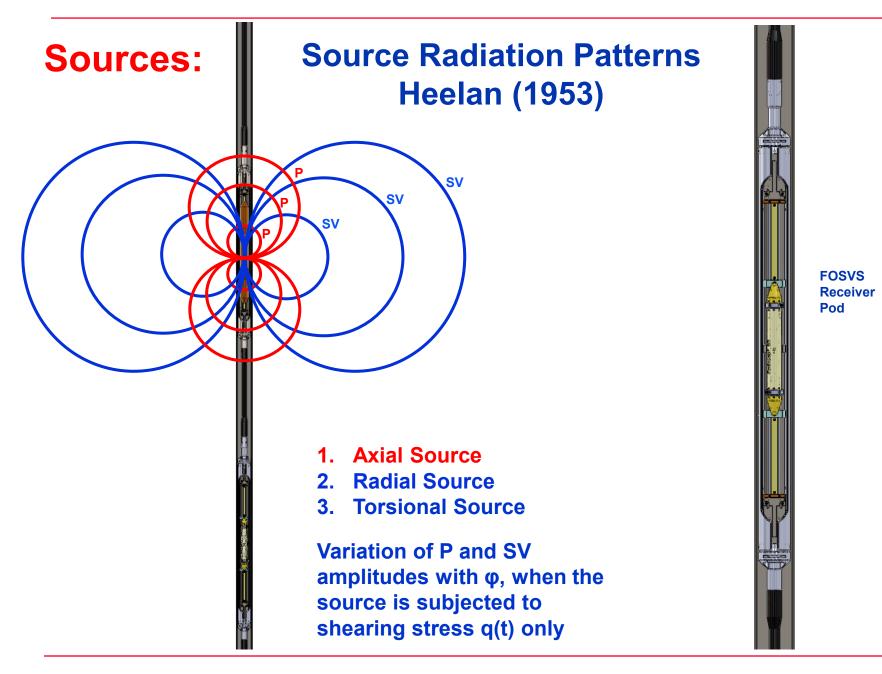
A Single Well Seismic System: Deploying the Source and the Receivers in the same well.

This is NOT a well Logging System – this is a Seismic System with a 10 – 3,200 Hz Operating Frequency.

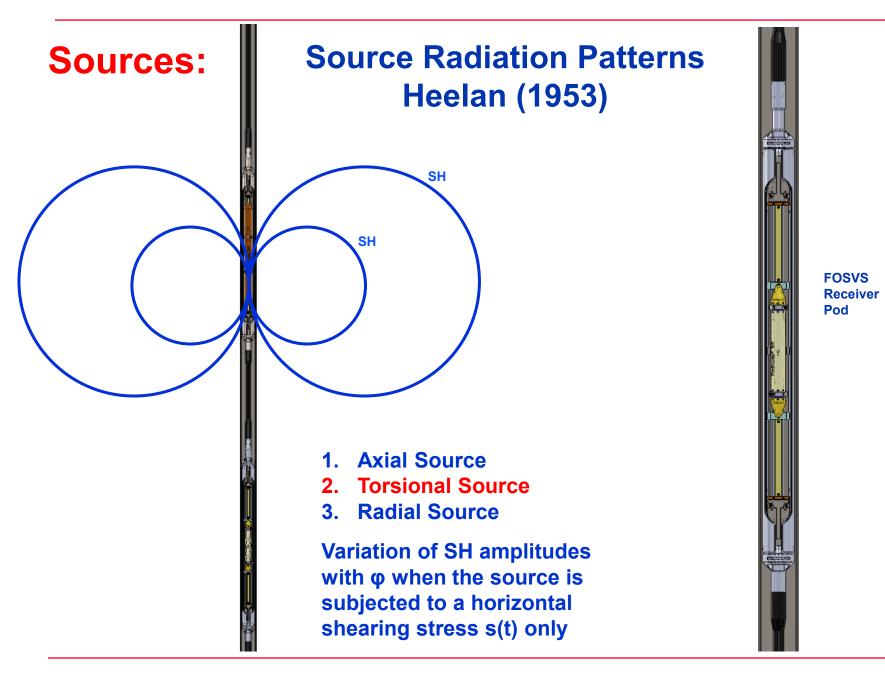
This system will be able to image to a radius of >1,000 m (3,000 ft) – Q dependent of course.



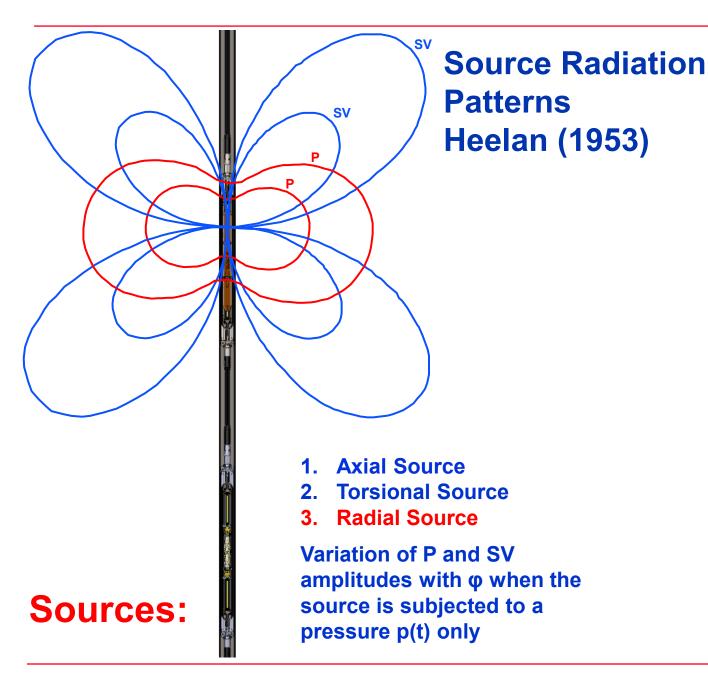










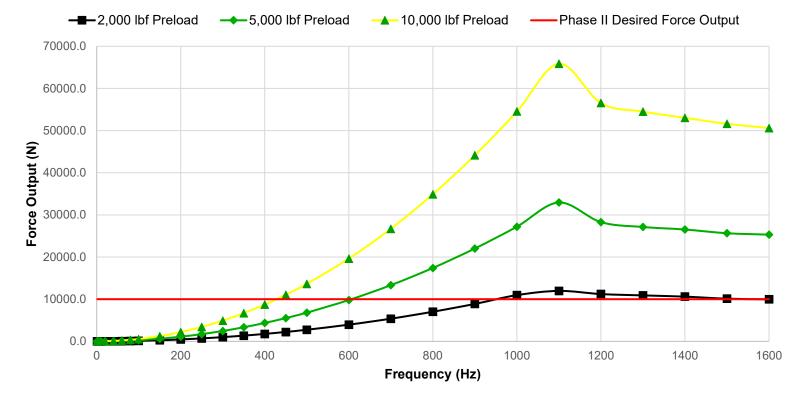


FOSVS Receiver Pod



Task 1: Preliminary Model and Lab Test Results

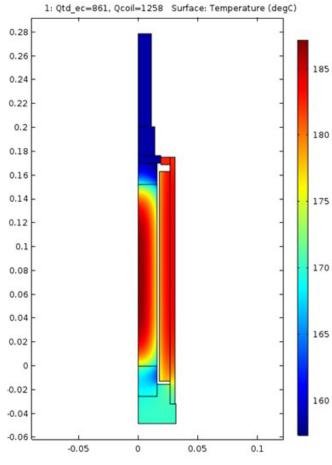
Force Output vs. Frequency For 6" Terfenol Rod and 20Kg Moving Mass – providing >10,000 lbs. Force



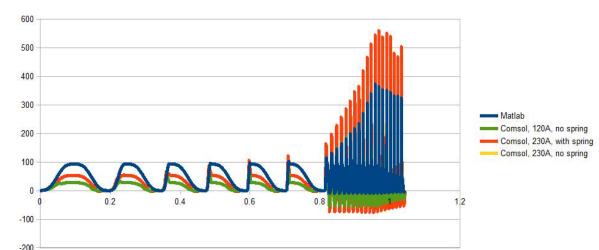
Preload has a big effect on force output. Generally, higher preload = higher force output.



Task 3: Finite Element Analyses (FEA) Using Multi-Physics By Comsol



Temperature distribution for 120 ampere peak input with turbulent flow force convection cooling.



Comparison of voltage predictions between analytical MATLAB model and Comsol finite element analysis for –9,817 lbf compression preload. Horizontal axis is time in seconds, vertical axis is voltage in volts.

| Table II. Total actuator heat losses. | | | | | | | | | | | |
|------------------------------------------|-------------|-------|-------------|---------------|-------------------|-------|--|--|--|--|--|
| Current, Amperes, Dissipated Heat, Watts | | | | | | | | | | | |
| <u>Preload</u> | <u>Peak</u> | RMS | <u>Coil</u> | Eddy (10 Lam) | <u>Hysteresis</u> | Total | | | | | |
| _2,000 psi | 57 | 35.8 | 476 | 235 | 16 | 968 | | | | | |
| –8,000 psi | 120 | 75.6 | 2,116 | 861 | 16 | 2,993 | | | | | |
| _8,000 psi | 230 | 144.9 | 7,773 | 1,786 | 16 | 9,575 | | | | | |



Heat Dissipation by Eddy Current for Different Laminations

The Multi-Physics simulation by Comsol showed large heat dissipation with the original design. The simulation exposed the primary heat source as the wire coils and the secondary heat source as the Terfenol rod.

The table below shows by increasing the number of laminations of the Terfenol rod the heat dissipated in Watts produced by the rod dramatically decreases. This is because the increase in lamination reduces the eddy current losses.

More so, reducing the eddy current losses of the rod reduces the power loss of the rod. The decrease in power loss boosts the systems efficiency and therefor minimizes power requirement of the downhole source. This allows for the reduction of the current to the wire coils.

Thereby increasing the number of laminations, the system requires less power by <u>both</u> the primary heat source of the wire coil and the secondary heat source of the Terfenol rod, minimizing overall heat generation.

Assume the preload case is -8,000 psi @ 230 amps (worst case)

| frequency | _ | - | | 10 | 42 | 45 | 20 | |
|-----------|---------|--------|--------|--------|--------|--------|-------|-------|
| (Hz) | 3 | 5 | 8 | 10 | 12 | 15 | 20 | 40 |
| | | | | | | | | |
| 1600 | 11,023 | 5,650 | 2,556 | 1,786 | 1,154 | 739 | 416 | 104 |
| | | | | | | | | |
| 3200 | 44,092 | 22,600 | 10,224 | 7,144 | 4,596 | 2,951 | 1,662 | 414 |
| | | | | | | | | |
| 6400 | 176,368 | 90,400 | 40,896 | 28,576 | 18,092 | 11,725 | 6,635 | 1,657 |

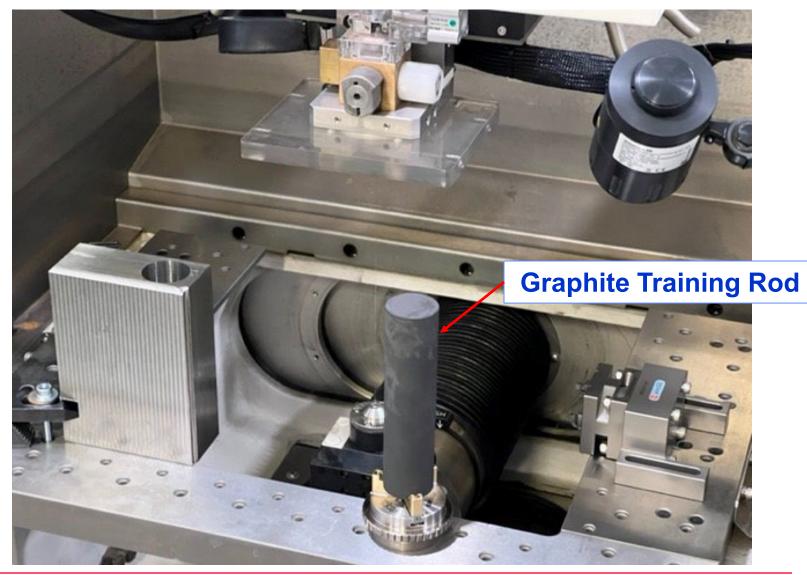
Heat Dissipated in Watts by Number of Laminations





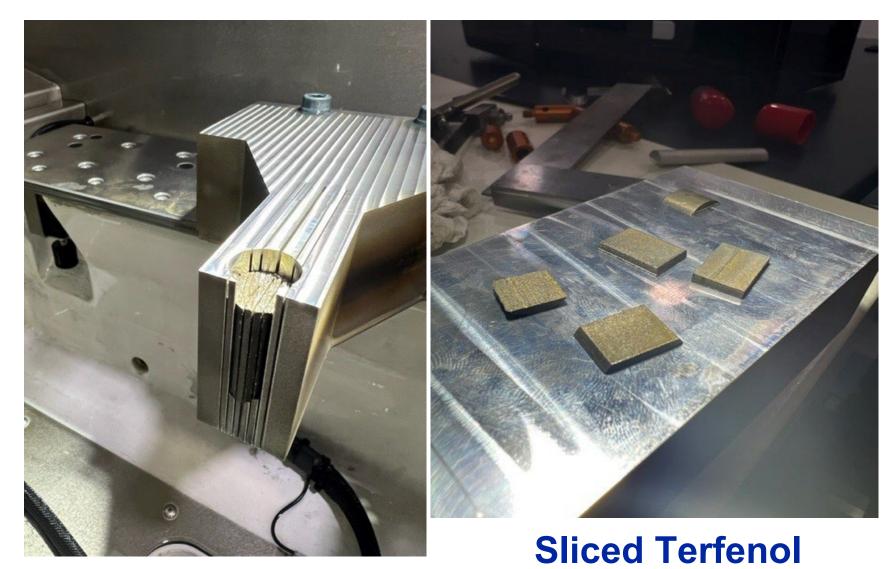


Current EDM set up and fixture system





Second generation EDM fixture system and set up





Single Well Seismic Source



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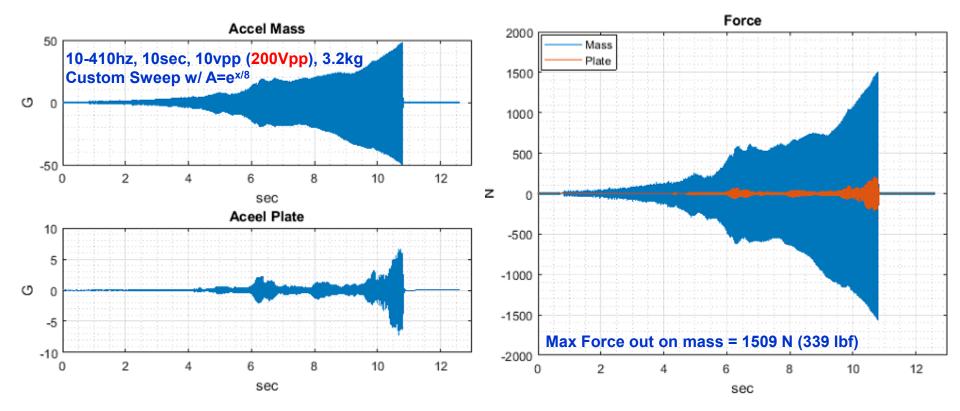
Laboratory and Small Scale Field Tests of Axial Vibrator Unit Developed under a US DOE Grant



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Laboratory test of a Downhole Seismic Vibrator The Maximum Force: 10 – 410 Hz was 1,509 N/339 lbf





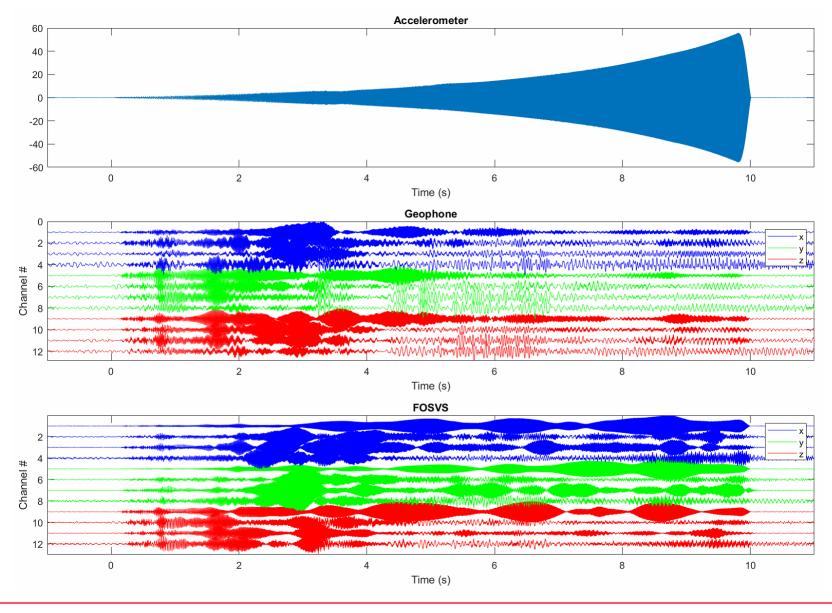
Source and Receiver On-Ground Experiment

- Sources:
 - 1. Impulsive source (The Piston): 50 kg (110 lbs..). ~60 g measured acceleration at impact.
 - 6,744 lbs. Force 20X the vibratory source
 - 2. Vibratory Axial Source: 10-410 Hz, 10 sec, 13.6 Vpp drive, Custom Sweeps.
 - 339 lbs. Force SAME S/N AS IMPULSIVE SOURCE
- Receivers:
 - 1. Geophone: 4 kHz sampling rate, 5ft, 15ft, 25ft, 35 ft offsets displayed
 - 2. FOSVS: 80 kHz sampling rate, 5ft, 15ft, 25ft, 35 ft offsets
 - 3. Mass and Baseplate Monitoring: VR Accelerometer: 75 kHz rate
- Processing:
 - 1. All data filtered with 5-10-410-500 Hz Ormsby filter
 - 2. All vibrator data correlated with custom correlation function to flatten spectrum.



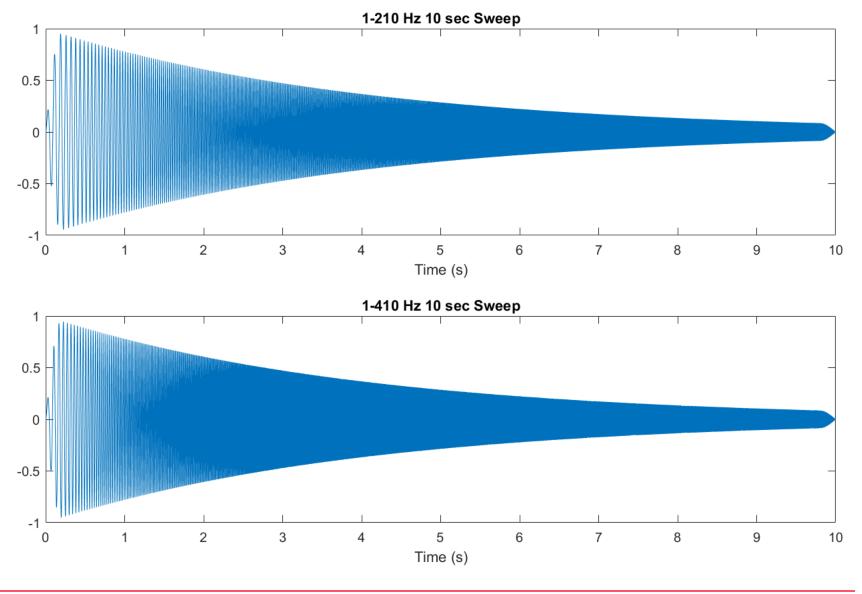
Test Fixture for a Downhole Seismic Vibrator: Actuator is the size of two soda cans 10-410hz, 10sec, 10vpp (200Vpp), 3.2kg, F=40 lbs. Custom Sweep w/ A=e^{x/8} Weight drop: 50 kg @ 60g

Vibrator Uncorrelated Data: 10-410 Hz, 10 sec sweep, 13.6 Vpp drive



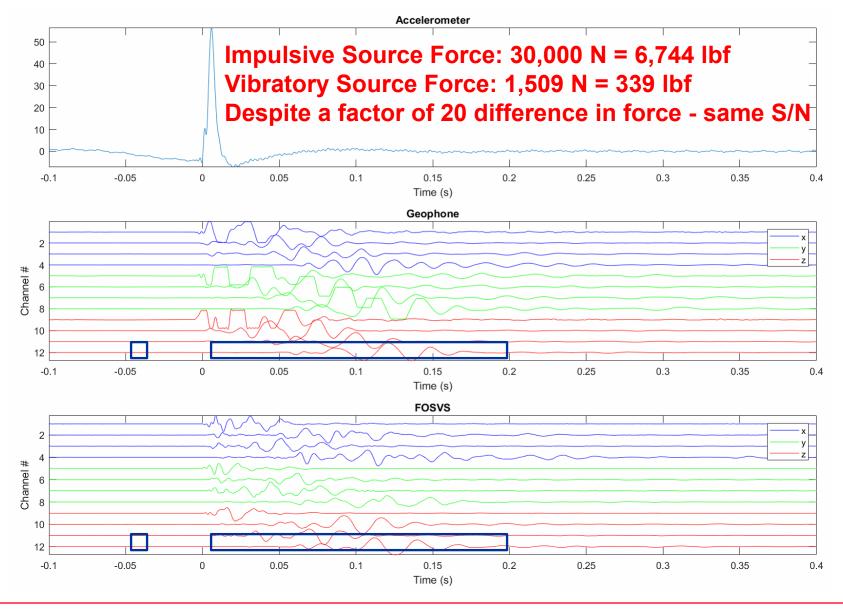


Theoretical 10 Second Sweeps used for Correlation - Case 4



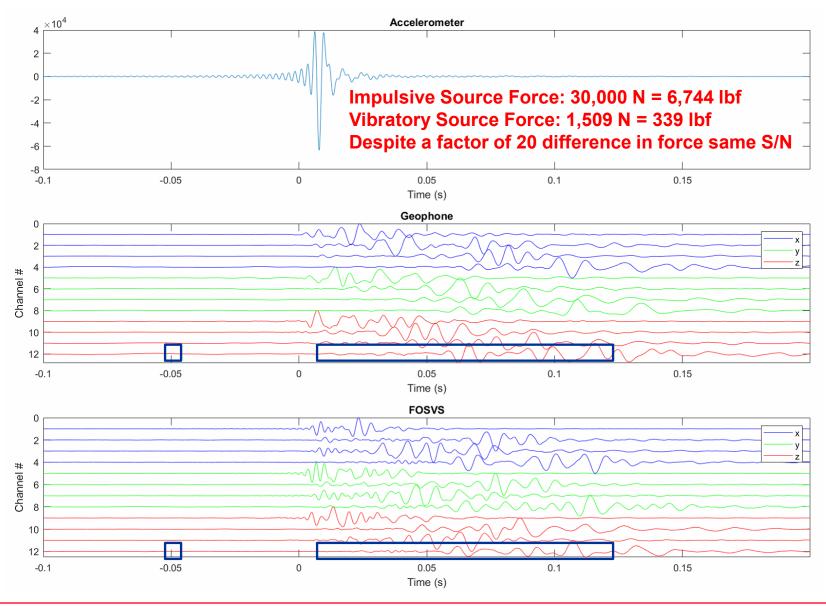


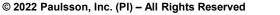
Impulsive Source: 50 kg (110 lbs..) @ 60g. Hit Data – Zoomed In





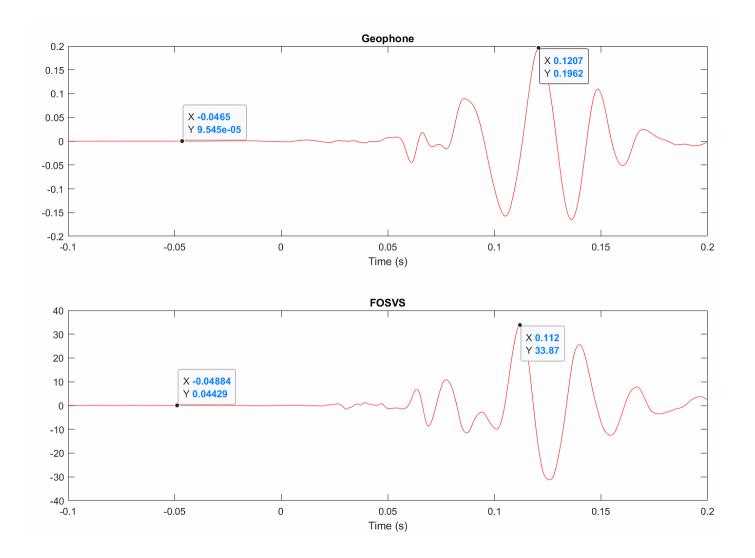
Vibrator Correlated Data: 10-410 Hz, 10 sec, 13.6 Vpp - Case 4





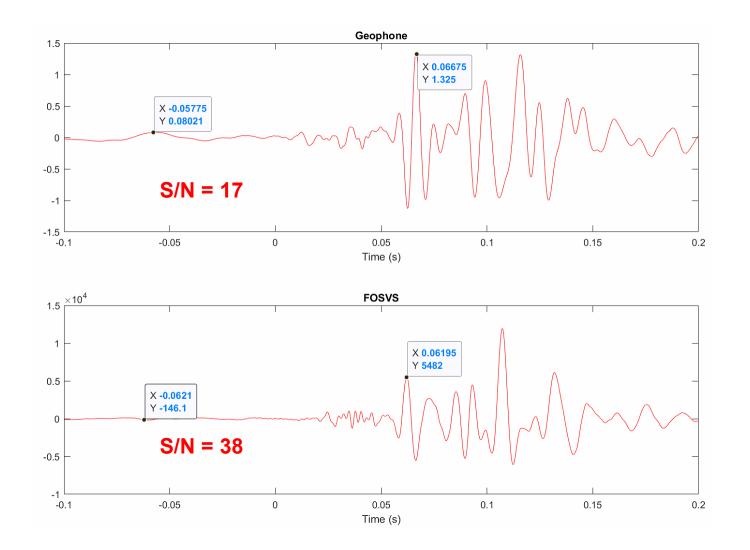


Impulsive Source: 50 kg (110 lbs..) @ 60g. Hit Data – Zoomed In

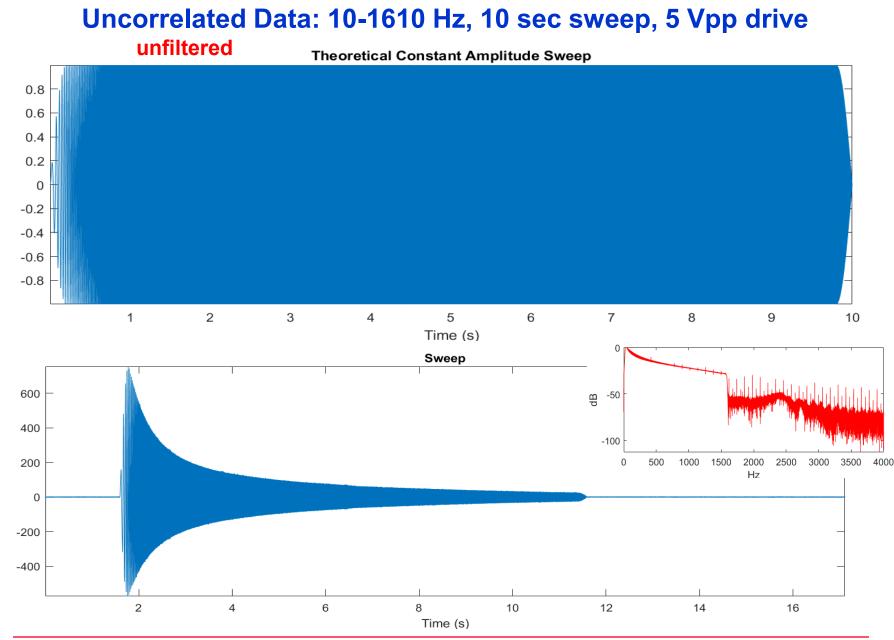




Vibrator Correlated Data: 10-410 Hz, 10 sec sweep, 13.6 Vpp drive - Case 4

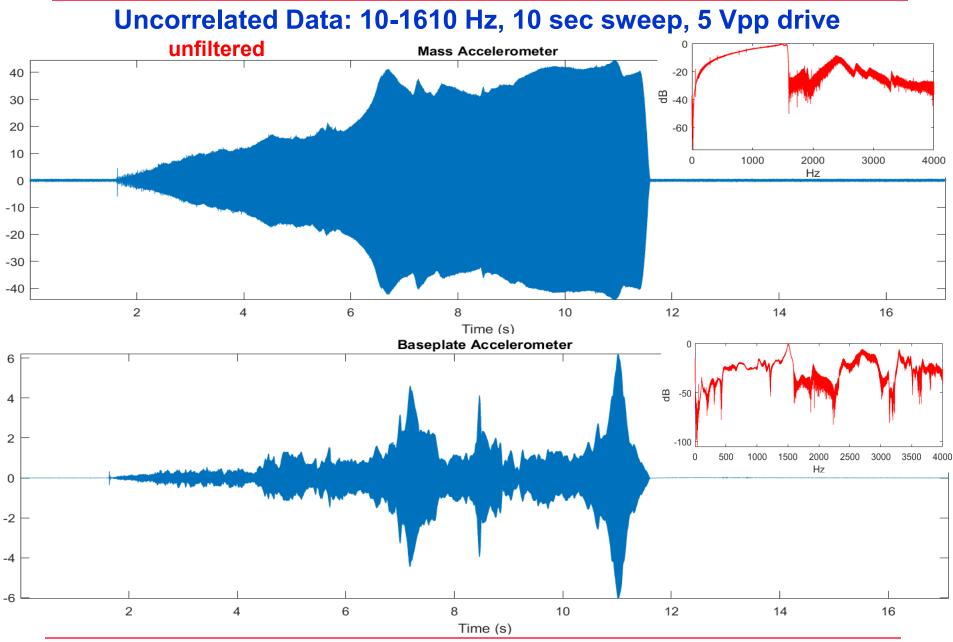




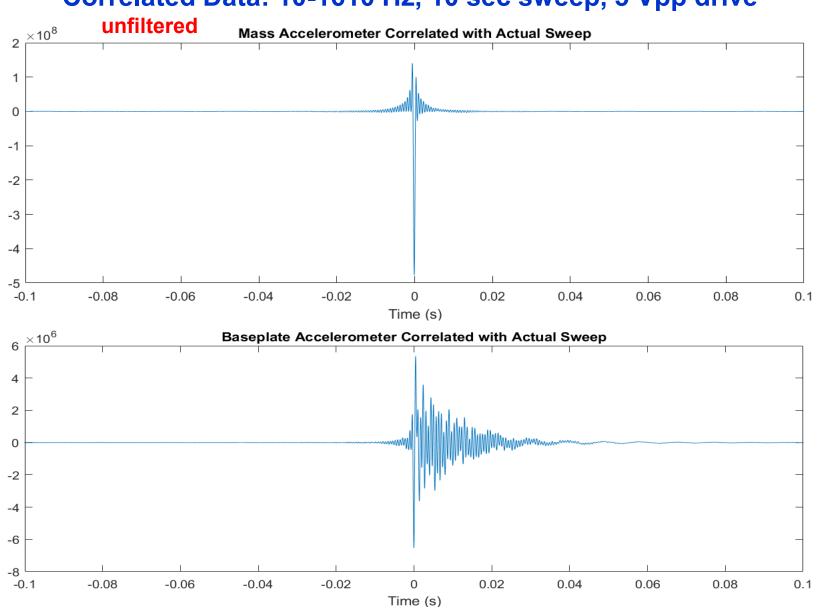


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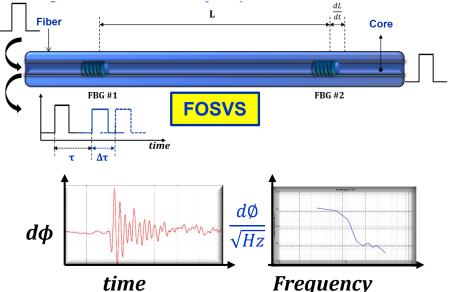
Correlated Data: 10-1610 Hz, 10 sec sweep, 5 Vpp drive

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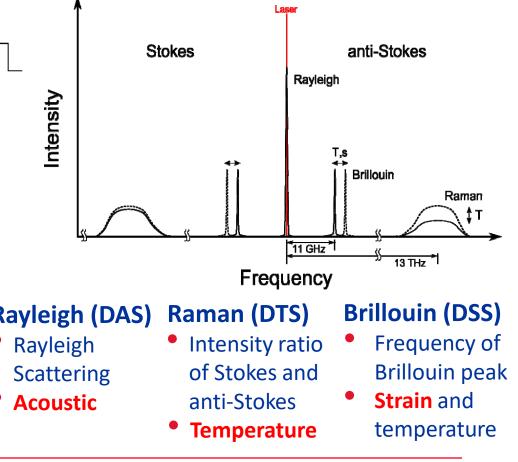


Several All-Optical Sensors are Part of Our Borehole System

DOE supported Paulsson Point Sensors include: Accelerometers, Hydrophones & Pressure Sensors.



Distributed Fiber Optic Sensor Technologies for Acoustic, Strain & Temperature measurements.



Interferometric Sensing

Two FBGs: Measure phase changes/time between two laser reflections from the two FBG's

Rayleigh (DAS)



Summary

- To Image Geology in high enough resolution to guide injection of CCUS, UGS+H2, EGS, EEOR to we must use 3D/3C borehole seismic technology. This requires:
 - Large arrays of 3C seismic sensors
 - High frequency Borehole VibroSeis units
 - Accurate real-time on-site processing & imaging

- To Monitor CCUS, UGS+H2, EGS, EEOR production we need to use high frequency sensors that can record 2,000 – 8,000 Hz at M-5 to M-7 magnitudes
 - Fiber Optic Seismic Vector Sensors (FOSVS)



Acknowledgement

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 - DOE Contract DE-FE0004522 (2010)
 - RPSEA Contract 09121-3700-02 (2011)
 - DOE Contract DE-EE0005509 (2012)



- California Energy Commission Contract GEO-14-001 (2013)
- DOE Contract DE-FE0024360 (2014)
- DOE SBIR II Grants DE-SC0017222 & DE-SC0017729 (2018)
- DOE SBIR II Grant DE-SC0018613 (2018) Downhole Source

The support and assistance from these grants made it possible to develop the fiber optic sensor and deployment technologies described in this presentation. The support from Karen Kluger for DE-FE0004522, Bill Head for RPSEA Contract 09121-3700-2, Bill Vandermeer for DE-EE0005509, Cheryl Closson for GEO-14-001 and Bill Fincham for DE-FE0024360 and SBIR Grants DE-SC0017222/17729/18613 is gratefully acknowledged.



Thank You!

For questions please contact Björn Paulsson via e-mail: <u>bjorn.paulsson@paulsson.com</u> or Mobile: +1-310-780-2219



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