

A GENERAL DRAG MODEL FOR ASSEMBLIES OF NON-SPHERICAL PARTICLES CREATED WITH ARTIFICIAL NEURAL NETWORKS

SUBTITLE: PREDICTION OF THE FLOW DYNAMICS OF A PARTICLE TRANSLATING NEAR A PLANE WALL AT LOW REYNOLDS NUMBERS USING A MULTI-OUTPUT DEEP LEARNING MODEL

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Project Overview

- Development of Neural Network Models (This presentation)
- Simulations of Drags of Non-spherical Particles





Velocity vectors and contours of 100 spherocylinders in a periodic cube at solid fraction 0.4.



Dimensionless mean drag of the assemblies

Introduction

- Wall-effect on the flow dynamics of sphere have been studied
 - Analytically
 - Experimentally
 - Numerically.
- Modeling this particulate flow system has applications in:
 - Microfluidic devices/systems
 - Fluidized beds
 - Sedimentation in streams/riverbeds

Introduction

- Use of DL models to predict dynamics of particulate flow systems has increased in recent years
- Many DL models reported on employ strategy of developing multiple models to achieve desired level of accuracy
- Current work utilizes a multi-output DL regression model approach to model a simple particulate flow system
 - Well-trained model can decrease computation time
 - Continuous learning

Wall Effect on Drag of a Sphere

- Wall boundary increases the drag of a sphere relative to the unbounded case
- The wall effect increases with decreasing Reynolds number and decreasing wall gap
- This effect arises from flow field asymmetry in the fore and aft regions of the sphere particle, resulting in an increased viscous effect
- Shear stress effects in the gap region also contribute to the net drag force when particle rotation is considered

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$$\frac{F_D}{F_{D,\infty}} > 1$$

Where F_D = bounded drag force, and $F_{D,\infty}$ = unbounded drag force

Wall Effect on Lift of a Sphere

- A wall boundary has a similar, stronger influence on the lift force
 - Pressure differential exists in wall gap and unbounded region
- Other hydrodynamic contributions to the lift force to consider
 - Saffman lift force (linear shear flow)
 - Magnus lift force (rotating particle, uniform cross flow)
- Here, we study how the particle's rotational speed, direction, and proximity to wall affects net C_L
 - linear shear flow condition not imposed





Project Overview

- Generate a set of drag and lift data using a direct numerical simulation (DNS) method that is based on simple model of a sphere particle translating next to a plane wall
- Use the DNS data to develop and train a Deep Neural Network (DNN) to accurately predict the drag and lift coefficients simultaneously over a range of flow conditions
- Use the DNS data to develop correlations for drag and lift of the sphere particle

IB-DNS Method

- Immersed Boundary method with direct forcing scheme used to simulate drag & lift data used for training.
 - (a) Description of the particle and fluid domains
 - (b) Discretization of the particle surface
 - (c) Transformation of particle-fluid boundary to Lagrangian point forces
 - (d) Transposition of boundary forces onto neighboring Eulerian grid points



Adapted from E. E. Michaelides and Z.-G. Feng, "Computational Methods: The Immersed Boundary Method.," in Multiphase Flow Handbook, Boca Raton, CRC Press, 2016, pp. 126-135.

DNS Method - continued

• The no-slip boundary condition is maintained:

$$\frac{\partial \mathbf{X}(\mathbf{s},t)}{\partial t} = \mathbf{u}(\mathbf{X}(\mathbf{s},t),t) \qquad \mathbf{x} = \mathbf{X}(\mathbf{s},t)$$

• Governing momentum and continuity equations:

$$\boldsymbol{\rho}\left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u}\right) = \boldsymbol{\mu} \nabla^2 \mathbf{u} - \nabla \boldsymbol{p} + \mathbf{f} \qquad \nabla \cdot \mathbf{u} = 0$$

• Direct forcing:

$$\mathbf{f} = \boldsymbol{\rho} \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) - \boldsymbol{\mu} \nabla^2 \mathbf{u} + \nabla \boldsymbol{p}$$

• Fluid body force density and velocity defined as:

$$f(\mathbf{x},t) = \int_{\Gamma} \mathbf{F}(\mathbf{s},t) \delta(\mathbf{x} - \mathbf{X}(\mathbf{s},t)) d\mathbf{s}$$
$$\frac{\partial \mathbf{X}}{\partial t} = \int_{\Omega} \mathbf{u}(\mathbf{x},t) \delta(\mathbf{x} - \mathbf{X}(\mathbf{s},t)) d\mathbf{x}$$

DNS Method – continued

• Velocity at a boundary point X_s :

 $\boldsymbol{U}_s = \boldsymbol{U}_c + \boldsymbol{\omega} \times (\boldsymbol{X}_s - \boldsymbol{X}_c)$

• Force spreading:

$$\delta(r) = \begin{cases} \frac{1}{4} \left[1 + \cos\left(\frac{\pi r}{2h}\right) \right], & |r| \le 2h \\ 0, & |r| > 2h \end{cases}$$

$$D(\mathbf{x} - \mathbf{x}_{mn}) = \delta(x - x_{mn})\delta(y - y_{mn})\delta(z - z_{mn})$$

DNS Model

- Simulation Box
 - Eulerian grid 120x80x320
 - Box size 9Dx6Dx24D
 - I < Re < 20
 - Box size 9Dx9Dx24D
 - Re = 0.5

 L_{x}

Schematic diagram of a sphere translating and rotating in a simulation box filled with a viscous, quiescent fluid.

- Sphere Surface
 - 3200 Lagrangian points

DNS Model

- Dimensionless parameters used to represent different particle movements:
 - *L/D* [0.75, 2.5]
 - $Re = \frac{\rho U_z D}{\mu}$ [0.5, 20]
 - $Re_{\omega} = \frac{\rho \omega_{y} D^{2}}{\mu}$ [-5, 5]

- Drag and Lift Coefficients:
 - $C_D = \frac{2F_D}{\rho U^2 A} = f(\frac{L}{D}, Re, Re_{\omega})$

•
$$C_L = \frac{2F_L}{\rho U^2 A} = f(\frac{L}{D}, Re, Re_{\omega})$$

• 715 samples in total

DNS Model Validation

- DNS drag compared to Beard, Schiller-Naumann correlations (no wall effect)
- DNS drag & lift compared with wall-effect simulation results found in literature

Table 1: Drag and lift coefficients of a sphere translating near a wall at $\frac{L}{D} = 1$ and Re = 10:

	Zeng et al.	DNS (9Dx6Dx24D)	Difference in percentage
C_D	4.72	4.79	1.5%
C_L	0.351	0.362	3.1%



Drag coefficient of a sphere at Reynolds numbers ranging from 0.5 to 20, $Re_{\omega} = 0$

DNS Drag Results

Drag coefficients at Re = 0.5

Re _ω	L/D = 0.75	L/D = 1.0	L/D = 2.5
-5.0	73.0	68.1	60.3
0	77.4	68.1	59.3
5.0	81.7	67.8	57.6

Re _ω	L/D = 0.75	L/D = 1.0	L/D = 2.5
-5.0	-5.68%	0.0	1.69%
5.0	5.56%	-0.44%	-2.87%



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DNS Drag vs. Reynolds Number

DNS Lift Results

- Asymmetry in the lift coefficient distribution
- Opposing forces near wall
 - Magnus
 - Wall-Effect
- Dependent on rotational direction

Re _ω	L/D = 0.75	L/D = 1.5	L/D = 2.5
-5.0	-1.47	-5.3	-7.83
0	1.13	1.05	0.83
5.0	11.3	9.80	9.75



Related Work – Literature Survey

- Samantary et. al. (2017)
 - Used standard drag curve correlation to train ANN and predict $C^{}_{\rm D}$
 - I hidden layer, tanh activation, 745 samples, single input (Re)
- Nikolopoulos et. al. (2021)
 - Used simulation data to predict Heterogeneity index for fluidized Reactor
 - 3 models developed for different ranges of void fraction
 - 2 hidden layers in each model, 7 inputs, 1 output
- Viquerat & Hachem (2020)
 - Used CNN to predict drag of arbitrary 2-D shapes
 - Bezier curves \rightarrow IB-DNS \rightarrow CNN Learning (12,000 samples)

Machine Learning Approach

- Python / Jupyter Notebook
- Tensorflow 2.3.0 / Keras API
 - Multi-output Regression
 - Densely connected
 - Multi-layer Perceptron (MLP)
- 3 Inputs/Features
 - L/D, Re, Re_{ω}
- 2 Outputs/Labels
 - C_D, C_L

[1]: import matplotlib.pyplot as plt import numpy as np import pandas as pd import os

from sklearn.model_selection import KFold

[2]: import tensorflow as tf

from tensorflow import keras
from tensorflow.keras import layers
from tensorflow.keras import utils
from tensorflow.keras.callbacks import LambdaCallback

print(tf.__version__)

2.3.0

[3]: import tensorflow_docs as tfdocs import tensorflow_docs.plots import tensorflow_docs.modeling

Data Transformation & Normalization

• Drag Coefficient to "K-factor"

•
$$K = \frac{C_D}{\frac{24}{Re}}$$

- Lift Coefficient to "L-factor"
 - $L_T = 10 + \frac{C_L}{\frac{4}{Re}}$
- Data Normalization (-1 to 1)

• $X' = a + \frac{(X-X_{min})(b-a)}{X_{max}-X_{min}}$

• Data shuffled before each test



Final Multi-Output FNN Architecture

Layer	Nodes	Activation
Input	3	N/A
Hidden 1	15	tanh
Hidden 2	25	Softmax
Output	2	Identity







Other Hyperparameters

- Kernel Initializer = HeUniform
 - Scales variance of initial weight tensor
- Learning Epochs = 4000
- Learning Rate = .0005
- Optimizer = RMSProp

•
$$E[g^2]_t = 0.9E[g^2]_{t-1} + 0.1\left(\frac{\delta C}{\delta w}\right)^2$$

•
$$w_t = w_{t-1} - \frac{\eta}{\sqrt{E[g^2]_t}} \left(\frac{\delta C}{\delta w}\right)$$

• Loss = Mean Squared Error (MSE) • $MSE = \frac{\sum (y_i - O_i)^2}{n}$

•
$$MAE = \frac{\sum |y_i - O_i|}{n}$$

•
$$RMSE = \sqrt{\frac{\sum(y_i - O_i)^2}{n}}$$

• Validation Split for Learning = 0.15

Model Performance vs. Number of Nodes

- 100 models trained adding a single node with each new model
- RMSE based on 715 samples
- Marginal improvement beyond
 7 nodes in each hidden layer

Parameter	Value
Learning Rate	0.001
Epochs	1200



K-Fold Cross Validation

- 8-Fold Cross Validation Test
 - ~20% test split for each fold
 - 0.0002 learning rate
 - 2500 epochs
 - 15% validation split



Comparison of Hold-out CV vs K-fold CV method used for regression model validation.

	Avg. MAE	Std. Dev. MAE	Avg. RMSE	Std. Dev. RMSE		Avg. MAE	Std. Dev. MAE	Avg. RMSE	Std. D RMS
	0.0062	0.0011	0.0091	0.0019	Train	0.0088	0.0006	0.0144	0.00
lest K					Validation	0.0090	0.0006	0.0127	0.00
Test L _T	0.0174	0.0033	0.0292	0.0105	Test	0.0095	0.0017	0.0153	0.004

Final Model Selection & Performance

- K-fold models did not predict the full set of C_D and C_L data very well
- 715 samples used for final learning with 15% validation split
- Overall error similar to k-fold performance (K, L_T)



Final Model Prediction Error Distribution



- 100% drag predictions within ± 5% from DNS
- 91% lift predictions within ± 10% from DNS
- 96% lift predictions within ± 20%



- Largest error in regimes were $C_L < 0.01$
- ~50% of high error predictions -2.5< ${\rm Re}_{\omega}{\rm <}$ -1.0
 - sign change in C_L

C_L Prediction Error – Near Wall

- Largest prediction errors in creeping flow (Re=0.5), near wall, clockwise rotation
- NN Model tends to overpredict C_L in the creeping flow, near wall condition



C_L **Prediction Error – Far from Wall**

- Far from wall, clockwise rotation, small Re_{ω} , very small C_L
- Small absolute error amplified when expressed as %



Final Hold Out Validation Test

- New dataset for final hold out test
- 39 Randomly generated DNS inputs/combinations for $(Re_{\omega} > 0)$
- Predictions evaluated for deviation from DNS drag and lift coefficients
- 97.4% C_D predictions within ± 5% Error
- 100% C_L predictions within ± 7.5% Error



Wall Effect Impact Factor

- $K_f = \frac{C_D}{C_{D,\infty}}$
- Faxen Analytical Solutions
 - $K_{fF30\parallel} = 1 + \frac{9}{16}\kappa + \frac{81}{256}\kappa^2 + \frac{217}{4096}\kappa^3$
 - $K_{fF50\parallel} = \left[1 \frac{9}{16}\kappa + \frac{1}{8}\kappa^3 \frac{45}{256}\kappa^4 \frac{1}{16}\kappa^5\right]^{-1}$
- *K*_{*f*,*FNN*} used Schiller –Naumann correlation for C_{D,∞}



Figure 19. Comparison of Faxen 3rd and 5th order analytical solutions for wall effect drag correction factor K_f vs. L/D with K_{FNN,S-N} (Re=0.5, Re_o=0).

Wall effect and Magnus Lift Coefficient

- Oesterle & Bui Dinh Correlation for used for Magnus lift coefficient
 - $C_{LM} = 0.45 + \left(\frac{Re_{rot}}{Re_s} .45\right)e^{-.05684Re_{rot}^{0.4}Re_s^{0.3}}$
 - Symmetry with respect to Re_{ω}
- Greatest deviation from C_{LM} near wall, clockwise rotation with Re_{ω}
 - Opposing forces



Difference between DNS, NN model C_L and the Magnus lift coefficient equation 12 C_{LM} versus Re at different angular speeds (Re_{ω}=-5.0, -2.5, -0.5, 0, L/D=0.75)

Conclusions

- A Multi-Output FNN Regression Model was developed to predict drag and lift coefficients simultaneously at low Reynolds numbers
- DNS data showed particle rotation has little effect on drag, but heavily influences net lift force.
- FNN lift prediction errors are higher when sign of Re_{ω} is negative (clockwise rotation) and when C_{L} is small.
- Wall-effect drag and lift correlations were developed for a fixed Re_{ω} and showed good agreement with Analytical and other numerical simulation results