

Background

- Amine-appended metal organic frameworks (MOF) have shown promising attributes for post combustion capture (long-term stability, CO₂ selectivity, maintained performance under humid conditions) accompanied by a unique step-shaped adsorption isotherm.
- Unique isotherms and dynamic sorbent processes present difficult modeling and optimization challenges.

Objectives

- Development of an isotherm model for a tetraamine-appended MOF.¹
- Development of fixed-bed contactor and moving-bed contactor models.
- Techno-economic optimization of post-combustion capture processes from natural gas combined cycle (NGCC) flue gas.

Isotherm Model

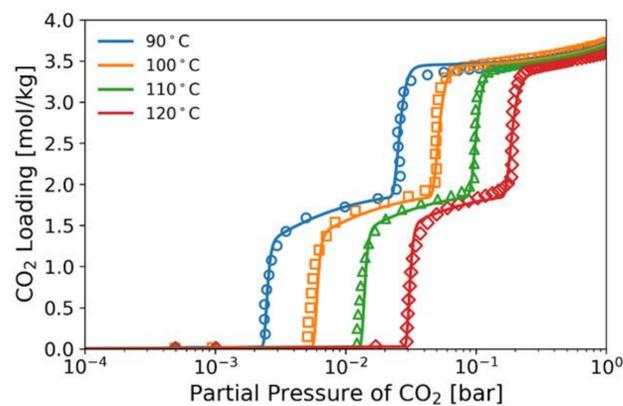
- Weighted Langmuir model extended to multiple adsorption steps.

$$q_{CO_2}^* = (1 - \omega_1)q_1^* + (\omega_1 - \omega_2)q_2^* + \omega_2q_3^*$$

- Parameter Estimation.

θ : Set of isotherm parameters

$$\min_{\theta} \left(\frac{q_{CO_2,exp}^* - q_{CO_2,model}^*(\theta)}{q_{CO_2,exp}^*} \right)^2 \sum_{i=1}^n \left(\frac{q_{CO_2,exp}^* - q_{CO_2,model}^*(\theta)}{q_{CO_2,exp}^*} \right)^2$$



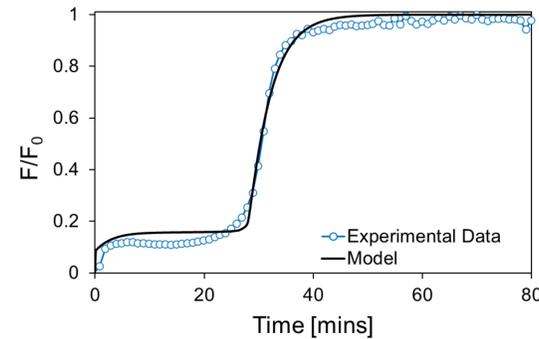
References

- [1] Kim, E.J., et al. Cooperative Carbon Capture and Steam Regeneration with Tetraamine-Appended Metal–Organic Frameworks. *Science* **2020**, No. 369, 392–396. <https://doi.org/10.1126/science.abb3976>.
- [2] James, III, R., et al. *Cost and Performance Baseline for Fossil Energy Plants Volume 1: Bituminous Coal and Natural Gas to Electricity*; 2019; NETL-PUB-22638, 1569246. <https://doi.org/10.2172/1569246>.
- [3] Miller, D., et al. "Innovative computational tools and models for the design, optimization and control of carbon capture processes," *26th European Symposium on Computer Aided Process Engineering – ESCAPE 26*, pp. 2391-2396, 2016.
- [4] Du, Y., et al. "Zero- and negative-emissions fossil-fired power plants using CO₂ capture by conventional aqueous amines," *International Journal of Greenhouse Gas Control*, vol. 111, p. 103473, 2021.

Contactor and TSA Process Models

- Dynamic, non-isothermal, first-principles contactor models (Aspen Custom Modeler).
- Mass transfer model developed using experimental fixed-bed breakthrough data.

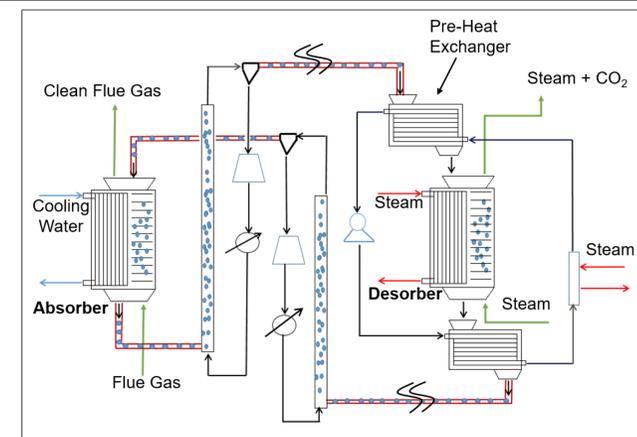
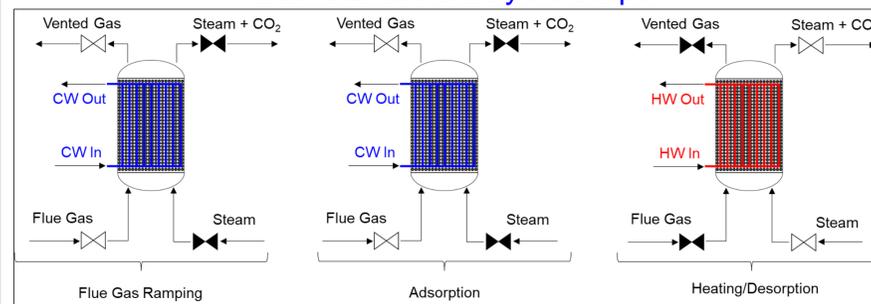
Linear driving force equation: $\frac{dq_{CO_2}}{dt} = k_I(q_{CO_2}^* - q_{CO_2})$



Process Models

- Sized to capture CO₂ from a 650 MW NGCC plant.²
- Designed for 90% CO₂ capture.
- Embedded heat exchangers used to aid in thermal management.

Fixed Bed TSA Cycle Steps



Techno-Economic Optimization

Cost Model

- Closely follows the NETL costing guidelines.²
- Main costing components:
 - Annualized capital cost.
 - Fixed O&M.
 - Variable O&M (utilities such as steam and electricity).

Optimization Framework

- Connection to derivative-free optimization algorithms within the FOQUS tool.³

$$\min_x f(x) \quad \text{Total annualized cost (\$MM/y)}$$

$$s. t.$$

$$x^L \leq x \leq x^U \quad x \rightarrow \text{Decision variables}$$

$$h(x) = 0 \quad \text{Rigorous, first principles models in ACM}$$

$$g(x) \leq 0 \quad \text{CO}_2 \text{ capture, velocity constraints, etc.}$$

- Decisions Variables (x).

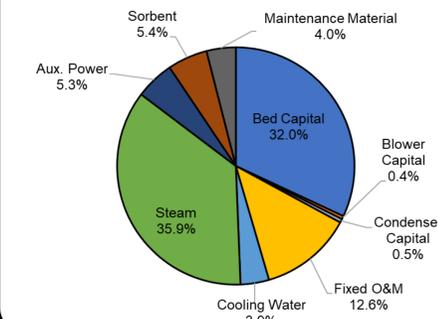
- Fixed Bed: $L, D, \text{tube pitch}, F_{FG}, F_{steam}, \text{step times}$.
- Moving Bed: $L_{ads}, D_{ads}, L_{des}, D_{des}, \text{tube pitch}, \text{lean sorbent loading}$.

Results

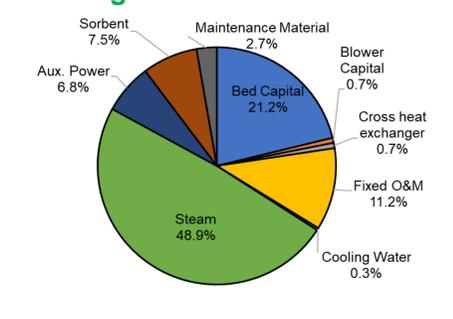
- Enhanced driving forces due to counter-current flow pattern in the moving-bed process reduces sorbent/reactor volume and results in lowest cost of capture.

	Fixed Bed Process	Moving Bed Process	MEA Reference ⁴
Total Annualized Cost (\\$MM/y)	193.1	118.2	-
Cost of Capture (\\$/tonne CO ₂)	109.4	67.4	73.9

Fixed-Bed Cost Breakdown



Moving-Bed Cost Breakdown



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