A New Thermal Swing Adsorption Process for Post-Combustion Carbon Capture from Natural Gas Combined Cycle Plants (DE-FE-0032151)



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Project Team and Objectives



& Research

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Project Duration

- **Start Date = July 15, 2022** •
- End Date = July 14, 2025 ٠

Budget

- **Project Cost = \$3,125,524** ٠
- DOE Share = \$2,500,000 ٠
- **TDA & its partners = \$625,000** ٠

- Demonstrate the viability of a transformational microwave-assisted thermal swing adsorption (MTSA) based carbon capture process to efficiently capture CO₂
 - CO_2 capture efficiency target $\geq 95\%$
 - CO_2 product purity target \geq 95% CO_2
 - CO₂ source is flue gas from a natural gas combined cycle power plant (simulated)
- Reduce the cost of capture by more than 25% against a reference NGCC plant with liquid amines (e.g., Cansolv[®])

BP	Period	Main Activity
1	Year 1	Material synthesis Adsorption & CFD modeling Bench-scale system design Preliminary TEA
2	Year 2	Bench-scale system fabrication Commissioning/troubleshooting
3	Year 3	Bench-scale evaluations Techno-economic Assessment Life Cycle Analysis EH&S nalysis



MTSA-Based Carbon Capture Process



- A mild temperature swing adsorption process (30-40°C temperature difference) is employed to remove and concentrate the CO₂
- The regeneration heat is provided by a microwave system to achieve rapid heating of the bed
- Fast cycling improves the sorbent utilization (i.e., CO₂ productivity)



Heating Options - Conventional vs Microwave



- In conventional approach, CO₂ desorbing from the bed is circulated through an external heater to supply the heat for regeneration
- A fraction of this is removed from the circulating loop for purification and compression
- Heating rate is controlled by external heater temperature and circulation rate
- Heater temperature limited by sorbent material temperature tolerance
 - Higher circulation rates increase heating rate, but at the expense of electric power (blower) and thermal load (heater)



Why Use Microwave Heating?

- Microwave heating is common in several industrial settings
- Uniform heating can be achieved by optimizing the RF frequency, wave penetration depth (sorbent) and reactor geometry
- As confirmed by experimental measurements, heating times can be reduced to a few minutes with full-cycle times <10-20 min



- Sorbent packing in the bed is increased by eliminating heat transfer elements from the bed volume—reducing vessel size and cost
- Through cavity/reactor integration, directed/precision heating can be achieved
- Heat can be only applied to the sorbent (not heating the vessel and structure) improving overall efficiency



Polymeric Sorbent



Various forms of polymer sorbent: (left) pellets (middle) laminate and (right) 3D printed monolith

- A new polymer sorbent will be used in the process
- Reasonable thermal stability
- Potential for use in pellets, laminates and 3D printed structures
- TRL = 3-4



Synthesis in 22L reactor



Structured Sorbent Preparation



- Structured sorbent will be prepared to reduce pressure drop through the gassolid contactor
- Microwave guides will be integrated into the structure for rapid heating



Sorbent films are laser cut (A and B) stacked alternating with spacer grids in a holder (C and D) to make a module or stack (E)



Scale-up of the Laminates



- Membrane Technology Research will assist with the scale-up work
- Preparation of large sheets using their existing equipment
- Similar collaboration in an SBIR Phase IIB project



Adsorption Isotherm for the Polymer Sorbent



CO₂ adsorption isotherms at 60°C (orange) and 90°C in the form of beads

- Working capacity of ~1.2 mmol/g is expected
- High CO₂/N₂ and CO₂/O₂ selectivity
- Heat of adsorption of CO₂ is estimated as 51 kJ/mol



Thermogravimetric Analysis



- TGA tests showed relatively rapid release and uptake of CO₂
- Regeneration will be the rate limiting step
 - All adsorbed CO₂ is released in less than 7 min upon heating the media from 60 to 90°C



Sorbent Stability



 TDA's material shows good thermal stability in multi-cycle TGA screening (conventional heating)



Field Testing Sorbent (Conventional Heating)



Wyoming Integrated Test Center (WITC) Basin Electric's Dry Fork Station Gillette, WY



TDA's 4-bed scale-up system (right) in the TDA-built shelter at the Wyoming Integrated Test Center



Field Testing Sorbent (Conventional Heating)





Inner porous sorbent support and top/bottom supports with baffled inserts ready for assembly



 We expect the productivity to increase over 60g CO₂ / kg sorbent –hr with MTSA



Experimental Setup



Microwave-Assisted Regeneration

Single Cycle; ADS < 20 Minutes; DES < 8 Minutes Regen Adsorption (md 35000 30000 25000 25000 15000 Temp (°C) 478 482 Time (Minutes) ADS ADS DES ADS DES DES 00000 (b) 00000 (c) 0000 (c) 00000 (c) 0000 (c)

[CO2] Outlet

Heating and the subsequent CO₂
 recovery are nearly instantaneous
 upon microwave energization—
 allowing for reduced regeneration
 cycle times

•Microwave On

(°C); Microwave

Temp (

State

ADS



Preliminary TEA

Power Plant Type	Natural Gas Combined Cycle Power Plant			
Case No.	B31A	B31B	TDA - 1	
CO ₂ Capture Technology	No Capture	Amine based CO ₂	TDA's MTSA based	
		Capture Case 10	CO ₂ Capture	
CO ₂ Capture, %	0	90	90	
GT Power Generated, MW _e	477	477	477	
ST Power Generated, MW _e	263	213	263	
Gross Power Generated, MW _e	740	690	740	
ST Power Lost <i>,</i> MW _e	-	50	0	
CO ₂ Capture Auxiliaries, MW _e	-	11	29	
CO ₂ Compression Power, MW _e	-	17	29	
Other Auxiliaries, MW _e	14	16	16	
Total Auxiliary Load, MW _e	14	44	74	
Net Power, MW _e	727	646	666	
Net Plant Efficiency, % HHV	53.6	47.7	49.1	
Natural Gas Feed Rate, kmol/h	5383	5383	5383	
Total Plant Cost, \$/kW	780	1984	1302	
COE without CO ₂ T&S, \$/MWh	43.3	70.9	59.1	
COE with CO ₂ T&S, \$/MWh	-	74.4	62.5	
Cost of CO ₂ Captured, \$/tonne	-	80	47	
Cost of CO ₂ Avoided, \$/tonne	-	102	63	

DOE baseline no capture and CO₂ capture plants for NGCC plant comparison



Project Tasks

Task 1. Project Management

- BP1 Task 2. Production of the Sorbent
 - Subtask 2.1 Testing and Characterization
 - Task 3. Preparation of Structured Sorbent (sheets by MTR 12"x12" in size) Subtask 3.1 Testing and Characterization

Task 4. Design of Integrated Test SystemSubtask 4.1 Adsorption ModelingSubtask 4.2 CFD Analysis

- Task 5. Preliminary Techno-economic Analysis
- BP2Task 6. Fabrication of the Bench-scale System (2-3 scfm of simulated flue gas)
Subtask 6.1 Sorbent Reactor Module Fabrication
Subtask 6.2 Modifications to Bench-Scale System
 - Task 7. Life Tests
- BP3 Task 8. Shakedown Testing Task 9. Full-scale System Design Task 10. Bench Scale System Testing and Optimization Task 11. Proof-of-Concept Demonstration (min 1,000 hours) Task 12. Final Techno-economic Analysis Task 13. Life Cycle Analysis Task 14. Environmental Health & Safety Assessment



Microwave Reactor Design



- Initial experiments will be carried out using sorbent prepared in the form of beads
- Reactor is made out of PEEK and PTFE materials
 - Low Dielectric Loss (Poor Microwave Absorbance)
- Stainless-Steel TC Sheath Requires External Grounding
- Gas Inlet/Outlet Via Teflon Tubing with Bulkhead Fittings in Microwave Wall



Node Characterization

- Commercial microwaves operate by creating a standing wave inside the microwave cavity
- This standing wave creates
 'hotspots' or nodes
- The distance between nodes is given by:

$$d = \frac{\lambda}{2}$$

- For a frequency of 2450 MHz we expect d ~6.1 cm
- When nodes are experimentally verified we see both the expected distance and more random heating depending on vertical position in cavity





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