



## Project Review Meeting DE-FE0031597 Mixed-Salt Based Transformational Solvent Technology for CO<sub>2</sub> Capture

Palitha Jayaweera

Principal Scientist

Integrated Systems and Solutions Division

SRI International



August 18, 2022

# Presentation Outline

- Technology Background
- Project Structure
  - Budget, Team, Tasks and Schedule
- Budget Period 1 (Completed)
  - VLE Measurements
  - Kinetic studies
  - Solvent stability
  - Process modeling
- Budget Period 2 (Ongoing)
  - Large Bench Scale Absorber and Regenerator testing
  - Integrated Testing
  - Technoeconomic Analysis
  - Technology Maturation Plan
- Acknowledgements

# Mixed-Salt Based Transformational Solvent Technology for CO<sub>2</sub> Capture

- Need:
  - Reducing capture costs beyond the current values and develop a pathway to reach DOE 2030 CO<sub>2</sub> capture goals
- Approach:
  - New transformational technologies that provide a step reduction of the regeneration energy
    - Low regeneration energy by solvent pairing
    - Water-lean solvents to reduce sensible heat
    - Energy recovery by advanced heat integration
- Technology:
  - Advanced Mixed Salt Process
    - Development of a solvent formulation that contain ammonia, potassium carbonate, and a tertiary amine

# Advanced Mixed-Salt Process (A-MSP)

$K_2CO_3$ – $NH_3$ –amine– $H_2O$  system

Absorber operation at 20° - 40 °C at 1 atm

Regenerator operation at ~120 °C at ~10 atm

Key advancement in A-MSP over MSP:  
Increased solvent concentration

Increased  $CO_2$  loading

Reduced parasitic energy load

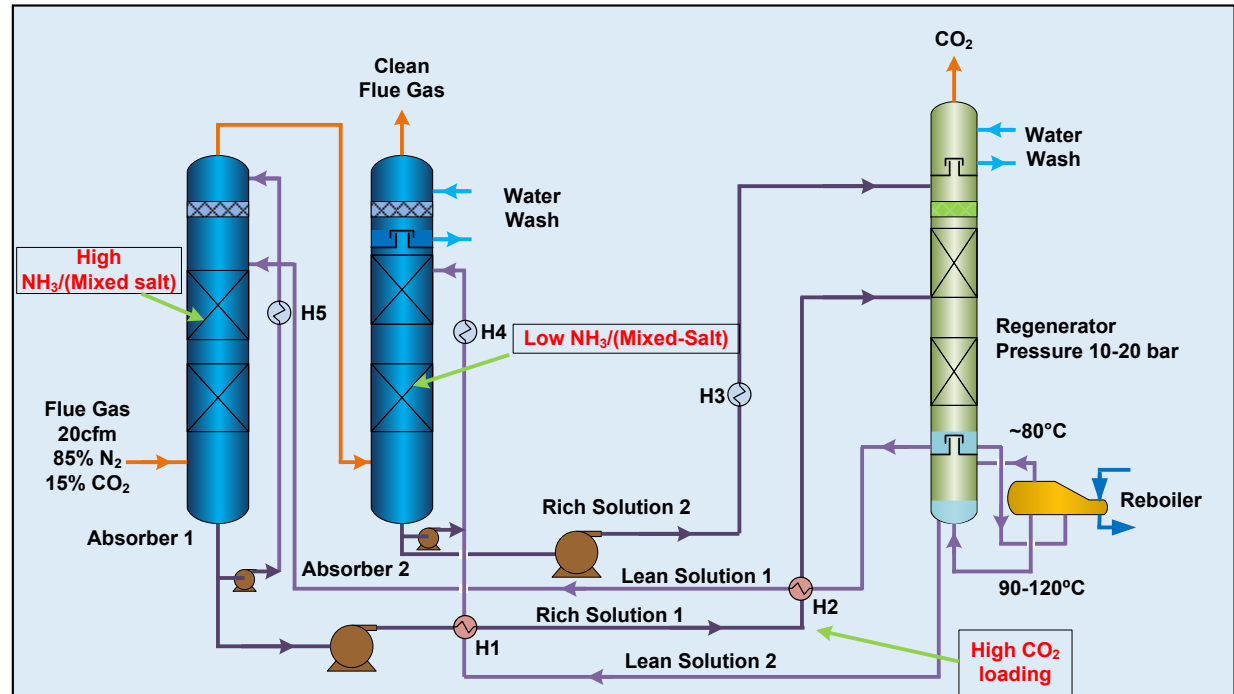
**A significant step change  
for reaching DOE's reduced  
 $CO_2$  capture cost targets.**

A-MSP will retain MSP advantages:

Reduced Ammonia Emission

Reduced Reboiler duty

Reduced  $CO_2$  Compression Energy



**Improved Absorber Kinetics  
Improved Regenerator Performance**

# Project Objectives, Budget and Period of Performance (Contract No: DE-FE0031597)

- Project Objectives
  - High CO<sub>2</sub> loading capacity
  - Water lean solvent system
  - Potential to reach DOE cost target \$30/ton CO<sub>2</sub> by 2030
- Period of Performance
  - BP1: 6/1/2018 to 12/31/2020
  - BP2: 1/1/2021 to 03/31/2023
- Project budget
  - DOE Funding: \$3,105,797
  - Partner Share: \$951,897

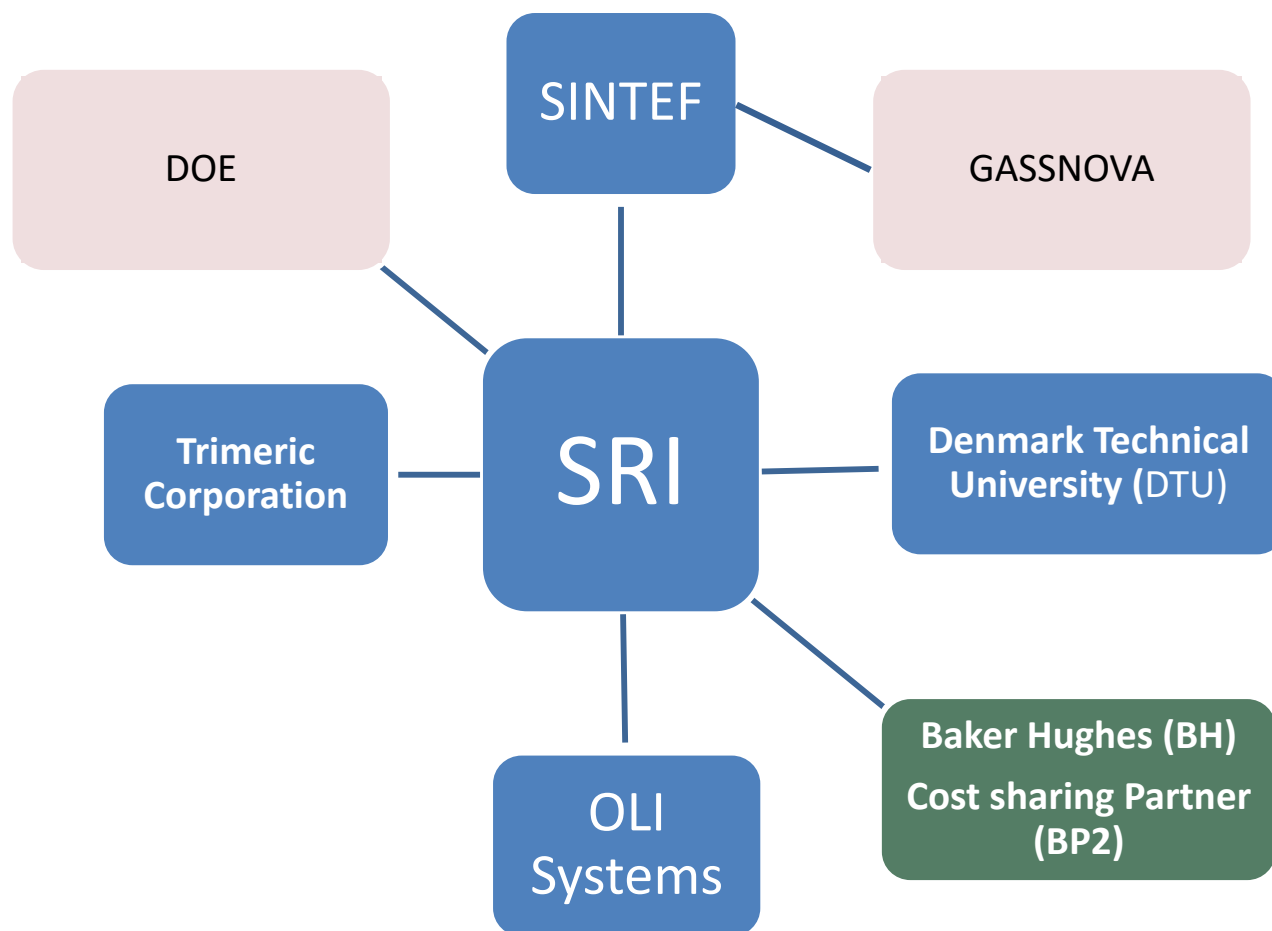
# Project Team

## *Mixed-Salt Based Transformational Solvent Technology for CO<sub>2</sub> Capture*

**Project Manager:** Krista Hill, NETL

**Prime Contractor:** SRI International

**Project Team:** US and International Partners



# Work Organization

- SRI International, USA (Prime contractor)
  - Project management
  - Advanced mixed-salt composition development and testing
  - Heat capacity measurements
  - Absorption and desorption kinetic measurements
  - Integrated system testing
- DTU, Denmark (Cost-share partner)
  - VLE Measurements & Thermodynamic modeling
- OLI Systems, USA
  - Flowsheet Modeling (energy and mass balance)
- Trimeric Corp., USA
  - Process Techno Economic Analysis
- SINTEF, Norway (Cost-share partner - BP1)
  - Degradation studies
  - Alternative Mixed-salt composition development
- Baker Hughes (Cost share partner - BP2)

# Project Tasks

- Task 1: Project management and Planning  BP1 & BP2
- Task 2: Vapor-Liquid-Equilibria (VLE) Measurements
- Task 3: Process Kinetic Assessment
- Task 4: Degradation and Emission Assessment
- Task 5: Rate-Based Model Development
- Task 6: Preliminary TEA  BP1
- Task 7: Integrated System Testing at SRI Site
- Task 8: Flowsheet Development
- Task 9: Techno-economic Analysis  BP2



# BP1 Project Status

## *Success Criteria and Decision Points*

| Decision Point                   | Basis for Decision/Success Criteria   |
|----------------------------------|---|
| A. Completion of Budget Period 1 | Successful completion of all work proposed in Budget Period 1 ✓   |
|                                  | Submission of a Technology Maturation Plan ✓  |
|                                  | Submission of Preliminary Techno-Economic Analysis topical report ✓   |
|                                  | Experimentally validate at least 10 bar pressure in the regenerator ~120°C ✓  |
|                                  | Partnering agreement finalized ✓  |
|                                  | Successful completion of the VLE model development and demonstrating the lower regeneration (less than 120°C) potential of the A-MSP solution ✓ |
|                                  | Completion of the spread-sheet model by OLI to demonstrate the regeneration energy to be less than 2.3 GJ/tonne CO <sub>2</sub> ✓               |

- The team completed the BP1 scope of work and achieved the associated milestones and success criteria on schedule (December 31, 2020) and within budget.
- The project team is continuing the project in BP2 (1/1/21-03/31/23) with no change in scope or budget.

# Representative Data - VLE Measurements

*Comparison of measured values with model predictions*



Photograph of the VLE measurement setup

Commonly Available

$\text{NH}_3 + \text{CO}_2 + \text{H}_2\text{O}$

$\text{K}_2\text{CO}_3 + \text{CO}_2 + \text{H}_2\text{O}$

Amine +  $\text{CO}_2 + \text{H}_2\text{O}$

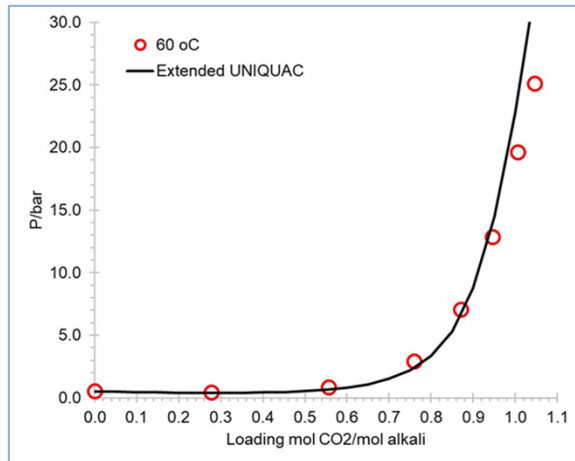
Generated under current program

$\text{NH}_3 + \text{K}_2\text{CO}_3 + \text{CO}_2 + \text{H}_2\text{O}$

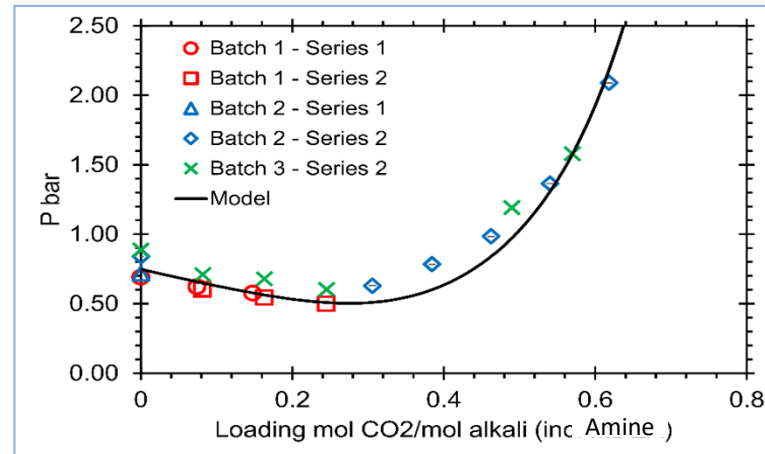
$\text{K}_2\text{CO}_3 + \text{Amine} + \text{CO}_2 + \text{H}_2\text{O}$

$\text{NH}_3 + \text{Amine} + \text{CO}_2 + \text{H}_2\text{O}$

$\text{NH}_3 + \text{K}_2\text{CO}_3 + \text{Amine} + \text{CO}_2 + \text{H}_2\text{O}$

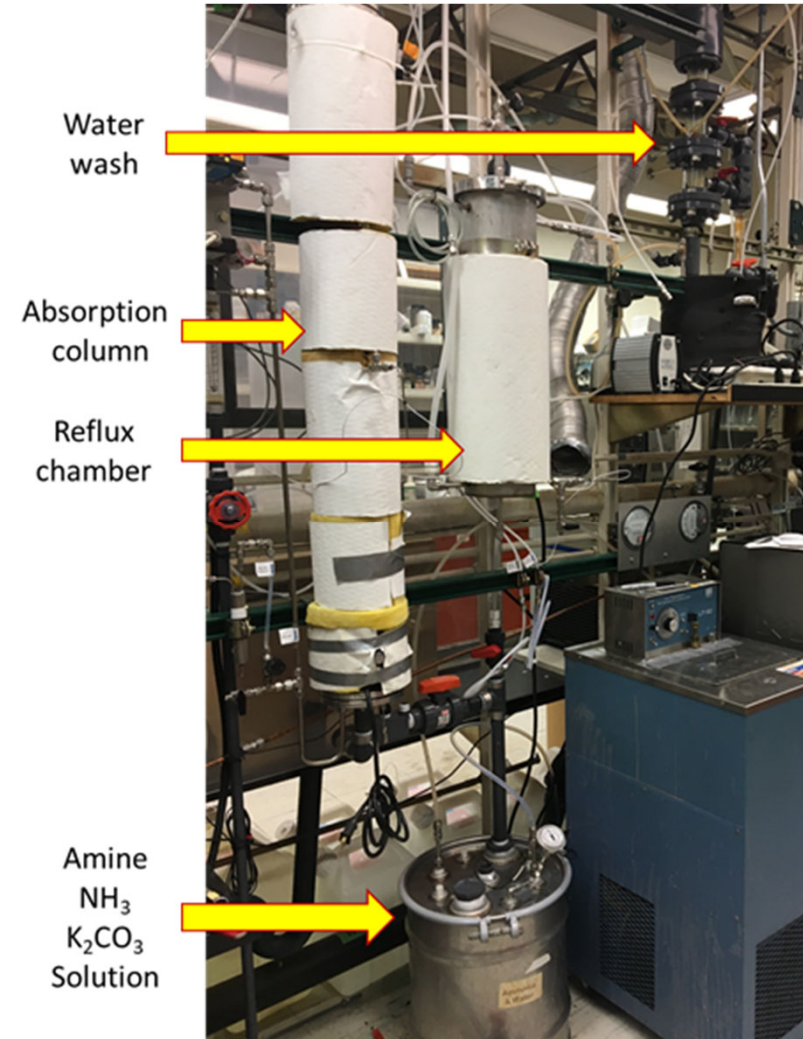
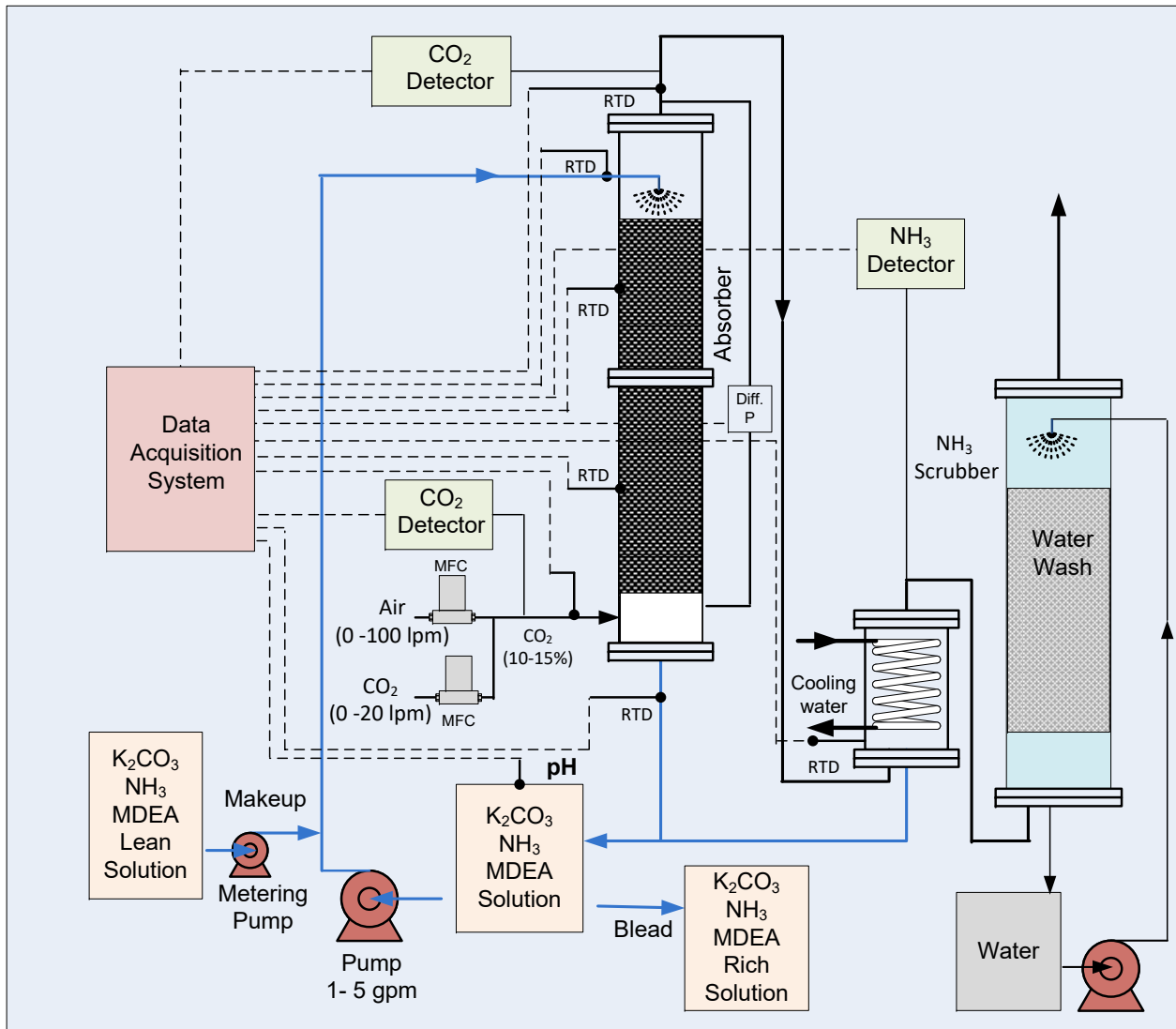


VLE measurements for  $\text{NH}_3\text{-CO}_2\text{-H}_2\text{O}$  mixtures at  $60^\circ\text{C}$  compared to the predictions of the Extended UNIQUAC model



VLE measurements (approx.  $60^\circ\text{C}$ ) compared to the preliminary parametrization of the Extended UNIQUAC model

# Representative Data - Process Kinetic Assessment



Small bench scale absorber system for AMSP testing

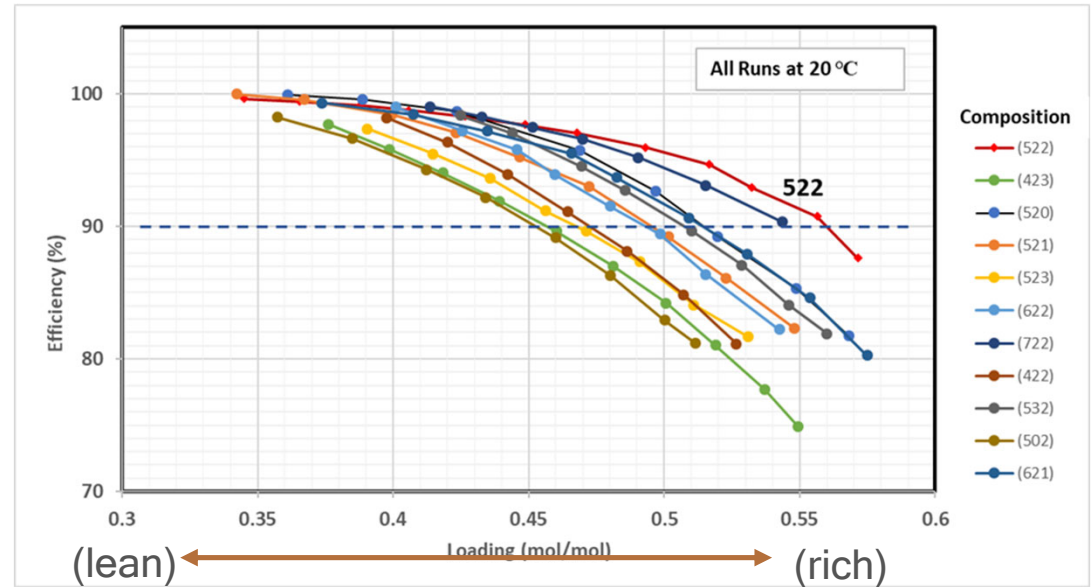
Gas flow rate: 10-40 slpm, solution composition: 20-55 wt.%, solution temperature: 20- 40°C

# Representative Data - Process Kinetic Assessment

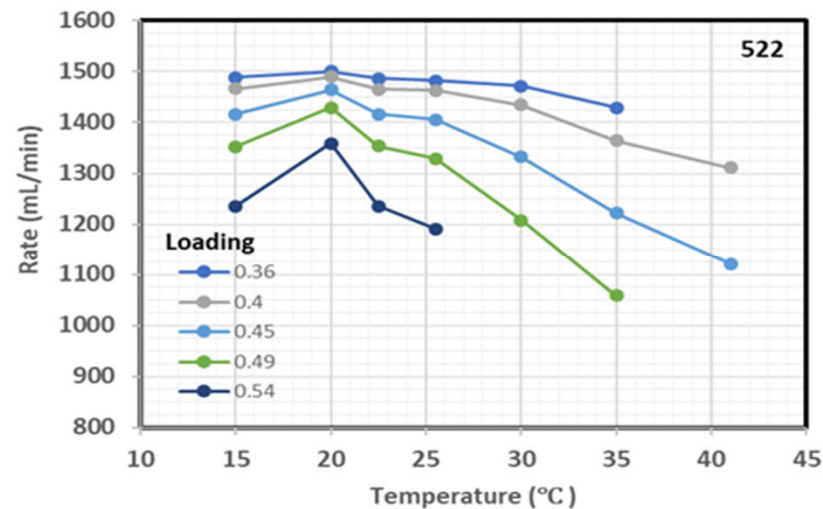
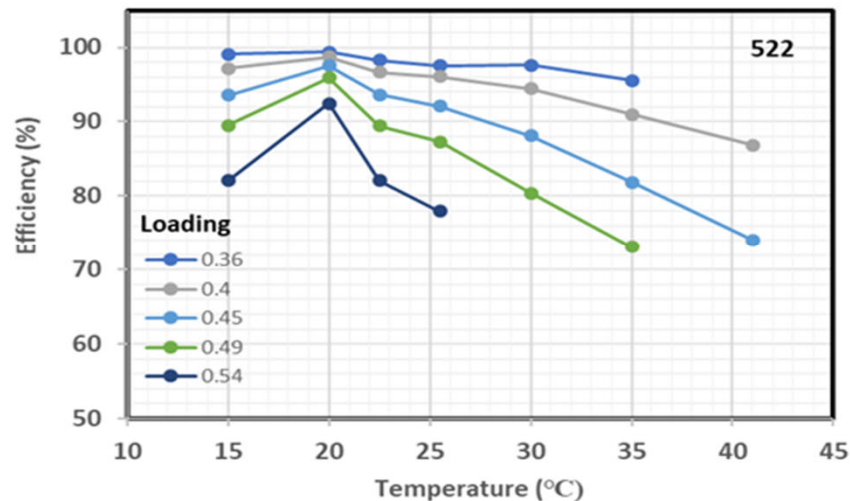
## *Rapid Design of Experiment for the Kinetic Study*

Sample parametric test performed at 20°C

| Composition Label | Absorber Temperature | loading (initial) | loading (final) |
|-------------------|----------------------|-------------------|-----------------|
| 522               | 20°C                 | 0.35              | 0.65            |
| 521               | 20°C                 | 0.37              | 0.57            |
| 423               | 20°C                 | 0.38              | 0.56            |
| 520               | 20°C                 | 0.36              | 0.59            |
| 521               | 20°C                 | 0.34              | 0.57            |
| 523               | 20°C                 | 0.39              | 0.54            |
| 622               | 20°C                 | 0.40              | 0.55            |
| 722               | 20°C                 | 0.41              | 0.56            |
| 422               | 20°C                 | 0.40              | 0.54            |
| 532               | 20°C                 | 0.42              | 0.56            |
| 502               | 20°C                 | 0.36              | 0.51            |



Absorption efficiency as a Function of CO<sub>2</sub> loading

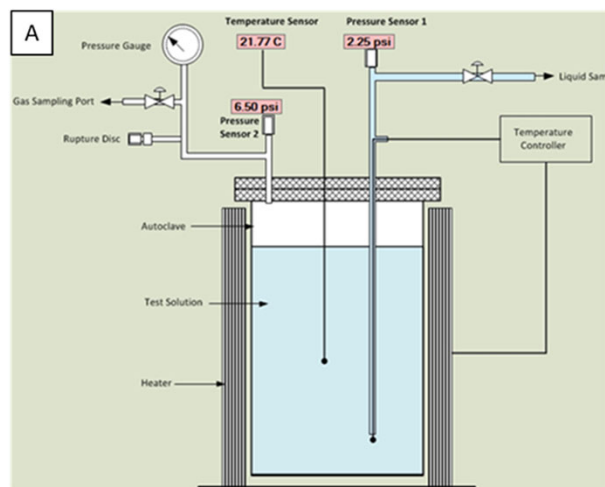


Effects of temperature on efficiency (left) and absorption rate (right) for a given loading.

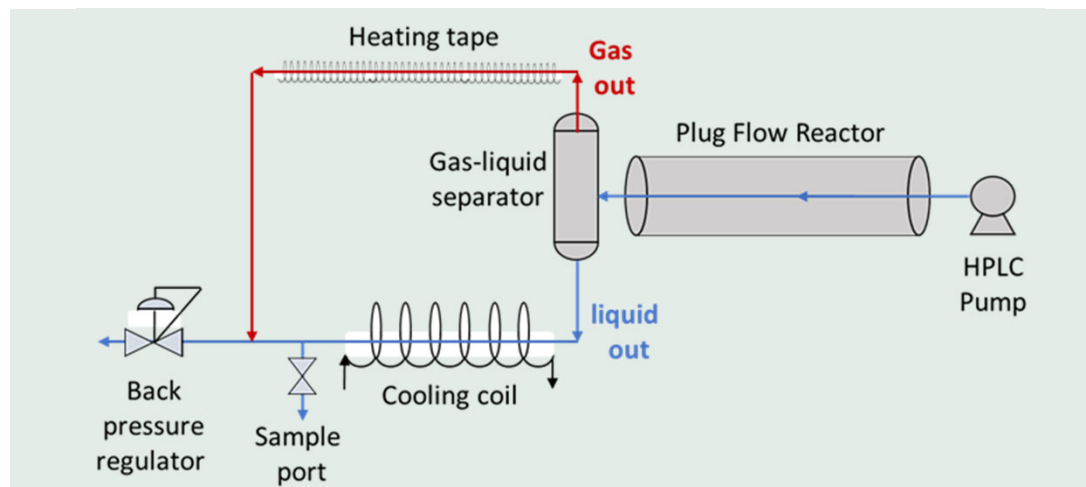


# Representative Data - Desorption Measurements

## *Static and Dynamic Regenerator Measurements*



Static Autoclave System  
(Operability Limit: up to 250°C and 300 psi)



Continuous Flow, Plug Flow Reactor System  
(Operability Limit: up to 400°C and 4000 psi)

### Static System

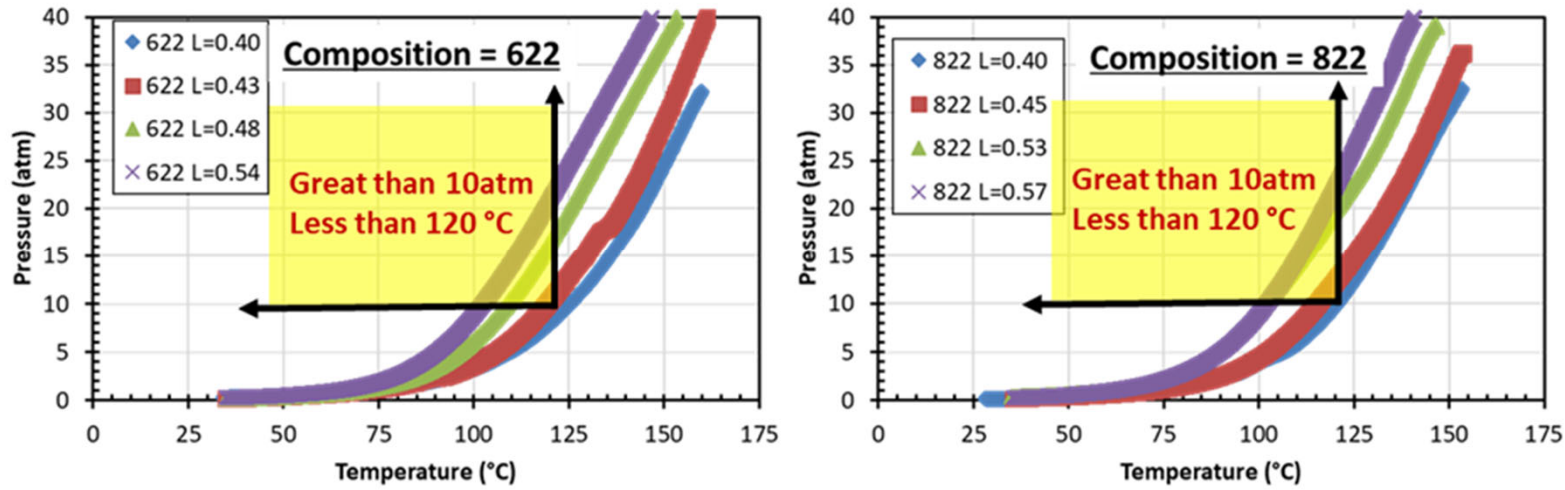
Slow Heating  
Long retention time  
VLE Curve

### Continuous Flow System

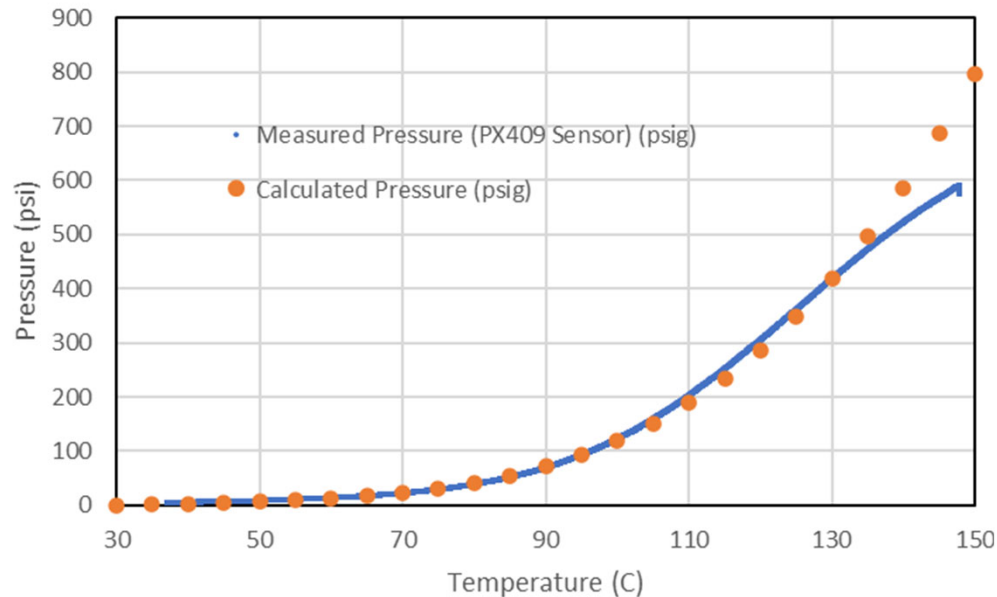
Rapid Heating  
Short retention time  
Rate Profile

# Representative Data - Desorption Measurements

## *Static Regenerator Measurements*



Regeneration pressure as a function of temperature and CO<sub>2</sub> loading



Model and measured data comparison.

# Representative Data - Solvent Degradation Assessment

## *Oxidative and Thermal Decomposition Study of Amine at SINTEF*

- Test conditions
  - Oxidative decomposition performed at 55°C to get accelerated results
  - Thermal decomposition studies performed at 120, 135 and 150°C
  - Testing duration is about 6 weeks
  - Solutions were analyzed by LC-MS, TOC, and ICP-MS
- Results
  - SINTEF reported the oxidative degradation results that showed the selected amine in A-MSP solution is far more stable than MEA and other widely used amines in CO<sub>2</sub> capture.
  - The results for the amine thermal degradation showed it was stable at 120°C.
  - Based on the weight loss, some amine degradation at higher temperatures (>150°C) is predicted.

# BP2 Project Tasks (ongoing)

- Task1: Project management and Planning
- Task 4. Process Emission Assessment
  - Subtask 4.1: Emission Assessment of the Selected AMSP formulation
- Task 7. Integrated System Testing at SRI Site
  - Subtask 7.1: Development of the Test Plan
  - Subtask 7.2: Integrated Testing with A-MSP Compositions
  - Subtask 7.3: Regenerator Steam Use Measurements
  - Subtask 7.4: Test Data Analysis
- Task 8. Flowsheet Development
  - Subtask 8.1: Development of Process Flowsheet Model
  - Subtask 8.2: Evaluation of Process Heat and Mass Balances
- Task 9. Techno-economic Analysis and Required Reports
  - Subtask 9.1: Techno-economic Analysis
  - Subtask 9.2: Update State-Point Data Table
  - Subtask 9.3: Technology Gap Analysis
  - Subtask 9.4: Environmental Health and Safety Assessment
  - Subtask 9.5: Technology Maturation Plan



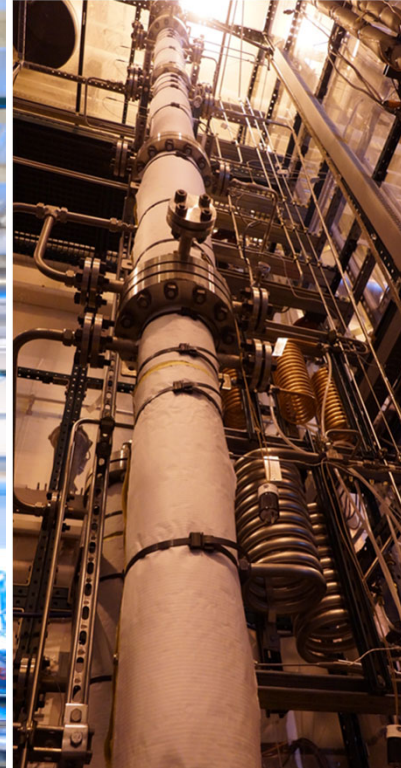
# Integrated Testing in SRI Large Bench Scale System



Analytical and  
Control Systems



Absorbers



Regenerator



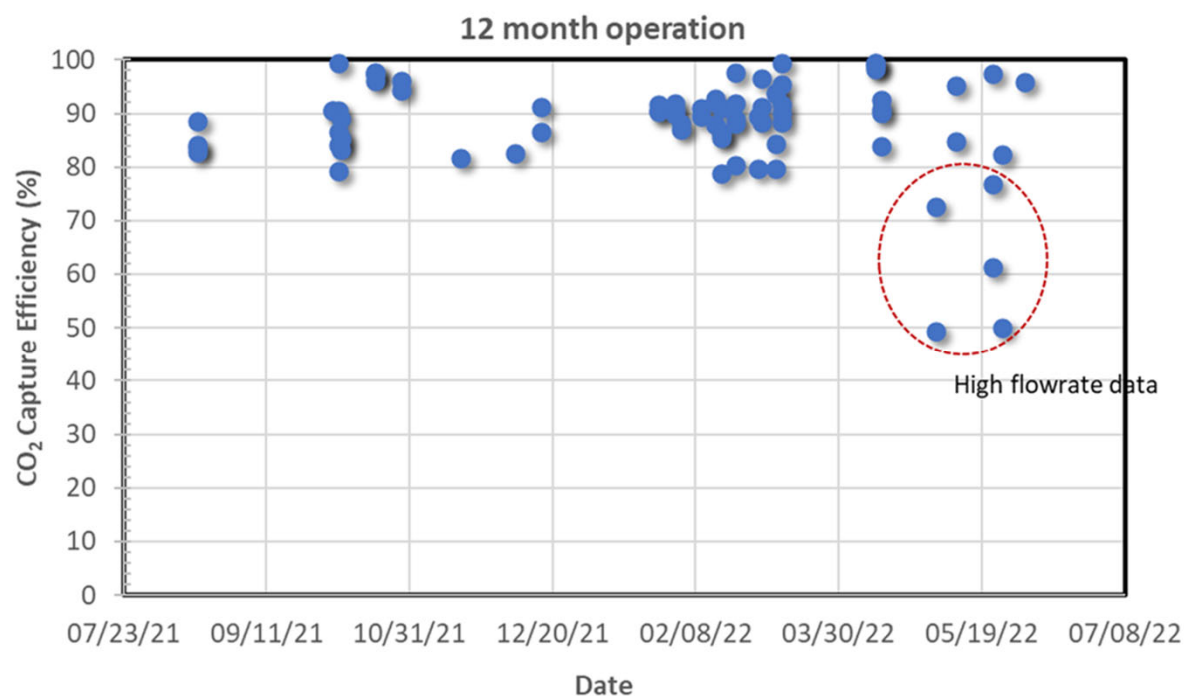
Integrated system after  
modification in 2020

Absorbers (0.25 t-CO<sub>2</sub>/day capacity)

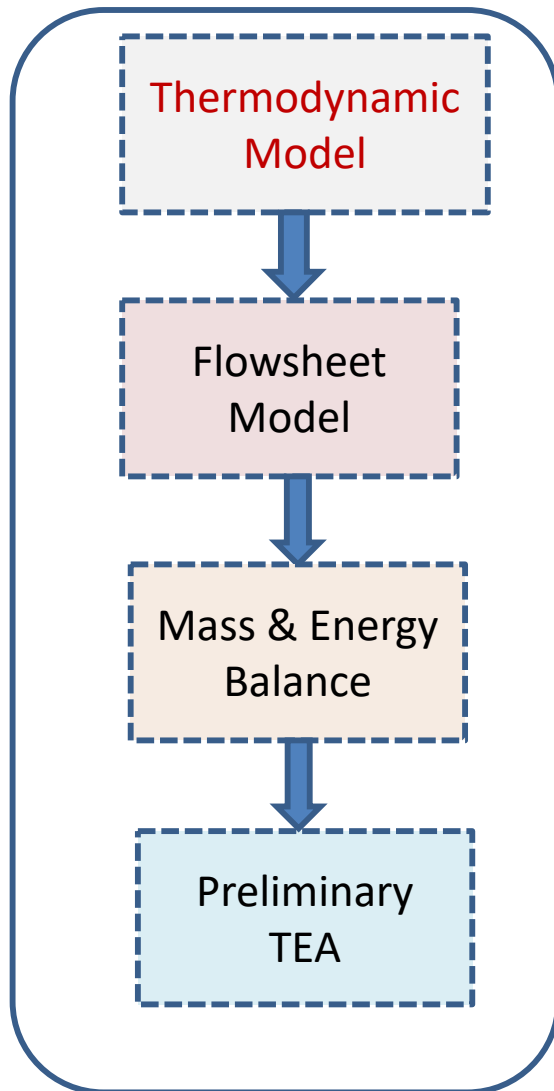
Continuous operation of the integrated system is ongoing

# Parametric testing in the integrated system

| Run No. | Gas Flow rate (lpm) | Alkalinity (Molar) | Rich-1 Flow to Regenerator (lpm) | Rich-2 Flow to Regenerator (lpm) | Regen Mid Temp (C) | Regen Bottom Temp (C) | CO <sub>2</sub> Capture Efficiency (%) |
|---------|---------------------|--------------------|----------------------------------|----------------------------------|--------------------|-----------------------|--|
| 33      | 304.8               | 5.26               | 1.9                              | 0.5                              | 116.9              | 130.7                 | 90.7                                   |
| 34      | 302.5               | 5.255              | 1.9                              | 1.0                              | 116.3              | 130.9                 | 91.9                                   |
| 40      | 301.4               | 5.27               | 1.9                              | 0.5                              | 122.7              | 130.9                 | 92.7                                   |
| 41      | 347.9               | 5.29               | 1.9                              | 0.5                              | 122.8              | 130.8                 | 92.1                                   |
| 51      | 405.7               | 5.29               | 1.9                              | 0.5                              | 121.6              | 151.0                 | 91.9                                   |
| 56      | 305.0               | 4.73               | 1.4                              | 0.5                              | 117.7              | 141.1                 | 91.2                                   |
| 57      | 302.9               | 4.15               | 1.4                              | 0.5                              | 144.6              | 151.4                 | 96.6                                   |
| 65      | 402.9               | 4.9                | 1.4                              | 0.5                              | 126.8              | 146.2                 | 90.1                                   |
| 66      | 405.7               | 5.16               | 1.4                              | 0.5                              | 126.8              | 147.1                 | 91.8                                   |
| 67D     | 300.1               | 7.14               | 1.4                              | 0.5                              | 111.3              | 130.9                 | 98.3                                   |



# Process Model Development Progress



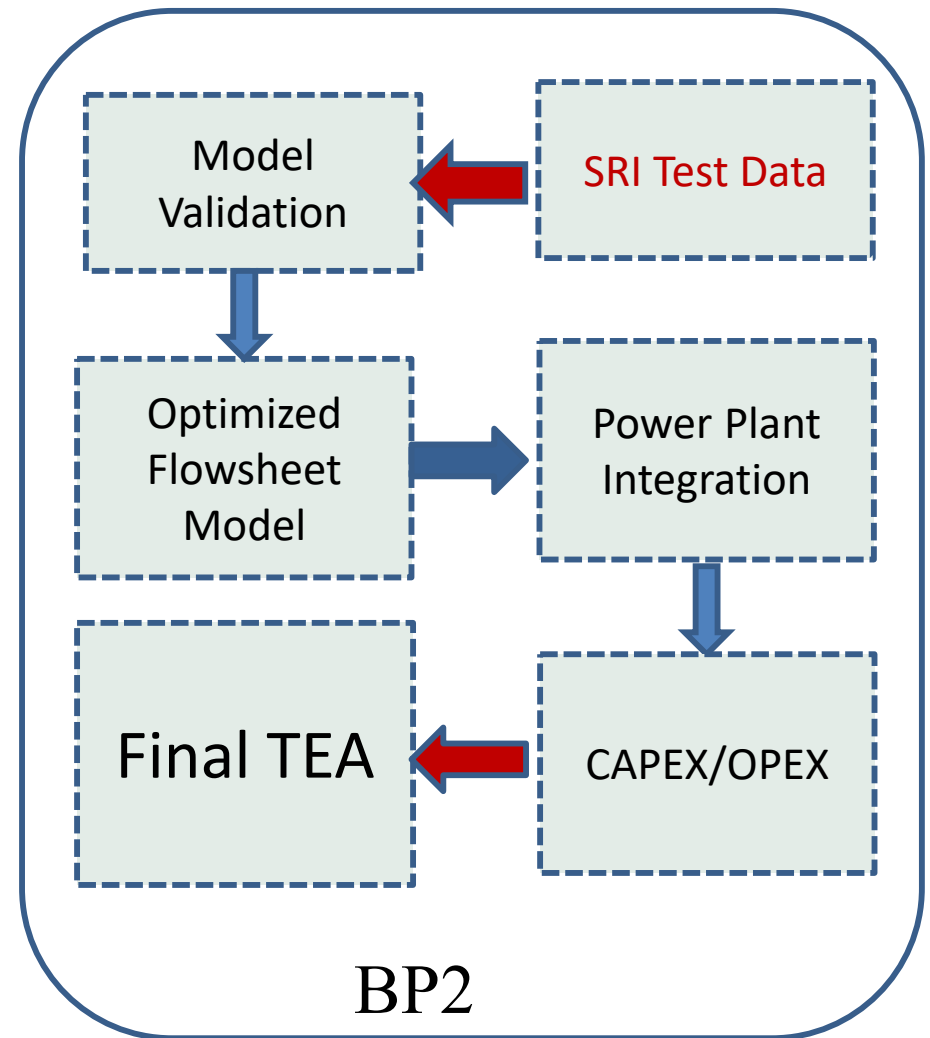
- Thermodynamic model validated with measured VLEs, calculate vapor/liquid compositions- DTU, SRI
- Rate based model to refine the performance under dynamic conditions- OLI Systems
- Preliminary flowsheet model to predict the performance of the process and calculate heat and mass balances of process streams for TEA - OLI Systems
- Preliminary Technoeconomic analysis- Trimeric Corporation

# Preliminary Technoeconomic Analysis

- Generation of stream tables with heat and mass balance data for TEA
  - Physical properties
    - Temperature, Pressure, pH, Moles(mol/hr), Mass(kg/hr), Volume (L/hr)
  - Phase Flows
    - Liquid moles (mol/hr), Vapor moles (mol/hr), Solid moles (mol/hr)
  - Phase Fraction
    - Liquid mole fraction, Vapor mole fraction, Solid mole fraction
  - Thermodynamic Properties
    - Enthalpy, Ionic strength, Density, Osmotic pressure, Viscosity
- Demonstrated regeneration energy performance consistent with the development pathway outlined for BP1.
  - Regeneration energy 2.2 GJ/tonne CO<sub>2</sub>
- Electricity requirements for the A-MSP are ~18% lower than Case B12B.

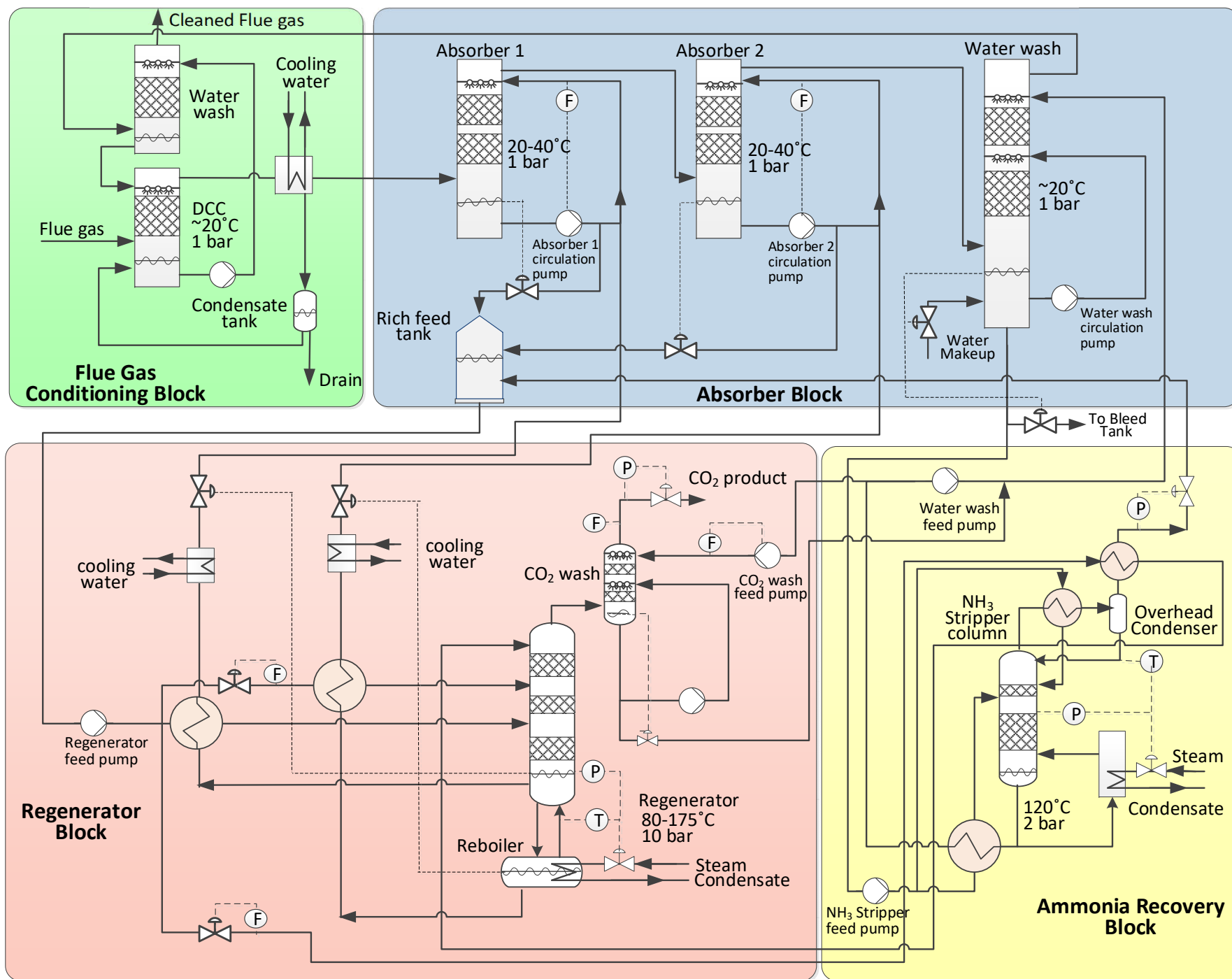
# Complete Flowsheet Model and TEA

- Model validation with integrated bench scale data
- Stream tables with heat and mass balances
- Sensitivity analysis to identify critical operating parameters
- Power plant integration
- Itemized costs of installed components





# Power Plant Integrated System



# Technology Gap Analysis

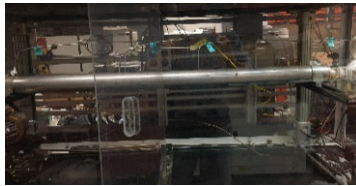
- Integration of column functions, particularly for the atmospheric pressure columns.
- Detail evaluation of column designs such as flooding, packing type, mass transfer performance
- Low-cost, alternative materials for absorption column construction.
- Regenerator design consideration-Alternative reboiler designs
- Regenerator and heat exchanger optimization to further reduce regeneration energy

# Technology Maturation Plan

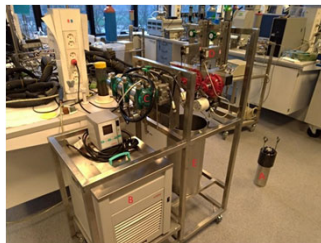
- TRL 2 to TRL 4

Proof of concept, kinetic studies,  
and small bench testing  
(1 to 40 *slpm*)  
2018-2020  
Budget Period 1

Large bench-scale testing  
200 to 400 *slpm*  
2021-2022  
Budget Period 2



*Lab-Scale Kinetic Study*



*V-L-E Study*



*Integrated testing  
at SRI*

*Slipstream Testing*

**Future Projects**

*Opportunities for reducing CO<sub>2</sub> from small and large-scale applications*



# Acknowledgements

## **NETL (DOE)**

- Krista Hill, Andrew Jones, Jose Figueroa, Lynn Bricket, John Litynski and other NETL staff members

## **SRI Team**

- Palitha Jayaweera , Indira Jayaweera, Elisabeth Perea, Milad Yavari, John Chau, William Olson, Chris Lantman

## **US and International Collaborators**

- SINTEF (Hanne Kvamsdal and Karl Anders Hoff)
- OLI Systems (Prodip Kondu, Ron Springer and Andre Anderko),
- DTU (Kaj Thomsen, Philip Loldrup Fosbøl and Lucas Farias Falcchi Corrêa)
- Trimeric Corporation (Andrew Sexton)
- Baker Hughes –Cost sharing partner

# Thank You

Contact:

Palitha Jayaweera

[palitha.jayaweera@sri.com](mailto:palitha.jayaweera@sri.com)

1-650-859-2989

**Headquarters**

333 Ravenswood Avenue  
Menlo Park, CA 94025  
+1.650.859.2000

Additional U.S. and  
international locations

**[www.sri.com](http://www.sri.com)**

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