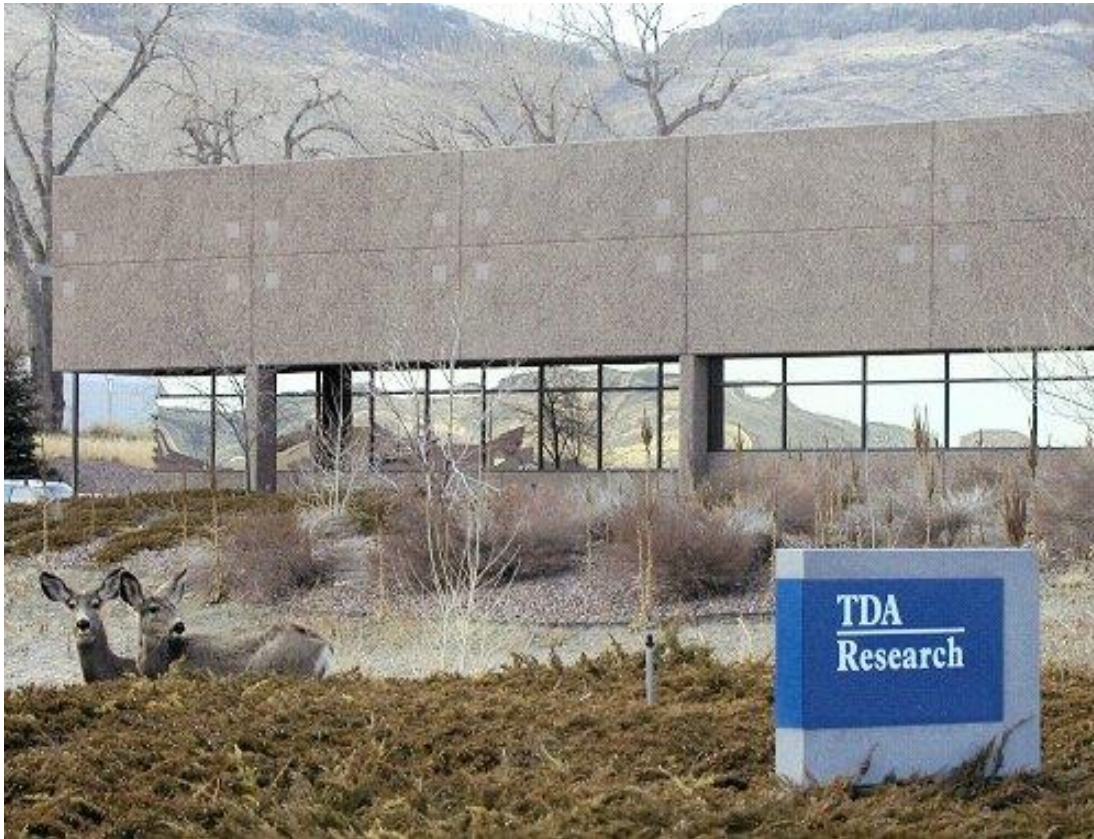


Transformational Sorbent System for Post-Combustion Carbon Capture (DE-FE0031734)



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**2022 Carbon Management Project
Review Meeting
Capture from Power Generation
Lab/Bench-Scale Research**

August 18, 2022

Project Objective and Team



Overall Project Duration

- Start Date = June 1, 2019
- End Date = May 31, 2024

Budget

- Project Cost = \$3,750,000
- DOE Share = \$3,000,000
- TDA and its partners = \$750,000

- **Objective is to develop a transformational sorbent based on a metal-organic framework (MOF)**
 - 90+% capture efficiency of CO₂
 - 95% purity recovered CO₂ purity
 - 30% lower costs than amine based systems with <\$30 per tonne of CO₂

• Main Project Tasks

BP1

- Demonstrate sorbent performance at the bench scale
- Assess impact of flue gas contaminants (SO₂, NO_x)
- Develop cycle sequence
- Preliminary TEA

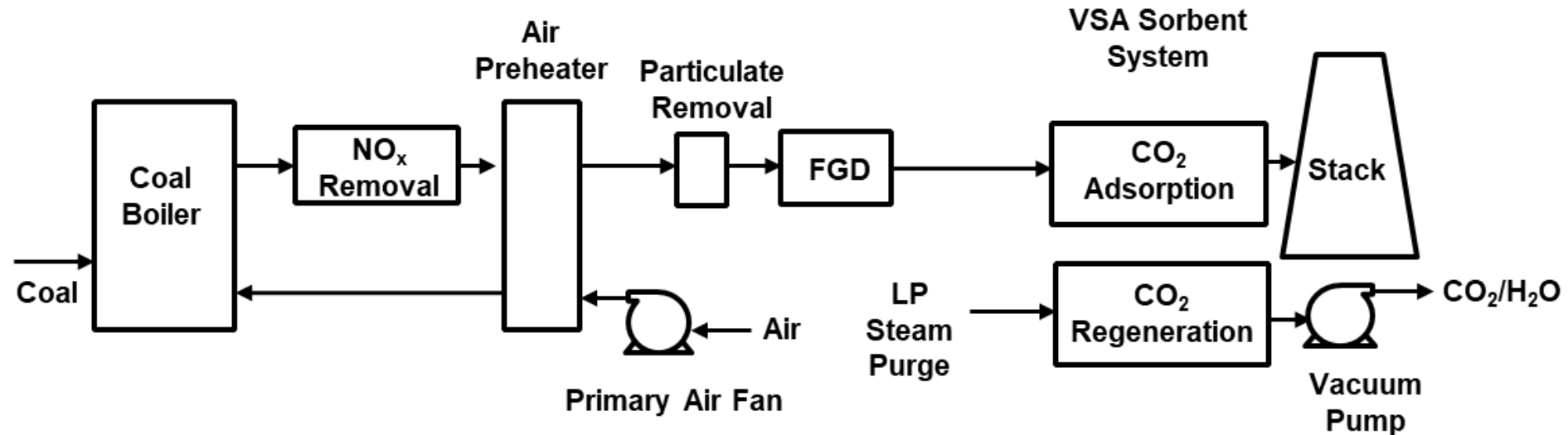
BP2

- Scale-up sorbent production
- Complete Life/Durability Tests
- Optimize adsorption cycles and update TEA

BP3

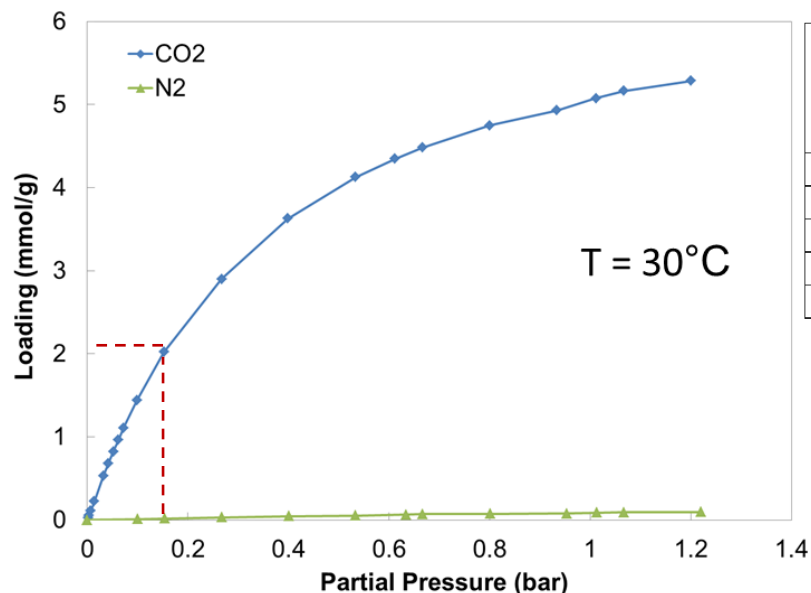
- Slipstream field tests (6 months)
- High Fidelity TEA and EH&S

Process Schematic



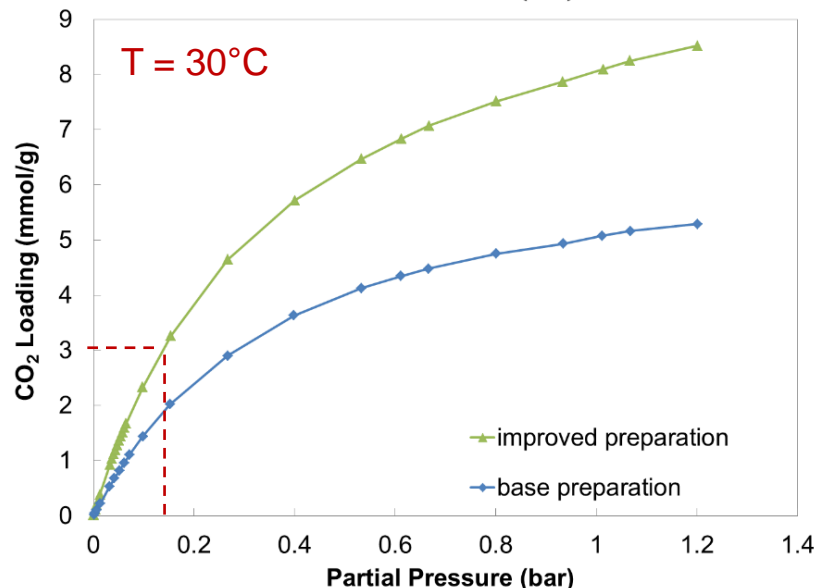
- **Sorbent operates between 30-50°C under vacuum (0.2-0.3 atm)**
 - Commercially available vacuum equipment
- **Capability to achieve 99% CO₂ removal efficiency**
- **High CO₂ selectivity results greater than 95% CO₂ product purity**
- **A new reactor design to ensure low pressure drop and reduced parasitic load**
- **Similar technology can also be applied to NGCC applications, with higher steam purge/energy penalty**

CO₂/N₂ Adsorption Isotherms

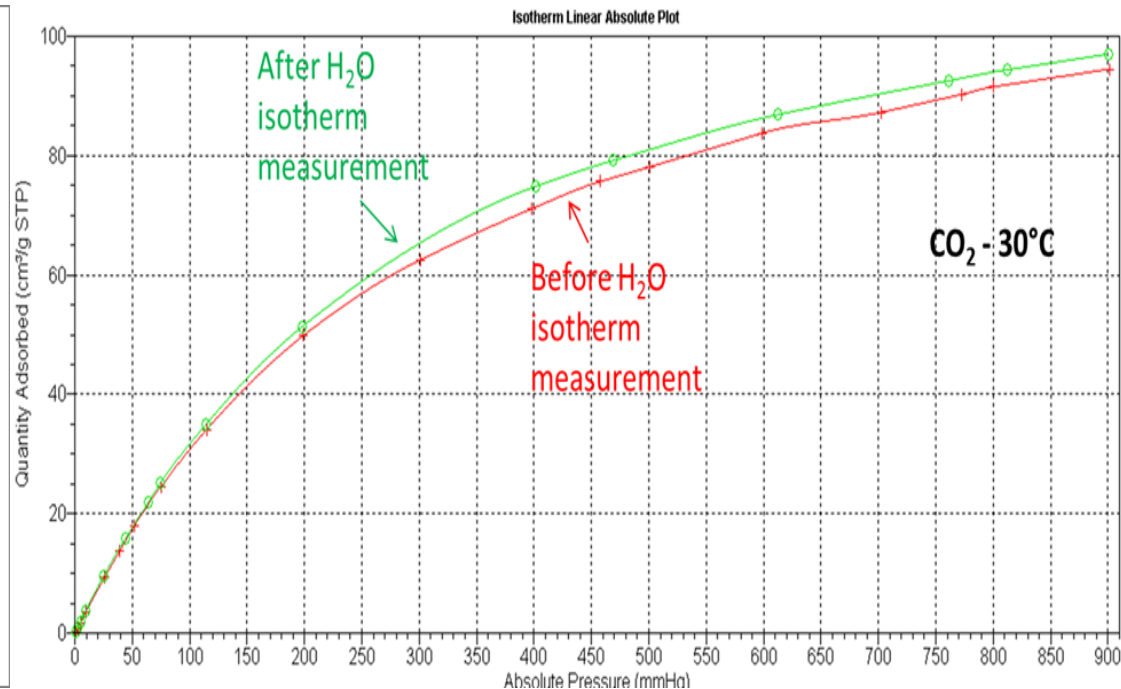
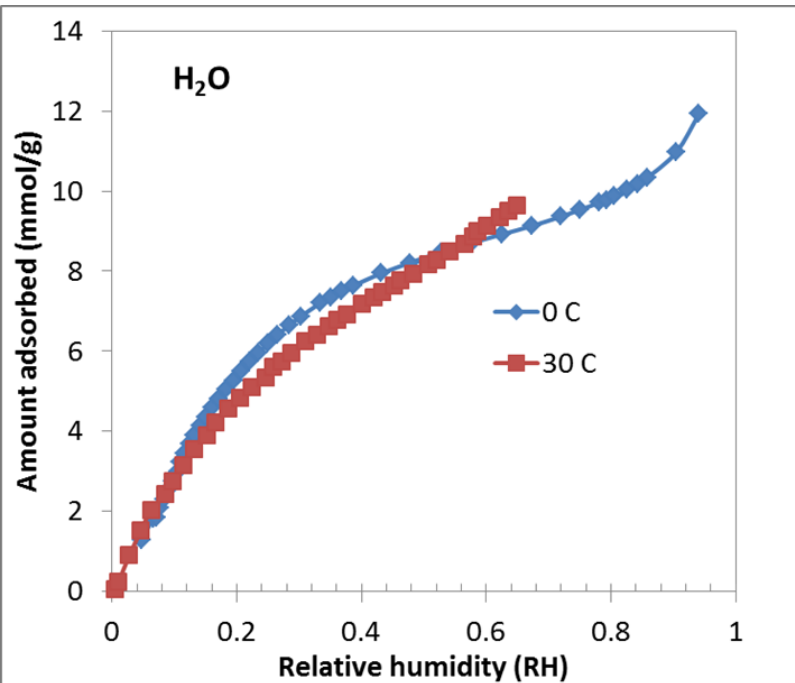


| Physical Parameter | Units | TDA's MOF Adsorbent | | TDA MOF P _{CO2} (bar) | Selectivity CO ₂ /N ₂ |
|-----------------------|--------------------|---------------------|----------------------|-----------------------------------|--|
| | | Base preparation | Improved preparation | | |
| BET Surface Area | m ² /g | 200.8 | 526.6 | 0.05 | 9.32 |
| Langmuir Surface Area | m ² /g | 246.4 | 618.2 | 0.1 | 16.29 |
| Nanoparticle Size | nm | 29.9 | 113.9 | 0.15 | 22.92 |
| Pore Volume | cm ³ /g | 0.134 | 0.342 | 1 | 57.52 |
| Median Pore Width | Å | 17.0 | 14.4 | | |

- **High CO₂ uptake**
 - >2 mmol/g at 0.15 bar
 - ~3 mmol/g for the modified version
- **Very high selectivity towards CO₂ over N₂, which ensures a very high product purity**
 - Over 95% without any downstream purification needs
- **Heat of adsorption of CO₂ is measured as 11 kcal/mol at low surface coverage and 8 kcal/mol at higher coverages**
- **Improvements in linker synthesis results in very high CO₂ uptake**

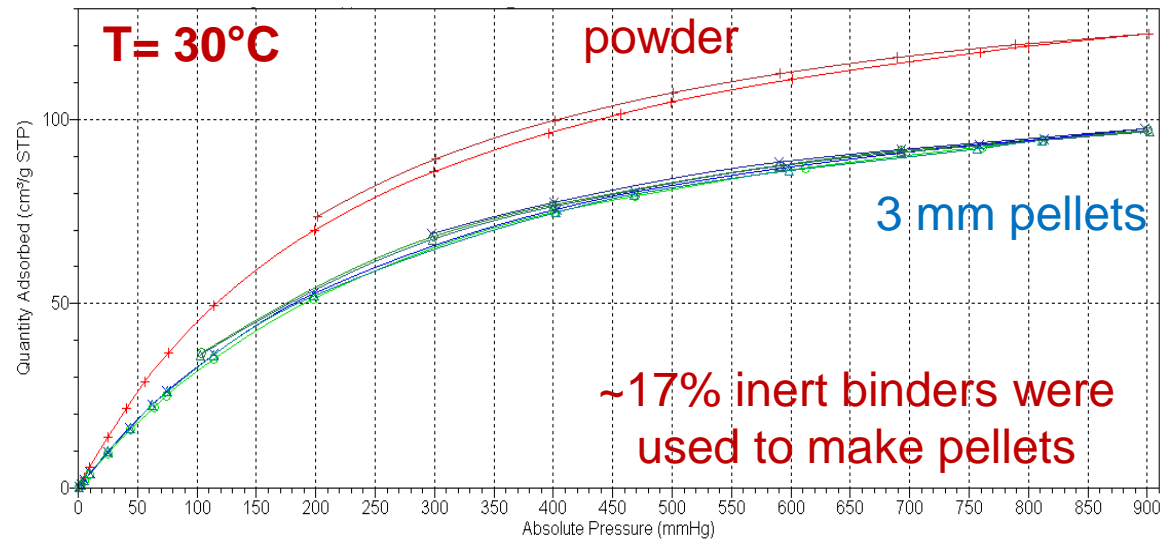
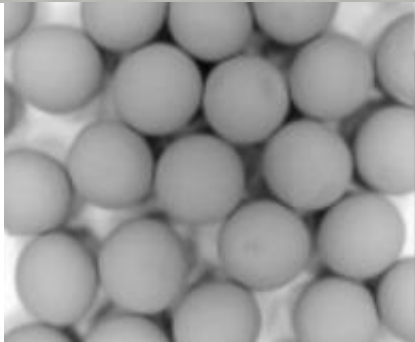


Water Adsorption Isotherms



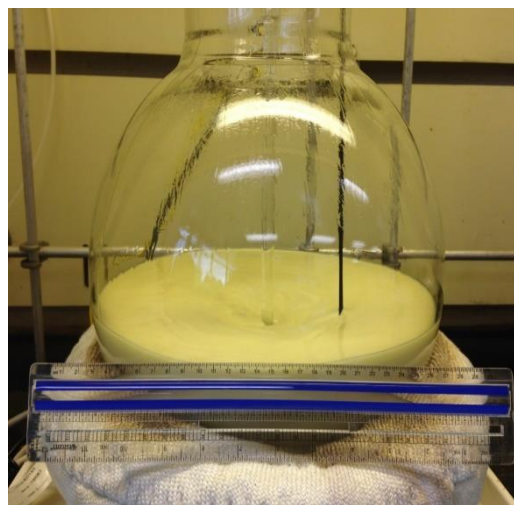
- Low pressure water isotherms are linear indicating that water easily desorbs from the sorbent surface
- No change in low pressure isotherm before and after water isotherm measurements

Pelletization of the MOF Sorbent



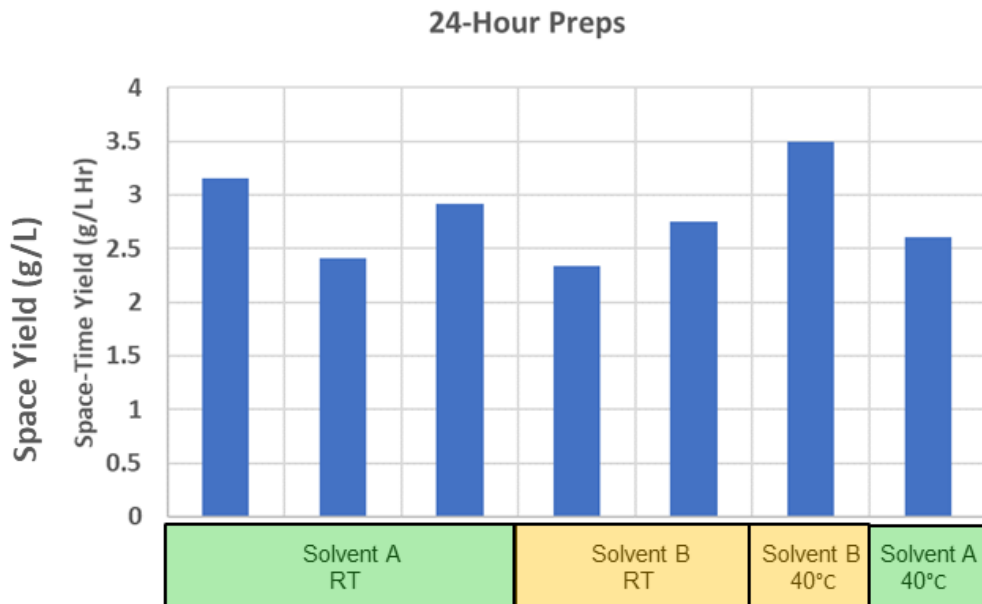
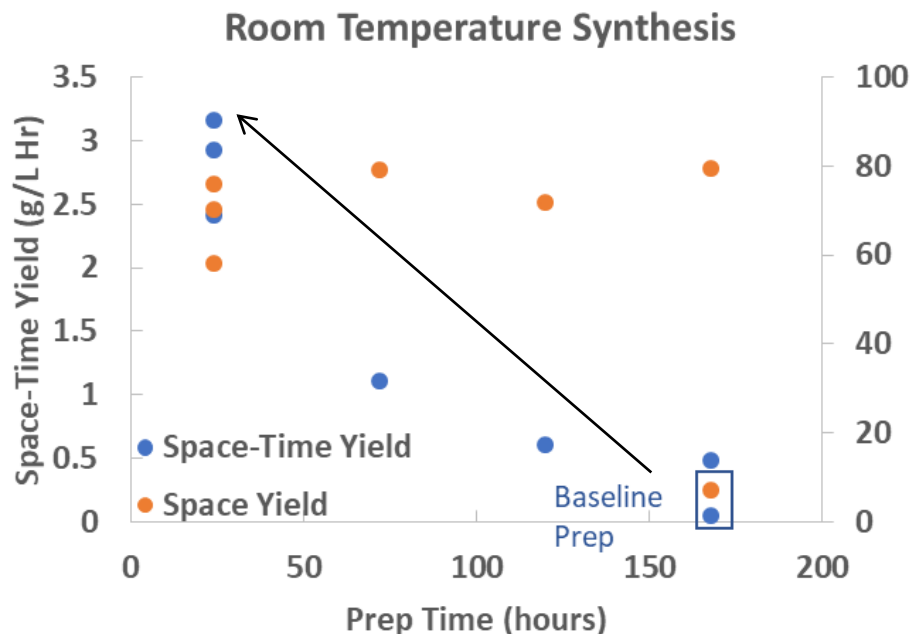
- MOFs are difficult to pelletize or granulate
- Conventional powder compaction techniques could potentially damage the MOF structure
- TDA developed a pill-pressing method that results in pelletized sorbent to retain >95% of their capacity when normalized based on active MOF weight

Scale-up of MOF Production



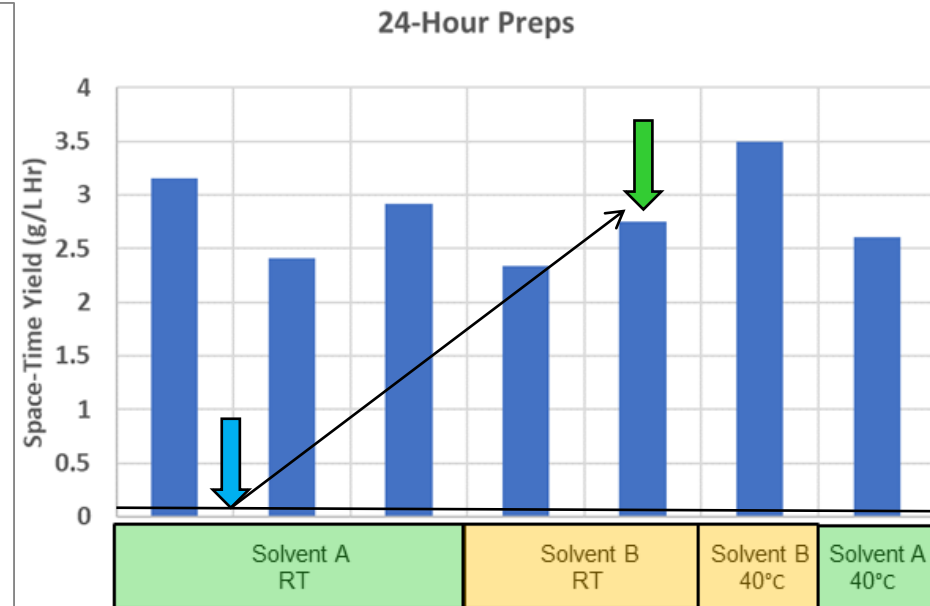
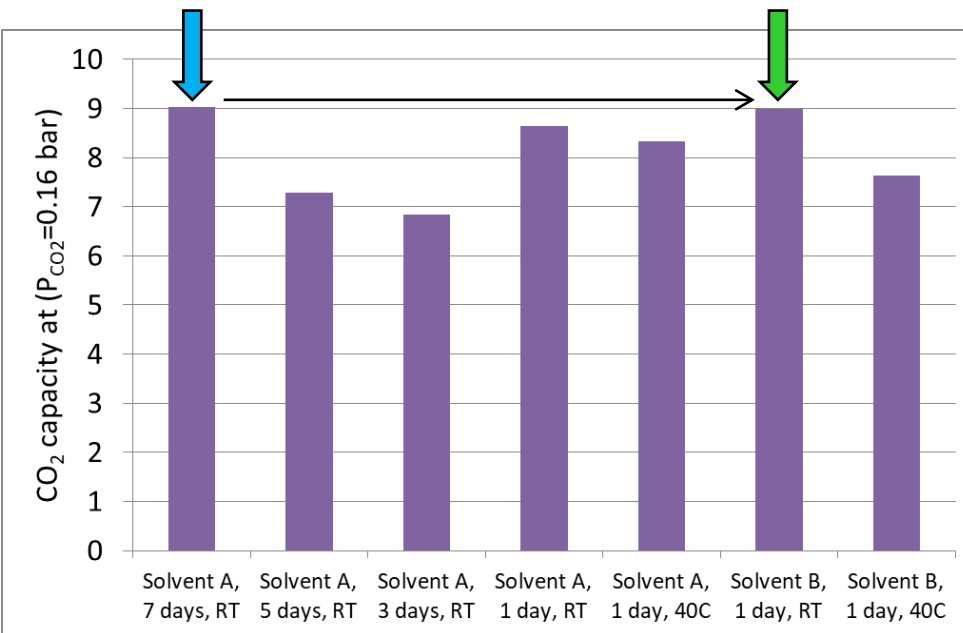
- **Scale-up from 1L to 22L flask and to 180L Hastelloy reactor in BP2**
- **BP1 evaluations have focused on improving synthesis parameters and space-time yields while conserving raw materials (via recycle)**
 - Space yield improvements of 10-15X
 - Time yield improvements of 5-8X
- **MOF synthesis, Filtration/Rinsing, Drying/Devolatilization are all sequentially carried out in the same reactor**
- **A classified area is designed and built to handle the equipment and solvents required for MOF processing**

Optimization of Space Time Yield



- Space Yield was increased from <10 g/L to 75-80 g/L
- Synthesis time was reduced from 7 days to 1 day (24 h)
- We were able to increase the space time yield from <0.1 g/L/hr to >3.0 g/L/hr

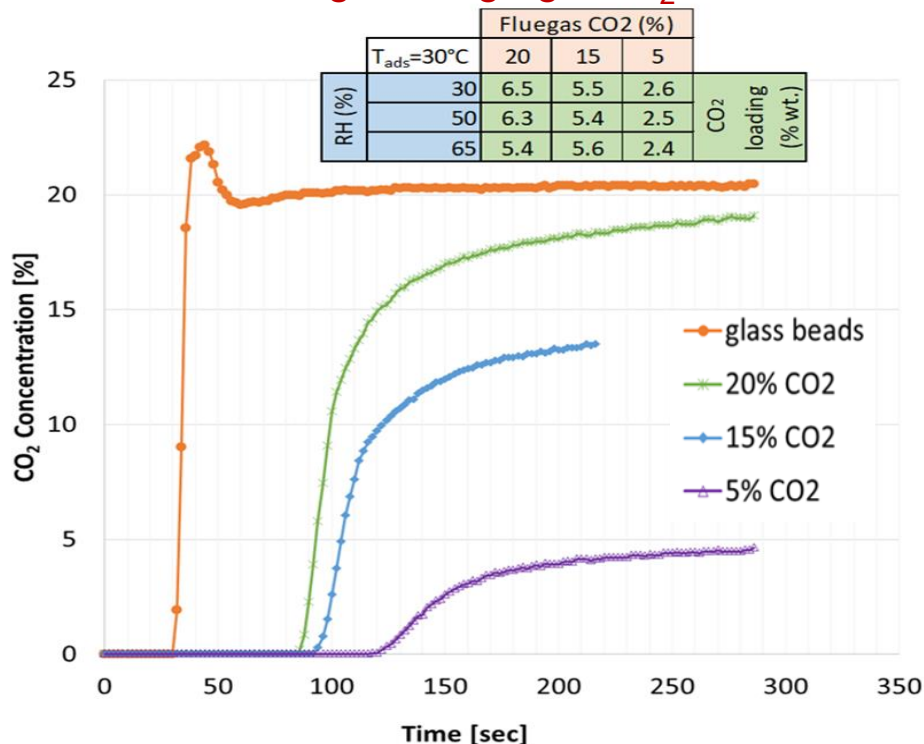
Sorbent Performance – Optimized Preparation



- **Reduced Preparation time of 24 hours was still able to provide a high yield while retaining the CO₂ adsorption capacity (Sorbent performance)**

Performance in Flow Experiments

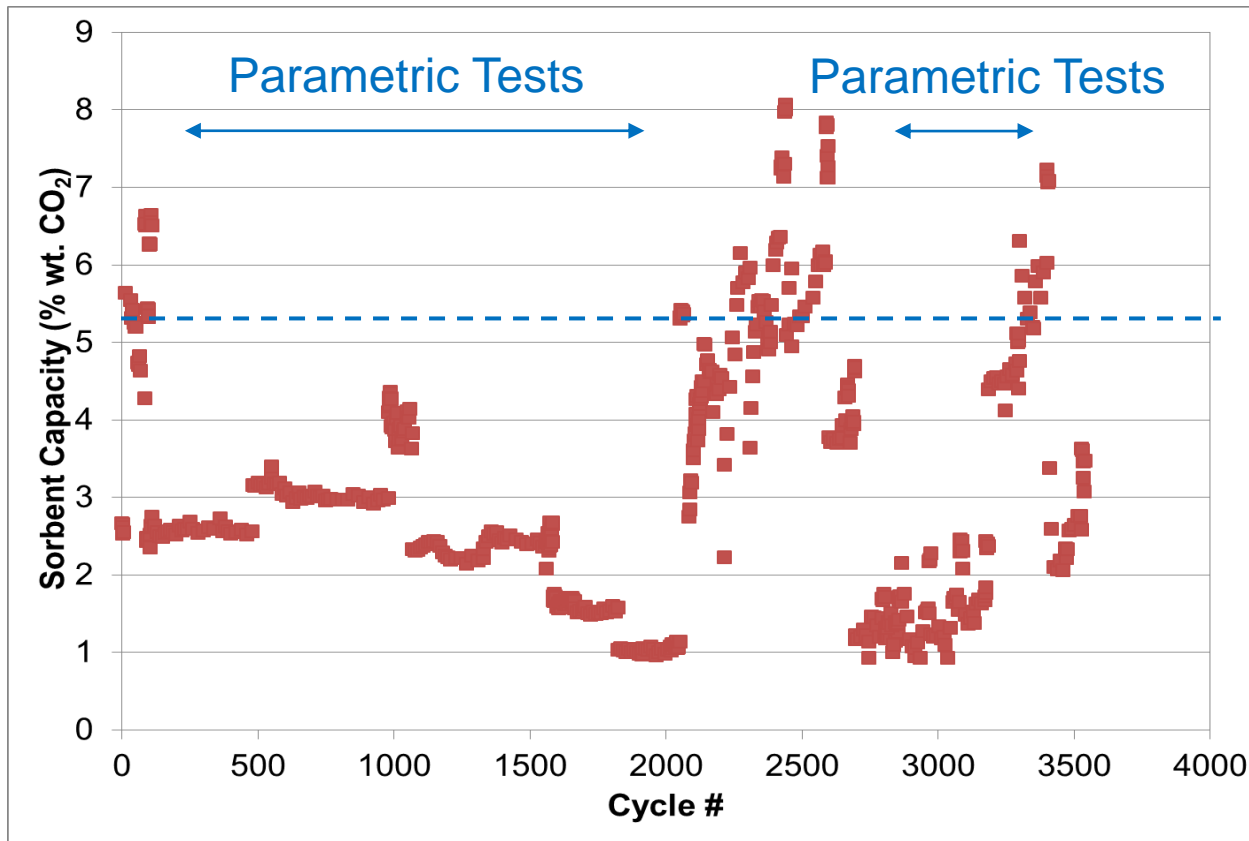
5/15/20% CO₂ in N₂ at T = 30°C, GHSV = 2,400 h⁻¹,
30/50/65% RH Regen Purge gas: N₂, Counter flows



- **A working capacity of 5+% wt. CO₂ at ~15% vol. CO₂ was demonstrated**
 - ~2.5% wt. CO₂ at 4% vol. CO₂
- **Temperature and humidity have limited impact on working capacity**
 - Higher temperatures lowered the working capacity
 - No significant impact of humidity up to 65%

Evaluation of Sorbent Life

5/15/20% CO₂ in N₂ at T = 30°C, GHSV = 2,400 h⁻¹, 30/50/65% RH
Regen Purge gas: N₂, Counter flows

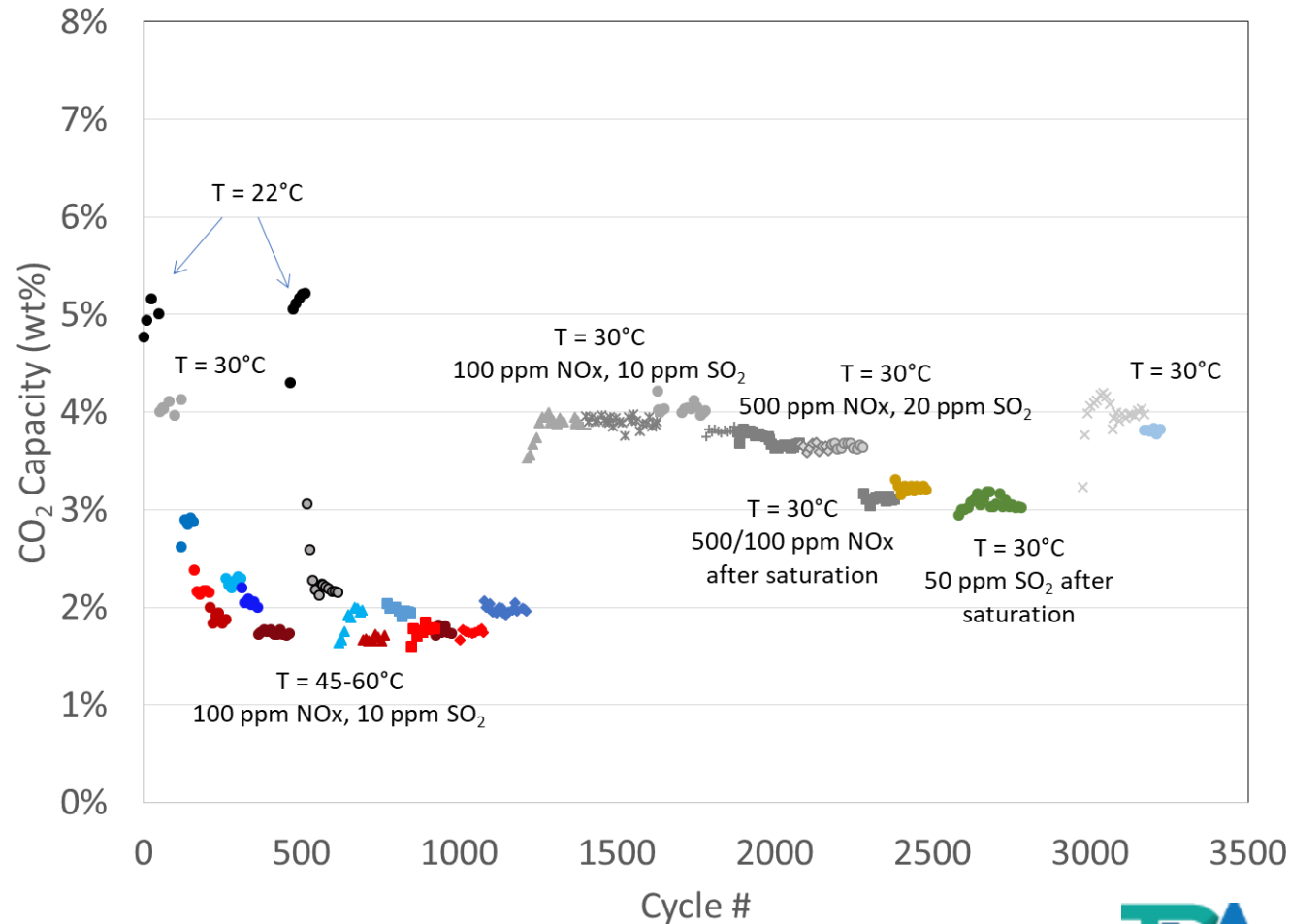


- A stable working capacity of 5.5% wt. CO₂ was demonstrated in counter flow desorption under simulated coal flue gas conditions

Life Tests in Presence of Contaminants

- **Stable working capacity in the presence of flue gas contaminants such as humidity, NO_x and SO_x**
- **High stability up to 65% RH, 500 ppm NO_x, 50 ppm SO_x**
- **Maximum ~20% drop in capacity under high SO_x and NO_x concentrations**

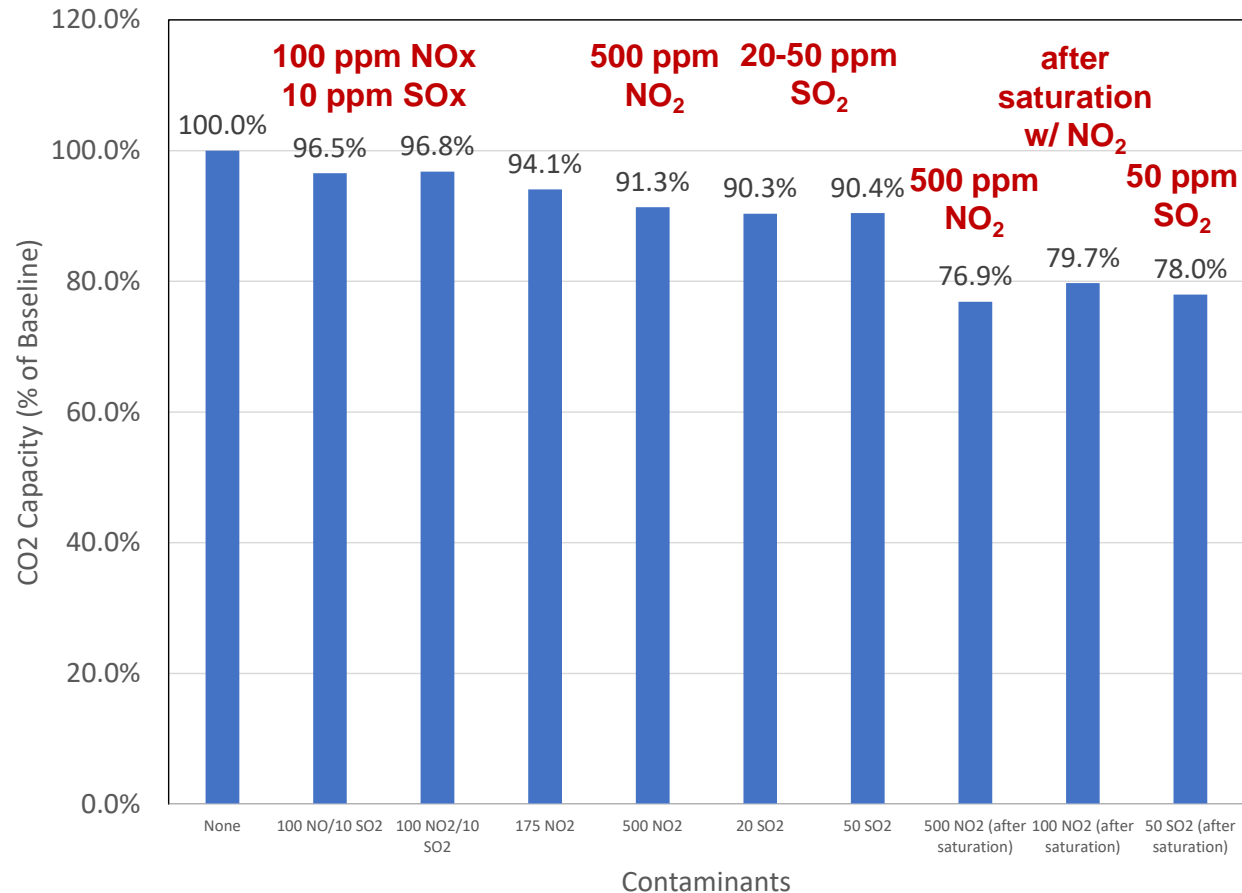
15% CO₂ in N₂ at T = 30/45/60°C, GHSV = 1,000 h⁻¹,
0-6% H₂O - Regen Purge gas: N₂, Counter flows



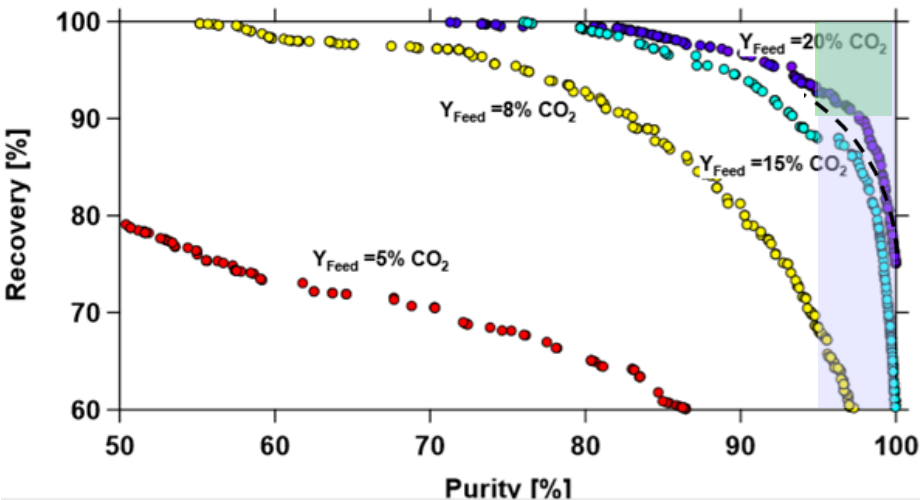
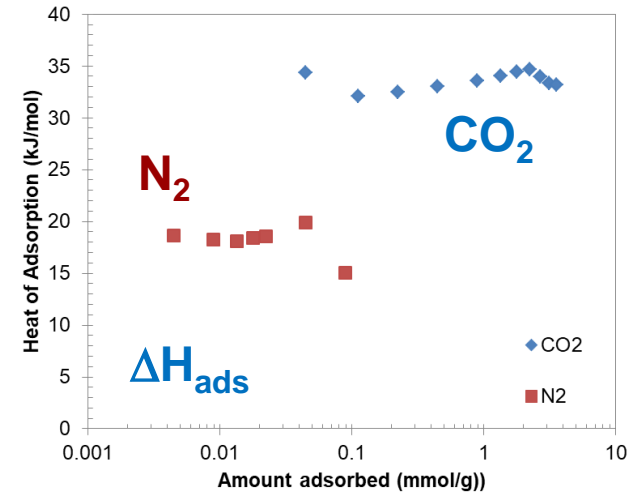
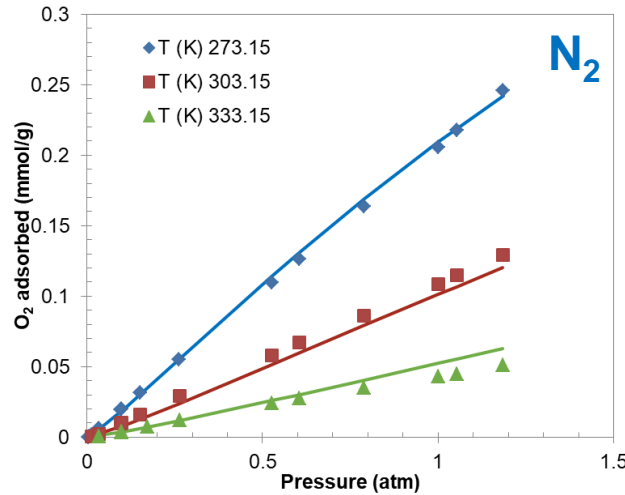
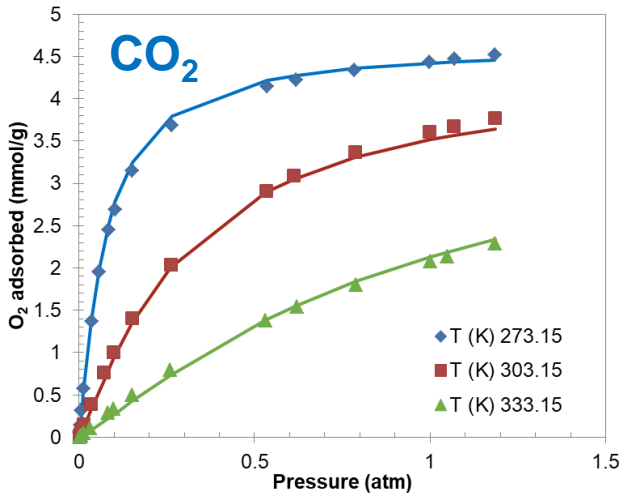
Impact of Contaminants

- Only <5% drop in working capacity was observed at 100 ppm NO_x and 10 ppm SO_x
- At 500 ppm NO_x and 50 ppm SO_x the working capacity dropped by 10%
- After saturating the sorbent with 500 ppm NO_x or 50 ppm SO_x the sorbent working capacity dropped by ~ 20%

15% CO₂ in N₂ at T = 30/45/60°C, GHSV = 1,000 h⁻¹, 0-6% H₂O - Regen Purge gas: N₂, Counter flows



Adsorption Cycle Modeling



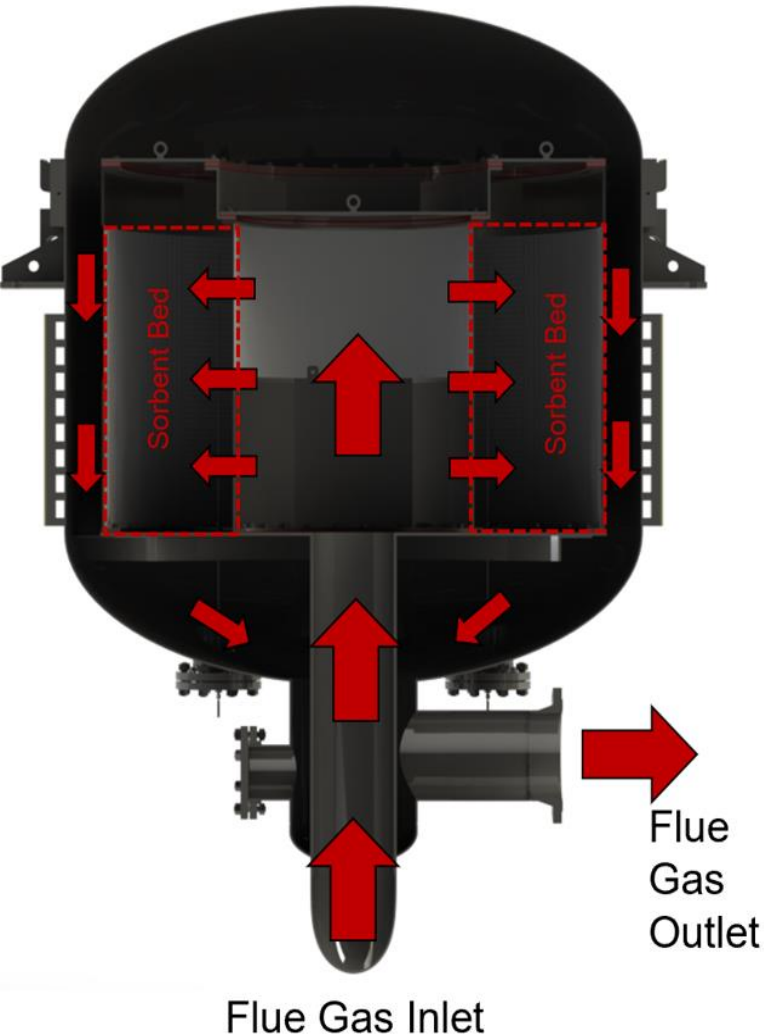
- Initial modeling results from University of Alberta shows simple cycle schemes without addition of steam purge can get close to DOE targets
- More advanced cycle schemes with steam assisted VSA results in 95% CO_2 purity with a CO_2 levels in flue gas as low as 4% (NGCC simulation)

Process Simulation (Rev. 4 basis)

| Capture Technology | Sorbent Only | Amine | No Capture |
|--------------------------------------|--------------|-------------|-------------|
| Case Studies | Case 1 | B12B | B12A |
| Gross Power, kWe | 795,063 | 770,000 | 685,000 |
| CO ₂ Capture/Removal, kWe | 47,679 | 29,530 | - |
| CO ₂ Purification, kWe | - | - | - |
| CO ₂ Compression, kWe | 58,141 | 44,380 | - |
| Balance of Plant, kWe | 39,243 | 46,050 | 35,040 |
| Total Auxiliaries, kWe | 145,063 | 119,960 | 35,040 |
| Net Power, kWe | 650,000 | 650,040 | 649,960 |
| Net Plant Efficiency, % HHV | 33.4 | 31.5 | 40.3 |
| Carbon Capture, % | 90 | 90 | 0 |
| Coal Feed Rate, kg/h | 258,208 | 273,628 | 214,112 |

- Energy for CO₂ capture is 26% lower compared to amine scrubbing

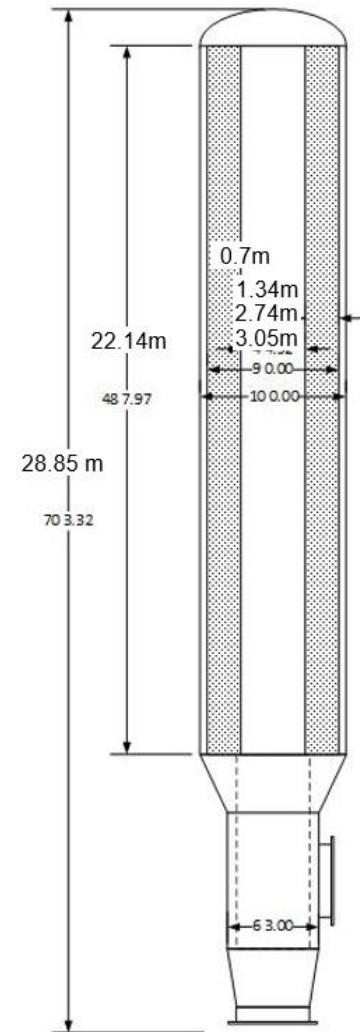
Reactor Vessel Design and Costing



Total ΔP (across the entire system)
=105 mbar

| | |
|-----------------------|---------------------------|
| Module Size: | 137.5 MW |
| No. of Trains: | 4 |
| Beds/Train: | 4 |
| Total Beds: | 16 |
| Flue Gas Flow: | 116.5 m ³ /s |
| CO ₂ Flow: | 1.96 tonne/min |
| Capacity: | 3.6% Wt% |
| Cycle Time: | 1 min |
| Sorbent Inventory: | 54.5 tonne/m ³ |
| Sorbent Density: | 0.55 tonne/m ³ |
| Bed Volume: | 99.5 m ³ |
| Bed Area: | 7.3 m ² |

- Four radial beds per train (total of 16 beds)
- SA516-70 carbon steel, 0.5" thickness
- 120 in OD x 872 in T/T

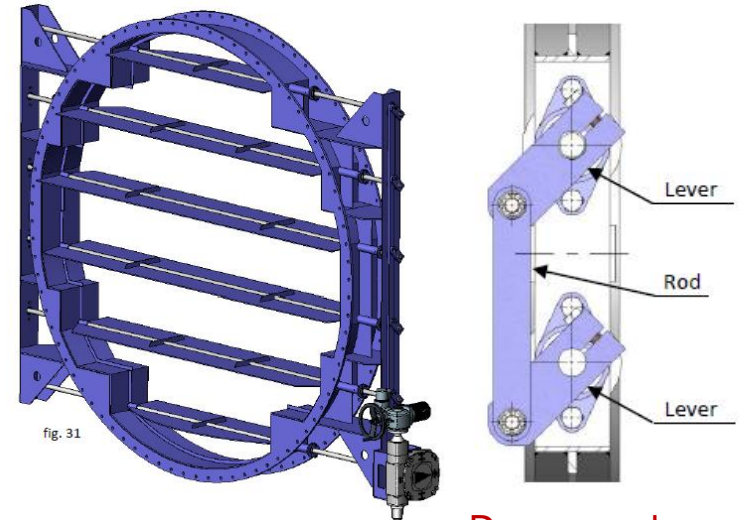


Reactor Vessel Design and Costing

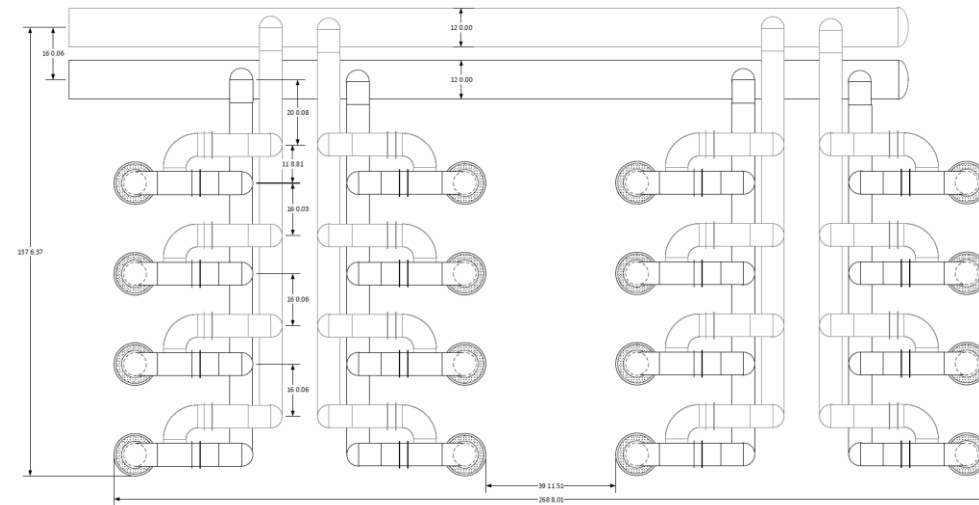
Sorbent Only System

| | Stage I | | Stage II | | Stage III | | Stage IV | |
|-------|---------|-----|----------|-----|-----------|-----|----------|-----|
| Bed 1 | | | | | | | | |
| Bed 2 | | | | | | | | |
| Bed 3 | | | | | | | | |
| Bed 4 | | | | | | | | |
| 336s | 21s | 21s | 21s | 21s | 21s | 21s | 21s | 21s |

| | | |
|--|--|-----------------------------|
| | Adsorption - Flue gas flow | Cocurrent Blowdown |
| | Desorption - CO ₂ Product Out | Desorption - Air Purge flow |

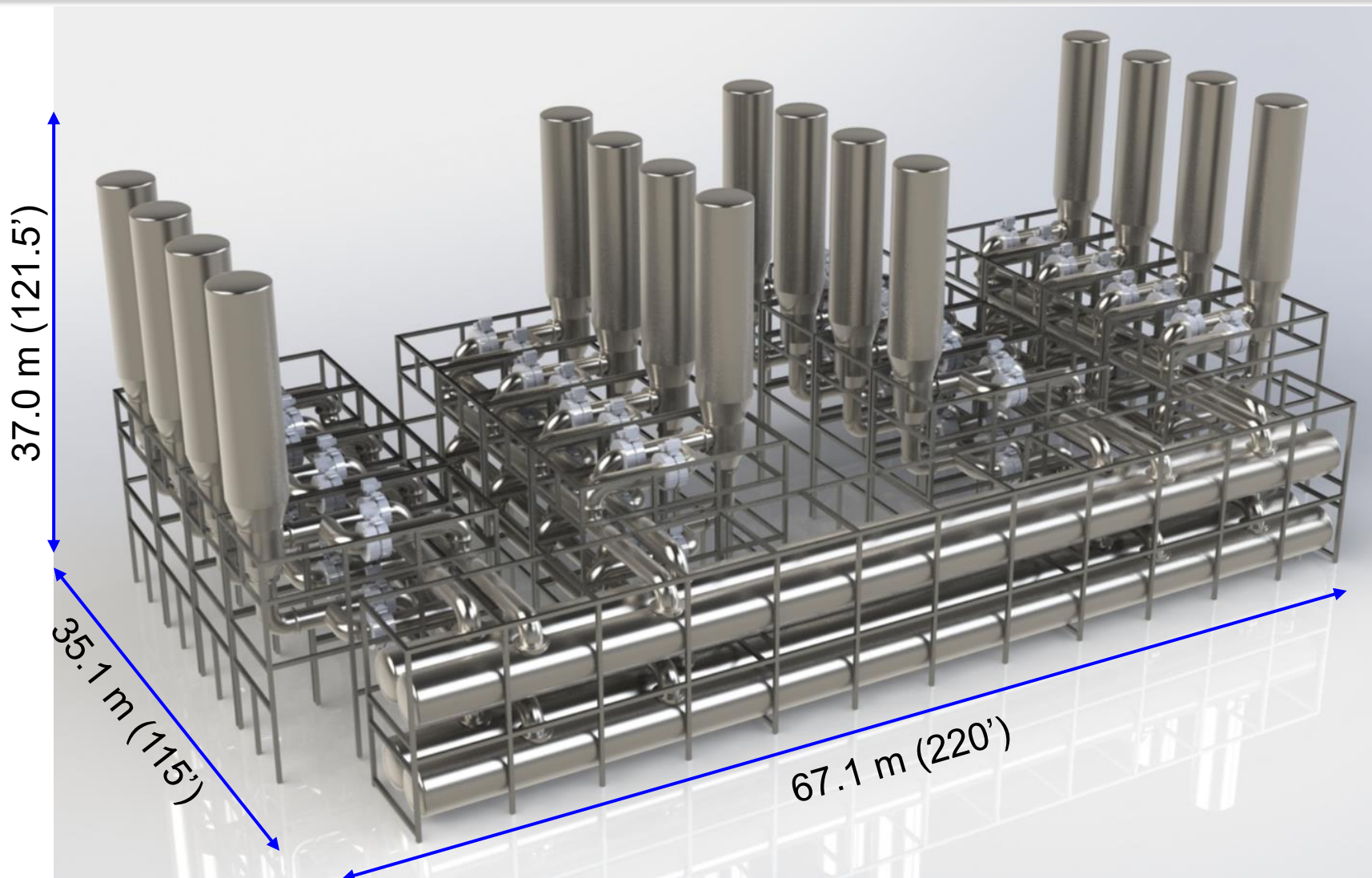


Damper valves
Price basis is 72" size



- Rapidly actuating valves are identified to change the bed position in a few seconds
- 60 in NPS, 0.375 in thickness (standard schedule) process piping for flue gas and air regeneration lines

3-D Layout of the Sorbent System

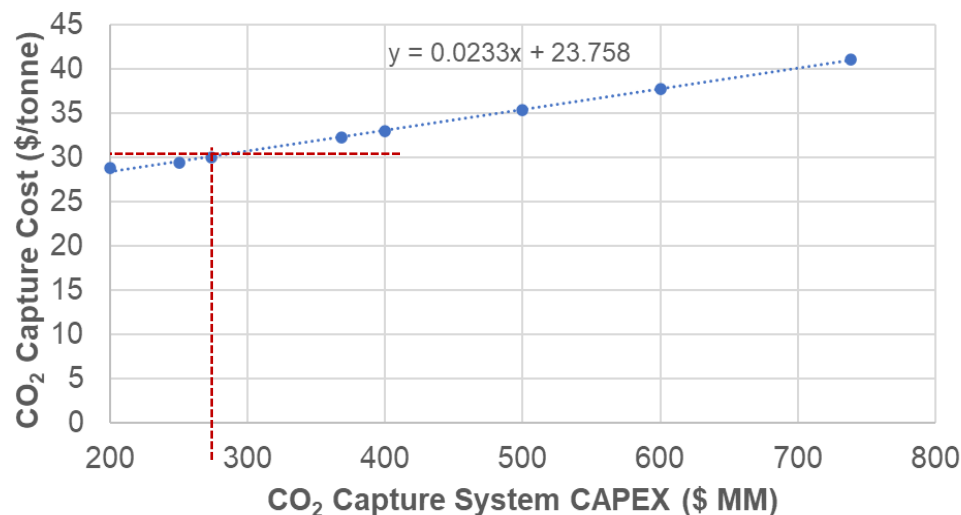


Cost of Capture Summary (Rev. 4 basis)

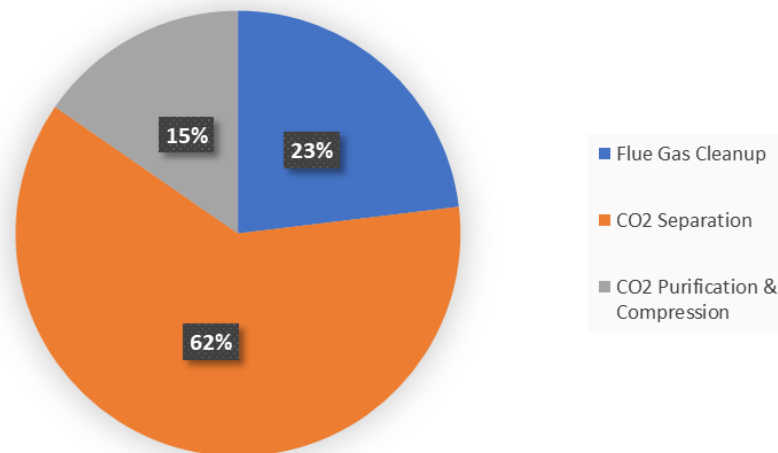
| Capture Technology | Sorbent Only | Amine | No Capture |
|--|-----------------|-----------------|-----------------|
| Case Studies | Case 1 | B12B | B12A |
| Basis for Cost Estimates (Year) | 2018 | 2018 | 2018 |
| Net power, MW | 650 | 650 | 650 |
| Capacity factor (CF), % | 85 | 85 | 85 |
| Total plant cost (TPC), \$ | 2,053,929,454 | 2,468,373,000 | 1,364,033,000 |
| Total overnight cost (TOC), \$ | 2,553,134,556 | 3,023,049,325 | 1,678,411,825 |
| Total as spent capital (TASC), \$ | 2,946,317,278 | 3,488,598,921 | 1,937,578,752 |
| LCOE | \$/MWh | \$/MWh | \$/MWh |
| Capital Charge (0.0707 X TASC) | 43.04 | 50.96 | 28.30 |
| Fixed Charges | 13.73 | 16.13 | 9.48 |
| Variable Costs | 12.15 | 14.00 | 7.72 |
| Fuel Costs | 22.75 | 24.08 | 18.87 |
| Byproducts (Credit) | 0.00 | 0.00 | 0.00 |
| Total (Excluding T&S) | 91.67 | 105.18 | 64.37 |
| CO2 T&S Costs | 8.45 | 8.96 | 0.00 |
| Total (Including T&S) | 100.12 | 114.14 | 64.37 |
| Cost of Capture | \$/tonne | \$/tonne | \$/tonne |
| Breakeven CO2 Sales Price (compared to SCPC W/O capture) | 32.25 | 45.52 | - |
| Breakeven CO2 emissions penalty (compared to SCPC W/O capture) | 52.29 | 73.40 | - |

- Cost of CO₂ capture with VLP steam purge is ~\$32.25/tonne
- Cost of CO₂ captured is considerably lower for TDA's CO₂ capture system about 29.2% lower the reference Amine Case

Sensitivity Analysis – CAPEX (Rev. 4 basis)



CO₂ Capture and FlueGas Cleanup



- Total cost of CO₂ Capture System including flue gas treatment and compression is \$368 MM
 - Cost of CO₂ capture ~\$32.25/tonne
- CAPEX for CO₂ capture needs to go below \$274 MM to meet transformational CO₂ capture targets (<\$30/tonne)

Acknowledgments

- DOE/NETL Project Manager - Andrew O'Palko
- University of Alberta - Dr. Arvind Rajendran
- University of California, Irvine - Dr. Ashok Rao (retired)
- Wyoming Integrated Test Center - Dr. Will Morris

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