

CCSI² Process Modeling and Optimization Highlights

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Presentation Outline

- Overview of CCSI² Program and CCSI Toolset
- Highlights of EY21 Work
 - Modeling and Optimization
 - Integrated NGCC-MEA System with High CO₂ Capture Levels
 - Advanced Flash Stripper Configuration
 - Sorbent Systems Metal Organic Framework
 - Large Pilot Support
 - RTI Non-Aqueous Solvent
 - MTR Membrane System
 - Hybrid TDA Sorbent / MTR Membrane System
 - Model Development CESAR1 Blend
- Future Directions in CCSI²
 - Industrial Capture Systems
 - Conceptual Design and Robust Optimization



CCSI² – Carbon Capture Simulation for Industry Impact

- CCSI² Mission: Accelerate CO₂ Capture Research and Development
 - Collaborations among national laboratories, academia, and industry to identify promising novel CCS technologies and reduce scale-up risk through rigorous modeling, optimization, uncertainty quantification, and economic analysis
 - Development of CCS models from multiple classes (solvents, sorbents, membrane technologies)
 - Maintenance and continuing development of CCSI Computational Toolset (2016 R&D 100 winner)
 - Flagship software platform FOQUS enables advanced modeling capabilities for process analysis

Upcoming Presentation:

CCSI² FOQUS/Toolset Capabilities Anuja Deshpande (NETL) Wednesday, August 17, 2022 (5:05 PM) Point Source Carbon Capture Session



https://github.com/CCSI-Toolset/foqus

https://github.com/CCSI-Toolset/



Solvent-Based CO₂ Capture: Techno–Economic Analysis for High Capture Levels

Project Objectives

- Optimize model of NGCC plant with aqueous MEA solvent-based CO₂ capture system for capture levels beyond net-zero emissions
- Understand incremental cost of high capture compare with direct air capture (DAC) and other net-negative emission technologies
- Understand optimal operation and design of CCS unit to achieve high capture with minimal increase in cost

Problem Formulation in FOQUS

Carbon Capture System Process Model (Aspen Plus [®])		Economic Model (Python)		Optimization	Formulation
Lean Loading MEA & H ₂ O Makeup CO ₂ to Compression Makeup	Variable Transfor	Calculates levelized cost of electricity (LCOE) for integrated NGCC-MEA		$\min_{\tilde{x}} f(\tilde{x})$ s.t.	Minimize LCOE
Absorber Packing Height Height Flue Gas (NGCC) Height Rich Solvent Temperature Flue Gas (NGCC) Height Reboiler Steam – from IP/LP Crossover In Sector	Iransfer I I I I I I I I	 System. Developed from: NETL cost and performance baseline [1] for NGCC system CSIRO study [2] for capture unit 	 	$\tilde{x}^{L} \leq \tilde{x} \leq \tilde{x}^{U}$	Bounded decision variables: design and operation of capture unit
				$h(\tilde{x})=0$	Fixed level of CO ₂ capture & material/energy balances
Decision Variables for Optimization Problem (\tilde{x})			 _	$g(\tilde{x}) \le 0$	Maximum flooding in columns: 80%

Poster Presentation: Deshpande, A., Morgan, J., Paul, B., Zamarripa, M., Matuszewski, M., Omell, B., **Techno-Economic Analysis and Optimization of Integrated NGCC – MEA System at High CO₂ Capture Levels**. [1] James, R., Zoelle, A., Keairns, D., Turner, M., Woods, M., Kuehn, N., 2019. Cost and performance Baseline for Fossil Energy Plants Volume 1: Bituminous Coal and Natural Gas to Electricity. NETL-PUB-22638

[2] Li, K., Leigh, W., Feron, P., Yu, H., Tade, M., 2016. Systematic study of aqueous monoethanolamine (MEA)-based CO₂ capture process: technoeconomic assessment of the MEA process and its improvement. Applied Energy 165: 648-659.

Solvent-Based CO₂ Capture: Techno–Economic Analysis for High Capture Levels

Optimization Results



Optimal lean loading remains flat for 90-95% CO₂ capture, and then decreases with increasing CO₂ capture to alleviate the rapid rise in reboiler duty and steam extraction. As a result, solvent circulation rate drops and absorber height increases.

Cost of Avoided Carbon

$$COAC[i] = \frac{LCOE[i] - LCOE[0]}{\frac{CO_2 \ Emissions[0]}{Plant \ Net \ Power[0]}} - \frac{CO_2 \ Emissions \ [i]}{Plant \ Net \ Power[i]}$$

[0] Plant without CO₂ capture

[i] Plant with given level of CO₂ capture

Incremental Cost of Avoided Carbon

 $\Delta COAC[i + \Delta i] = \frac{LCOE[i + \Delta i] - LCOE[i]}{\frac{CO_2 \ Emissions[i]}{Plant \ Net \ Power[i]} \frac{CO_2 \ Emissions \ [i + \Delta i]}{Plant \ Net \ Power[i + \Delta i]}}$

Associated with increase in CO_2 capture level from i to i+ Δi



Advanced Flash Stripper Modeling and Optimization



- AFS configuration increases heat recovery from stripper overhead vapor → trade-off in capital costs associated with additional heat exchangers
- Model development and optimization for aqueous solvent systems (MEA and piperazine) and novel water-lean CO₂BOL solvent system (collaboration with PNNL) with simple stripper and advanced flash stripper configurations
- Modeling results predict ~ 2% reduction in COE for aqueous solvent systems (subject to model and economic uncertainty) for AFS process but no improvement for CO₂BOL due to negligible water evaporation
- Future application of work: Conceptual design and superstructure optimization of advanced absorber and stripper configurations



Techno-Economic Analysis for Metal Organic Framework (MOF) – Based CO₂ Capture from NGCC Applications

Project Objectives

Isotherm Model

- Development of isotherm model for a tetraamine-appended MOF
- Development of fixed bed and moving bed contactor models
- Techno-economic optimization of post-combustion capture processes from NGCC flue gas



Process Models

Poster Presentation: Hughes, R., Caballero, D.Y., Zamarripa, M., Bhattacharyya, D., Matuszewski, M., Omell, B., Techno-Economic Analysis for MOF-based CO₂ Capture from NGCC Applications.



Techno-Economic Analysis for Metal Organic Framework (MOF) – Based CO₂ Capture from NGCC Applications

Optimization Problem

Process models (fixed and moving bed contactors) integrated with costing module and derivative free optimization algorithms within the FOQUS tool



Optimization Results

Compared to reference MEA system, the optimal cost of capture:

- Increases 48% for fixed bed process
- Decreases 9% for moving bed process

Fixed Bed Cost Breakdown

Moving Bed Cost Breakdown



Poster Presentation: Hughes, R., Caballero, D.Y., Zamarripa, M., Bhattacharyya, D., Matuszewski, M., Omell, B., Techno-Economic Analysis for MOF-based CO₂ Capture from NGCC Applications.





Photograph from www.tcmda.com



- catching our future

Large Pilot Support

- Multiple collaborations between CCSI² and industrial organizations focused on demonstration of novel CO₂ capture technologies at Norway's Technology Centre Mongstad (TCM) - one of the world's largest venues for testing capture technologies (~ 12 MWe)
- CCSI² contributed expertise in process modeling and sequential design of experiments (SDoE)
 - SDoE ensures efficient allocation of resources for expensive test campaigns → extract maximum information with a fixed budget
 - Forthcoming Presentation: SDoE Capabilities, Progress, and Applications (Abby Nachtsheim – Los Alamos National Laboratory)

INTERNATIONAL

Research Triangle Institute: Non-Aqueous Solvent (NAS)



Membrane Technology & Research: Novel Membrane System



TDA Research: Sorbent System



Large Pilot Support: RTI Non-Aqueous Solvent

Project Objectives

- Collaboration between RTI and CCSI² on multi-scale modeling of non-aqueous solvent system (NAS)
- Leverage SDoE to guide NAS test campaign at TCM → focused on demonstrating high levels of CO₂ capture with low solvent emissions and regeneration energy requirement

TCM Test Campaign

- CCSI² team contributed separate designed experiments for gas-fired combined heat and power (CHP) [3.7 vol% CO₂] and residual fluidized catalytic cracker (RFCC) [13.5 vol% CO₂] flue gas sources
- Each designed experiment includes a series of test matrices with 12-22 proposed operating conditions for flexibility in design size

<u>Design factors</u>: CO_2 Capture: 85 - 95%Absorber L/G Ratio: 2.5 - 6.5 kg/kg Stripper Pressure: 0.9 - 3.2 barg



- Ongoing work for development of thermodynamics and other sub-models of NAS solvent system, followed by validation of process models for TCM (12 MWe) and Tiller (60 kWe) pilot plant facilities.
- Work expected to wrap up at the end of 2022



Large Pilot Support: Membrane Technology Research

Project Highlights

- 1D model developed for MTR flat sheet membrane with non-uniform channel heights
- SDoE performed with commercial nitrogen membrane model to demonstrate the potential for stochastic parameter estimation

Flat Sheet Membrane Model



Example of MTR's 100 m² plate-and-frame module.



Iterative Solution Methodology Membrane Performance Compared to Ideal Module Initialize h_{layer} and ΔP Calculate 0.8 permeate until Integration convergence Solve Q_{tot} , Q_R Along Length 0.7 **Recovery in Retentate** 0.0 0.0 0.0 0.0 0.0 Given x_i , calculate y_i Calculate Q_n using Flux eqns Update $y_{i,new}$ with Q_i 0.2 O Update $Q_{R,new}$ ΔP based on $Q_{tot,new}$ within 0.1 solution range? 0 0 0.005 0.01 0.015 0.02 0.025 0.03 0.035 **CO₂ Retentate Composition** Calculate x_i , y_i -- Ideal -- Matlab - Ideal -- Matlab - Variation

Large Pilot Support: TDA-MTR Technology



Primary Air Fan

Model Developed and Validated at Multiple Scales

SBIR Phase II B: Hybrid Membrane/Sorbent System for Capture 1 ton/day CO₂



50 kWe system



More instrumentation than SBIR Phase II B System

Adsorption-desorption cycle data available

TCM (1 MWe system)

- Highly instrumented
- Can blank off 50%
- of the bed to avoid channeling at low flow
- Design of experiments developed for test runs to be conducted in Dec 2022 – Jan 2023



Future work will focus on validation with additional data from TCM, process optimization, and uncertainty quantification



Model Development and Validation – CESAR1

- CESAR (CO₂ Enhanced Separation and Recovery) project funded by EU (2008-2011)
- CESAR1: Aqueous blend of 2-amino-2-methyl-1-propanol (AMP) and piperazine (PZ)



- Blended system combines advantages associated with PZ (high reactivity) and AMP (relatively low heat requirement for solvent regeneration)
- Process model developed and validated with seven steady-state data sets collected from ALIGN-CCUS campaign at TCM (12 MWe) using natural gasbased combined cycle turbine flue gas





Model Development and Validation – CESAR1

Model Validation Data

	C5	D5	E1	F4	AA2	BB3	A5
Absorber	18	18	12	18	24	24	24
Packing Height (m)							
Flue Gas Flowrate	59853	59803	59821	70675	60101	60086	60451
(kg/hr)							
Absorber L:G Mass	0.66	0.92	1.09	0.57	0.74	0.58	0.66
Ratio							
Lean CO ₂ Loading	0.135	0.109	0.147	0.087	0.135	0.049	0.176
(mol CO ₂ /mol alkalinity)							
Rich CO ₂ Loading	0.404	0.314	0.312	0.402	NA	0.415	0.454
(mol CO ₂ /mol alkalinity)							
Lean Solvent Molality	5.206/	5.077/	4.907/	5.022/	5.460/	5.541/	4.490/
(AMP/PZ)	2.616	2.669	2.574	2.470	2.482	2.492	2.314
Flue Gas	40.00	40.12	40.15	40.20	40.13	40.17	30.43
Temperature (°C)							
Stripper Pressure (kPa)	191.9	191.9	191.8	221.4	192.0	192.1	191.4



Average percent error

- Future work will focus on uncertainty quantification in process submodels (e.g., thermodynamics, mass transfer/interfacial area, reaction kinetics, hydraulics)
- Model will be released to open-source CCSI Toolset and applied to process modeling efforts in the Sustainable OPeration of post-combustion Capture plants (SCOPE) program → focus on characterization of amine emissions



CCSI² Process Modeling: Future Directions (EY22 and Beyond)

• Pilot Support

- Wrap-up of TCM SDoE projects (RTI, MTR, TDA)
- Initiate work on small-pilot support for natural gas-based point sources

Solid Sorbent Technology Initial work will focus on development of rotary packed bed contactor model

Develop generic capabilities for sorbent properties and kinetic modeling

Implement newly-developed capabilities in sciencebased design of experiments (SBDoE) for testing technology at pilot scale

- Industrial Capture Modeling
- Conceptual Design and Robust Optimization
- Development of Rigorous Cost Analysis Methods for CCS Equipment

EEMPA Solvent System

Low-aqueous diamine solvent system developed by PNNL to be tested at National Carbon Capture Center (~ 0.5 MWe)

Initial work will focus on model development and improvement through bench-scale experimentation and uncertainty quantification



Pacific Northwest



Industrial Capture Modeling & Pilot Support

Preliminary Analysis

• Integrated cement kiln model (MATLAB) with MEA-based carbon capture model (Aspen Plus) in FOQUS



Future Directions

- Rigorous modeling of steel production process with focus on understanding key sources of emissions and energy consumption and integration with CCS systems
- Initiate work on characterization of cryogenic CO₂ separation with focus on modeling thermodynamic processes and heat integration
- Expected to provide support to pilot projects for CCS from industrial sources



Conceptual Design and Robust Optimization

Motivation

- Achieving net-zero CO₂ emissions in CCS applications in an economically efficient manner requires consideration of various classes (solvents, sorbents, membranes, etc.) and configurations of technologies → need for rigorous process modeling and optimization
- Complexity of modeling effort compounded by economic and epistemic uncertainties in process sub-models and variability in feedstock quality

Example: Decision Points for Solvent-Based CO₂ Systems



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Conceptual Design and Robust Optimization



Application areas include superstructure-based optimization under uncertainty for advanced configurations of solvent-based CO₂ capture systems



Robust Optimization – PyROS Capability in IDAES

MEA Solvent System Example

- Optimization Problem: Minimize equivalent annual cost of CO₂ capture unit subject to minimum capture of 85%
- Decision variables: Absorber and stripper sizes, lean-rich heat exchanger area
- Control variables: Reboiler and condenser duties



$$2 MEA + CO_2 \stackrel{K_{eq-1}}{\longleftrightarrow} MEA^+ + MEACOO^-$$
$$MEA + CO_2 + H_2O \stackrel{K_{eq-2}}{\longleftrightarrow} MEA^+ + HCO_3^-$$
$$K_{eq-1} = a_1 + b_1 \ln(T) + \frac{c_1}{T}$$
$$K_{eq-2} = a_2 + b_2 \ln(T) + \frac{c_2}{T}$$
Uncertain Parameters

Advanced Energy SN

 Generalized Robust Cutting Set (GRCS) algorithm yields optimal robust solution in four iterations – constraints satisfied for full parametric uncertainty set

Capability can be leveraged in future CCSI² work to ensure process designs for systems with high levels
of CO₂ capture are robust in light of epistemic uncertainty associated with property and process submodels

Example adapted from:

Isenberg NM, Akula P, Eslick JC, Bhattacharyya D, Miller DC, Gounaris CE, 2020. A generalized cutting-set approach for nonlinear robust optimization in process systems engineering. *AIChE J*. 2021;67:e17175 <u>https://doi.org/10.1002/aic.17175</u>



Summary and Conclusions

- Multi-year collaborations with industrial partners testing novel CCS systems at TCM have resulted in successful test campaigns and improved understanding of technologies
 - Established statistical approaches to experimental design as best practice for pilot testing
 - Pilot support will remain foundational in CCSI² work in EY22 and beyond
- Process modeling efforts are shifting away from CCS system operation at baseline levels (e.g., 90%) to focus on higher capture levels - up to net-zero emissions for natural gas source systems
 - Necessitates enhanced focus on risk assessment through economic analysis, UQ, robust optimization, and conceptual design → synergistic application of these tools across projects will be a major EY22 priority
- New CCSI² projects initiated in EY22 will focus on expanding capabilities to industrial source CCS applications





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For more information <u>https://www.acceleratecarboncapture.org/</u>

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Backup Slides



TDA-MTR Technology*

- Membrane captures about 50% of CO₂ while the remaining desired amount of CO₂ is removed by TDA sorbent
- Boiled feed air is used as sweep gas for sorbent regeneration
- Solid sorbent is a mesoporous carbon with a surface functional group capturing CO₂ by physisorption
- Multi-scale radial-flow bed model developed by modeling both the bulk scale and particle scale and by incorporating inter-particle and intra-particle mass and heat transfer resistances.
- Particle scale model is validated using data available for functionalized MOF
- Model developed and validated for 3 scales





Three Different Systems Modeled



- SBIR Phase II B: Hybrid membrane sorbent system for capturing 1 ton CO₂ per day
- Lack of measurements



- 'Small Scale' system: 50
 kWe
- Adsorption-desorption cycle data available

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 More instrumented than the SBIR Phase II system



- TCM pilot plant: 1 MWe
- Highly instrumented
- Can blank off 50% of the bed to avoid channeling at low flow
- DoE developed for test runs conducted in December,2022-January, 2023



Model Validation and Observation

- Under same inlet conditions for adsorption and for same bed height and same solid volume, axial flow and radial flow beds have similar bed average loading and breakthrough time, but the pressure drop through the radial flow beds is about two order of magnitude lower than axial flow beds.
- For regeneration of the bed from similar initial loading to similar end-of-the desorption bed average loading, axial flow beds took about 3-5 times longer time for regeneration.
- Higher entrance loading for radial-flow due to higher surface area that facilitates easier cooling of solids at the entrance
- Future work will focus on validation with additional data from TCM, optimization and uncertainty quantification





Large Pilot Support: Membrane Technology Research

SDoE Performed for Commercial Nitrogen Module



Initial USF Design

NUSF Design – Targeted Regions with Greatest Model Discrepancy



with Greatest Model I



Stochastic Parameter Estimation



Q02; QN2 \rightarrow Permeance of O₂ and N₂

Framework for Optimization, Quantification of Uncertainty, and Surrogates



Comprehensive Analysis of Process Systems



Poster Presentation: Paul, B., Deshpande, A., Zamarripa, M., Boverhof, J., Sotorrio, P., Bartoldson, B., Caballero, D., Hughes, R., Matuszewski, M., Omell, B., **Framework for Optimization, Quantification of Uncertainty, and Surrogates – Updated Capabilities**.