

## Electrochemically Regenerated Solvent for Direct Air Capture with Cogeneration of Hydrogen at Bench-Scale DE-FE0032125

Ayo Omosebi, Xin Gao and Kunlei Liu University of Kentucky

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Funding: DOE \$1,313,887 and Cost Share \$329,084

Overall Project Performance Dates: 10/1/2021 – 9/31/2023

Project Participants: University of Kentucky, Vanderbilt University, and EPRI



#### **Project Objectives**

- Developing a capture technology to extract  $CO_2$  from the atmosphere that reduces the cost of capture through:
- Developing a 2-unit process operation with ≥90% CO<sub>2</sub> capture at gaseous pressure drop ≤0.2 psi in the CO<sub>2</sub> absorber while regenerating CO<sub>2</sub> at less than 3.5 V in the ER by using a catalytic electrode
- Achieving a H<sup>+</sup>/K<sup>+</sup> crossover (through a cation-exchange membrane) ratio of  $\leq 15\%$  in the ER by optimizing a flow channel design, and spacer thickness;
- Demonstrating a continuous and reliable DAC process at the air flow rate of 10 cfm with ≥90% CO<sub>2</sub> capture efficiency for ≥100 hours, thereby establishing the data for the next-scale development.

# **Technology Background**



<u>Key Electrochemical Reactions</u> (0V,  $2H_2O$  + electrons =  $H_2$  +  $2OH^-$ ) (-1.2V,  $2H_2O$  =  $O_2$  +  $4H^+$  + electrons)

$$\frac{CO_2 \text{ Capture}}{CO_2 + 2OH^2} = CO_3^{2^2} + H_2O$$
(Fast)

$$\frac{\text{CO}_2 \text{ Release}}{\text{H}^+ + \text{CO}_3^{2-} \rightarrow \text{HCO}_3^{-}}$$

 $H^+ + HCO_3^- \rightarrow CO_2 + H_2O$ or 2HCO<sub>3</sub><sup>-</sup> → CO<sub>2</sub> + CO<sub>3</sub><sup>2-</sup> + H<sub>2</sub>O via flashing

- A: Permeate chamber for  $CO_2$  absorption
- **B**: Feed chamber for mixture of KOH and K<sub>2</sub>CO<sub>3</sub>
- C: Positive chamber D: Negative chamber
- E: Open-tower for CO<sub>2</sub> absorption
- F: Air entrance and liquid sump

- Fast Kinetics Solvent
- Simplified Process and Operation
- Byproducts of  $H_2$  and  $O_2$  for sale

#### **Technology Background- UKy Previous Results**



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# **Project Scope**

#### Work plan

- Design, fabrication, and research on hybrid absorber (HA), electrochemical regenerator (ER), and integrated process (HA + ER) (Task 2-4, BP1)
- Evaluation of integrated HA and ER including parametric and long-term evaluation and process modeling (Task 5, BP2)
- Process analysis including TEA and LCA and develop TMP (Task 1, 6 & 7)

Project Success Criteria		
Decision Point	Date	Success Criteria
Completion of BP1	09/30/22	<ul> <li>For MA, ≥60% of OH<sup>-</sup> separation from CO<sub>3</sub><sup>2-</sup> at liquid delivery rate &gt; 2 L/hour</li> <li>For ER, ≤3.7 of operating voltage; ≤20% of H<sup>+</sup>/K<sup>+</sup> crossover ratio through membrane</li> </ul>
Project Completion	09/30/23	<ul> <li>10 CFM air DAC process with:</li> <li>&lt;0.2 psi gas-side pressure drop</li> <li>≥90% CO<sub>2</sub> capture for ≥100 hours</li> <li>≤2.7 V of operating voltage, and</li> <li>≤15% of H<sup>+</sup>/K<sup>+</sup> crossover ratio through membrane</li> </ul>



#### Membrane Evaluation for OH<sup>-</sup> Separation

~17

99%

50%

**Selectivity** 

#

3.74

2.39

6.47

4.40

4.66

4.19

Designation **NFX NF270** Brand Synder Filmtec NFX and NF270 Material Polyamide Polypiperazine **Selected** as Water Permeance (LMH/bar) ~4-7.5 membranes for MgSO<sub>4</sub> Rejection 99 % Hybrid Absorber NaCl Rejection 40 % Rejection  $(1 - [C_{X,permeate}/C_{X,feed}])$ Milestone:>60% NF270 Membrane **30 LMH Constant Flux** Start CO3 Conc. OH<sup>-</sup> permeance CO<sub>3</sub> Rej **OH Rej** (%) Feed / pН (%) (%) influent from Permeate with stream 0.1 11.83 83.90 39.74 Feed  $CO_{3}^{2}$ in 0.1 Permeate 11.61 concentrate 64.45 14.89 0.1 Feed 12.96 stream 0.1 Permeate 12.89 Achieved 100% 84.54 0\* Feed 11.84 **OH**<sup>•</sup> permeance Permeate 11.92 0\* influent Feed 12.97 77.28 from 12.99 Permeate stream with a 3 11.83 78.53 0\* Feed nominal 3 Permeate 12.29 selectivity ratio 3 76.13 0\* Feed 13.05 >4 3 Permeate 13.22

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# Membrane Evaluation for OH<sup>-</sup> Separation

Solvent Circulation: 100 mL/min Temperature: Room Conditions Membrane: Synder NFX Membrane Area: 140 cm<sup>2</sup>

Solvent	Osmotic Pressure at
5% K <sub>2</sub> CO <sub>3</sub> 0.3% KOH	<b>100% Rejection</b> ~421 psig



<u>Achieved ~100% OH<sup>-</sup> permeance from influent stream with a selectivity ratio of 4</u>

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## **Capture Performance of Nanofiltration**





140 cm<sup>2</sup> Flat-sheet Membrane

7.6 m<sup>2</sup> Spiral-wound Membrane

5 wt% K<sub>2</sub>CO<sub>3</sub> Feed, NF@ 30 psig back-pressure, CO<sub>2</sub> Fed to Permeate side



## **Testing of Capture in Spray Column Section**

	PJ20	PJ24	PJ32
2wt% KOH spray rate (L/min)	0.44	0.5	0.65
Nozzle pressure (psig)	120	90	40
Approximate coverage			
(inches)	12	16	22
Approximate spray height			
(inches)	6	8	11
Droplet size (µm)	41	50	62
Solution height (inches)	1.5	1.5	1.5
Air inlet above solution			
(inches)	3	3	3
Nozzle to solution (inches)	15.5	15.5	15.5







Capture enhanced at low flow (increased residence time) with ~90% achieved at 0.4 CFM Air

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#### Performance of Hybrid membrane System

A. 5 wt%  $K_2CO_3$  Feed, NF@ ~30 psig back-pressure, 0.36 CFM CO<sub>2</sub> Fed to Permeate side B. CO<sub>2</sub> from NF Permeate side continues to Spray Tower C. 2 wt% KOHFeed to spray section



#### Catalytic Electrode Selection for ER



Potential / V vs HgO

1. High current density under same potential means less energy to produce same  $H_2$ 2. Pt/C Cathode and Inconel (Ni-Fe-Cr) Anode appear as the best combinations

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## Full Cell ER Testing



#### **Testing Conditions:**

- Inconel anode and Pt-C cathode
- K<sub>2</sub>CO<sub>3</sub> circulated at room temperature
- 16 cm<sup>2</sup> active area
- Constant current charging technique was applied, and cell voltage was measured
- Zero electrode space gap to 3 mm gap configuration.

Liquid in

Liquid/gas out

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#### Full ER Cell – Suppressing Voltage loss

#### **Testing Conditions:**

- 0.27 to 0.95M  $K_2CO_3$  was circulated at 5-15 mL min-1 at room temperature;
- Constant current (3A) charging technique was applied, and cell voltage was measured;
- Electrode space gap was 1.5 mm each channel.
- The solvent regenerator was equipped with the Inconel anode and Pt-C cathode.



#### Concentration has a stronger effect on voltage

#### Full ER Cell – Suppressing Voltage loss and Mitigating Proton Crossover





Cell voltage (a) and  $H^+/K^+(b)$  as functions of  $K^+$  loading.

H/K increases with increasing loading factor (increasing current, decreasing concentration, decreasing flow rate)

# **Plans for Testing and Future Development**

- Boost hydroxide concentration and gas-liquid contact zones and complete scale up of hybridized membrane absorber for 90% capture from 5-15 CFM feed
- Explore internal integration of MA (Spray Tower with Nanofiltration) via tubular and flat-sheet membranes

- Parametric and long-term continuous testing of integrated absorber and ER at 5-15 CFM Air
- Scale-up of ER system to 5 kg CO<sub>2</sub>/hour (4000 CFM Air) and demonstrate negative emissions via solar integration

#### Summary

- (1) NFX and NF270 Nanofiltration membranes show capability to concentrate carbon loading (e.g.,  $CO_3^{2-}$ ) by removing OH- prior to sending ER for regeneration toward reducing energy consumption
- (2) Interim results show that the hybrid absorber including spray absorber and selective membrane is an effective absorber for DAC with capture facilitated by KOH solvent solvent
- (3) Electrochemical regeneration performance and energy requirement of the ER were found to strongly depend on inter-electrode spacing and loading factor - solvent concentration, flow rate and current

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- Vanderbilt: Shihong Lin

#### **Appendix - Organization Chart**



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# **Appendix - Gantt Chart**

Completion

	·		-	2021	2022	2023
#	TASK DESCRIPTION	Start Date	End Date	ONDJF	MAMJJAS	SONDJFMAMJJAS
1	Project Management and Planning	10/1/2021	9/30/2023			
BP1	Budget Period 1	10/1/2021	9/30/2022			
1.1	1A. Update Project Management Plan	10/1/2021	10/31/2021			
1.1	1B. Kickoff Meeting	10/1/2021	12/30/2021			
1.2	2A. Initial Technology Maturation Plan	10/1/2021	12/30/2021			
1.2	2B. Final Technology Maturation Plan	8/1/2023	9/30/2023			
2	Membrane Contactor Design and Fabrication	10/1/2021	5/31/2022			
2.1	Design Membrane Absorber	10/1/2021	11/30/2021			
2.2	Membrane Fabrication	12/1/2021	2/28/2022			
2.3	Modulation	3/1/2022	5/31/2022			
3	Electrochemical Regenerator Construction	10/1/2021	6/1/2022			
3.1	Catalytic Electrode Design and Fabrication	10/1/2021	1/31/2022			
3.2	Flow Channel Design	2/1/2022	6/1/2022			
4	System Integration	4/1/2022	9/30/2022			
4.1	Process Control and Monitoring and P&ID Development	4/1/2022	6/30/2022			
4.2	Procurement and Balance of Plant	6/1/2022	7/31/2022			
4.2	Startup and Commisioning	7/15/2022	9/30/2022			
BP2	Budget Period 2	10/1/2022	9/30/2023			
5	Parametric Study Through Longterm Operation	10/1/2022	7/31/2023			
5.1	Electrochemical Regenerator Cell Voltage Reduction	10/1/2022	3/1/2023			
5.2	Proton Transport Mitigation Through Membrane	10/1/2022	3/1/2023			
5.3	Effectiveness of CO <sub>2</sub> Capture	10/1/2022	3/1/2023			
5.4	Longterm Operation to Characterize Material Degradation	1/1/2023	7/31/2023			
6	Technoeconomic Analysis	4/1/2023	9/30/2023			
6.1	Process Modeling	4/1/2023	5/1/2023			
6.2	Technoeconomic Analysis	5/1/2023	9/30/2023			
7	Life Cycle Analysis	4/1/2023	9/30/2023			
7.1	Life Cycle Analysis	4/1/2023	9/30/2023			