Doping and Redoping Effects on Hybrid Polymer Membranes for Direct Air Capture of CO₂

Project Number: DE-FE0031968

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Outline

- a. Project Overview
- b. Technology Background
- c. Technical Approach/Project Scope & Objectives
- d. Team and Facilities
- e. Progress and Current Status of Project
- f. Plan for Future Development
- g. Summary
- h. Acknowledgements

Program Overview

- a. Funding: DOE \$799,985 and Cost Share \$200,001
- b. Overall Project Performance Dates: 01/01/2021 03/31/2023
- c. Project Participants: InnoSense LLC (Torrance, CA) and University of Utah (Salt Lake City, UT)
- d. Overall Project Objectives: Develop hybrid polymer membrane capable of direct air capture (DAC) CO₂ separating from ambient air at a low cost (low hundreds in \$) per metric tonne by 2030

Technology Background

- Carbon dioxide (CO₂), captured directly from ambient air, is a leading method for carbon management and reducing greenhouse gas emissions
- A recent study estimates that primary processes envisioned for large-scale CO₂ capture from ambient air can cost \$94–\$232 per metric tonne
- Current methods of DAC CO₂ separation from ambient air (~0.04%) are intrinsically inefficient due to:
 - Thermal energy losses
 - Large footprint
 - Degradation of sorbent materials
- Sorbents and solvents used in the DAC process have many disadvantages:
 - Need to build a very large structure
 - High cost and complexity of regenerative systems
 - Loss of moisture in dry environments

Technical Approach/Project Scope and Objectives

The current project scope and objectives are to develop hybrid polymer membranes (HypoMem) and laboratory-scale testing and evaluation of their performance to demonstrate potential for DAC CO₂ separation from ambient air at a reduce costs and energy penalties.

Project Technical Objectives

Objective 1. Formulation and Processing of Functional Polymer Materials for the Development of Hybrid Polymer Membrane (HypoMem).

Objective 2. Development and Characterization of HypoMem Samples for Determining their Physical, Morphological and Mechanical Properties.

Objective 3. Laboratory-Scale Testing and Evaluation of Flat and Stack HypoMem Sample Performance Under Simulated Air to Demonstrate Potential for DAC CO₂ Separation from Ambient Air at a Reduced Cost.



Team and Facilities

InnoSense LLC Team





Maksudul M. Alam, Ph.D. Chamila Manankandayalage, Ph.D. Mohammad Mushfiq, B.S. Principal Investigator Formulation and Testing Scientist



Senior Research Engineer

University of Utah Team



Professor Milind Deo, Ph.D. Subaward Project Director



Palash Panja, Ph.D. Subaward Co-Investigator

Cleanroom Certified ISO-7

Scanning Electron Microscope (SEM)

Gas Permeation Test Unit



Progress and Current Status of Project

Project Team working strategically to meet project objectives

- Developed different hybrid polymer formulations,
- Fabricated large size HypoMem samples and prepared undoped, doped, dedoped and redoped samples
- Characterized HypoMem samples using Fourier-transform infrared spectroscopy (FTIR), UV-Vis spectroscopy, scanning electron microscope (SEM), and thermogravimetric (TGA) analysis
- Constructed an on-site gas permeation testing set-up
- Measured permeance, permeability, and CO₂/N₂ selectivity of HypoMem samples at room and elevated temperatures
- Performed computer simulation and modeling of HypoMem system

Casting Hybrid Polymer Layer

Cast thin-films of hybrid polymer layer on glass substrate using a doctor blade



Fabrication of HypoMem Samples



Characterization of HypoMem Samples: FTIR Analysis

- 1. After drying the epoxy resin solution, the tri-layered membrane was formed
- 2. Delaminated the tri-layered membrane from the glass substrate easily by submerging in water with the thin-film lift off method (T-FLO), and then stored them
- 3. Characterized by FTIR, UV-Vis, SEM and TGA analysis



Observed characteristic FTIR peaks of PA, PBI, and GO in HypoMem samples

Characterization of HypoMem Samples: FTIR Analysis and Mechanical Flexibility



SEM Analysis of HypoMem Samples

HypoMem characterized with SEM analysis showing morphologies of both hybrid polymer and epoxy layer sides



Thermogravimetric Characterization of HypoMem Samples: Thermal Stability

TGA curves of four PA:HGrO:PBI (73:12:15 wt% and 60:10:30 wt%) HypoMem samples



Sample ID	PANi:HGrO: PBI Composition (w/w)	Decomposition Onset Temperature (°C)	Temperature (°C) of 10% Weight Loss	Temperature (°C) of 50% Weight Loss	Residual Weight (%) at 600 °C
0311CM01-CM1	73:12:15	263.21	263	437	12.07
0311CM02-CM2	60:10:30	227.71	240	437	6.20
0311CM02-CM3	73:12:15	251.11	262	458	12.71
PICMHGr-2-CM4	73:12:15	241.80	253	430	7.64

HypoMem samples show good thermal stability up to 250 °C

Doping, Dedoping and Redoping of HypoMem Samples

(A) Doping: 1 M HCl acid treatment for 4 h, (B) Dedoping: 1 M NH₄OH base treatment for 24 h, and (C) Redoping: 0.025 M HCl treatment for 16 h.



Photographs of (A) undoped, (B) doped, (C) dedoped, and (D) redoped. Top two rows are the active layer side, and bottom two rows are the support layer side.



Spectroscopic characterization of undoped, doped, dedoped and redoped HypoMem samples



New peak appeared at 462 nm for doped and redoped samples due to protonation

450

Wave Length (nm)

PANI Emeraldine Base (PANI-EB)

300

350

PANI Emeraldine Salt (PANI-ES)

550

SEM Characterization of undoped, doped and redoped HypoMem Samples



Observed no significant difference in morphologies (within the recorded magnifications) of the undoped, doped and redoped samples Elemental mapping by EDS analysis of undoped, doped, dedoped and redoped HypoMem samples

Undoped	Doped	Redoped
Yellow represents Ca	arbon content	
Green represents Ch	lorine content	
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Elemental distribution data for the undoped, doped and redoped samples

Element Name	Element Symbol	Weight Conc.		
		Undoped	Doped	Redoped
Au	Gold	70.10	77.98	73.82
С	Carbon	27.25	16.63	22.65
N	Nitrogen	1.80	1.65	1.83
0	Oxygen	0.84	0.66	0.72
CI	Chlorine	-	3.07	0.98

Doped and redoped samples contain chlorine which came from HCl treatment

Constructed On-Site Gas Permeation Testing Setup

Gas permeation testing set up for evaluating permeability, permeance and CO₂ Selectivity



Components of Gas Permeation Cell and Method for Testing

Gas permeation method and cell designed for HypoMem performance testing

With this type of setup installed, the gas permeability was calculated using Eq. 1:

$$P = 10^{10} \times \frac{VL}{P_{Permeate}ART} \times \frac{dp(t)}{dt}$$
(1)

where, *P* is the gas permeability across the membranes (in Barrers) [1Barrer = 10^{-10} cm³ (STP) cm/cm² s cmHg], *P*_{Permeate} is the permeate pressure (in cmHg), *dp/dt* is the rate of the steady-state permeate side pressure increase (in cmHg/s), *V* is the standardized permeate volume (in cm³), *L* is the active layer thickness (in cm), *A* is the effective surface area of the membrane (in cm²), *T* is the experimental temperature (K), and *R* is the gas constant [0.278 cm³ cmHg/cm³ (STP) K]. Solving for permeance is a similar equation but does not factor in thickness of the sample *L*. Permeance *P*_{Permeance} is calculated using Eq. 2:

$$P_{Permeance} = 10^6 \times \frac{V}{P_{Permeate}ART} \times \frac{dp(t)}{dt}$$
 (2)

The ideal selectivity (α) was obtained from the ratio of permeability coefficients using Eq. 3:

$$\alpha_{A/B} = \frac{P_A}{P_B} \times \frac{P_{CO2}}{P_{N2}}$$
(3)

where, P_A and P_B are the permeability coefficients of the pure gases CO₂ and N₂, respectively.



- (A) Exploded view of the permeation cell
- (B) Closed permeation cell
- (C) Open permeation cell showing components

HypoMem's Membrane Performance: CO₂ Permeance and Selectivity



Test Conditions:

- Membrane diameter of 1 cm, active layer thickness of 9.0 μ m, and epoxy layer thickness ~ 225 μ m,
- Feed flow rate of 0.172 ml/s for both CO₂ and N₂ gases,
- Ambient temperature conditions and fixed upstream condition 75.9 cm Hg (101kPa),

Higher permeance value observed for CO_2 (6.83*10⁵) than N_2 (2.15*10⁵) for a pressure difference across the membrane of 70 cm Hg (~95 kPa)

PANI:GrO:PBI (60:10:30 wt%) HypoMem Performance: CO₂ Permeance and Selectivity



 CO_2/N_2 selectivity increased with doping and redoping stages

CO₂ Permeance and Selectivity of PANI:GrO:PBI (60:10:30 wt%) HypoMem



0311CM02 PA:HGr:PBI (60:10:30)	Selectivity (CO ₂ /N ₂) at Different Pressure differences (KPa)					CO ₂ Permeation (GPU)
	95	97	98	99	99.5	99.5 kPa
Undoped films	1.47	1.73	2.08	3.35	7.82	465000
Doped films	1.70	1.99	2.40	3.87	9.04	204000
Redoped films	2.45	2.88	3.46	5.59	13.04	2770000

CO₂ Permeance and selectivity increased with doping and redoping stages

73:12:15 wt% PANI:GrO:PBI HypoMem Performance: CO₂ Permeance and Selectivity



Observed CO_2/N_2 selectivity 10.94 for redoping sample

CO₂ Permeance and Selectivity of PANI:GrO:PBI (73:12:15 wt%) HypoMem



10.94

Redoped

12

Selectivity

4.65

Undoped

Selectivity (CO₂/N₂)

0311CM01 PA:HGr:PBI	Selectivity (Pressure	CO ₂ Permeation (GPU)		
(73:12:15)		99.5 kPa		
Undoped films		4.65		27500
Doped films		5.92		53600
Redoped films		10.94		80900

Different redoped 73:12:15 PANI:GrO:PBI membranes: Repeatability of membranes' performance



CO₂ Permeance and selectivity increased with doping and redoping stages

5.92

Doped

Doping Stage

Computer Simulation and Modeling on Direct Air Capture Membranes

Simulation of HypoMem membrane performance model will guide future work

- Material balances on species and permeance calculations performed to establish the membrane outlet characteristics
- Given certain operational parameters, the permeate and the retentate compositions are fixed
- Flow rates (volumetric and molar) for the species are dictated by their partial pressure differences between the outlet and the inlet
- The outlet concentration of CO₂ in the permeate is a function of the inlet concentration, the inlet and the outlet pressures, and the membrane selectivity
- The total throughput through the membrane is governed by its GPU and area.
- The parameters are adjusted so that the retentate CO₂ concentration is about the pre-industrial 300 ppm
- Reaching a selectivity of 10 at permeance of 10,000, a permeate CO₂ concentration of 7560 ppm can be achieved



Computer Simulation and Modeling : Co-current flow and single stage

 $Selectivity = \frac{Permeability of CO_2}{Permeability of N_2}$

Stage cut, $\theta = \frac{Permeate flow rate}{Feed flow rate}$

 $CO_2 Recovery = \frac{CO_2 mole in permeate}{CO_2 mole in feed}$

- Flux model : Constant permeability
- Flow pattern : Co-Current
- CO₂ con. in feed : **400 ppm**
- Upstream pressure, p' (kPa) : 110
- Downstream pressure, p" (kPa): 2
- Permeability of CO2 (Barrer) : 10000
- Selectivity: 2 to 200



- **Figure 1**: CO₂ purity (i.e., ppm in permeate) is <u>inversely</u> proportional to its recovery.
- **Figures 2 and 3**: CO₂ purity <u>increases with selectivity</u> for a fixed stage cut or membrane area.
- **Figure 4**: CO₂ purity is <u>inversely</u> proportional to CO₂ concentration in permeate due to equilibrium.

Computer Simulation and Modeling : Co-current flow and single stage



Computer Simulation and Modeling : Co-current flow and multi-stage

Some Basic Considerations for HypoMem Simulation

- Since the starting concentration is low (~400 ppm), multistage separation is essential
- Each stage is operated under vacuum
- The process is usually designed to maintain a concentration of 300 ppm in the retentate (preindustrial concentration of CO₂)
- CO₂ purity of about 50% possible after three stages
- Permeate concentration dependence
 - Pressure ratio (upstream to downstream for each stage)
 - Selectivity
- Throughput
 - · Combination of flowrate, GPU and membrane area
- In stage 1, increased selectivity has minimal impact on the permeate CO₂ concentration
- In stage 2, increased selectivity has a moderate impact on the permeate CO₂ concentration
- By stage 3, increased selectivity has a strong impact on the permeate CO₂ concentration

Schematic of three stage DAC CO₂ separation



Simulated effect of selectivity throughout three stages



Plans for Future Development

- In this project
 - Conduct gas permeation testing on HypoMem samples at different weathering conditions such as elevated temperatures and icy condition.
 - Optimize permeance, permeability, and CO₂ selectivity performance.
 - Continue performing computer simulation and modeling based on HypoMem experimental data/results, and process economics.
- After this project
 - Optimize fabrication processes for large size membrane and scaleup production.
 - Prototype development and field level testing for DAC CO₂ separation from ambient air.

Summary

- Developed hybrid polymer formulations and fabricated HypoMem samples with different compositions.
- Characterized HypoMem samples by FTIR analysis and their morphologies (both active polymer and support epoxy sides) and thickness by scanning electron microscope (SEM) analysis.
- Performed doping, dedoping and redoping of HypoMem samples and characterized them by microscopy and spectroscopy.
- Observed CO₂ selectivity of ≥10 with permeance ≥8x10⁴ GPU for redoped samples at a pressure difference of 99.5 kPa across the membrane.
- Observed a trend of an increase in CO₂ permeance and selectivity with doping stage
- Computer simulation and modeling suggested that multi-stage process is required to achieve the desired CO₂ permeate concentration for successful DAC CO₂ separation

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