

A Novel Reactive Separation Method for Carbon Dioxide Capture From Flue Gas

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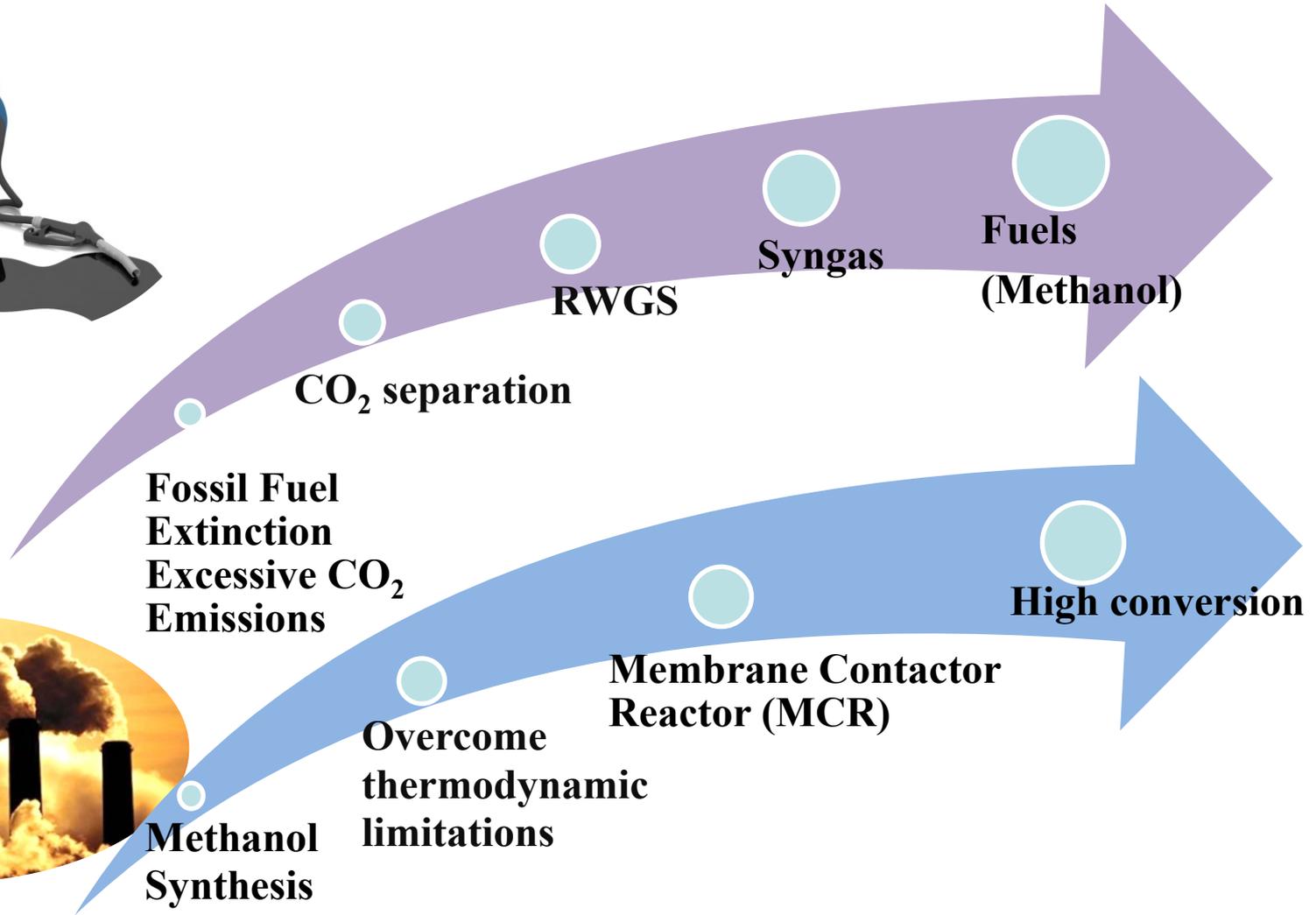
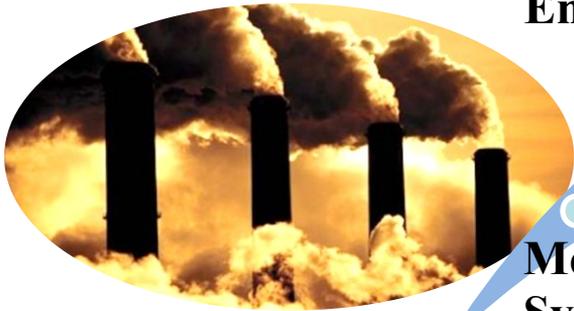


UCFER Annual Review Meeting, October 5-6, 2021

Talk Outline

- **Introduction**
- **Experimental Approach**
- **Preliminary Results**
- **Conclusions and Future Work**

Motivation and Project Goals

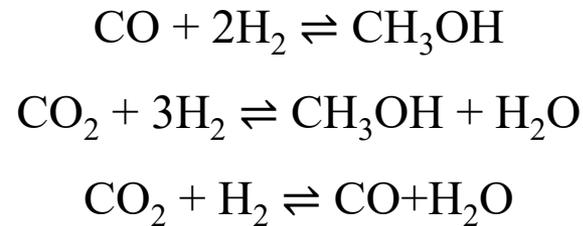
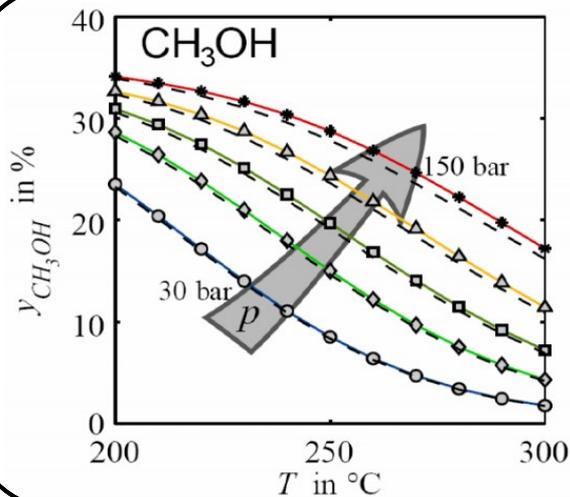


Overcoming MeS Equilibrium Limitations

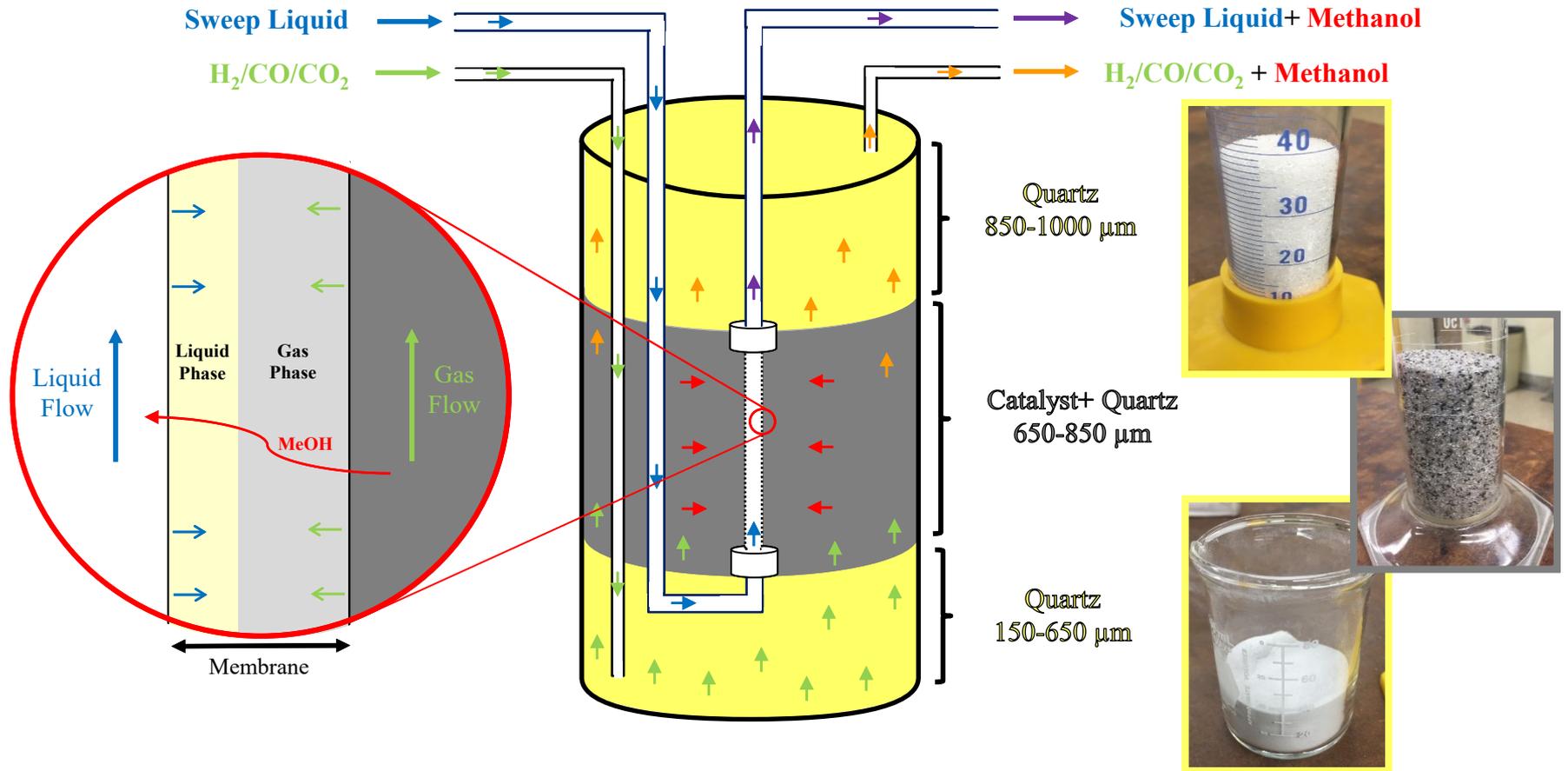
P=30-100 bar
T=220 °Cz

**Conversion
per
pass=<25%**

**Use a
Membrane
Contactor
Reactor
(MCR)**



Lab-Scale MCR System



MeS-MCR Advantages

- **Higher Process Synergy** - From combining reaction and separation in the same unit
- **Overcoming Equilibrium Limitations** - Through in-situ product removal
- **Higher Energy Efficiency** - The liquid sweep also serves as an effective coolant
- **A More Compact and Flexible Design**

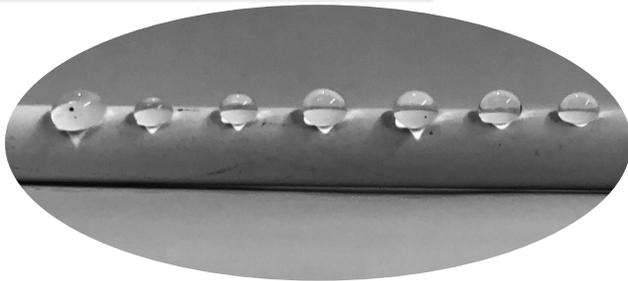
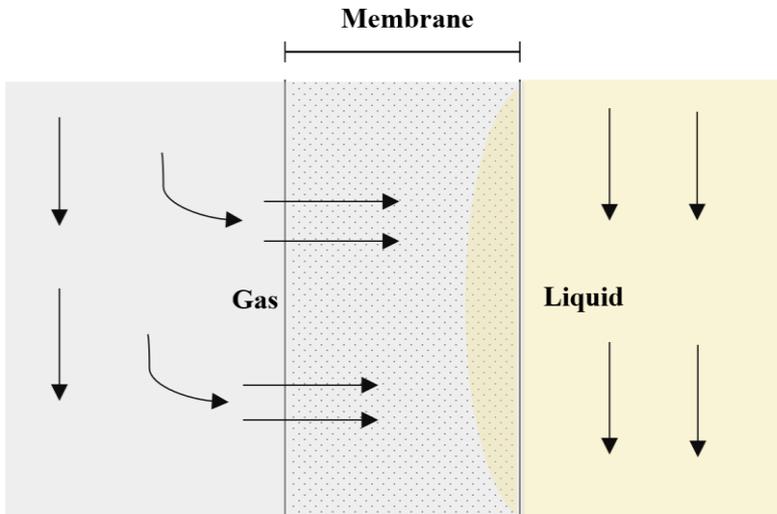
Project Objectives

- **Investigate the performance of novel integrated process combining a RWGS reactor (RWGSR) and a MCR for efficient methanol synthesis from waste CO₂. Study its performance for a broad range of pressure and temperature conditions.**
- **Use an experimentally-validated model to assess the full range of attainable conversions, aiming to obtain >90% carbon capture and utilization.**
- **Carry out a techno-economic analysis (TEA) of the proposed RWGSR/MCR process to compare performance with that of the conventional, absorption-based carbon separation and capture (CSC) technologies.**

Membrane Modification

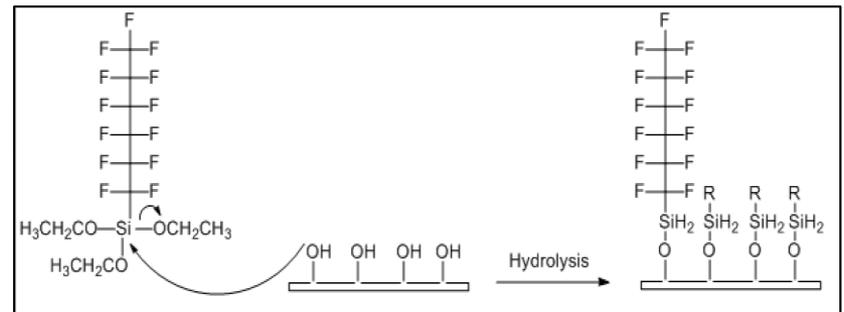
- **Modified Ceramic Membrane**

- Hydrophobic Instead of Hydrophilic (OH-)
- Avoid Complete Wetting of the Membrane
- Fluoroalkylsilane (FAS) Agents



Properties of the ceramic membrane

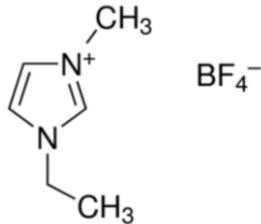
Layer	Material	Thickness (μm)	Average Pore Size (Å)
Support	α-Alumina	1100	2000-4000
First Layer	α-Alumina	10-20	500
Second Layer	γ-Alumina	2-3	100
Length (cm)			9
Outer Diameter (mm)			5.9
Inner Diameter (mm)			4.7



Sweep Liquid

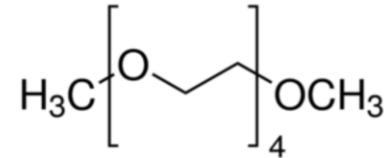
Ionic Liquid (IL)

Ethyl-3-methylimidazolium tetrafluoroborate



Organic Solvent

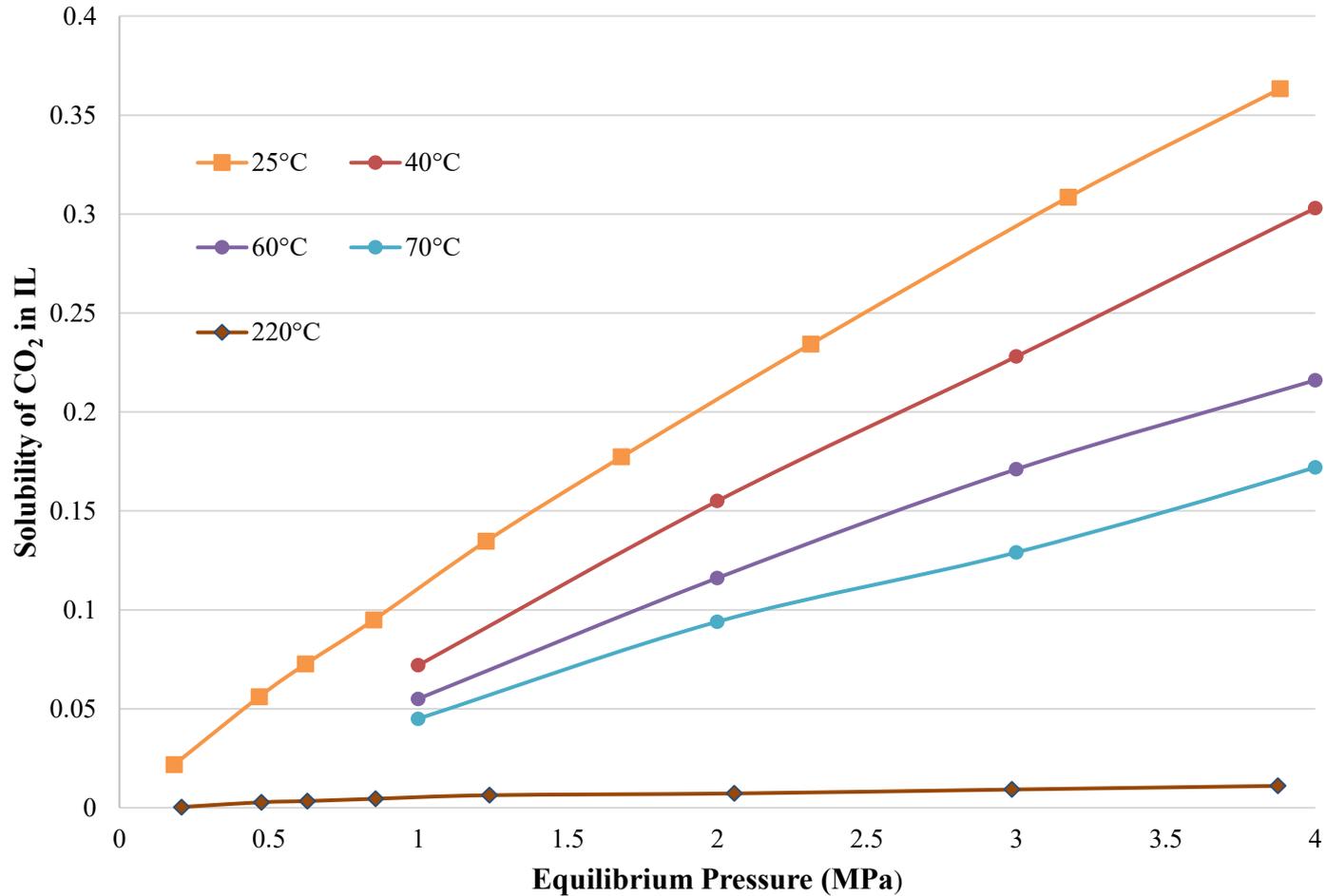
Tetraethylene glycol dimethyl ether (TGDE)



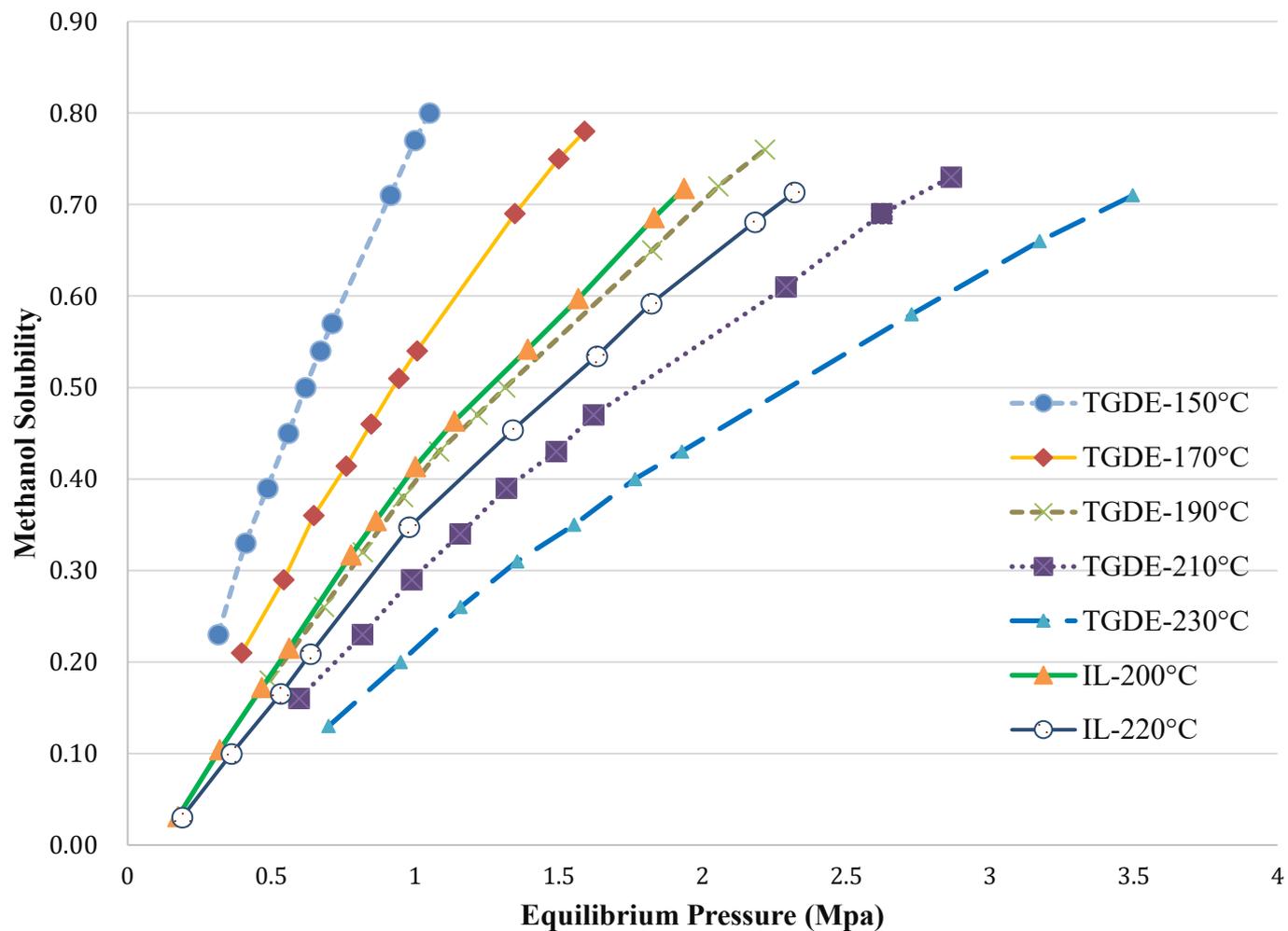
Ionic liquid advantages

- ❑ Highly polar compounds; MeOH has considerably higher solubility than CO and H₂ in them
- ❑ Typical IL's have extremely low vapor pressures (<10⁻⁹ bar), which is advantageous when compared to other low boiling point (B.P.) organic solvents
- ❑ Significantly simplified downstream separation of the MeOH from the solvent
- ❑ Very high decomposition temperatures
- ❑ High thermal capacity (thermal energy storage)

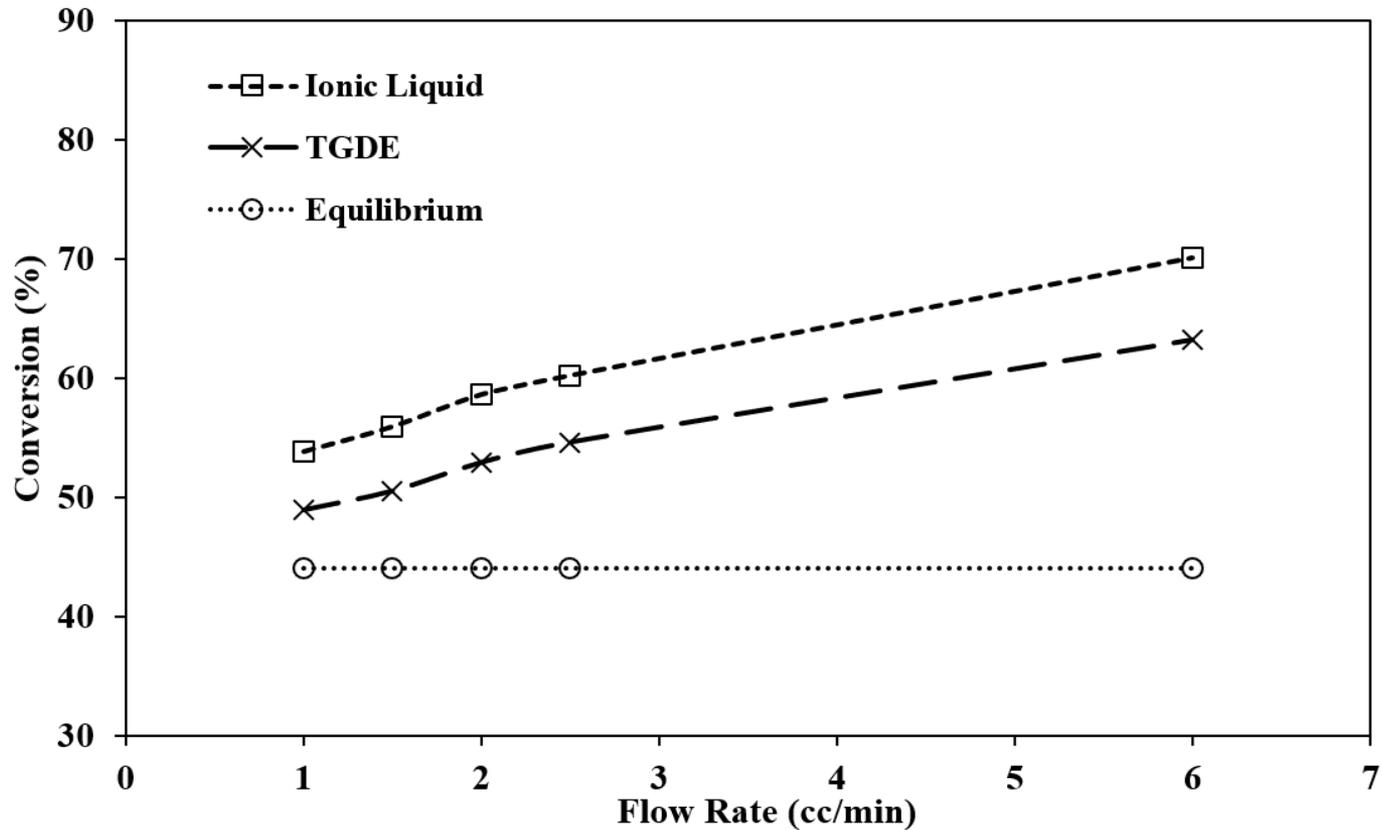
CO₂ Solubility in the IL



MeOH Solubility in the IL and TGDE



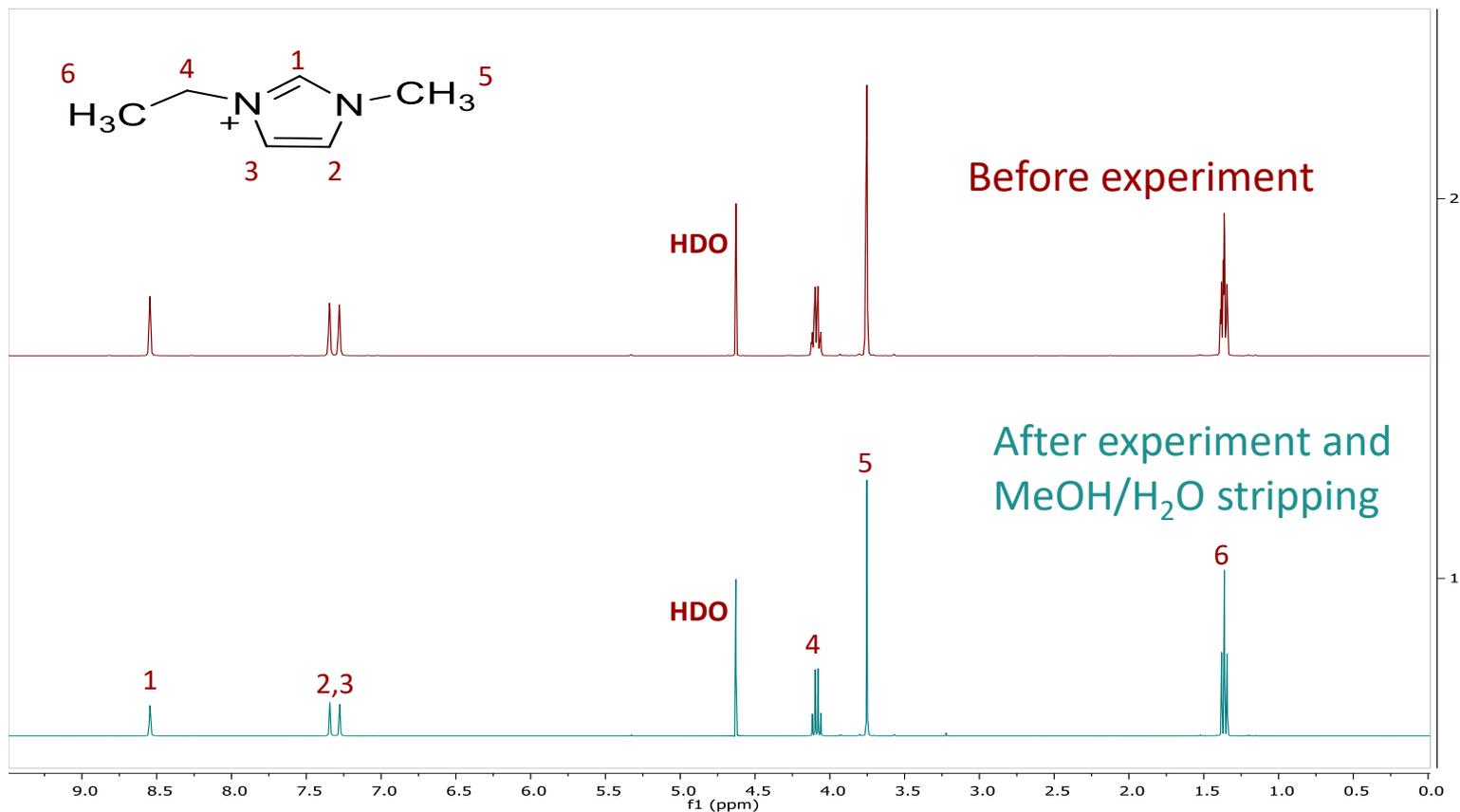
MeS-MCR Performance



Effect of liquid sweep flow rate on MR conversion. $P = 32$ bar, $T = 220^{\circ}\text{C}$, $W/F = 47.2$ g*h/mol

IL Stability Under Reaction Conditions

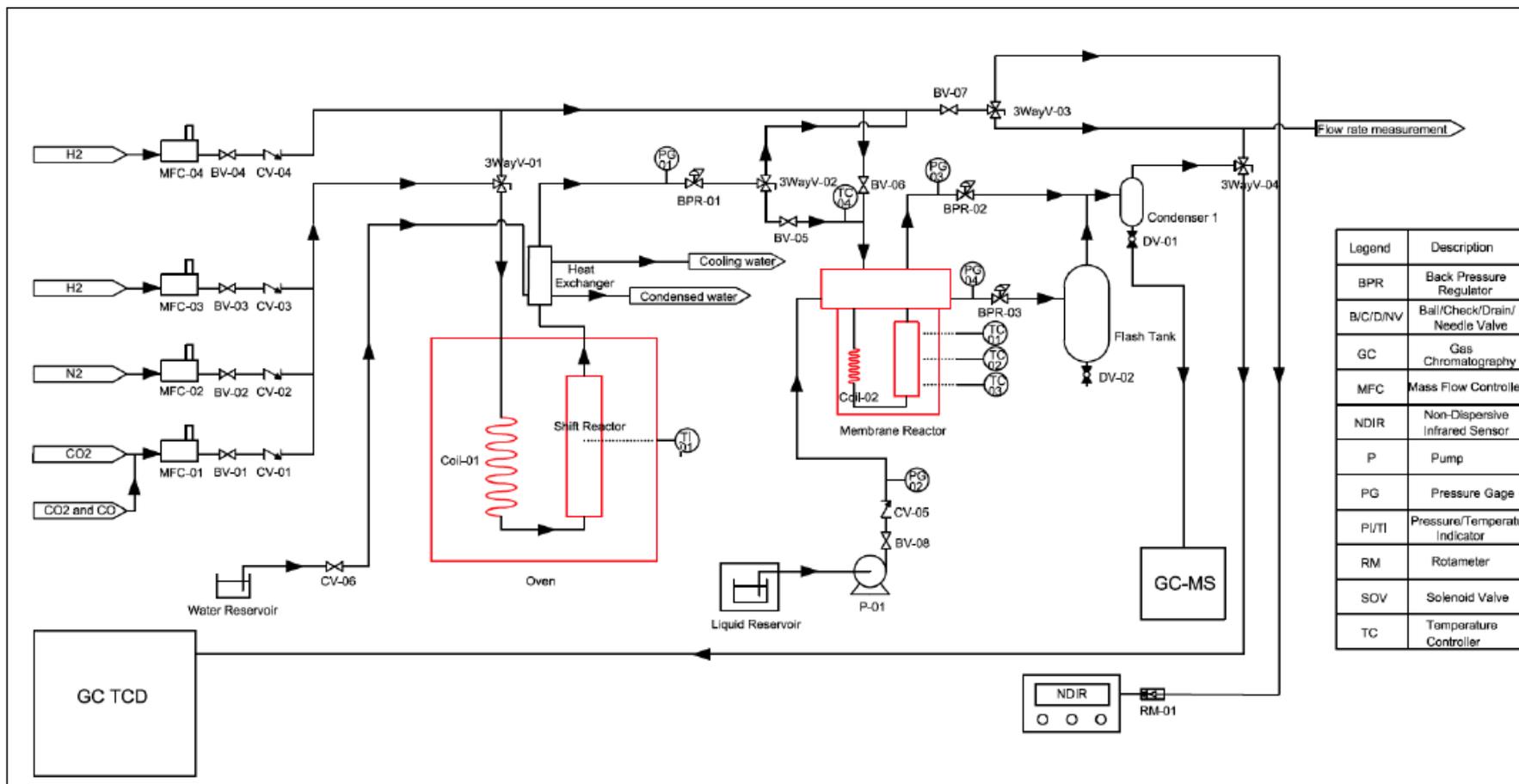
NMR studies show that the IL structure is stable and no irreversible bonds with methanol and water are created.



400 MHz ¹H Nuclear Magnetic Resonance (NMR) Results of the [EMIM][BF₄] IL

Task 1.0 – Design and Construction of the RWGSR/MCR MeS System

Schematic of Experimental Set-up



Lab-Scale Experimental Set-Up



The combined RWGSR and MCR-MeS system.

Task 2.0 – Testing of the Individual RWGSR and MCR MeS Subsystems

MeS Kinetic Studies

■ Packed-Bed Reactor Model

$$\frac{dF_{CO}}{dW} = r_{RWGS}$$

$$\frac{dF_{CO_2}}{dW} = -r_{MeOH} - r_{RWGS}$$

$$\frac{dF_{H_2O}}{dW} = r_{MeOH} + r_{RWGS}$$

$$\frac{dF_{H_2}}{dW} = -3r_{MeOH} - r_{RWGS}$$

$$\frac{dF_{CH_3OH}}{dW} = r_{MeOH}$$

■ Rate Expressions

Van den Bussche et al. (1996)

$$r_{MeOH} = \frac{k'_{5a} K'_2 K_3 K_4 P_{CO_2} P_{H_2} [1 - (1/K_1^*) (P_{CH_3OH} P_{H_2O} / P_{H_2}^3 P_{CO_2})]}{(1 + (K_{H_2O} / K_3 K_4 K_{H_2}) (P_{H_2O} / P_{H_2})) + \sqrt{K_{H_2} P_{H_2} + K_{H_2O} P_{H_2O}})^3}$$

$$r_{RWGS} = \frac{k'_1 P_{CO_2} [1 - (K_3) (P_{CO} P_{H_2O} / P_{H_2} P_{CO_2})]}{(1 + (K_{H_2O} / K_3 K_4 K_{H_2}) (P_{H_2O} / P_{H_2})) + \sqrt{K_{H_2} P_{H_2} + K_{H_2O} P_{H_2O}})}$$

$$\log_{10} K_1^* = \frac{3066}{T} - 10.592$$

$$\log_{10} 1/K_3^* = \frac{-2073}{T} + 2.029$$

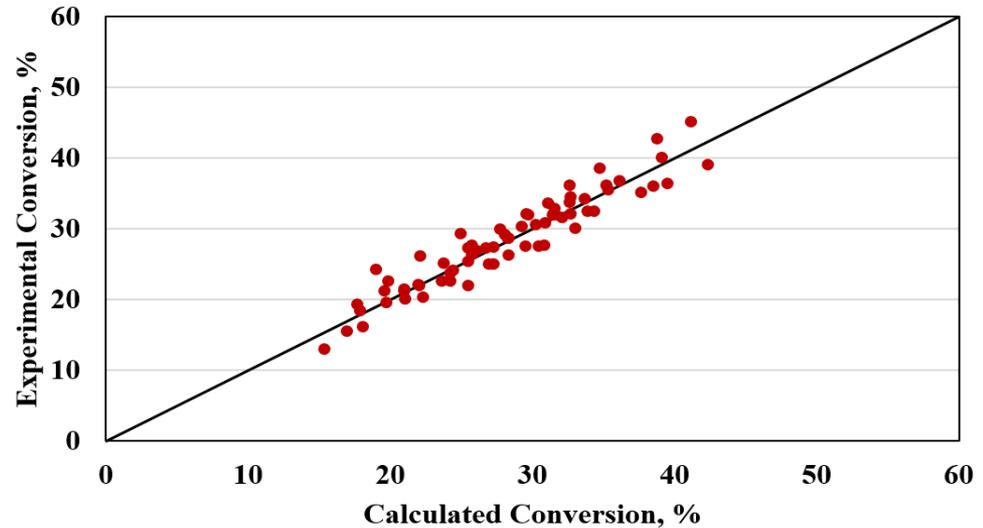
$$k_1 = k'_{5a} K'_2 K_3 K_4 \quad k_2 = K_{H_2O} / K_3 K_4 K_{H_2} \quad k_3 = \sqrt{K_{H_2}} \quad k_4 = K_{H_2O} \quad k_5 = k'_1$$

Rate Parameter Estimation

Temperature-Dependent Rate Constants

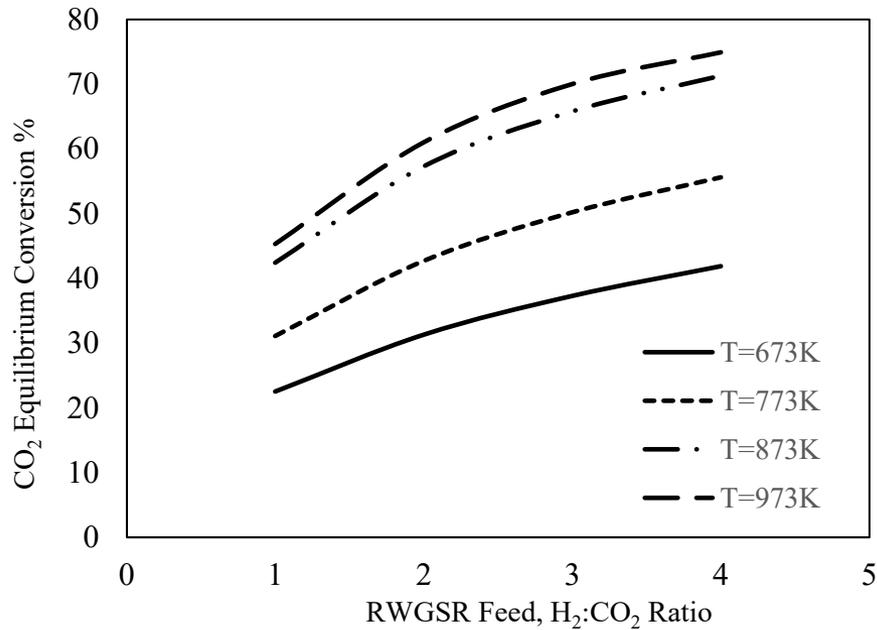
$$K = A(i)\exp(-B(i)/RT)$$

	A(i)	B(i)
k₅	1.459928	31575.31
k₄	18766.2	-0.00451
k₃	7.79461E-7	91306.78
k₂	4.64815E-11	126110.78
k₁	153463133.88	-73698.32

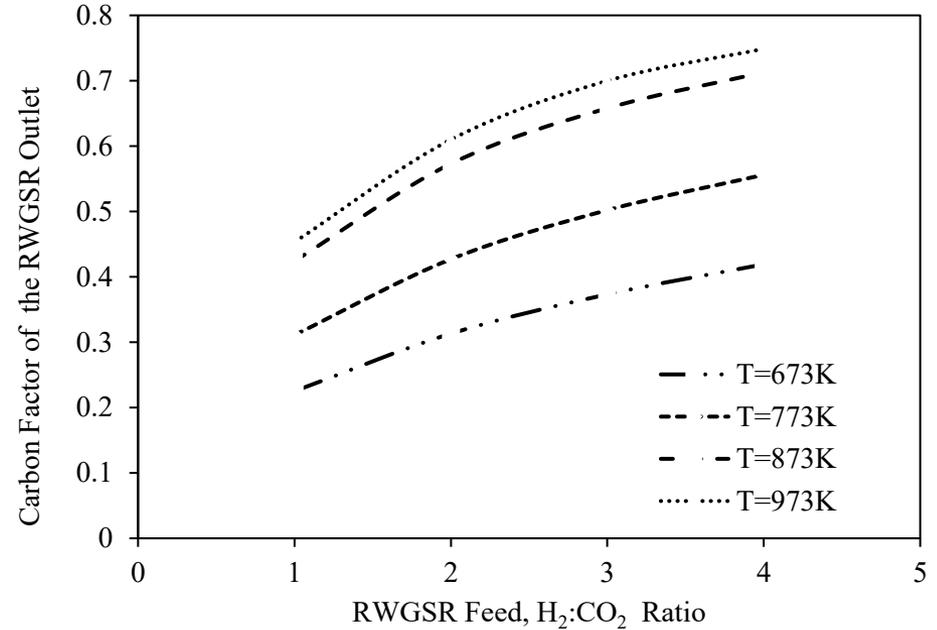


Comparison of experimental vs. calculated carbon conversions

RWGSR Performance at Equilibrium

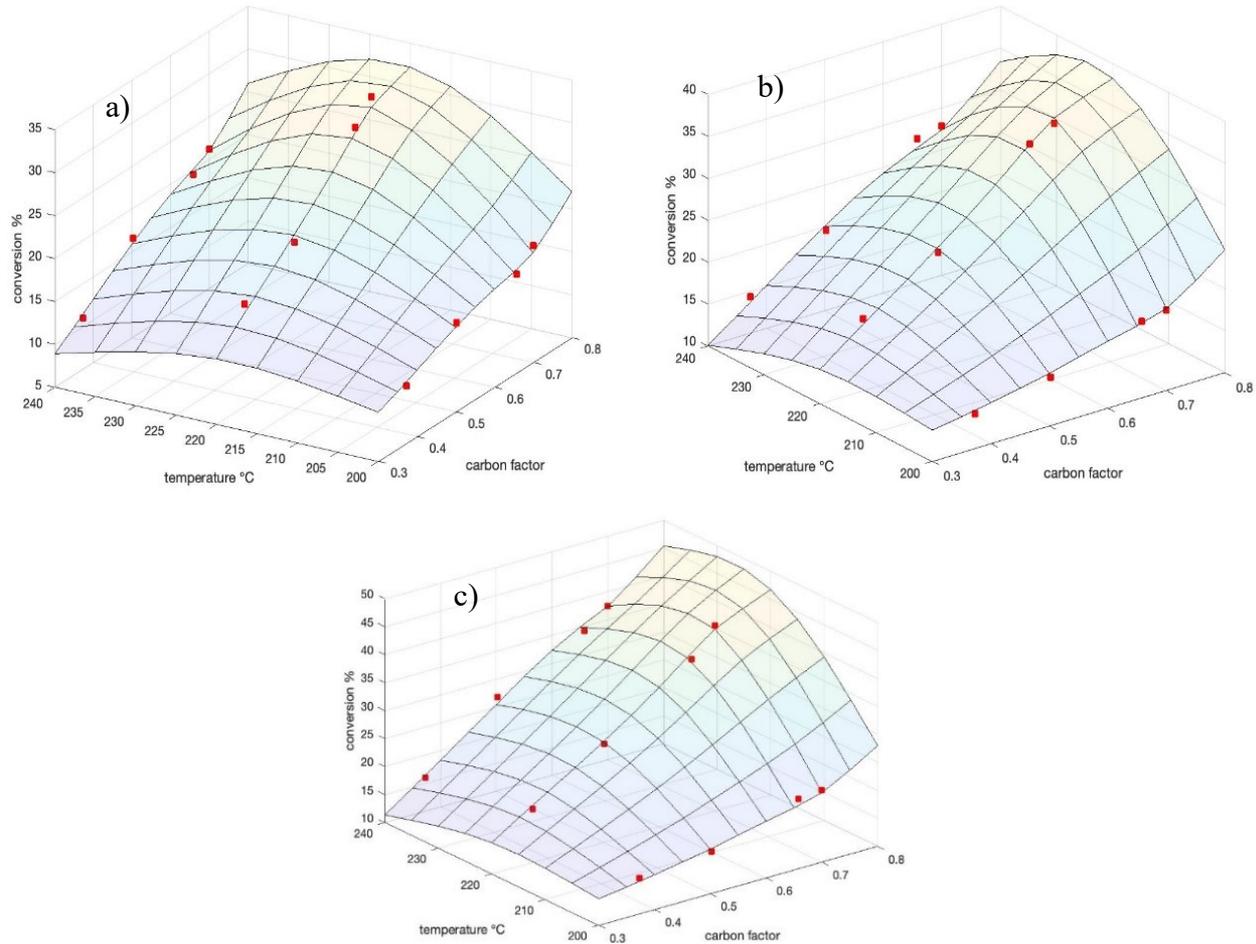


CO₂ equilibrium conversion in the RWGSR



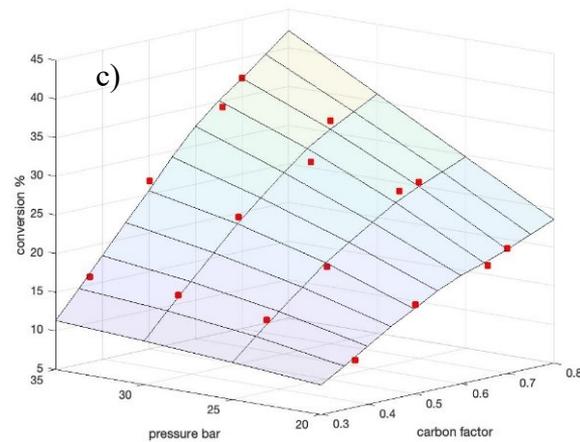
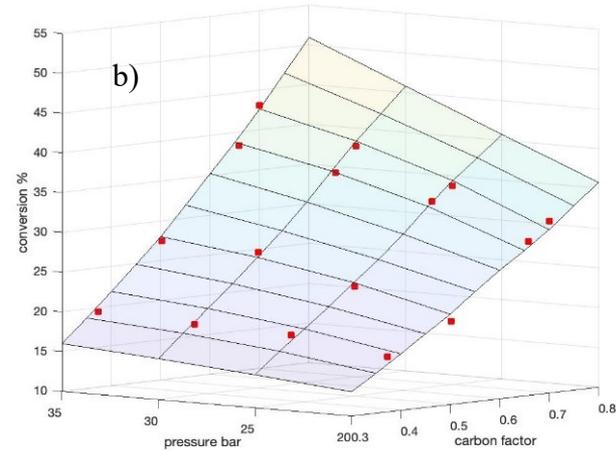
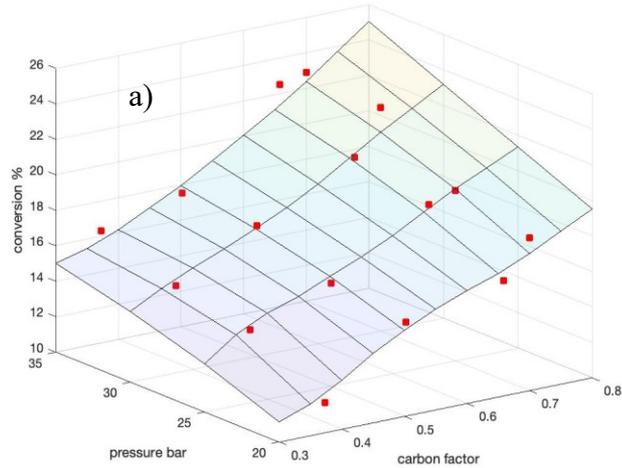
CF of gas mixture at the exit of the RWGSR at equilibrium.

MeS-PBR Conversion at Various T and CF



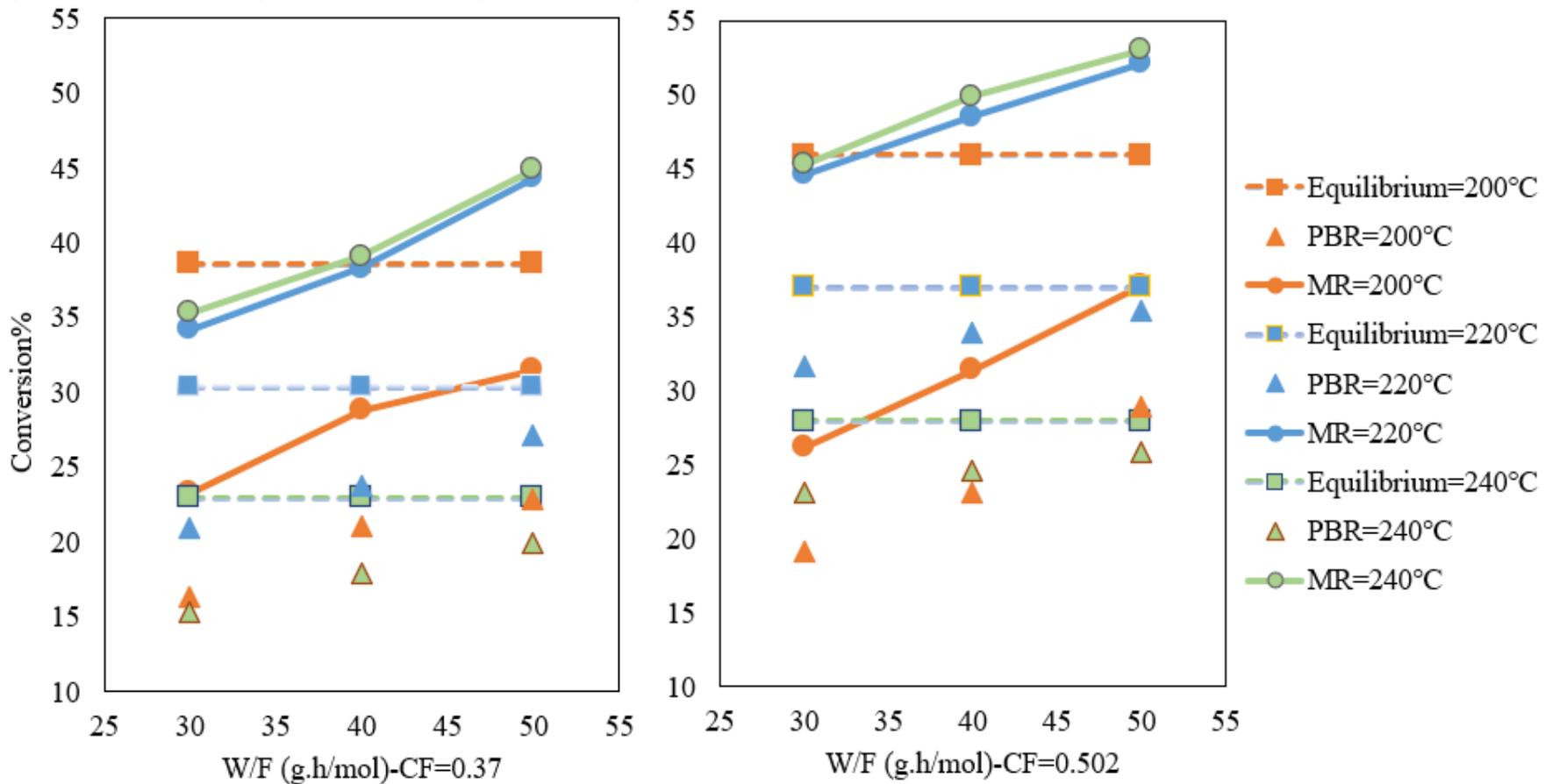
(a) P= 20 bar, (b) P=25 bar, (c) P=30 bar; dots are the experimental points and surfaces are model calculations

MeS-PBR Conversion at Various P and CF



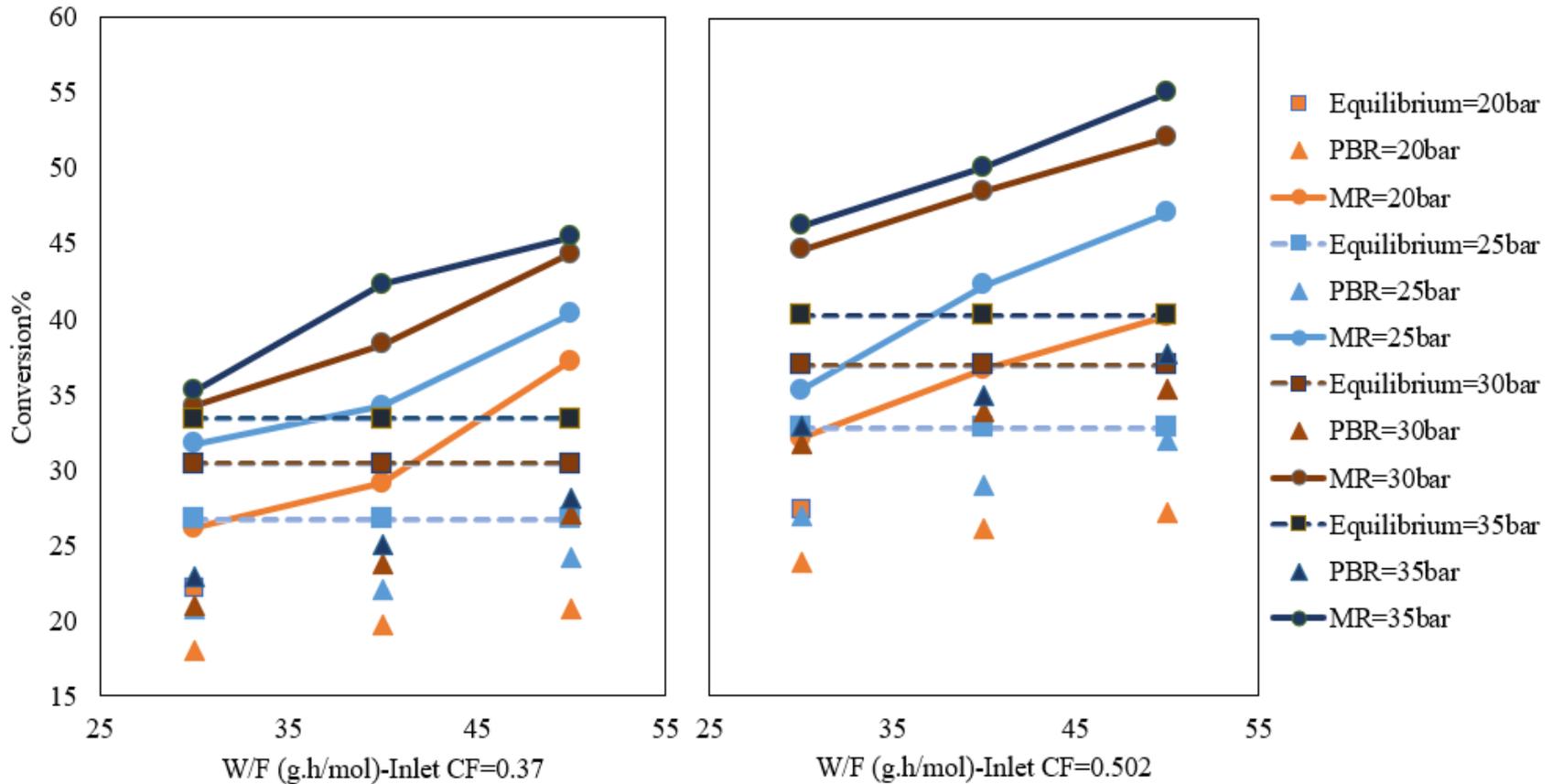
(a) $T= 200\text{ }^{\circ}\text{C}$, (b) $T=220\text{ }^{\circ}\text{C}$, (c) $T=240\text{ }^{\circ}\text{C}$; dots are the experimental points and surfaces are model calculations

PBR and MCR Conversion vs. W/F, Varying T



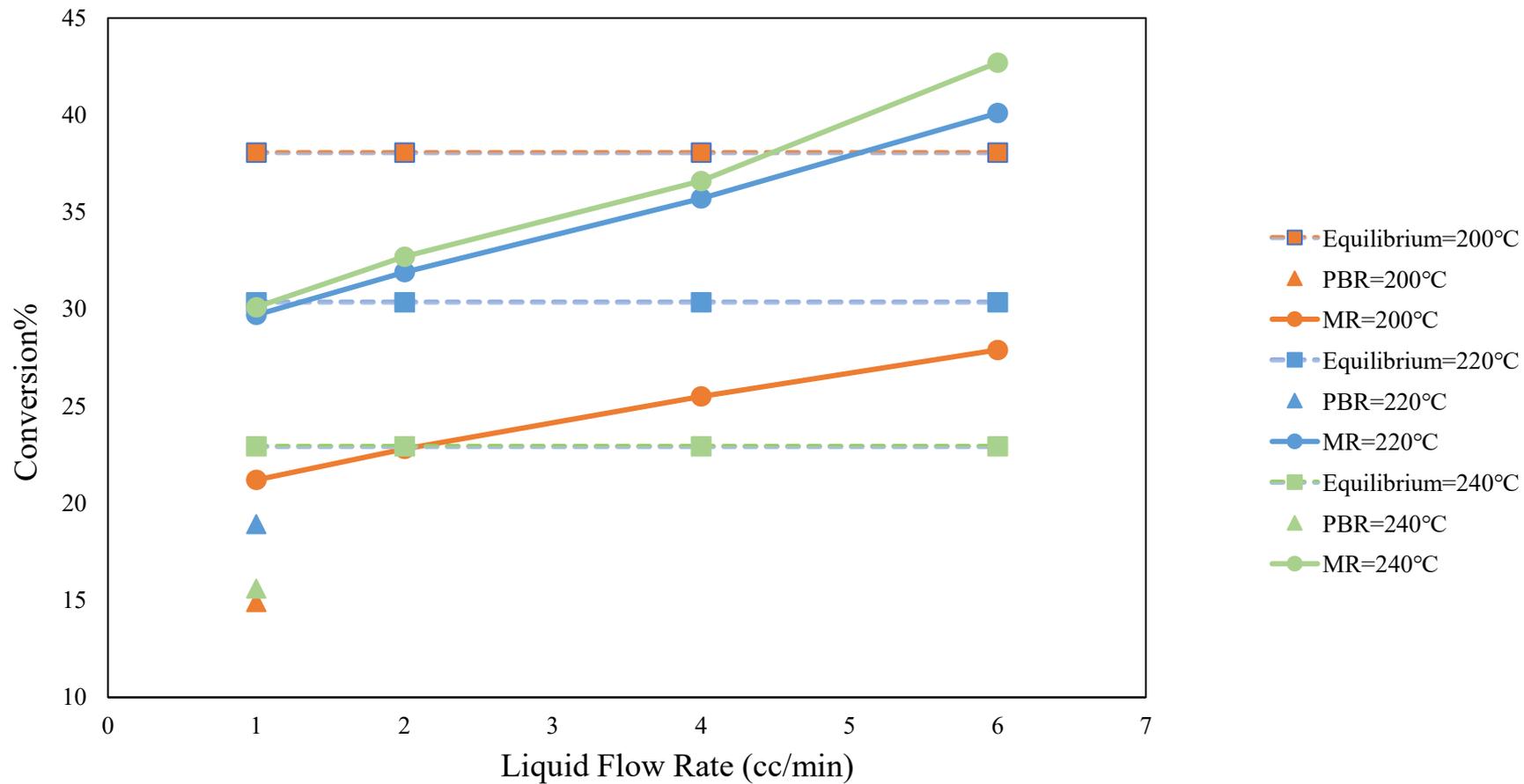
SN=2, P=30 bar, CF=0.37 (Left Side Plot), CF=0.502 (Right Side Plot)

PBR and MCR Conversion vs. W/F, Varying P



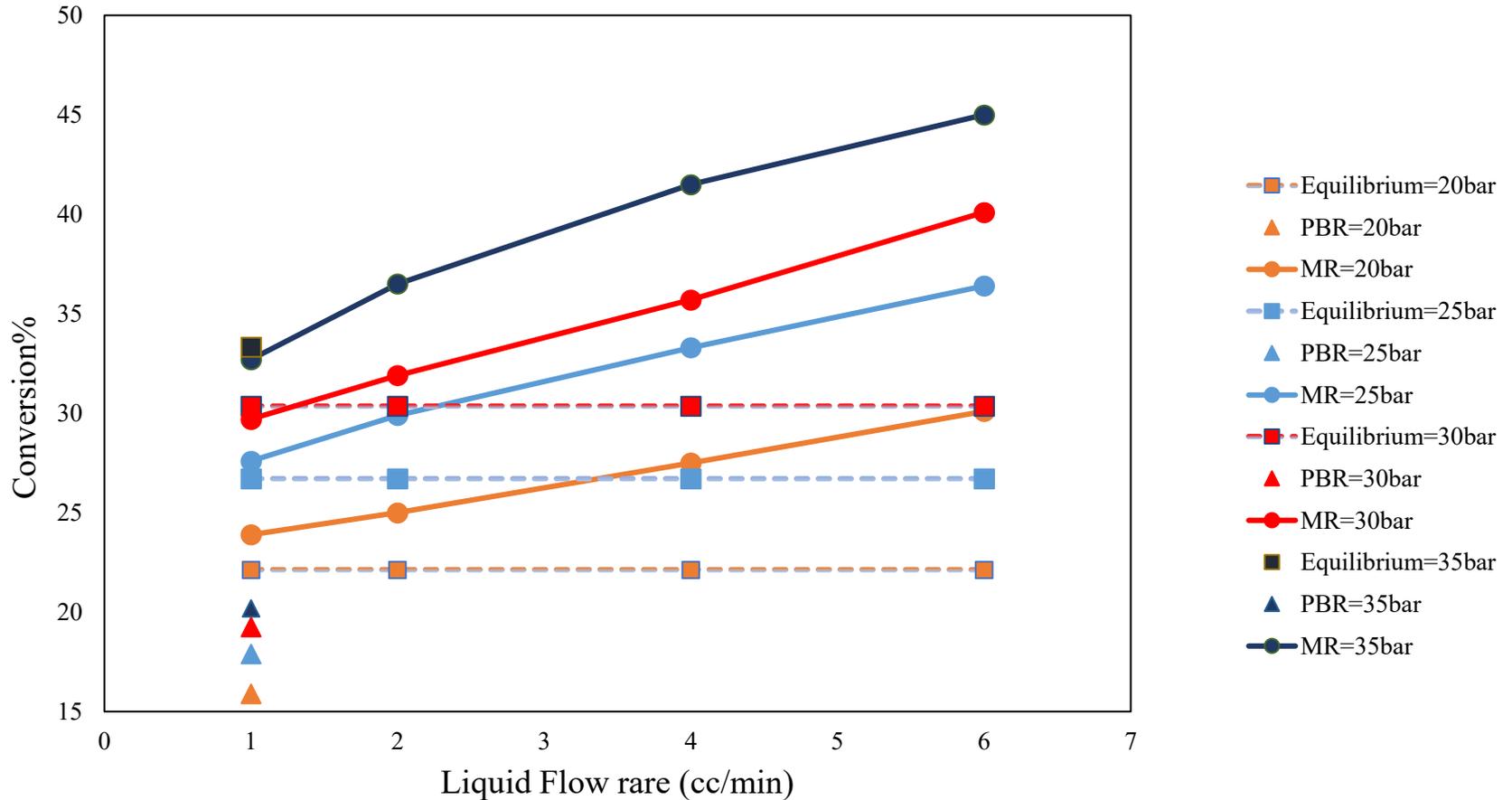
SN=2, T=220 °C, CF=0.37 (Left Side Plot), CF=0.502 (Right Side Plot)

PBR and MCR Conversion vs. LF, Varying T



SN=2, P=30 bar, CF=0.37, W/F=20 Kg*s/mol

PBR and MCR Conversion vs. LF, Varying P



SN=2, T=220 °C CF=0.37, W/F=20 Kg*s/mol

Progress To Date

- **RWGSR/MeS-MCR lab-scale system designed and constructed.**
- **Performance of the MeS-MCR subsystem studied and its ability to function as a 2nd stage following the RWGSR validated.**
- **In-house MeS kinetic model validated with the additional MeS-PBR data generated under conditions relevant to the proposed application.**
- **RWGS catalyst prepared and characterized. Testing to evaluate its catalytic performance under relevant experimental conditions currently ongoing.**

Future Work

- **Continue and complete the performance evaluation of the RWGSR subsystem. Initiate and complete the study of the integrated RWGSR/MeS-MCR system to evaluate its performance for a broad range of pressure and temperature conditions.**
- **Use the experimentally-validated model for process design and scale-up to assess the attainable region of conversions, aiming to obtain >90% carbon capture and utilization.**
- **Carry out a techno-economic analysis (TEA) of the proposed RWGSR/MeS-MCR process to compare performance with that of the conventional, absorption-based carbon separation and capture (CSC) technologies.**

Potential Areas of Collaborative Work with NETL

- **Preparation and characterization of novel RWGS catalysts (ongoing).**
- **Optimizing engineering design and reaction conditions for the novel CSC process and evaluating their impact on the balance of plant.**
- **Evaluating the economics and environmental aspects of the CSC process, and comparing them with those of the absorption-based processes.**

Acknowledgements

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