

Rapid Load Response of SOFC-GT Hybrid Systems to Grid Demand



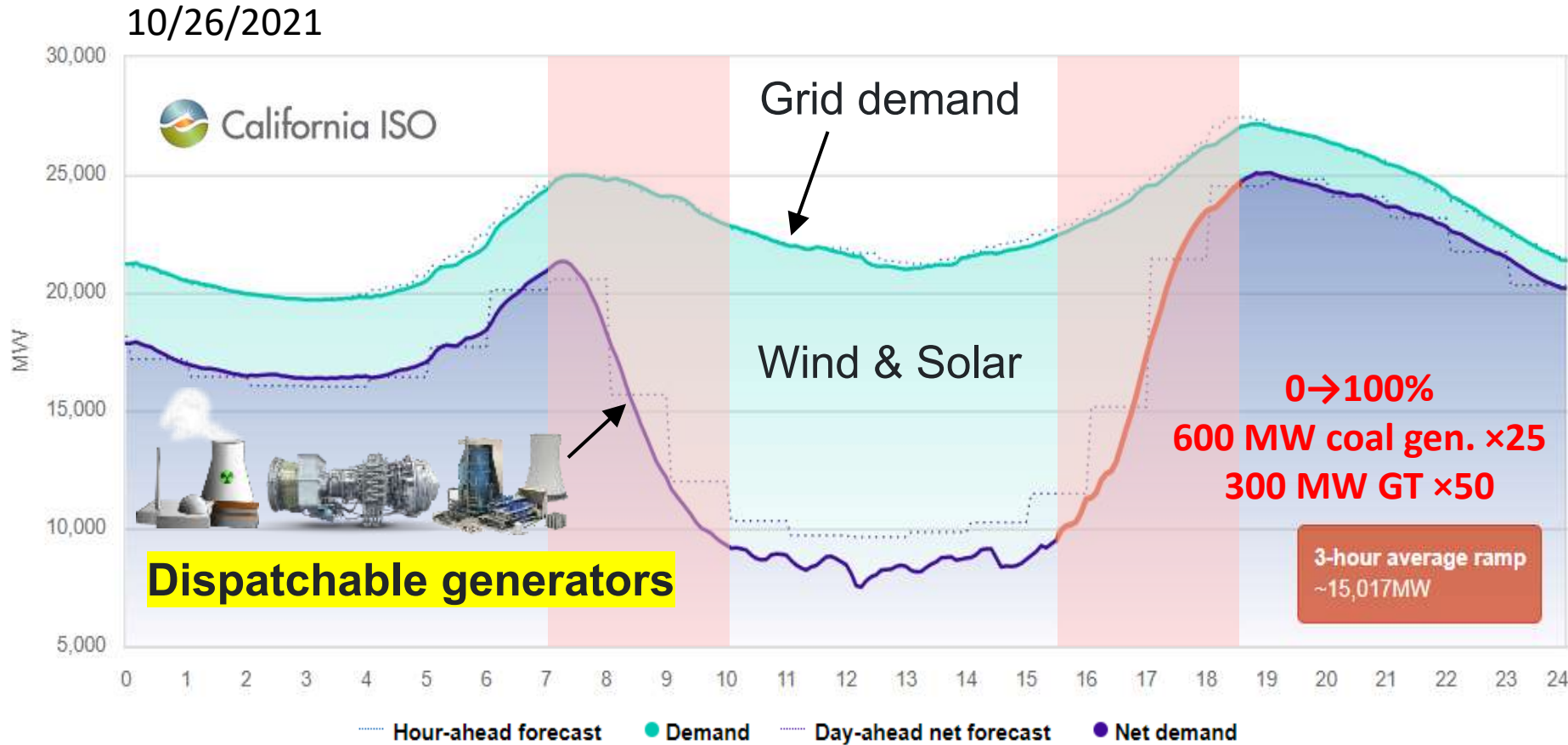
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Improved flexibility requirements



Requirements:

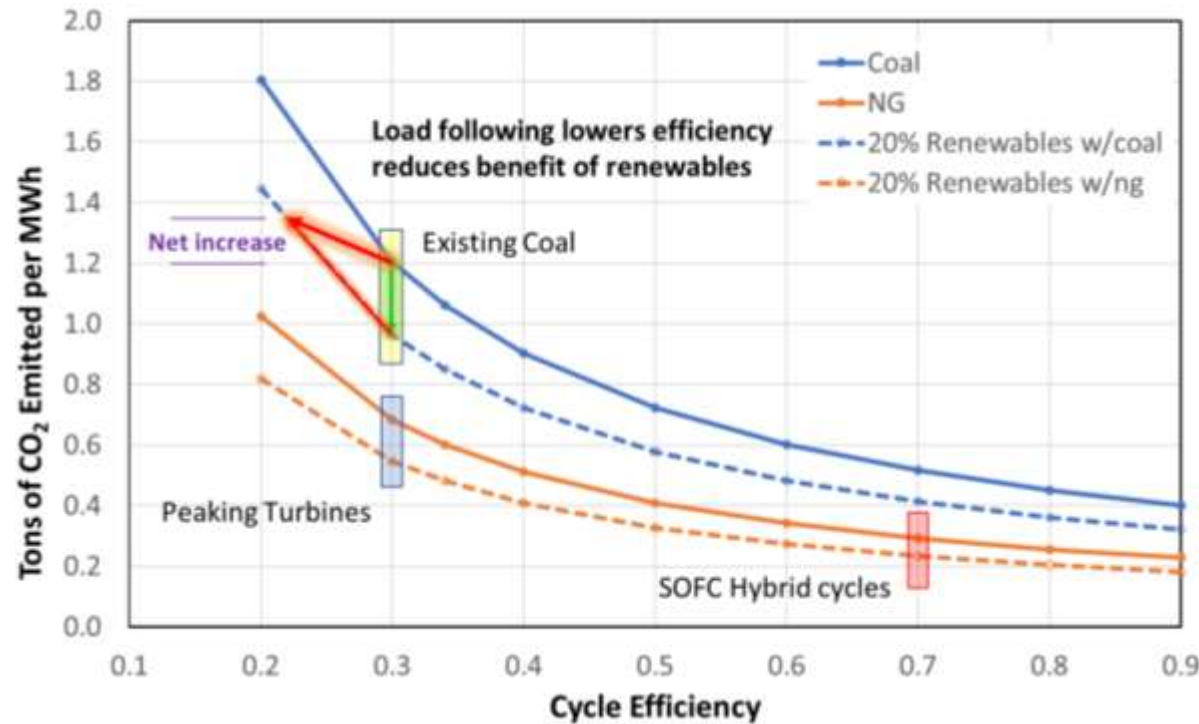
- *Deep turndown*
- *Rapid ramping*
- *Fast start-up*

Challenges:

- *Increased emission at part load*
- *Phase-out*

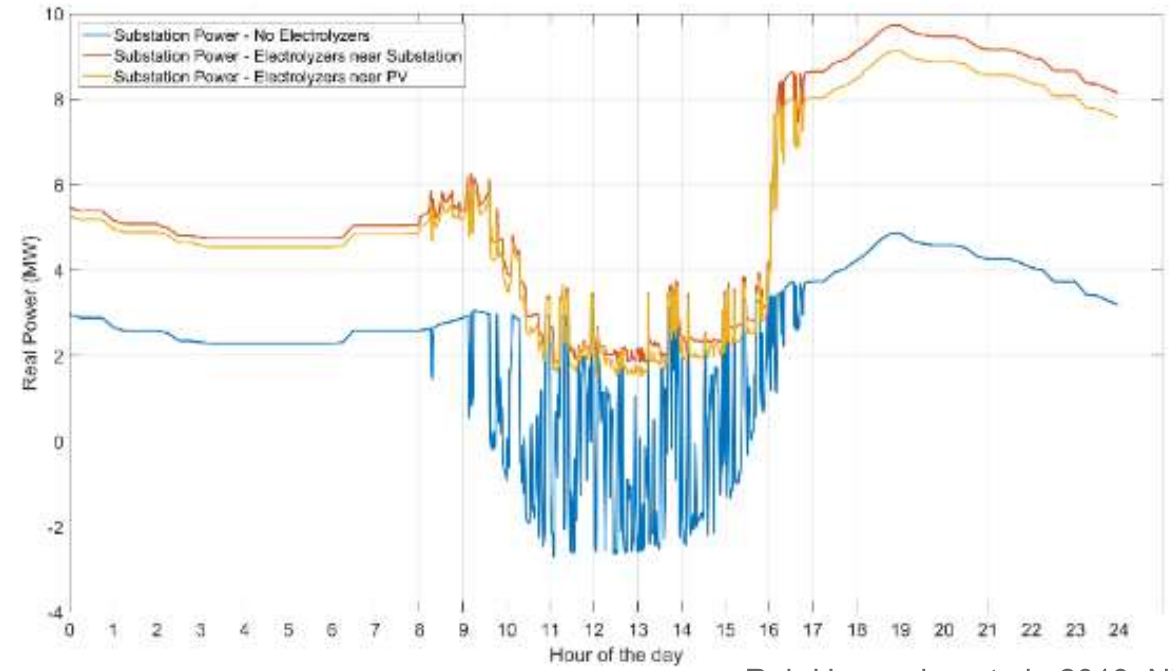
Rapid load transition is essential for integrated energy systems

SOFC-GT hybrids in integrated energy systems



High efficiency –

low emission <0.3 tons CO₂ per MWh (>75% reduction vs. conventional coal generator)

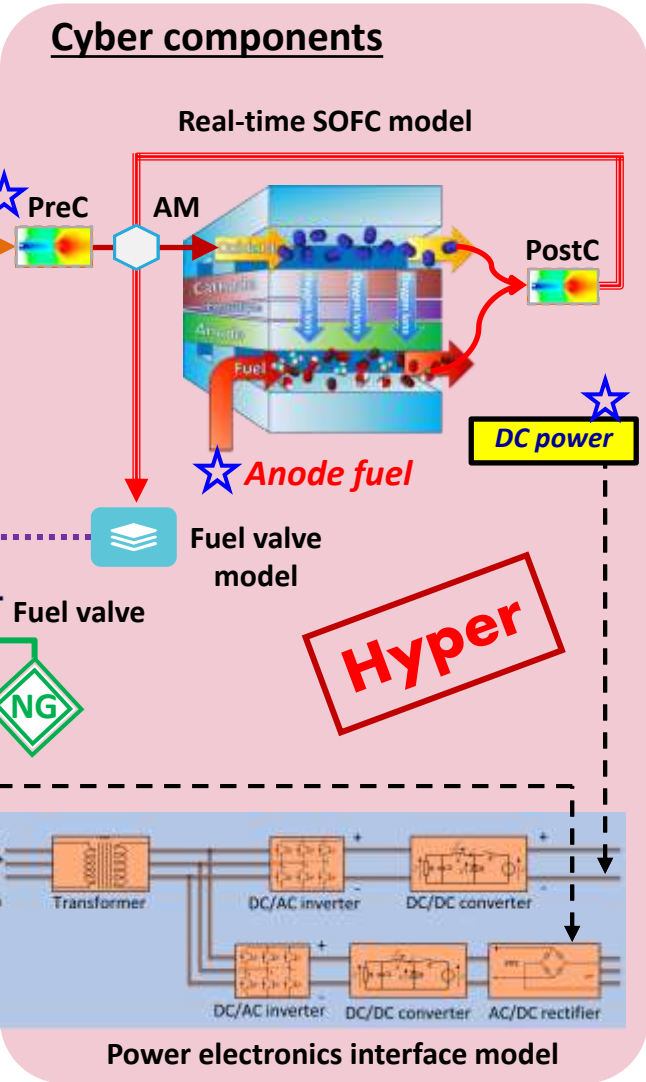
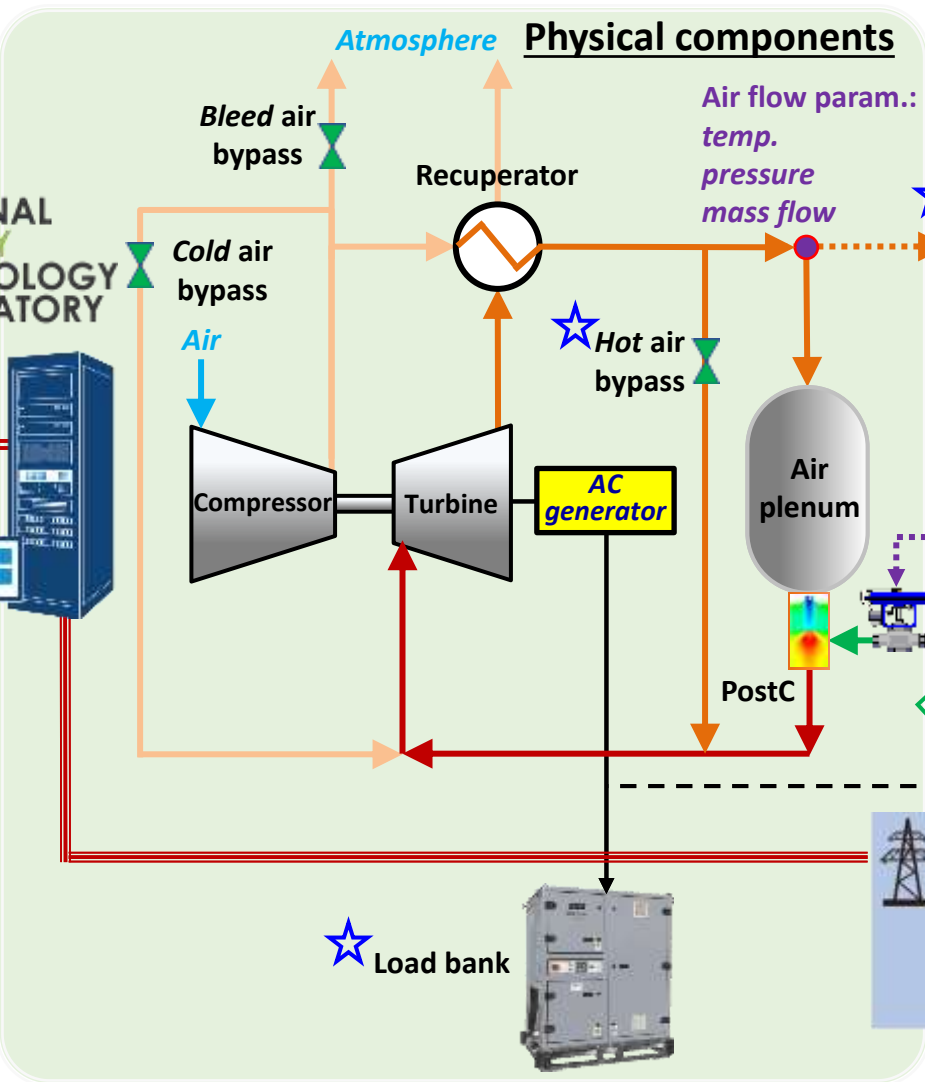
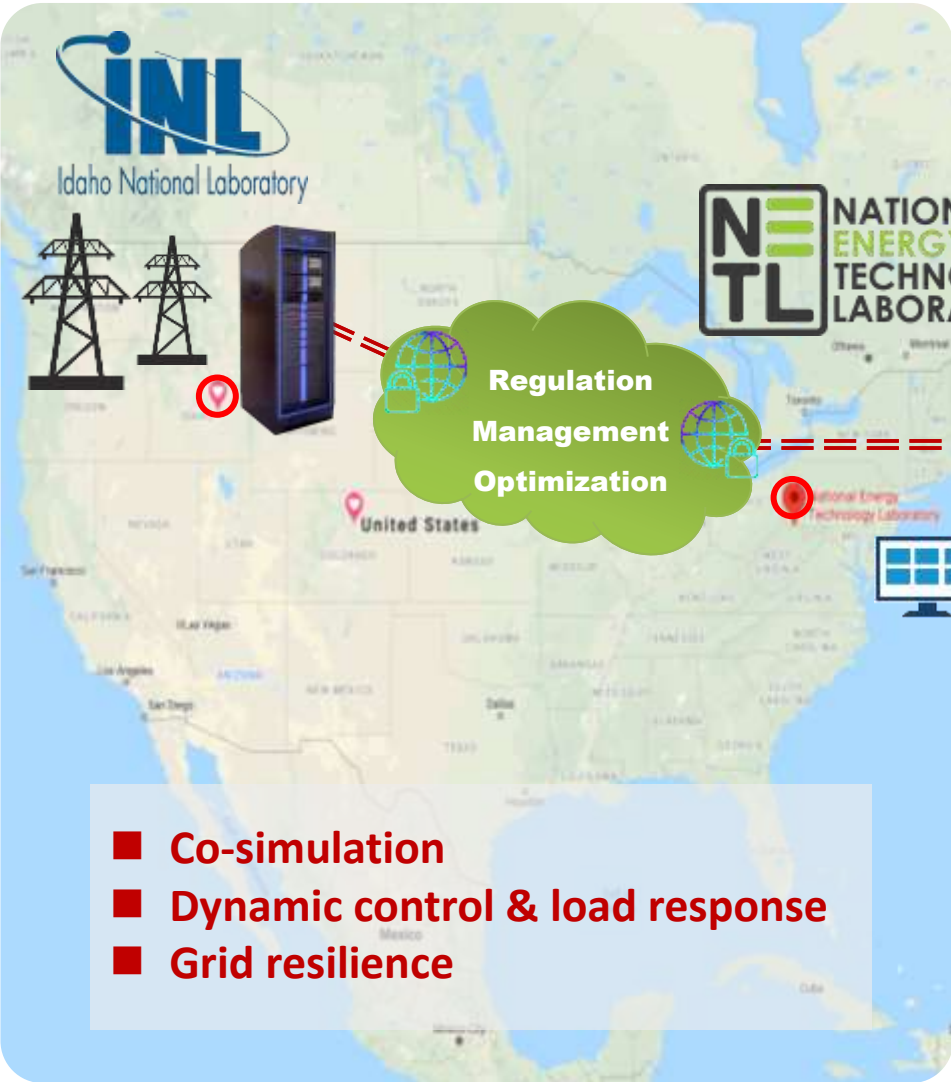


Rob Hovsapien et al., 2019, NREL

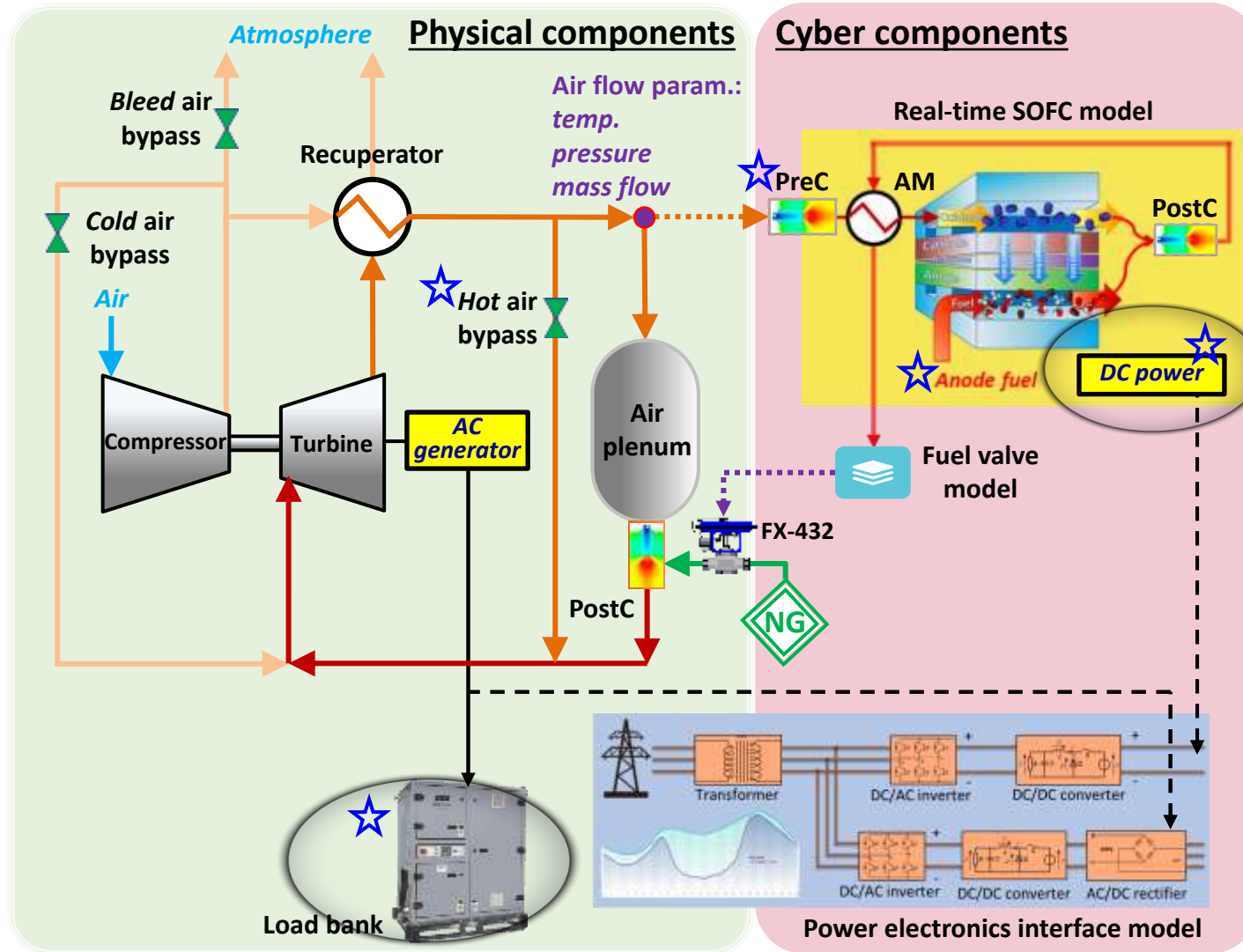
Rapid load transition –

reduced capacity requirement and load cycling of energy storage batterie / electrolyzers

Co-simulation platform between NETL and INL



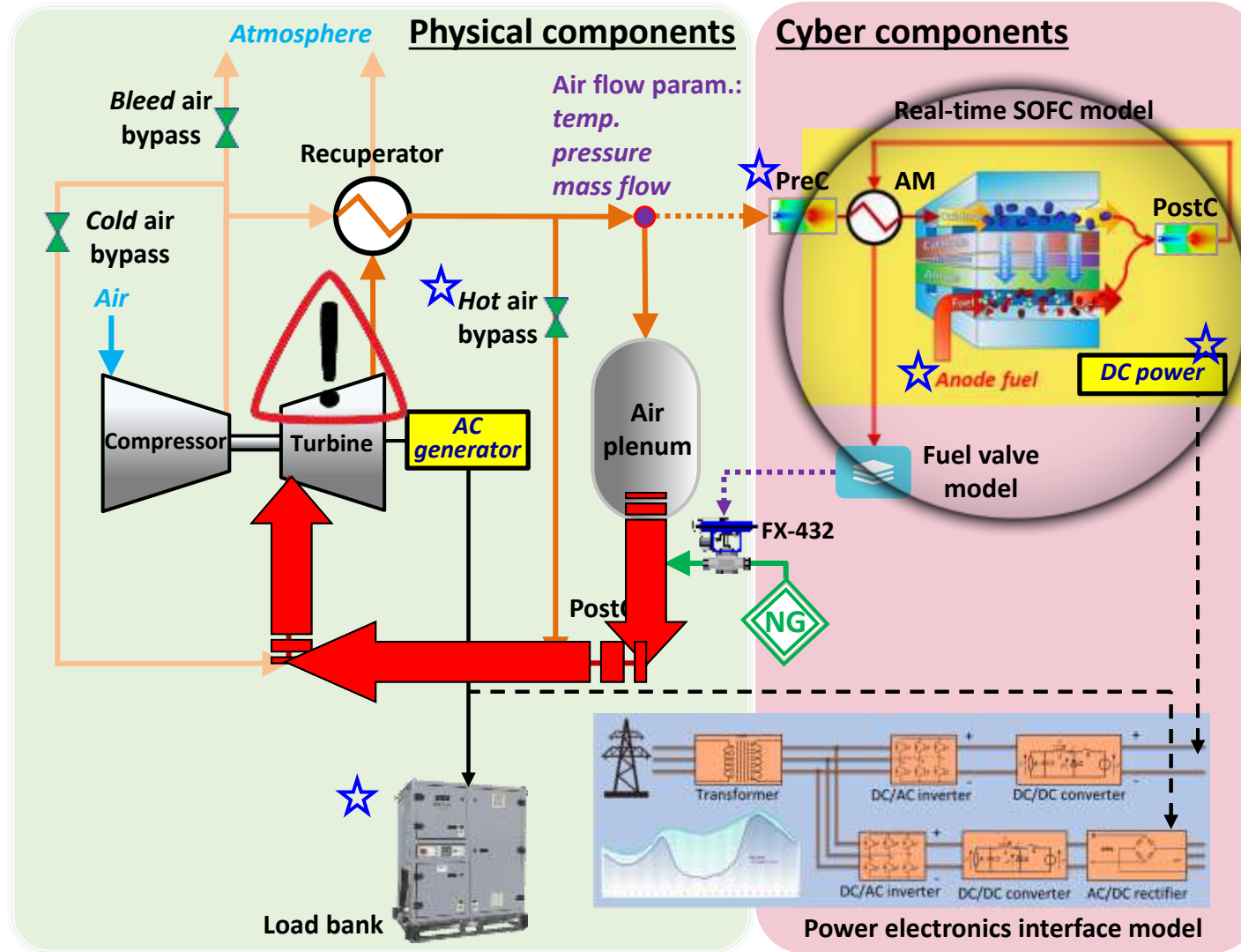
Rapid load transition strategies (**50% turndown in 10 s**)



Strategies:

- Ramp SOFC & GT load concurrently

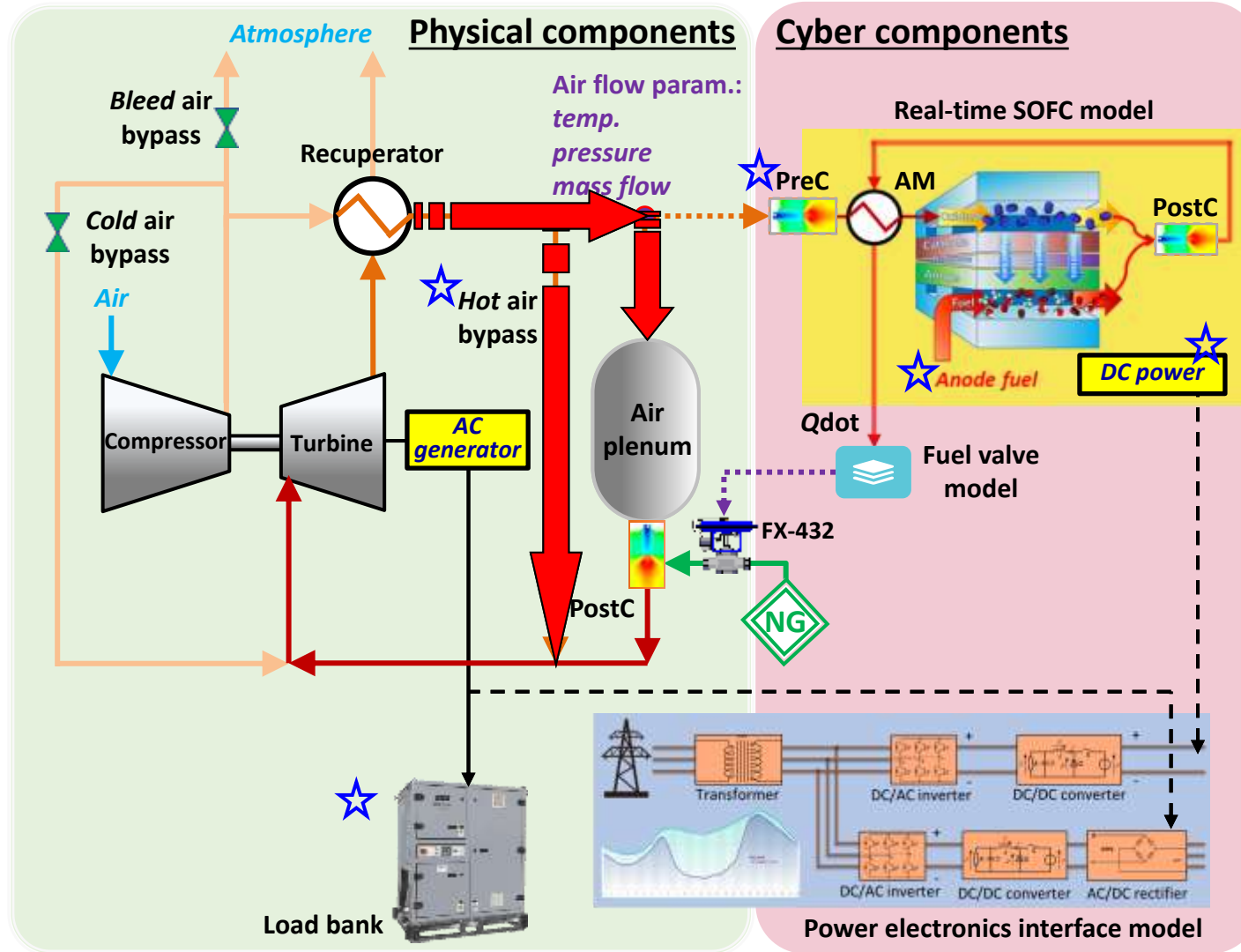
Rapid load transition strategies



Strategies:

- Ramp SOFC & GT load concurrently
- Manipulate SOFC anode fuel valve
(maintain SOFC FU at 65%)

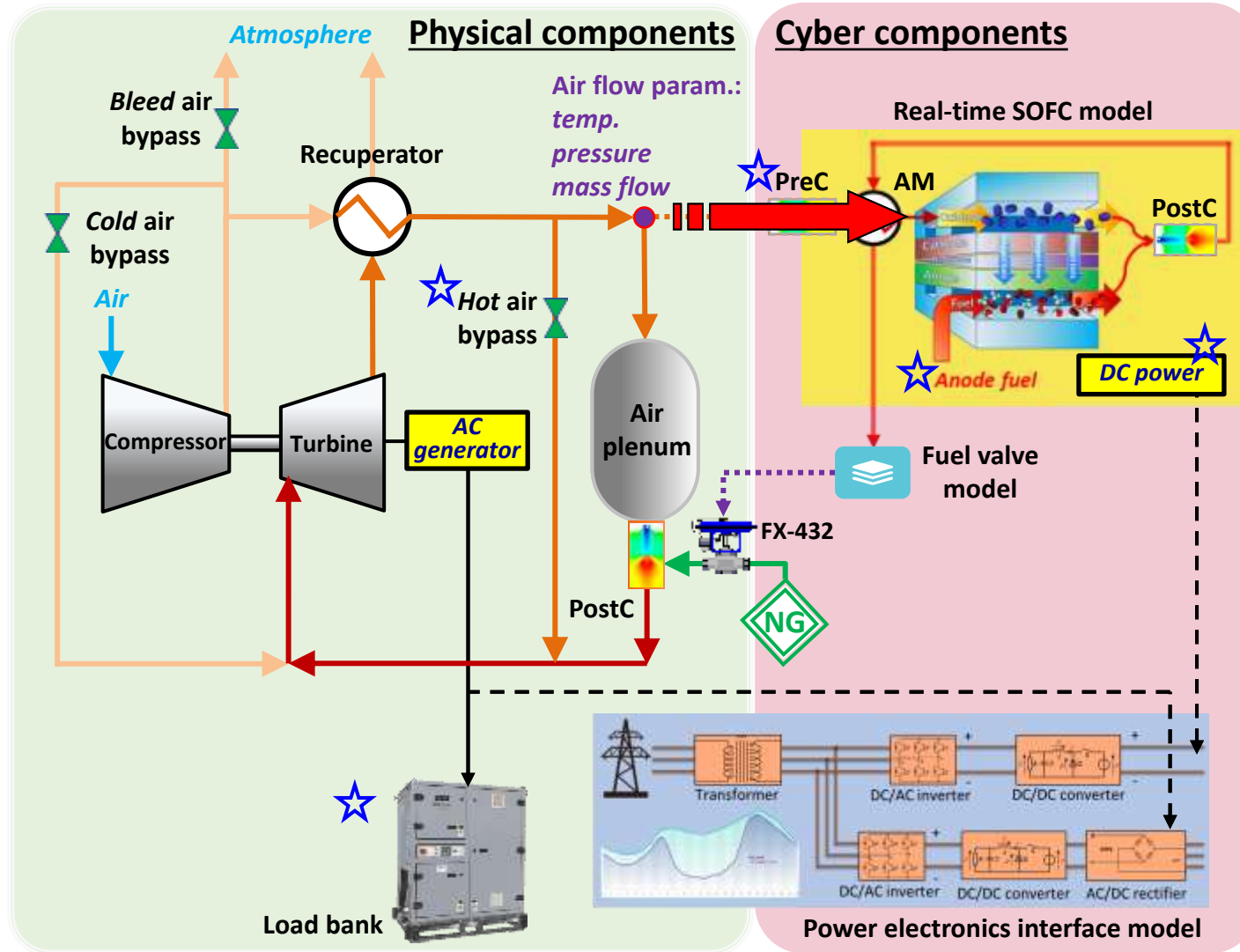
Rapid load transition strategies



Strategies:

- Ramp SOFC & GT load concurrently
- Manipulate SOFC anode fuel valve
(maintain SOFC FU at 65%)
- Manipulate hot-air bypass valve
(vary SOFC air flow)

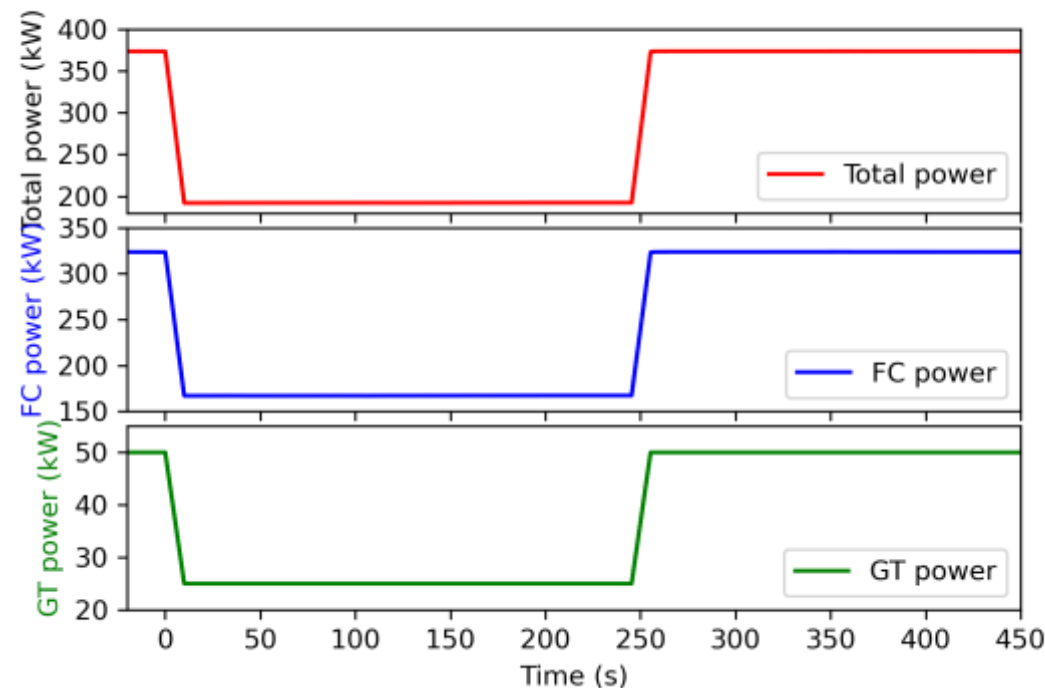
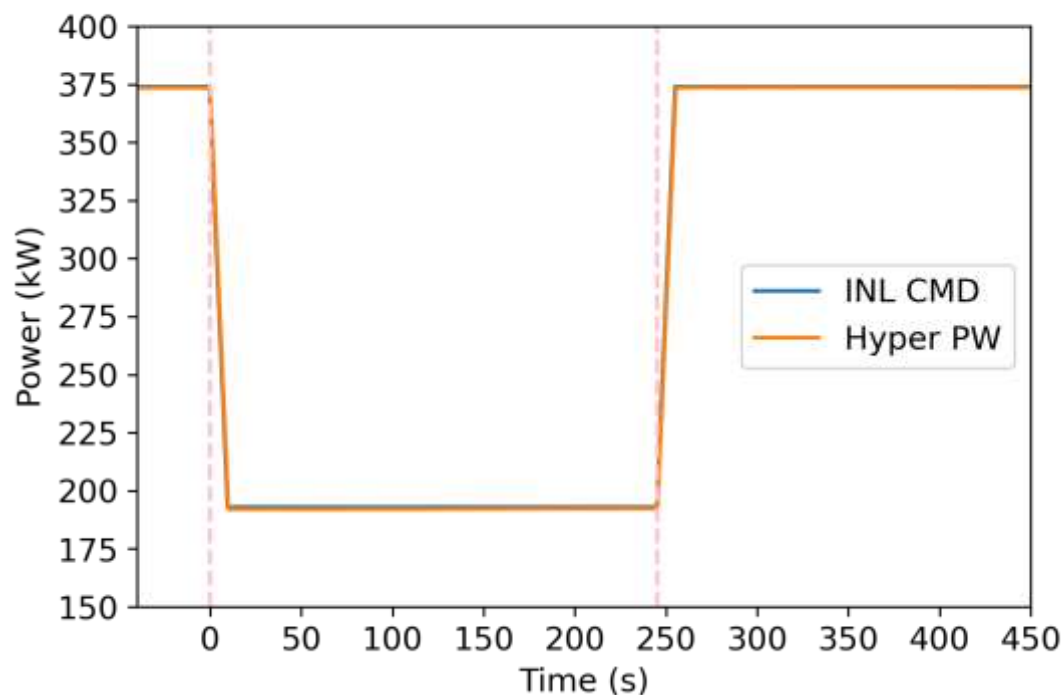
Rapid load transition strategies



Strategies:

- Ramp SOFC & GT load concurrently
- Manipulate SOFC anode fuel valve
(maintain SOFC FU at 65%)
- Manipulate hot-air bypass valve
(vary SOFC air flow)
- Manipulate fuel to pre-combustor
(maintain cathode inlet air temp.)

Rapid Load Response to Grid Demand Signals

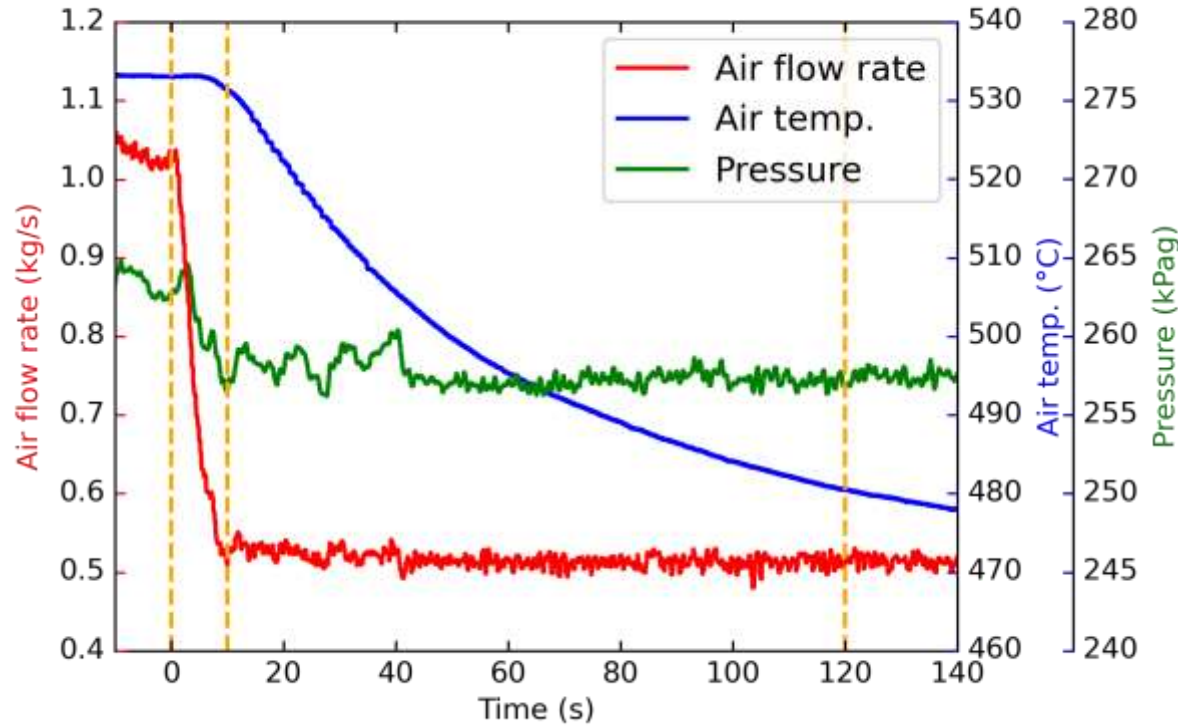


- NETL's Hyper facility load followed INL's grid demand signals
- Total power 373.6 kW → 192.6 kW (48.4% turndown) → 373.6 kW
- SOFC power 323.6 kW → 167.6 kW (48.2% turndown) → 323.6 k
- GT power 50 kW → 25 kW (50% turndown) → 50 kW

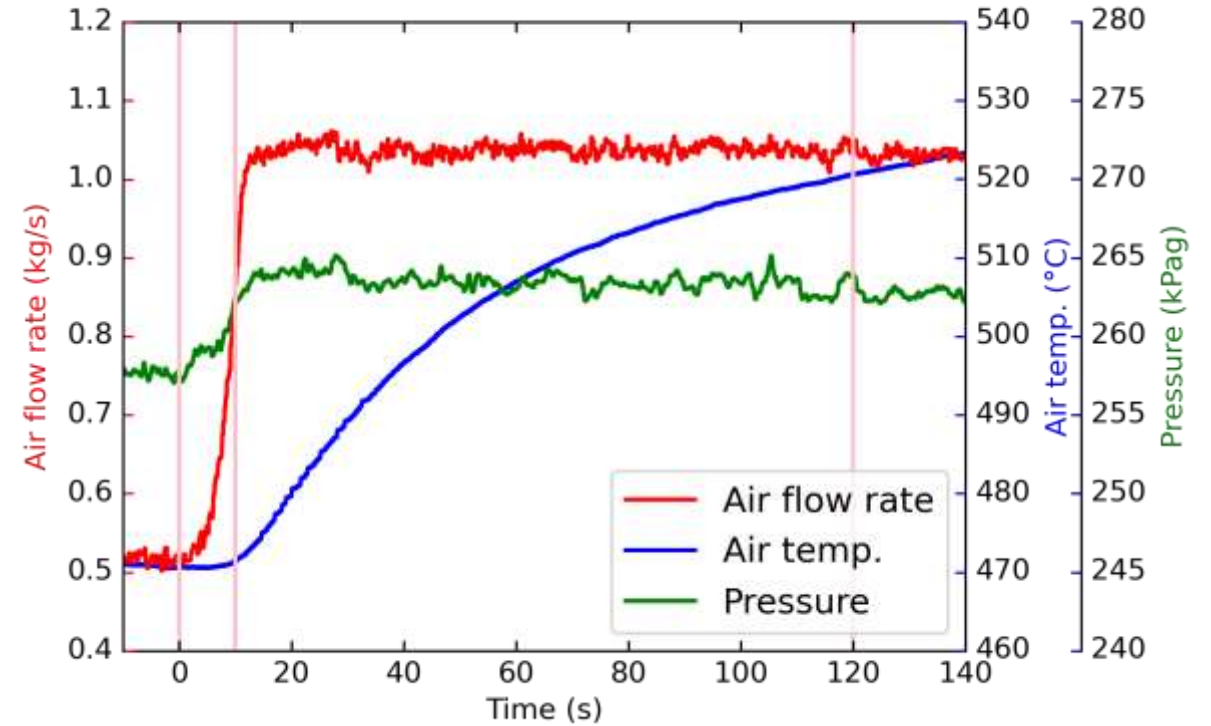
in 10 seconds

Air parameters measured from hardware (live inputs to the CPS SOFC models)

Turndown

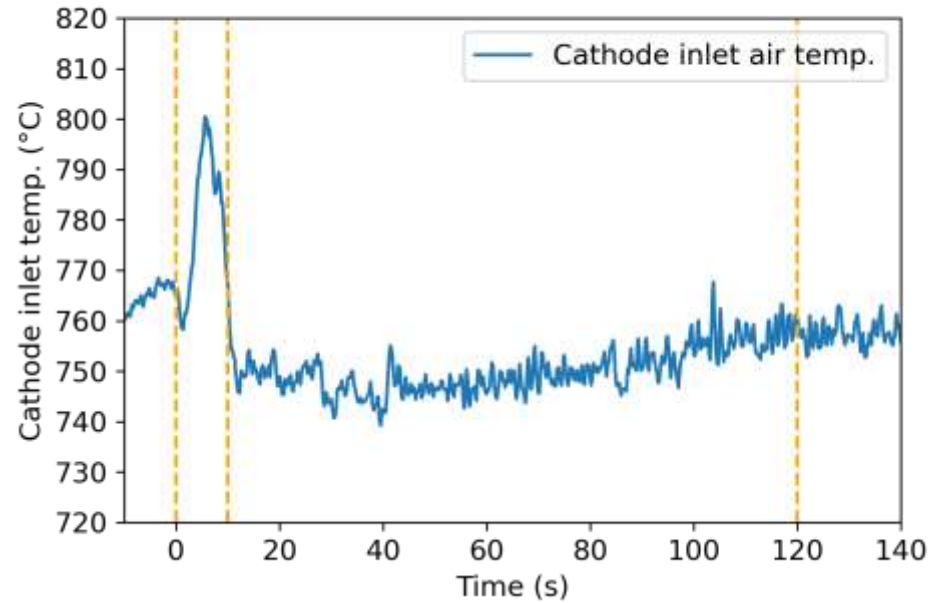


Ramp up

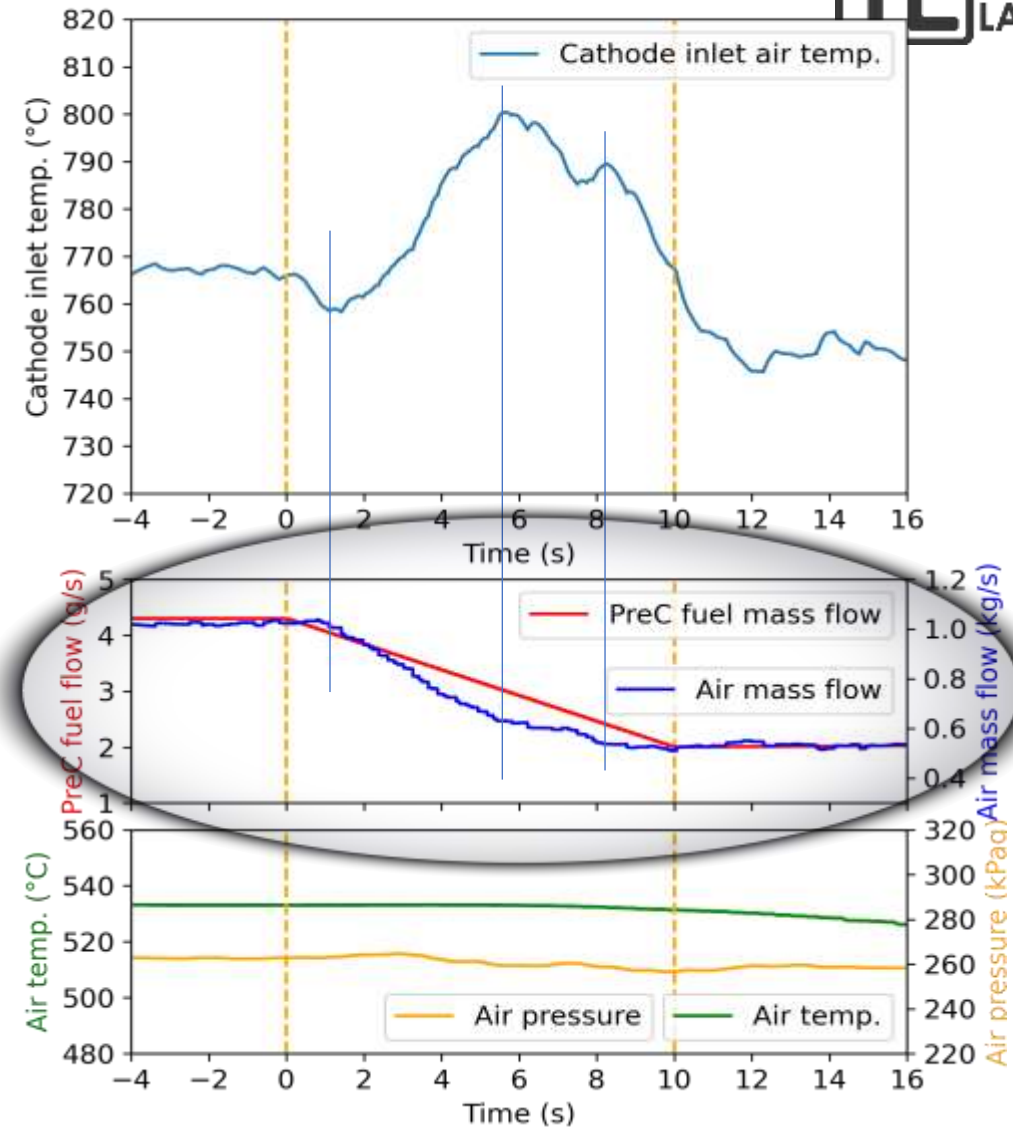


- The air flow rate was manipulated by the *hot air* bypass valve (25% opening → 100%)
- Air temperature transient reflected the coupling of SOFC-GT hybrid and the value of hardware-based simulation

Cathode inlet air temperature (turndown)

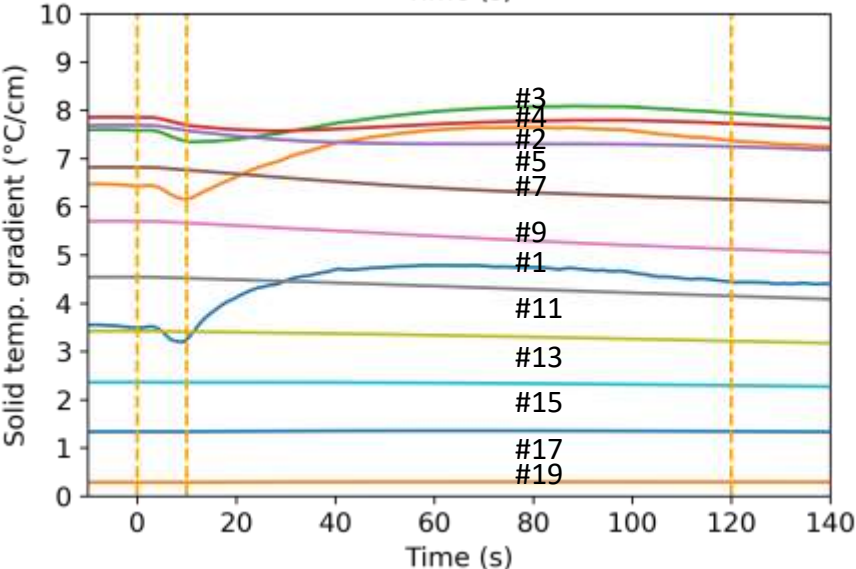
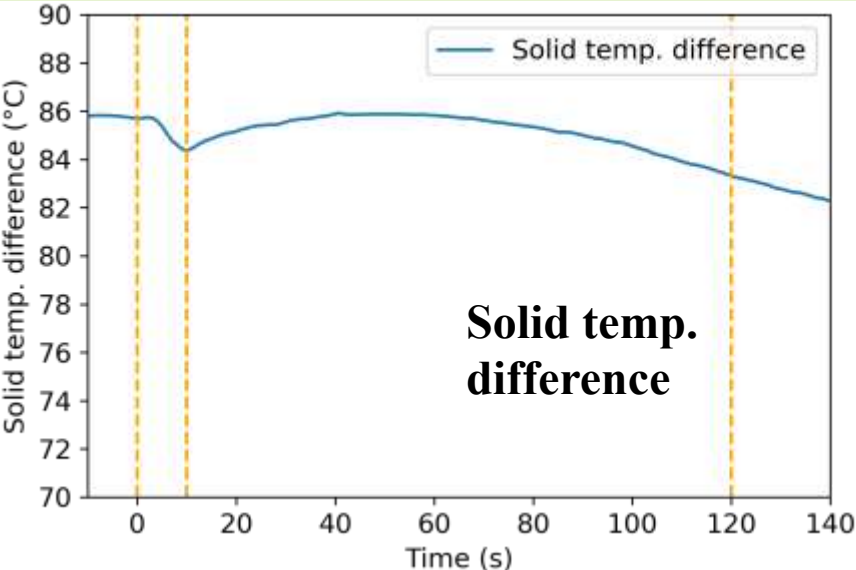


- Pre-combustor fuel flow and cathode airflow varied **linearly**
- Actual transients from real control hardware (i.e., *hot air bypass valve*) caused **non-linear** temperature response



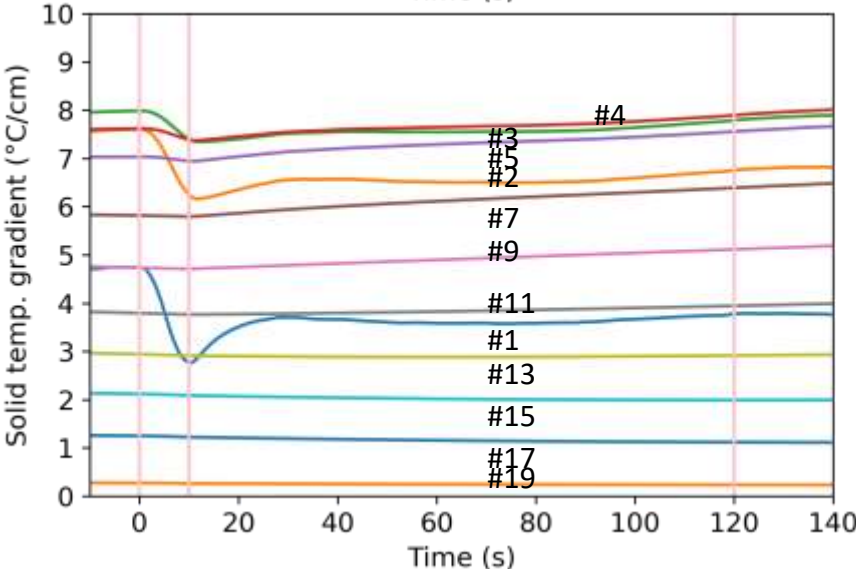
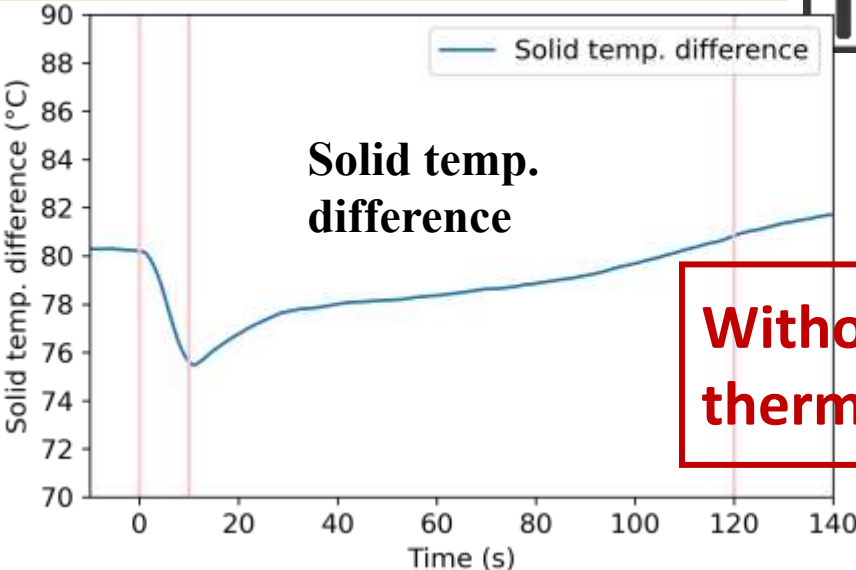
SOFC solid temp. difference & temp. gradient

Turndown



Solid temp.
gradient

Ramp up

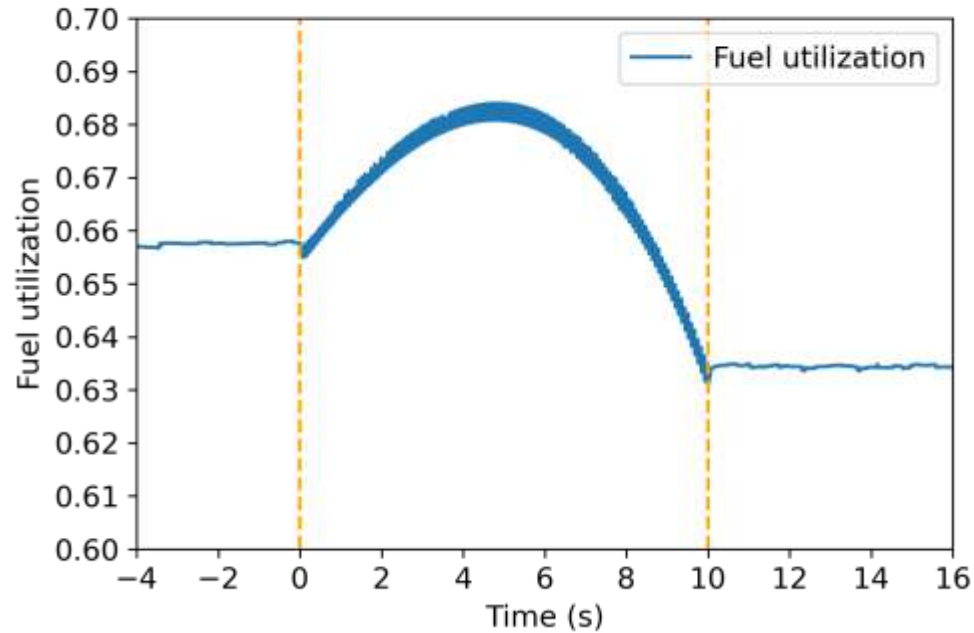


Solid temp.
gradient

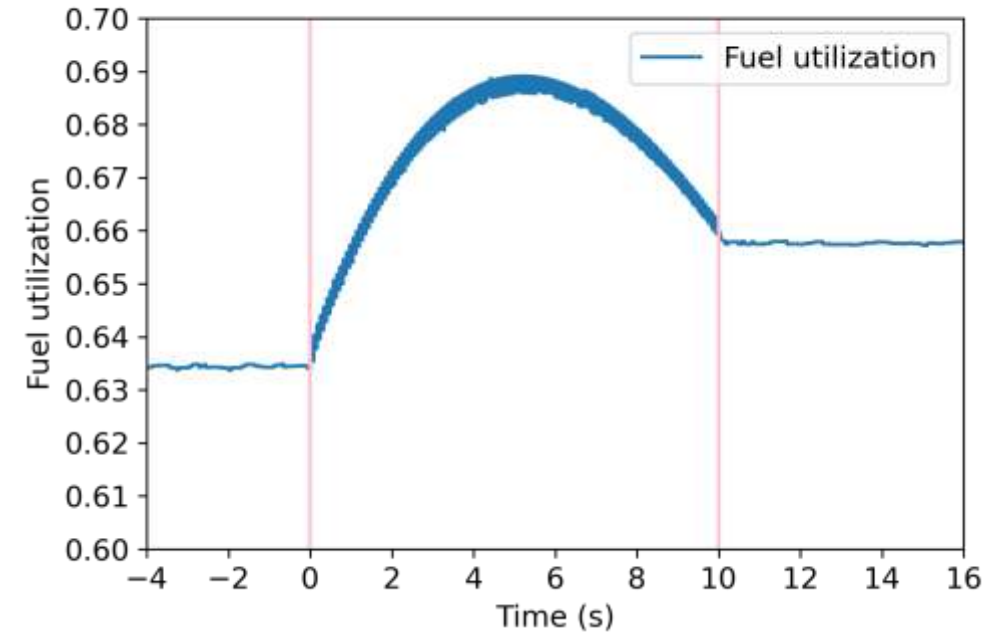
**Without violating
thermal constraints**

SOFC fuel utilization

Turndown



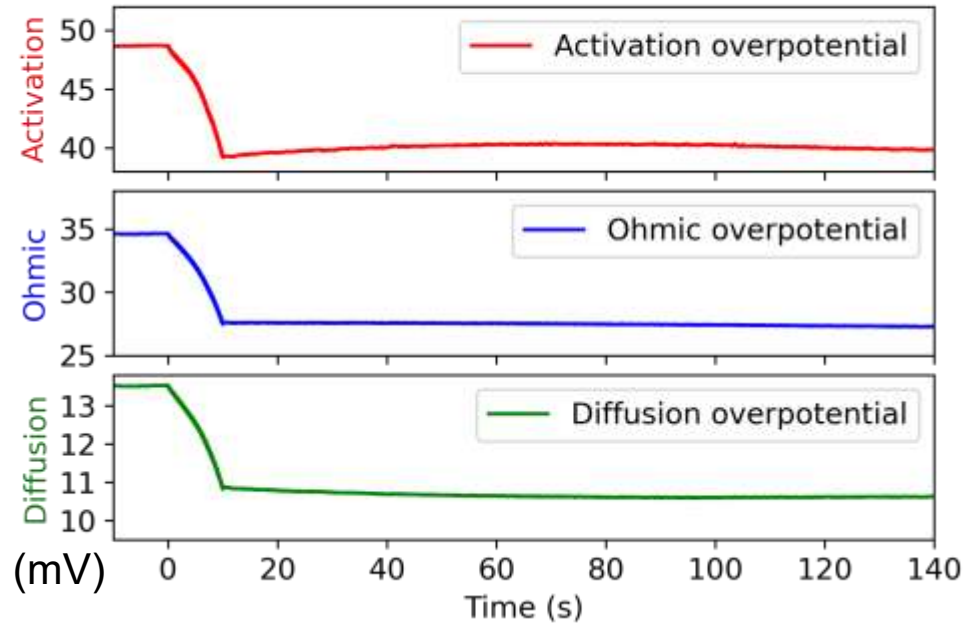
Ramp up



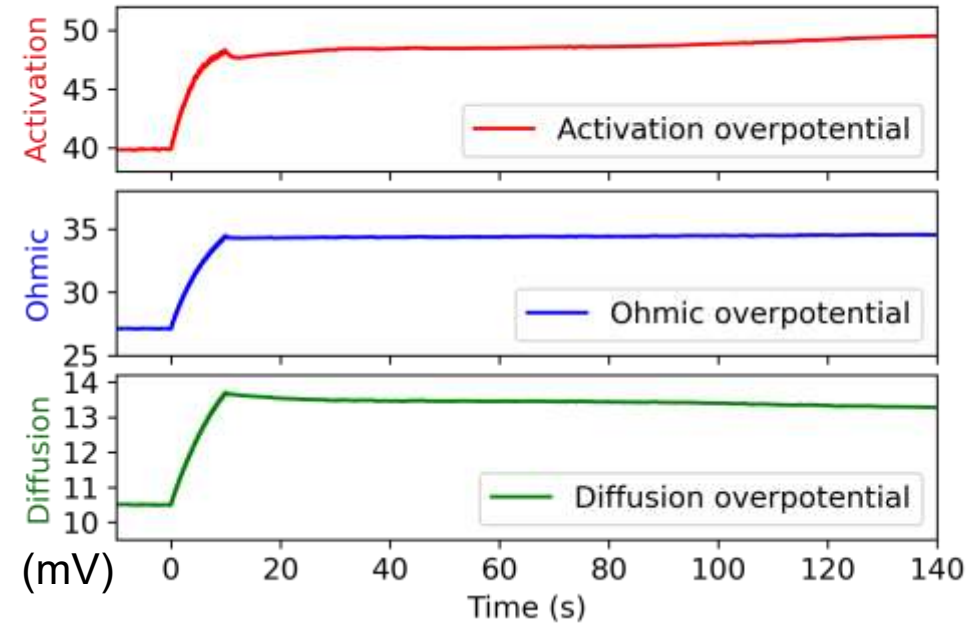
- SOFC current load and anode fuel valve opening varied **linearly**
- **Non-linear** transients were observed due to fuel mass flow transitions

SOFC overpotentials (on node #1)

Turndown



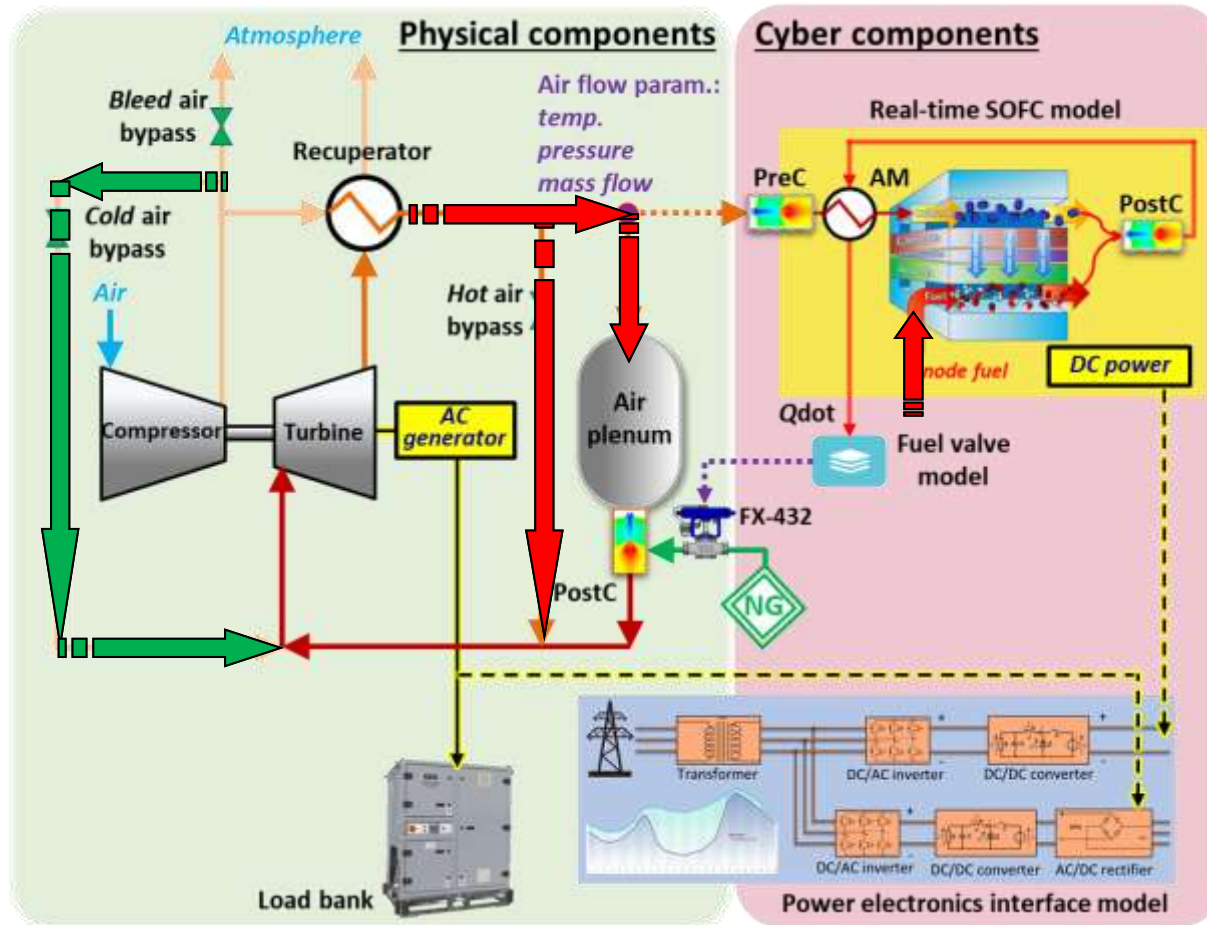
Ramp up



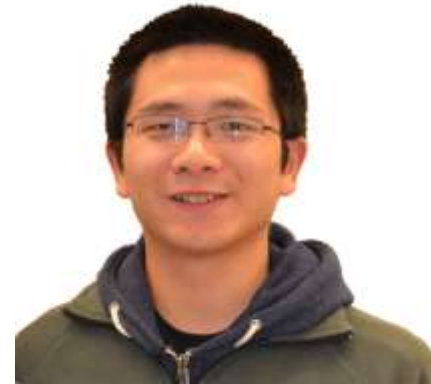
- Diffusion overpotential was much lower than the activation and ohmic overpotentials
- Fuel transfer limitation can be negligible during load transitions

SOFC was protected without violating operability constraints

The need for adaptive controls



- There could be a paradigm shift for the intended application of SOFCs: from **large baseload** to **flexible load responsive systems** to maintain grid stability
- This study highlighted the **non-linear nature** of tightly coupled SOFC-GT system components, especially the non-linear response of SOFC cathode inlet temperature controls
- **Adaptive controls** are under development



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