

Additively Manufactured Graded Composite Transition Joints (AM-GCTJ) for Dissimilar Metal Weldments in Advanced Ultra-Supercritical Power Plant

<u>Xingbo Liu¹</u>, Kostas Sierros¹, Zhili Feng², Yanli Wang², David Novotnak^{3,} Ron Alman³, Haiyang Qian⁴, Ray Chamberland⁴

^{1.}West Virginia University; ²Oak Ridge National Laboratory

³ Carpenter Additive; ⁴GE Steam Power.

June 10, 2021









DMWs in A-USC and HRSG





DMW:

- 1. Grade 91 Austenitic Stainless Steel
- 2. Ni based alloy Austenitic Stainless Steel



GE Steam: A-USC Mock Header





Program on Technology Innovation: Guidelines and Specifications for High Reliability Fossil Power Plants—Best Practice Guideline for Manufacturing and Construction of Grade 91 Steel to Austenitic Stainless Steel Dissimilar Metal Welds 3002007221 Final Report, December 2017



Mismatch of coefficient of thermal expansion and **thermal cycling:**



DMW with sharp material transition

- Mismatch of coefficient of thermal expansion between different materials lead to high strain range along the interface during thermal transients.
- Increasing demand in industry for flexible operation of steam boilers and more cycling capability of HRSGs.

Higher cycling requirements in power industry:

 Steam Boilers: A sample required number of cycles for a new unit

	Total # of cycles of 25 years
Cold Start	455
Warm Start	910
Hot Start	4550

 HRSGs: Typical required number of cycles for a cyclic operating CCPP

	Total # of cycles of 25 years
Cold Start	250
Warm Start	1250
Hot Start	4250





Current Dissimilar Metal Welds (DMWs)

Failures in DMWs @ the fusion boundary between Grade 91 and nickel based filler metal, often accompanied with considerable damages in the HAZ of Grade 91

HT exposure during PWHT or service causes carbon diffusion from the ferritic matrix toward the austenitic matrix. Leads to the formation of a carbon-depleted soft zone on the ferritic side and nucleation/growth of carbides on the ASS side that have very high hardness.

Under imposed residual, external, and thermal stresses caused by the CTE mismatch between different alloys of the DMW, creep and/or creep fatigue cracks can occur along the fusion boundary and HAZ.















AM-Graded Transition Joints (GTJs)



- "Conventional" AM (wire or powder) approach melts alloys A&B completely together
 - A critical issue is the continuous transition in composition creates complex and often undesired microstructure









Advantages of AM-GCTJ

 Solid-state Process, composites material" transition with constituents of known chemistry (such as P91, SS304, A182) mixed in controlled proportion

> •Solved the critical drawbacks of undesired/unpredictable phases/microstructure in conventional AM approach to fabricate the transition joint

- 100% smooth transitions
- Welding happens at A-A, and B-B, no DMWs
- Minimize scale-up issues expected to manufacture large quantity of joints





HRSG configuration highlighting potential DMW locations (1: tubing internal to the HRSG setting; 2: link piping; 3: outlet piping.)

Illustration of DM weld in power plants

* U.S. Patent Appl. No. 62/704,965 – Method to Produce an Additively Manufactured-Graded Composite Transition Joint

6









NATIONAL

TECHNOLOGY



PROJECT OBJECTIVES – PHASE I

- (1) To develop and demonstrate at the lab-scale the additively manufactured graded composite transition joints (AM-GCTJ) for dissimilar metal weldments (DMW) in next generation advanced ultra-supercritical (A-USC) coal-fired power plants, that can significantly improve the microstructural stability, creep and thermal-mechanical fatigue resistance, as compared with their conventional counterparts;
- (2) To prepare for Phase II of the project, in which we will manufacture and test the components with AM-GCTJ, to advance the technology readiness level to TRL-7, and manufacturing readiness level to MRL 6-7, for targeted commercial applications identified by GE Steam Power, the primary industry partner of the project team











PROJECT OBJECTIVES – PHASE I

- (1) To develop and demonstrate at the lab-scale the additively manufactured graded composite transition joints (AM-GCTJ) for dissimilar metal weldments (DMW) in next generation advanced ultra-supercritical (A-USC) coal-fired power plants, that can significantly improve the microstructural stability, creep and thermal-mechanical fatigue resistance, as compared with their conventional counterparts;
- (2) To prepare for Phase II of the project, in which we will manufacture and test the components with AM-GCTJ, to advance the technology readiness level to TRL-7, and manufacturing readiness level to MRL 6-7, for targeted commercial applications identified by GE Steam Power, the primary industry partner of the project team









DMW and **AM-GCTJ**

AM-GCTJ



Conventional DM Weld



Fabricated 2 types of welds using either SS309 or A182 weld wire









Hot Corrosion in Coal Ash - DMW



Temperature - $650 \,^{\circ}\text{C}$ Time - $30 \,\text{days}$ Coal Ash - $10\% \,\text{Na}_2\text{SO}_4$, 10% $K_2\text{SO}_4$, $10\% \,\text{Fe}_2\text{O}_3$, 35% $Al_2\text{O}_3$ and $35\% \,\text{SiO}_2$ Gas - $1 \,\text{vol.} \% \,\text{SO}_2$, $4 \,\text{vol.} \%$ O_2 , $15 \,\text{vol.} \% \,\text{CO}_2 \,\&\, 80 \,\text{vol.}$ $\% \,\text{N}_2$











Hot Corrosion in Coal Ash – AM-GCTJ



Temperature - $650 \,^{\circ}\text{C}$ Time - $30 \,\text{days}$ Coal Ash - $10\% \,\text{Na}_2\text{SO}_4$, 10% $K_2\text{SO}_4$, $10\% \,\text{Fe}_2\text{O}_3$, 35% $Al_2\text{O}_3$ and $35\% \,\text{SiO}_2$ Gas - $1 \,\text{vol.} \,\% \,\text{SO}_2$, $4 \,\text{vol.} \,\%$ O_2 , $15 \,\text{vol.} \,\% \,\text{CO}_2 \,\& \,80 \,\text{vol.}$ $\% \,\text{N}_2$











ORNL's ICWE Modeling Tool being Used to Design and Optimize the AM-GCTJ

- Designed AM-GCTJ to significantly reduce the strain accumulation at critical locations during thermal cyclic loading
- It will also significantly improve the creep failure life predicted failure will be shifted to Grade 91 base metal



ICWE Prediction of Creep Strain Accumulation and Rupture Life at 650 °C and 90 MPa



t = 200 h

Predicted life of conventional DMW: 230 hrs,

failure at the weld interface in the G91 HAZ







The predicted failure is in G91 base metal. Predicted rupture life is **1815** hours





Actual Creep Test – DMW vs Transition Joint (650 °C and 90 MPa)



Failed at **214** hrs in the G91 HAZ near the interface



Minimal strain localization on the transition joint at 200 hrs. Failed after **1259** hrs near the G91 base metal. Over 5.8x improvement of creep life









DIC Measurement of Creep Strain Evolution and Localization











Grade91-304H Transition Joint (650C-90MPa)



T=479hrs



Total lifetime: 1259 hrs

650C, 90MPa	Conventional DM	AM-GCTJ
Model Prediction	230 hrs, at G91 interface	1815 hrs, in G91 base metal (near interface)
Actual Test	214 hrs, at G91 interface	1259 hrs, near G91/Transition Joint interface









Model Captured Essential Features of Strain Distributions in Thermal Cyclic Loading (25-650°C, 2-2-2 h

Conventional DMW



Model prediction

DIC measurement

AM-GCTJ



Model prediction

DIC measurement



Experimental Measurement of Strain Evolution during Thermal Cyclic Test (On-going)

- Initial observations from in-situ DIC measurement:
 - Considerable reduction of thermal cyclic strain range with AM-GCTJ



AM-GCTJ: averaged over the transition region Conventional DMW: averaged over P91/SS304 interface region





Pipe: Conventional DMW vs AM-GCTJ

Conventional weld









Results after 40 thermal cycles



Summary



- We designed and fabricated a new class of AM-GCTJ
 - Avoid unknown & often undesired complex composition in the conventional AM-GTJ
 - Shows similar corrosion performance in coal ash as conventional DMW
 - Reduce the maximum strain & strain range, and (can) improve thermal mechanical fatigue life of DMW during cyclic operation of thermal-electric power plants
 - Significantly improve creep properties, as compared with convention DMW
- AM-GCTJ has broad applications in various energy systems, AUSC, Gas, CSP, NE, etc.









Phase II Plan

- Further optimize design and manufacturing
- Move up both TRL & MRL
- Detailed TEA
- Start code case
- Be ready for commercial applications



Original proposed 10 MWe











UNIVERSITY of NEBRASKA LINCOLN



NATIONAL

TECHNOLOGY

Acknowledgements

- This material is based upon work supported by the Department of Energy Award Number Award No. DE-FE31819
- DoE-HQ: Regis Conrad, Robert Schrecengost

- NETL: Briggs White, Michael Fasouletus, Anthony Zinn
- All Collaborators and Team Members









Disclaimer

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.







