

# DE-FE0031911 Annual Review

Advanced Coating Compositions and Microstructures to Improve Uptime and Operational Flexibility in Cyclic, Low-Load Fossil Plants

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### Bottom Line Up Front



- The objective is to deliver coating technologies that increase reliability of the steam path
- According to GE utility customers, the most effective way to do this is to protect boiler tubing and turbine components
- Boiler tubing requires hot corrosion resistance, especially for biomass
  - We are developing weld overlay coatings that are cheap enough to be broadly applied and incorporate many layers of protection mechanisms
  - Computation guides phase compatibility and weldability
  - Within that window, alloys are designed based on prior work and tested in hot corrosion
- High Pressure Steam Turbine components suffer from solid particle erosion
  - We are developing Ion Plasma Deposited coatings with maximized lifetime by increasing erosion resistance and increasing the maximum viable coating thickness
  - Initial results suggest that lifetime can be doubled compared to conventional coatings

# **Challenges and Opportunities**



#### **Problem Statement**





Hot corrosion leads to outages

Challenge is growing as combustion temperatures increase, fuels diversify Existing solutions are too costly to apply over a wide area Damage to Boiler Tubing:



Damage to HP Turbine Blades:



- Blade erosion leads to outages
- Challenge is growing with load following, inlet steam conditions
- Existing solutions are too weak to be effective or cause aerodynamic debit

#### Reliability at lower cost is needed by the current supply chain

### Objectives

- Enable a 25%-50% increase in time between scheduled outages for both boilers and HP turbines
- Eliminate or significantly reduce the Ni content in weld overlay to reduce material cost by at least 30%
- Provide adequate oxidation and erosion resistance for HP turbine inlet steam at >620 °C and >220 bar
- Apply coatings to actual components, using today's production-scale methods





#### Provide cost-effective, drop in coating solutions with smarter compositions

### Project timeline



#### Phase 1: Proof of Concept

#### **Develop Coating Compositions**

- Test for compatibility with service environment and manufacturing process
- Minimize wastage rate for weld overlay compositions
- Minimize solid particle erosion rate for Layered Ion Plasma Deposited (LIPD) compositions

#### **Phase 2:** Scale-up

#### **Develop Coating Methods**

- Ensure that composition of interest can be reliably and uniformly deposited on parts
- Vendor produces weld overlay on ferritic and austenitic tubing
- LIPD composition is deposited on HP Turbine blades

#### **Phase 3:** Evaluation

#### **Demonstrate Performance**

- Coated components are tested under field simulative conditions
- Weld overlaid tubing is mechanically tested in lab; corrosion tested in boiler
- LIPD-coated HP Turbine blades are evaluated with post-steam leading edge erosion testing



# Steam Turbine Coatings for Erosion Resistance



#### What we know about Erosion Protection for HP Turbines

Attack mechanism

 Spalled, oxidized material from cycling travels along steam path and enters HP turbine

Prior Work

- Requires redesign or protective barrier
- 250 micron thick Diamond Tuff<sup>™</sup> is protective, but heavy and not aerodynamic
- 3 10 micron thick IPD TiN is conformal, but does not provide adequate protection
- GE has developed IPD coatings with 4.5x the erosion resistance of TiN
- Cr layers provide oxidation resistance

Our Strategy

- Apply the most erosion resistant coating that is compatible with blade material
- Interlayer with Cr if additional steam oxidation resistance is needed Cr map:





## Phase 1 Roadmap for Steam Turbine Coatings



## Sample production with Ion Plasma PVD

- Gen 1: 12 Cr/Ceramic layered architectures were produced
- Gen 2: 30 additional ceramic compositions were produced



## Prototyping with Sputtering

- Slower but more modular form of Physical Vapor Deposition
- Used to optimize ceramic compositions
- Up to 6 elements can be combined
- Allowed us to explore the effect of various dopants









### **Erosion and Steam Testing**

- 100 hour, 600 °C steam exposure
- Erosion testing before and after
- Surface Roughness measured before and after
- 36/42 IPD compositions have been erosion tested in as-deposited condition
- 20 IPD compositions have been steam tested (2 compositions per week, 2 samples per composition)





### Gen 1 erosion results

- Wide range of layer thicknesses produced
- There is an optimized layer thickness for presteam erosion resistance
- Steam oxidation resistance effects TBD

**Gen 1 Coatings Erosion Performance** 



Sample Microstructures:











### Gen 2 erosion results

- Coating life ≈ Thickness x Erosion Resistance
  - 250 micron DiamondTuff is the baseline
  - TiN is limited to ~10 microns
- Increasing Thickness
  - With proper dopants, TiN can be deposited up to 30 microns thick.
  - Result: 1.3x coating life as DiamondTuff
- Increasing Erosion resistance
  - Novel compositions outperform TiN
  - Result: 2x coating life as DiamondTuff for only 10 microns of coating

**Gen 2 Coatings Erosion Performance** 

Resista Erosion "Ceramic C" Highlighted in Proposal **TiN Received from Vendor** DiamondTuff



## Ongoing work for IPD coatings

- (e)
- Further optimizing TiN dopants to maximize achievable deposition thickness
- Further exploring novel ceramic compositions to maximize erosion resistance
- Evaluating the performance of Gen 1 and Gen 2 components after steam exposure
  - If needed, interlayer Cr with erosion resistant ceramic.
- Scaleup (2022 effort)
  - Option A: Work with vendor to replicate their process for coating components at GE
  - Option B: Transfer coating "recipe" to vendor for them to coat components

# Boiler Tube Coatings for Hot Corrosion Resistance



#### What we know about Hot Corrosion Protection for Boilers

#### Attack mechanisms

- Oxidation
- Sulfate attack
- Alkali Chlorides (cofiring waste/biomass)

#### Prior Work

- Superheater tubes can be fabricated from high Cr Austenitic Steels (*e.g.* 310 HCbN) or weld overlaid with NiCr (*e.g.* alloy 72)
- Too expensive for widespread use
- Inadequate for high temperature cofiring DE-FE0031911

Our Strategy

- Reduce Ni content to minimize cost
- Move beyond simple Chromia protection



### Phase 1 Roadmap for Boiler Tubing







• We are targeting a single phase solid solution



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- Ni content should be  $\leq$  35%





- We are targeting a single phase solid solution
- Ni content should be  $\leq$  35%
- Cr should be maximized

...Two areas of interest are identified, guiding the Fe, Ni, and Cr content of alloys





## Computational weldability testing

• Compositions were further screened using a physics-based weldability simulation.



Fig. 12 — T- $(f_s)^{1/2}$  curves showing liquid/grain interfaces, liquid channels and tangents to curves at locations of maximum steepness. A — 2219 Al alloy; B — 6061 Al alloy. A longer, narrower channel hinders liquid feeding because of the resistance to flow caused by the viscosity of liquid.

TENNESSEE



Kou, 2015

#### Lessons learned from Prior Work

- 2007-2014 Babcock/Wilcox study: Example of DOE-funded research used as a basis for • alloy design.
- Corrosion data for 12 different alloys across 8 different coal-fired environments were • evaluated.
  - Data analysis reveals beneficial alloying elements. ΚY Mahoning Indiana Wastage [mils/year] HCI=.01% Cr content [wt. %] Pitt PRB Buelah Zap Gatling HCI<.01% Duplex Austenitic NiCr SO<sub>2</sub>>.20% <u>~ our tests</u> .10% < SO<sub>2</sub> < .20% SO<sub>2</sub><.05% .05% < SO<sub>2</sub> < .10%





(ee 86

HCI=.02%

~Biomass

Illinios

#### Hot corrosion test setup



- 700 °C
- 150 hrs to 500 hrs
- Synthetic ash based on Powder River Basin Coal
- Metal loss is measured after testing



1 sample @ 350 hr
2 samples @ 500 hr





3-zone furnace

#### **Initial Results**



- First round of samples have completed 150 hours and will be characterized
- Selected from a broad compositional spectrum: ferritic steel, austenitic steel, NiCr, CoCr
- Drawing knowledge from many branches of alloy development
- Probing a wide range of performance to establish sensitivity of test



Sample	Alloy Type	Observations
B-1	Ni (EI-2019)	Dull(er) surface, dark gray oxide
C-1	Fe (EI-2019)	Red oxides, ash sticking more
		than in other samples
D-1	APMT	Shinny surface, red-ish oxides
E-1	625+	Dark gray oxide
F-1	SS310	Dark oxide, gas side has a little
		red tint, in ash has a bit of
		blue/greenish tint
G-1	UMCO50	Greenish oxides on the top (gas
		part), in the ash, several large
		dark blotches

## Ongoing work for weld overlay coatings

- Corrosion screening of Gen 1 alloys is underway
- Gen 2 alloys are being cast
- Weldability trials of most promising candidates will begin in August
- Gen 3 alloy selection will be based on Gen 1 and Gen 2 results



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# **Backup Slides**



Testing

#### **Boiler Coatings**



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May 26, 2021 31

Tuble 1. Composition of maxed gas in volume 70.	Table 1:	Composition of	f mixed	gas in v	olume %.
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$N_2$	CO <sub>2</sub>	O <sub>2</sub>	$SO_2$	H <sub>2</sub> O
Balance	15	2.5	0.2	10

 Table 2: Composition of synthetic ash used in corrosion test (weight %)

Na <sub>2</sub> O	Fe <sub>2</sub> O <sub>3</sub>	Al <sub>2</sub> O <sub>3</sub>	SiO <sub>2</sub>	CaO	MgO	K <sub>2</sub> O	TiO <sub>2</sub>	<b>P</b> <sub>2</sub> <b>O</b> <sub>5</sub>	CaSO <sub>4</sub>	NaSO <sub>4</sub>	KSO <sub>4</sub>
2.2	5.9	16.3	29.1	23.8	5.2	0.3	1.3	0.9	5	5	5

