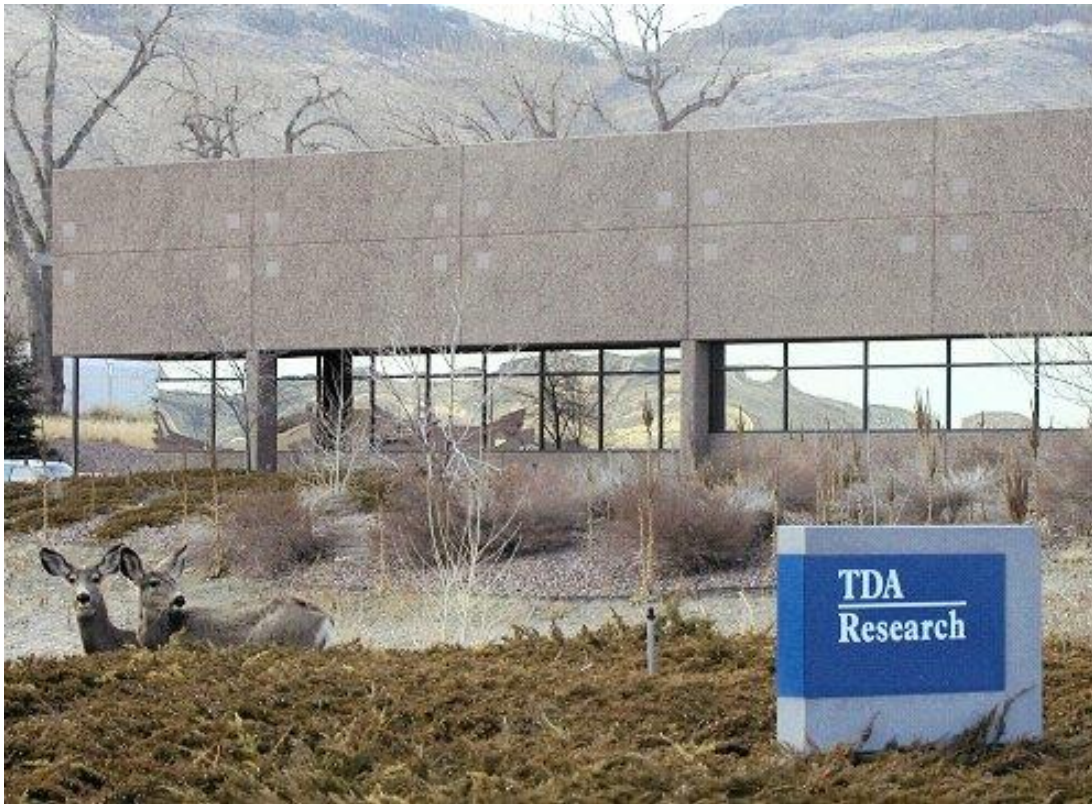


# **Integrated Water-Gas-Shift Pre-Combustion Carbon Capture Process (Contract No. DE-FE0023684)**



**Gökhan Alptekin, PhD  
TDA Research, Inc.  
Wheat Ridge, CO  
galptekin@tda.com**

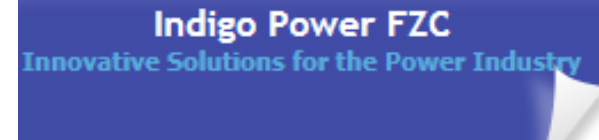
**2020 Gasification Systems  
Project Review**

**May 5, 2021**

# Project Objectives

- **The project objective is to demonstrate techno-economic viability of an integrated WGS catalyst/CO<sub>2</sub> removal system for IGCC power plants and CTL plants**
  - A high temperature PSA adsorbent is used for CO<sub>2</sub> removal above the dew point of the synthesis gas
  - A commercial low temperature catalyst is used for water-gas-shift
  - An effective heat management system is developed
- **Project Tasks**
  - Design a fully-equipped slipstream test unit with 10 SCFM raw synthesis gas treatment capacity
  - Design and fabricate CFD optimized reactors capable of managing the WGS exotherm while maintaining energy efficiency
  - Demonstrate critical design parameters including sorbent capacity, CO<sub>2</sub> removal efficiency, extent of WGS conversion as well as H<sub>2</sub> recovery using coal synthesis gas
  - Complete a high fidelity process design and economic analysis

# Project Partners



## Project Duration

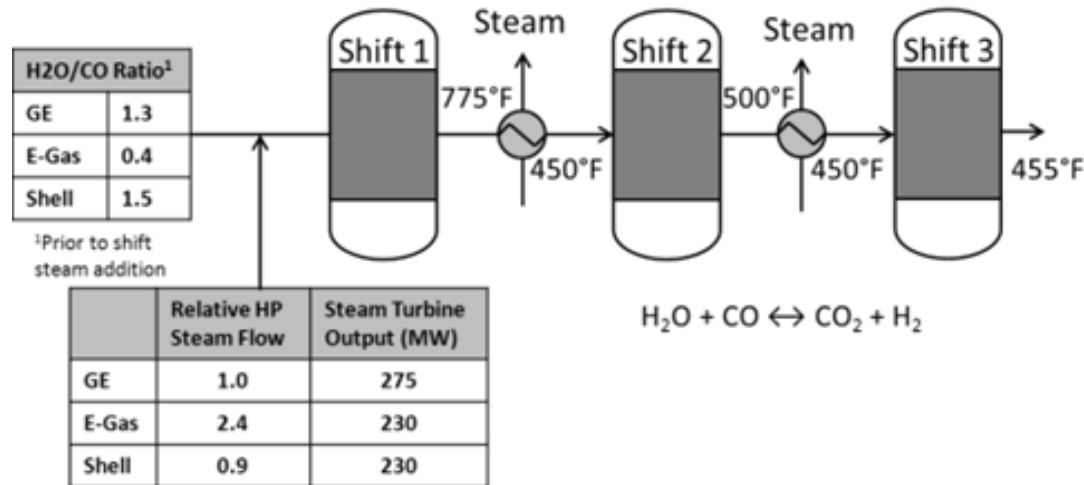
- Start Date = October 1, 2014
- End Date = September 30, 2021

## Budget

- Project Cost = \$5,632,619
- DOE Share = \$4,506,719
- TDA and its partners = \$1,125,900

# TDA's Approach

- Conventional IGCC plants use multi-stage WGS with inter-stage cooling
  - WGS is an equilibrium-limited exothermic reaction
- Water is supplied at concentrations well above required by the reaction stoichiometry to completely shift the CO to CO<sub>2</sub>

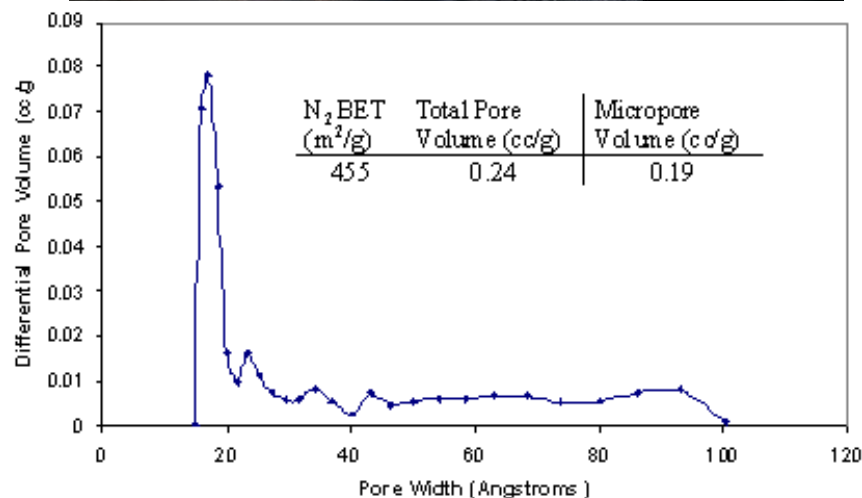


**3-stage WGS unit as described in the DOE/NETL-2007/1281**

- In our process, the WGS catalyst is combined with a high temperature CO<sub>2</sub> adsorbent to achieve high CO conversion at low steam:carbon ratios
- Reduced water addition increases process efficiency

# TDA's Sorbent

- TDA's uses a mesoporous carbon with surface functional groups that remove CO<sub>2</sub> via strong physical adsorption
  - CO<sub>2</sub>-surface interaction is strong enough to allow operation at elevated temperatures
  - Because CO<sub>2</sub> is not bonded via a covalent bond, energy input for regeneration is low
- Heat of CO<sub>2</sub> adsorption is **4.9 kcal/mol** for TDA sorbent
  - Net energy loss in sorbent regeneration is similar to Selexol; much higher IGCC efficiency can be achieved due to high temperature CO<sub>2</sub> capture
- Favorable material properties
  - Pore size is tuned to 10 to 100 Å
  - Mesopores eliminates diffusion limitations

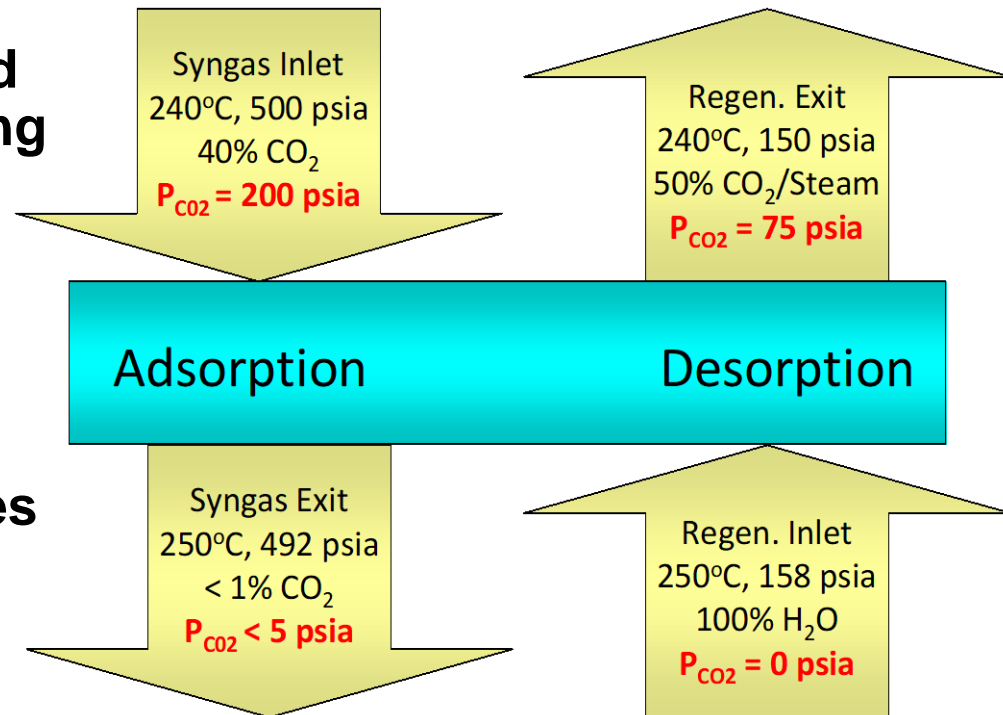


US Patent 9,120,079, Dietz, Alptekin, Jayaraman "High Capacity Carbon Dioxide Sorbent", US 6,297,293; 6,737,445; 7,167,354  
US Pat. Appl. 61790193, Alptekin, Jayaraman, Copeland "Pre-combustion CO<sub>2</sub> Capture System Using a Regenerable Sorbent"



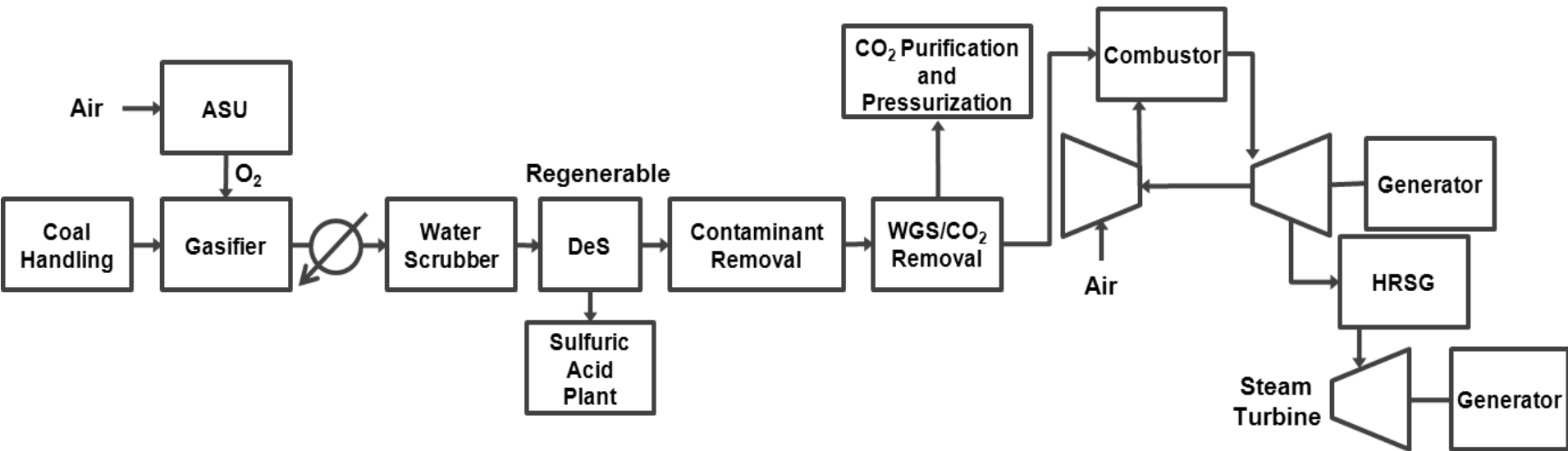
# Operating Conditions

- **CO<sub>2</sub> is recovered via combined pressure & concentration swing**
  - CO<sub>2</sub> recovery at ~150 psia reduces energy need for CO<sub>2</sub> compression
  - Small steam purge ensures high product purity
- **Isothermal operation eliminates heat/cool transitions**
  - Rapid cycles reduces cycle time and increases sorbent utilization
- **Similar PSA systems are used in commercial H<sub>2</sub> plants and air separation plants**
- **The WGS catalyst was subjected to the same cycle**



Source: Honeywell/UOP

# Integrated WGS/CO<sub>2</sub> Capture System

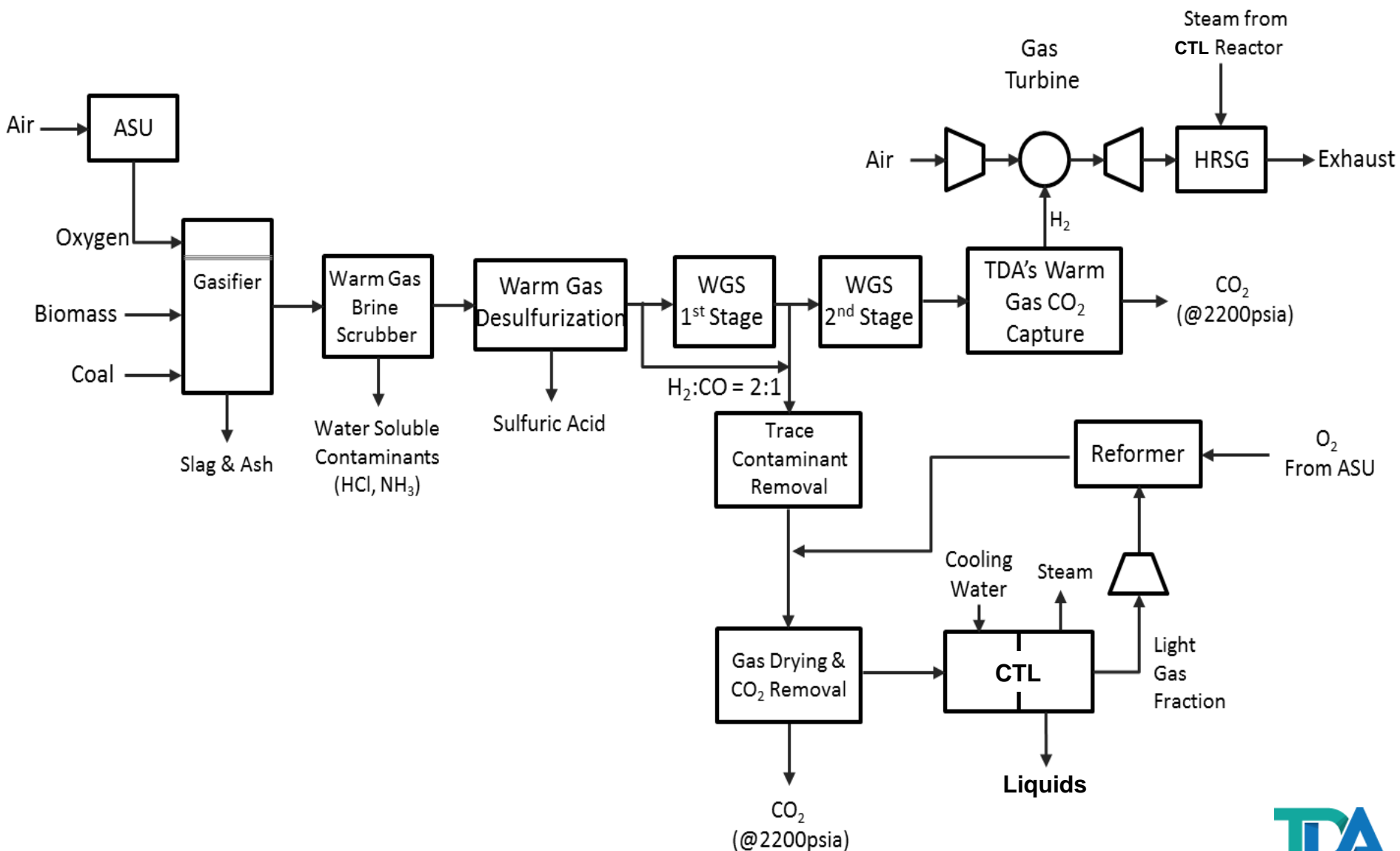


- **Reducing the use of excess steam improves power cycle efficiency**
  - Lower energy consumption to raise the steam
- **Process intensification could potentially reduce the number of hardware components and cost**

## Sorbent's point of view:

- **Less dilution with water increases CO<sub>2</sub> partial pressure and in turn improves sorbent's working capacity**

# Application of the Technology to CTL





# Sorbent Development Work



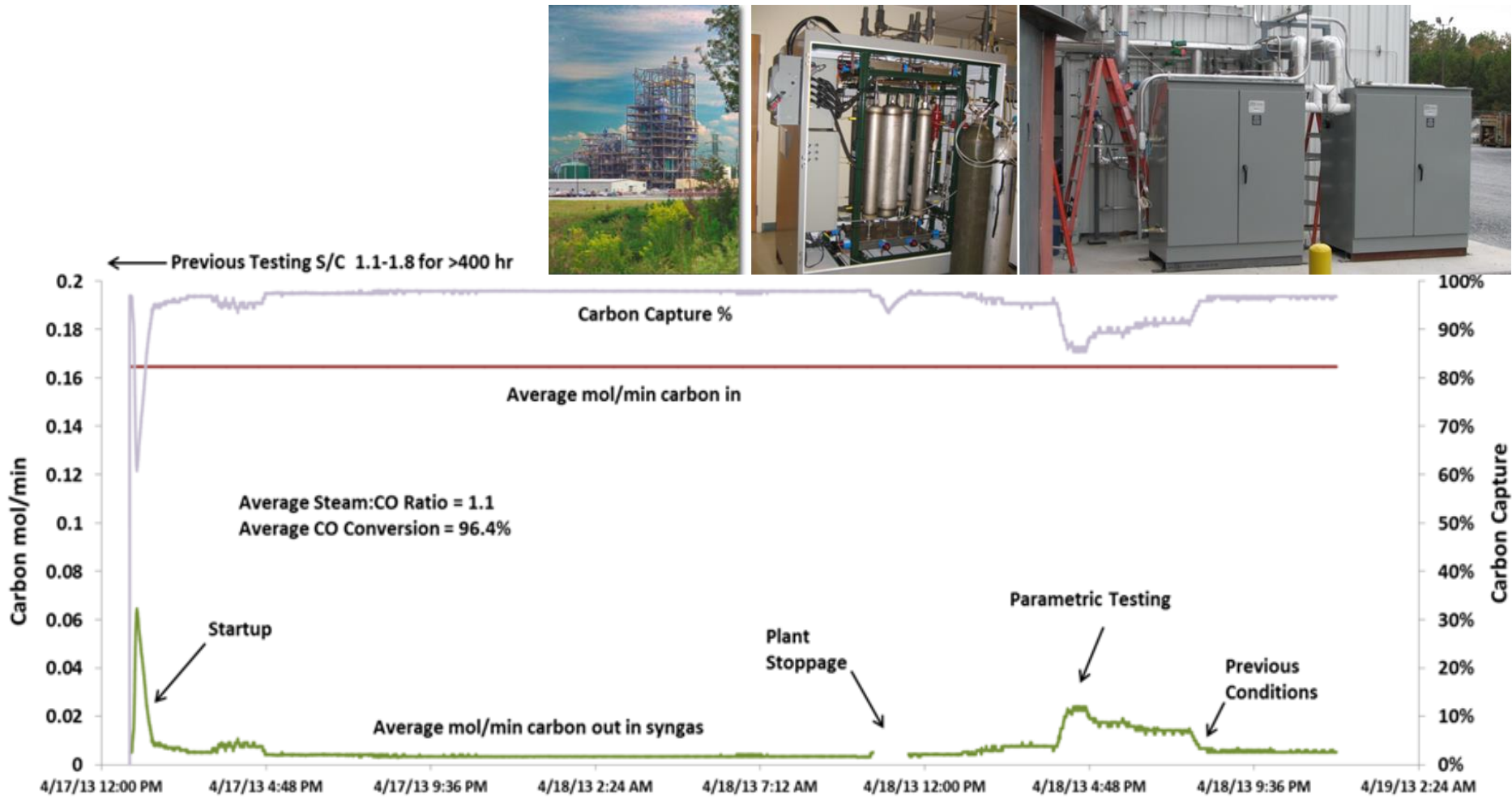
*TDA 0.1 MW pre-combustion carbon capture unit installed at the National Carbon Capture Center*

- **0.1 MW<sub>e</sub> test in a world class IGCC plant to demonstrate full benefits of the technology**
  - Field Test #1 at NCCC
  - Field Test #2 at Sinopec Yangtzi Petrochemical Plant, Nanjing, Jiangsu Province, China
- **Full operation scheme**
  - 8 reactors and all accumulators
  - Utilize product/inert gas purges
  - H<sub>2</sub> recovery/CO<sub>2</sub> purity



*Yangtzi Petro-chemical Plant*

# NCCC Field Test – Early Work



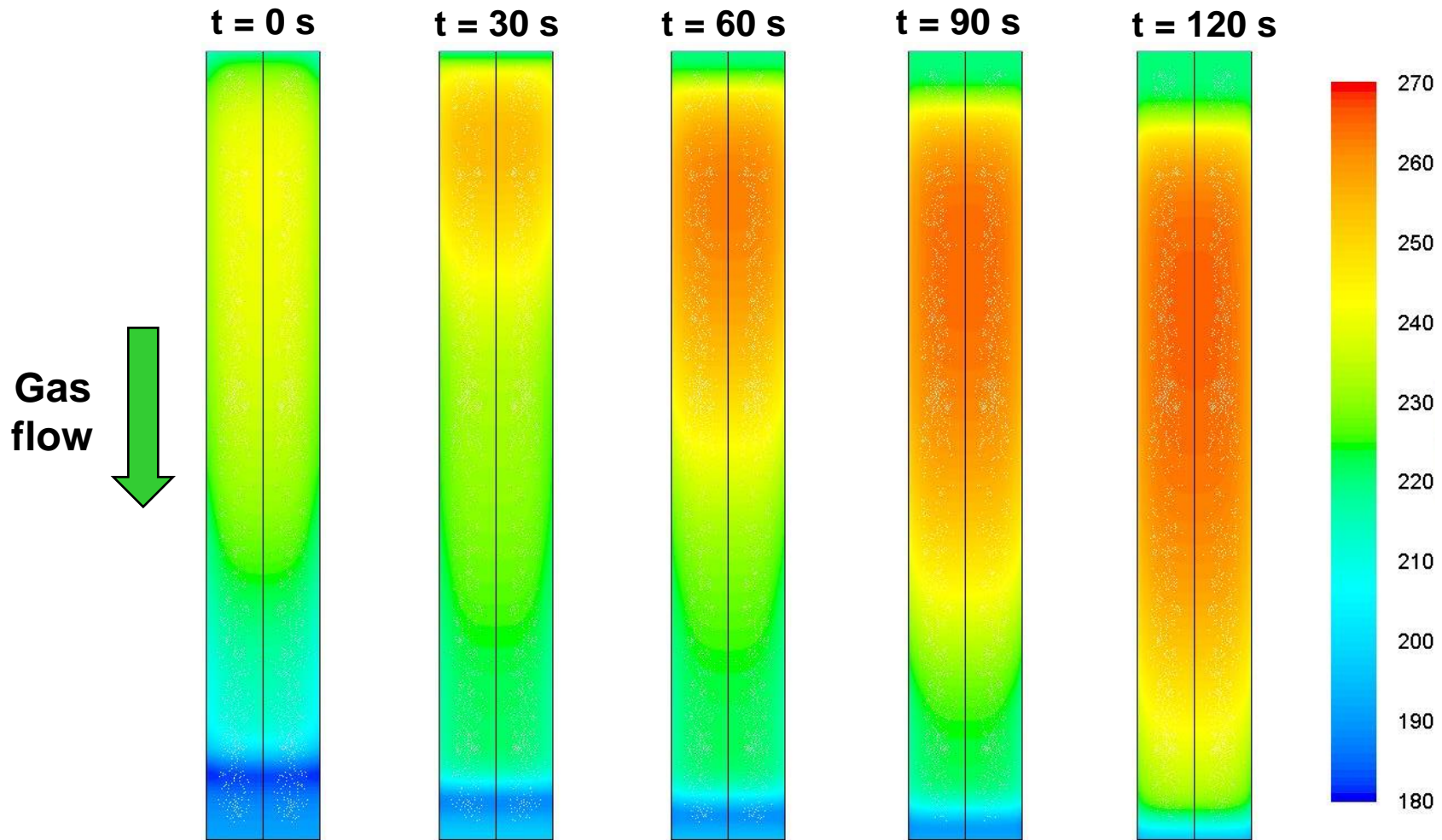
- 90+% capture at steam:CO ratio= 1:1.1 with average 96.4% CO conversion
- All objectives met (no coking etc.) but high reactor T was observed

# Technology Status/R&D Needs

- **Sorbent is developed under a separate DOE project (DE-FE0000469)**
- **WGS catalyst is commercially available mature technology**
- **Early-stage concept demonstration has already been completed (DE-FE0007966 and DE-FE0012048)**
  - Integrated sorbent/catalyst operation
  - Pointed out the need to incorporate effective heat management
  - Implemented the heat management scheme in a 4-bed PSA system using coal derived synthesis gas at 1 kg/hr CO<sub>2</sub> removal
- **Key R&D need is the design/development of a high fidelity prototype to fully demonstrate the concept using actual coal-derived synthesis gas**
  - Reactor design to address the heat management needs
  - A 10 kg/hr CO<sub>2</sub> removal is being developed
  - Testing of the high fidelity system will be carried out at Praxair

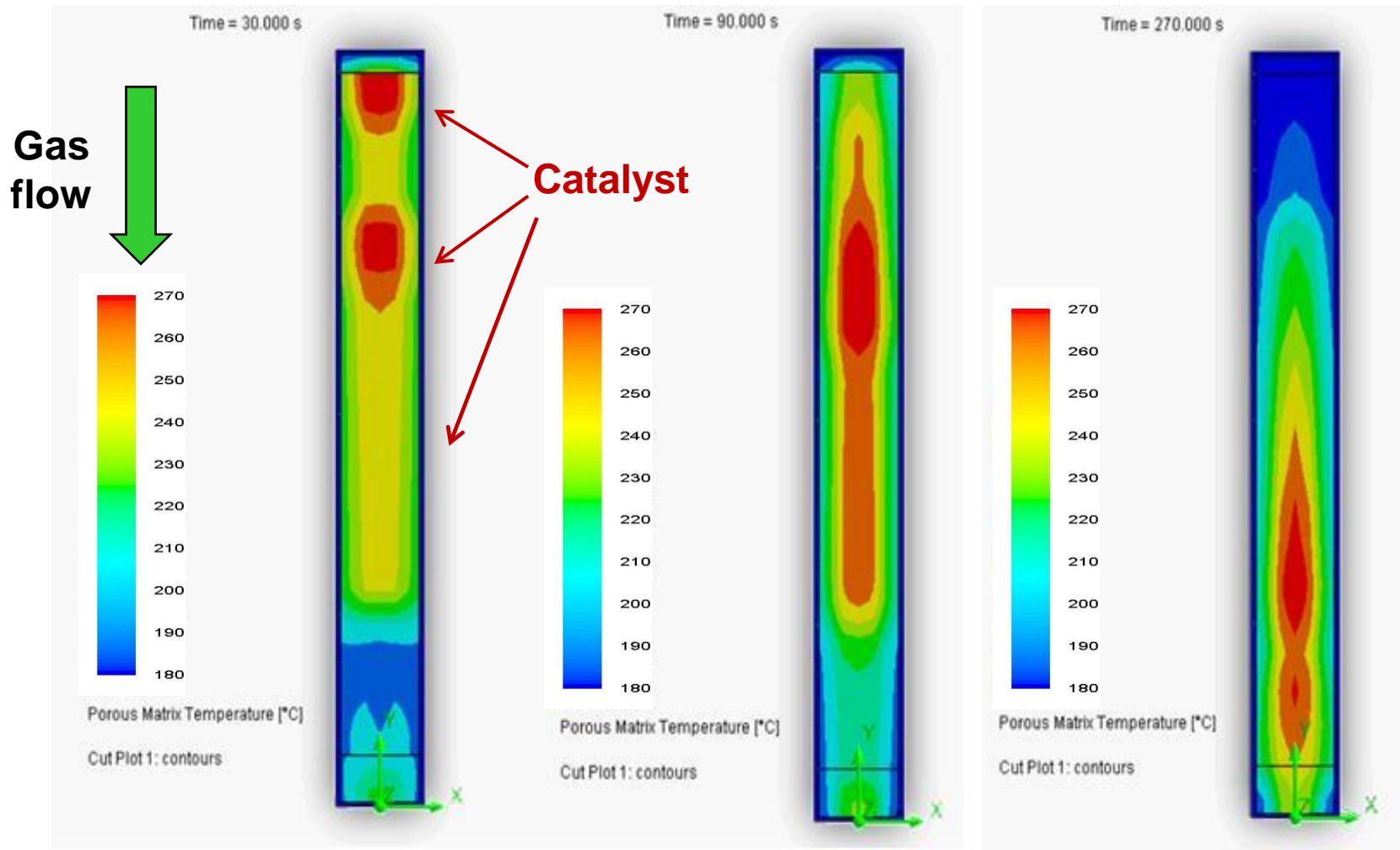


# T Profiles - During CO<sub>2</sub> Capture Only



- Heat generated during adsorption is removed during regeneration
  - Near isothermal operation through the cycle

# Heat Wave WGS & CO<sub>2</sub> Capture

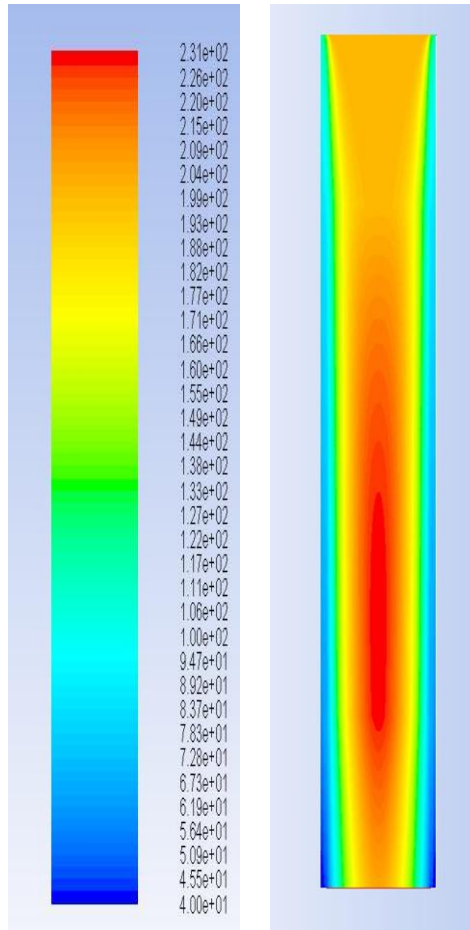


- Integrated WGS & CO<sub>2</sub> capture results in higher  $\Delta T$
- Not ideal for CO<sub>2</sub> capture (the WGS heat accumulates in the beds)

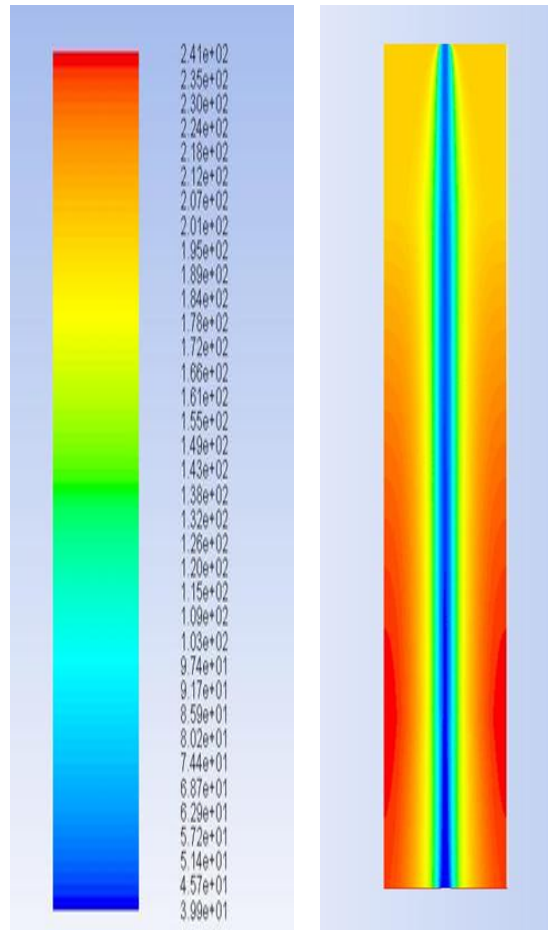
# Conventional Heat Management Options

## 10 kg/hr CO<sub>2</sub> Removal Pilot Test System – 6" reactors

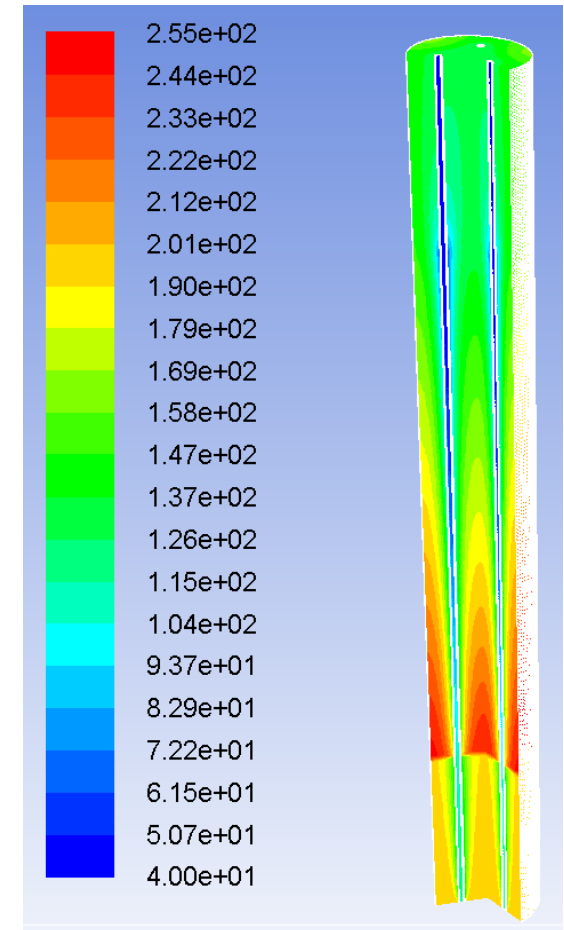
### Cooling Jacket



### Immersed Tube (1)



### Immersed Tubes (3)

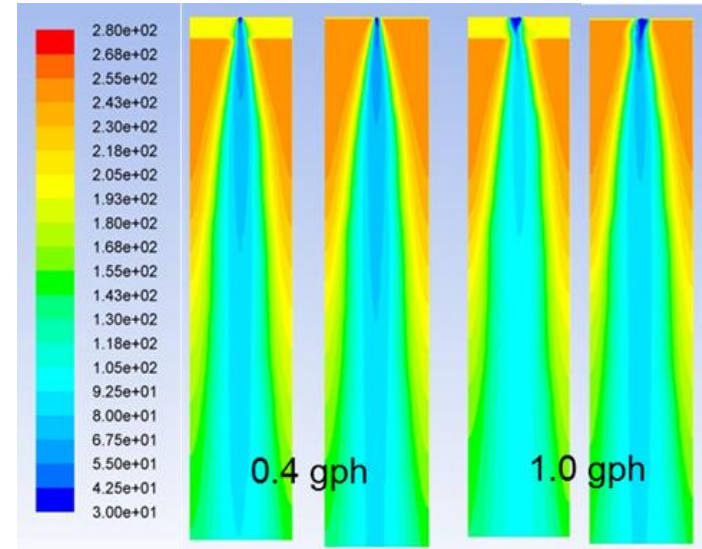




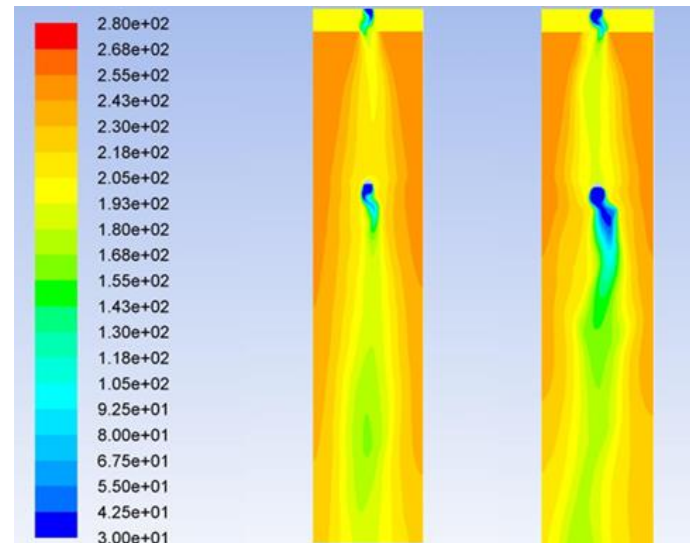
# Heat Integrated WGS & CO<sub>2</sub> Capture

- **Advanced heat management concept based on direct water injection has proven to achieve much better temperature control**
  - Also much better heating efficiency (i.e., kJ heat removed per kg water)
- **Objective is to achieve a more uniform cooling without having hot or cold spots**
- **The temperature rise is optimal when the catalyst is distributed into two layers with water injections before each layer**

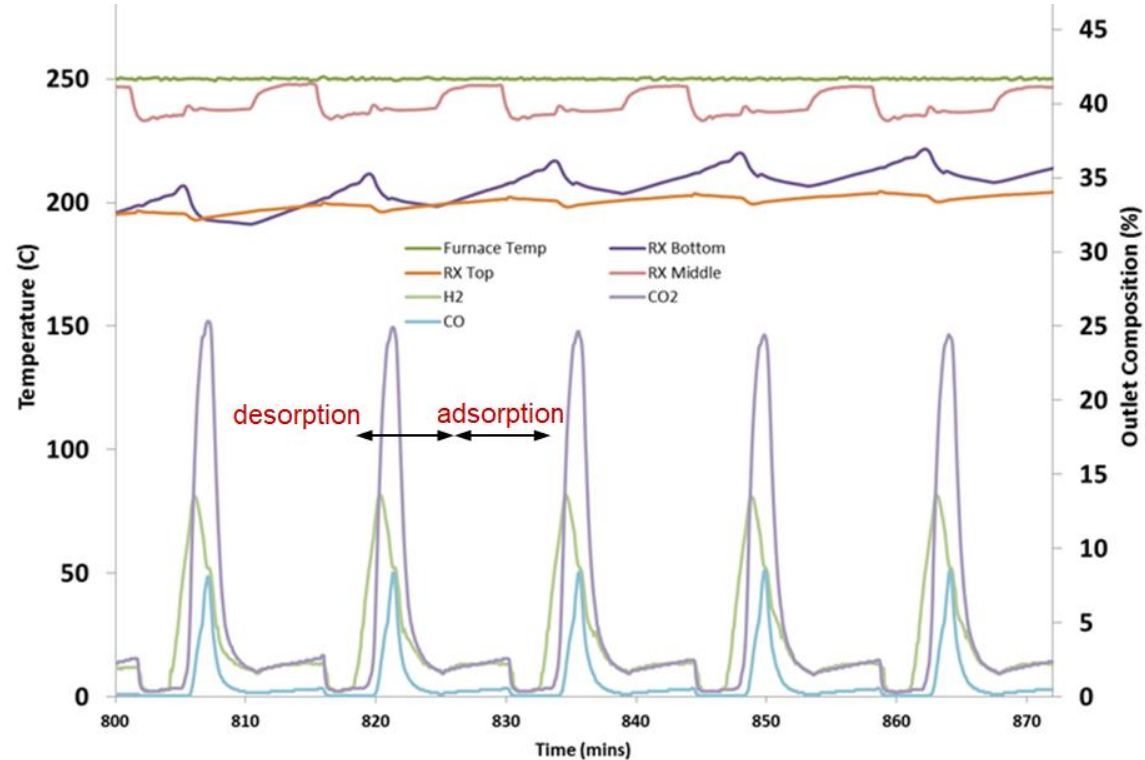
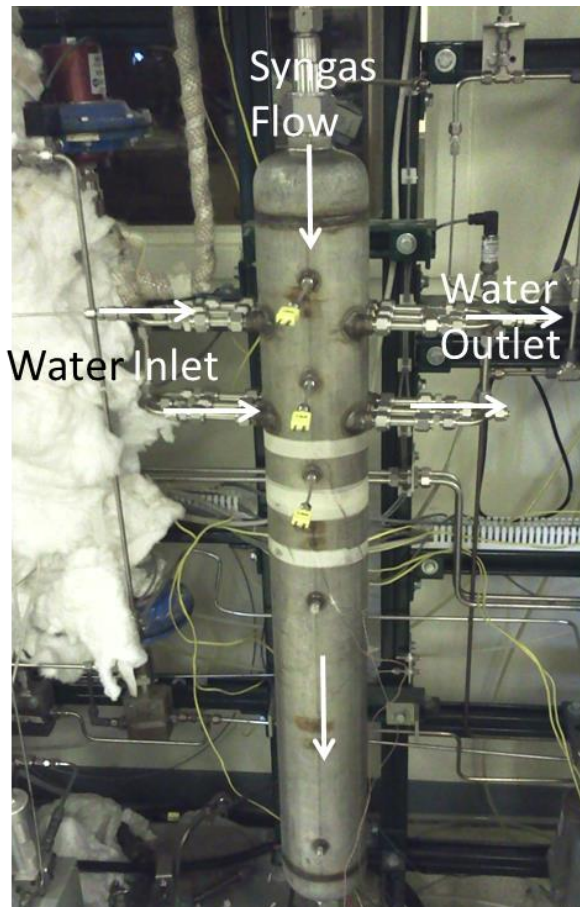
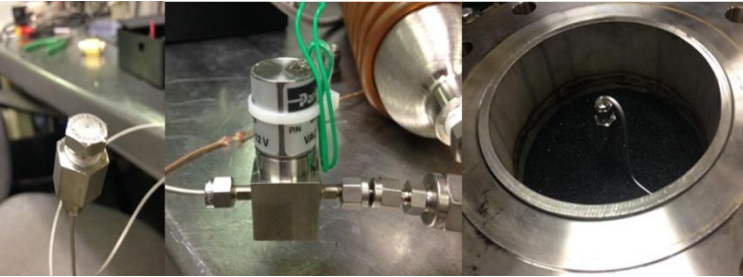
**T Contours (°C) Single Injection Layer**



**T Contours (°C) Multiple Injection Layers**

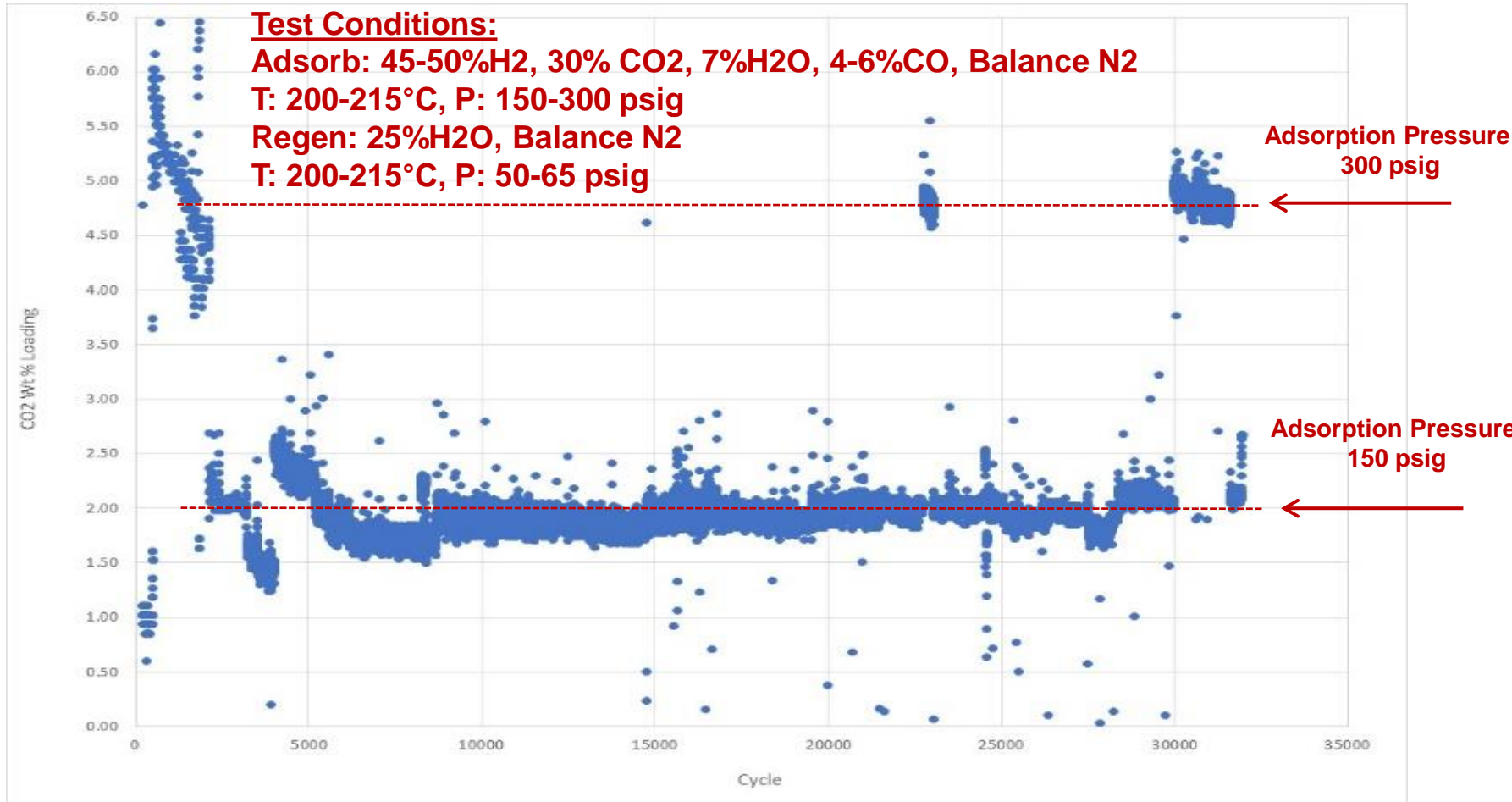


# Bench-Scale Evaluations



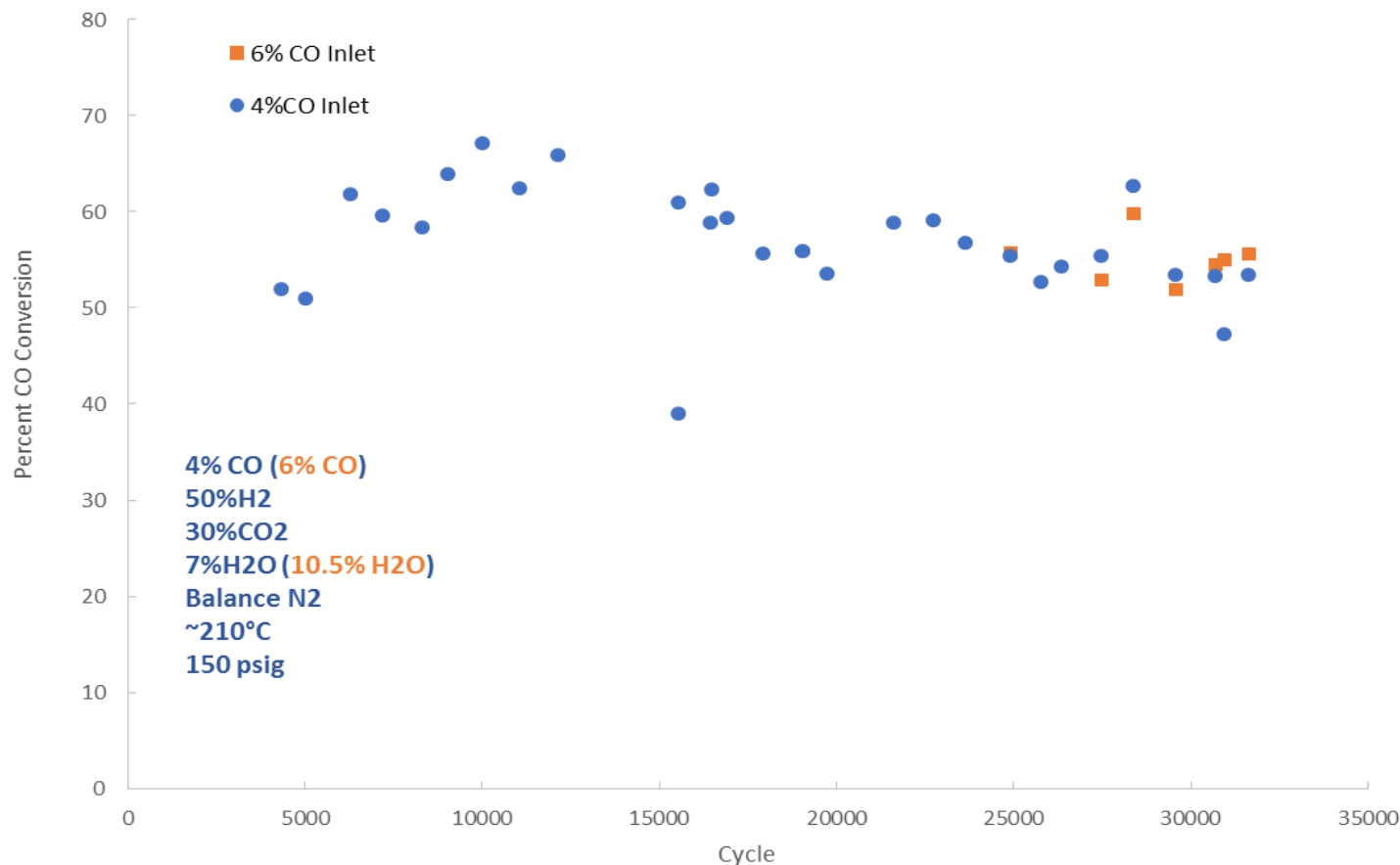
- 8L reactors were modified with water injectors
- Successful proof-of-concept demonstrations have been completed
- $\Delta T < 10^\circ\text{C}$  was maintained over extended cycling (much lower than those in early field tests)

# Life Tests – Sorbent Activity



- We completed 32,000 cycles showing stable performance for the WGS catalyst and CO<sub>2</sub> sorbent

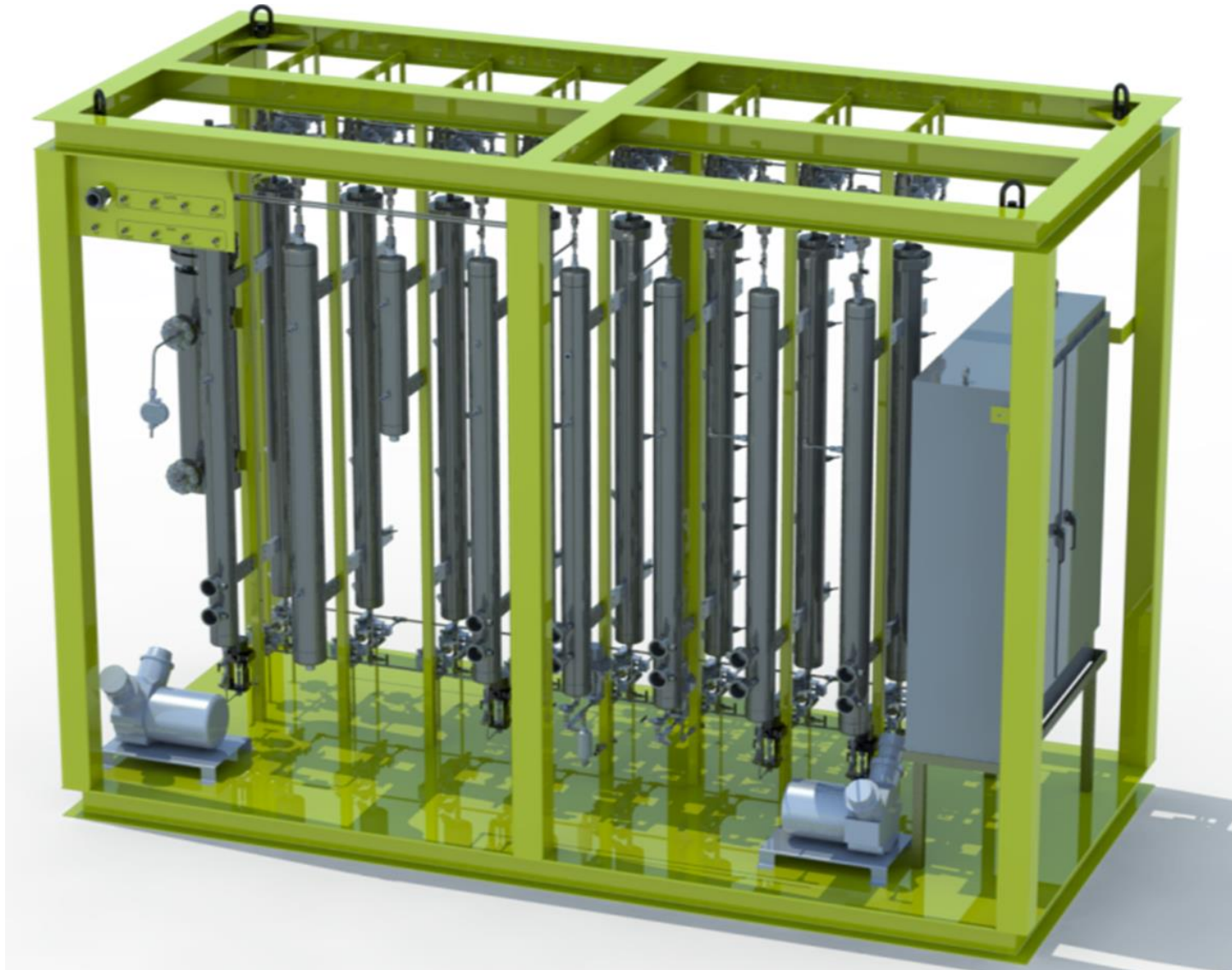
# Life Tests – Catalyst Activity



- By evaluating continuous catalytic activity (alone) we showed that cycling between reducing and oxidizing conditions (i.e., steam exposure) had no adverse effect on the WGS catalyst



# Integrated WGS/CO<sub>2</sub> Capture System



# Fabrication of the Prototype

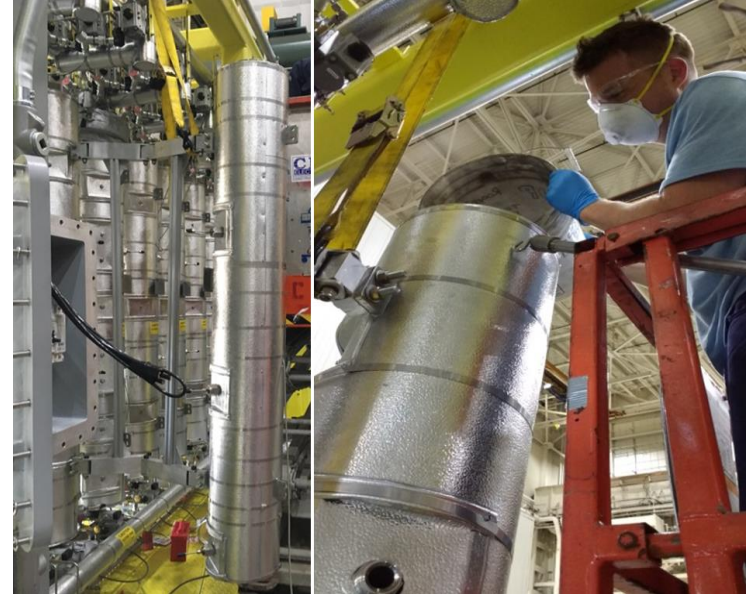




# Installation at Praxair

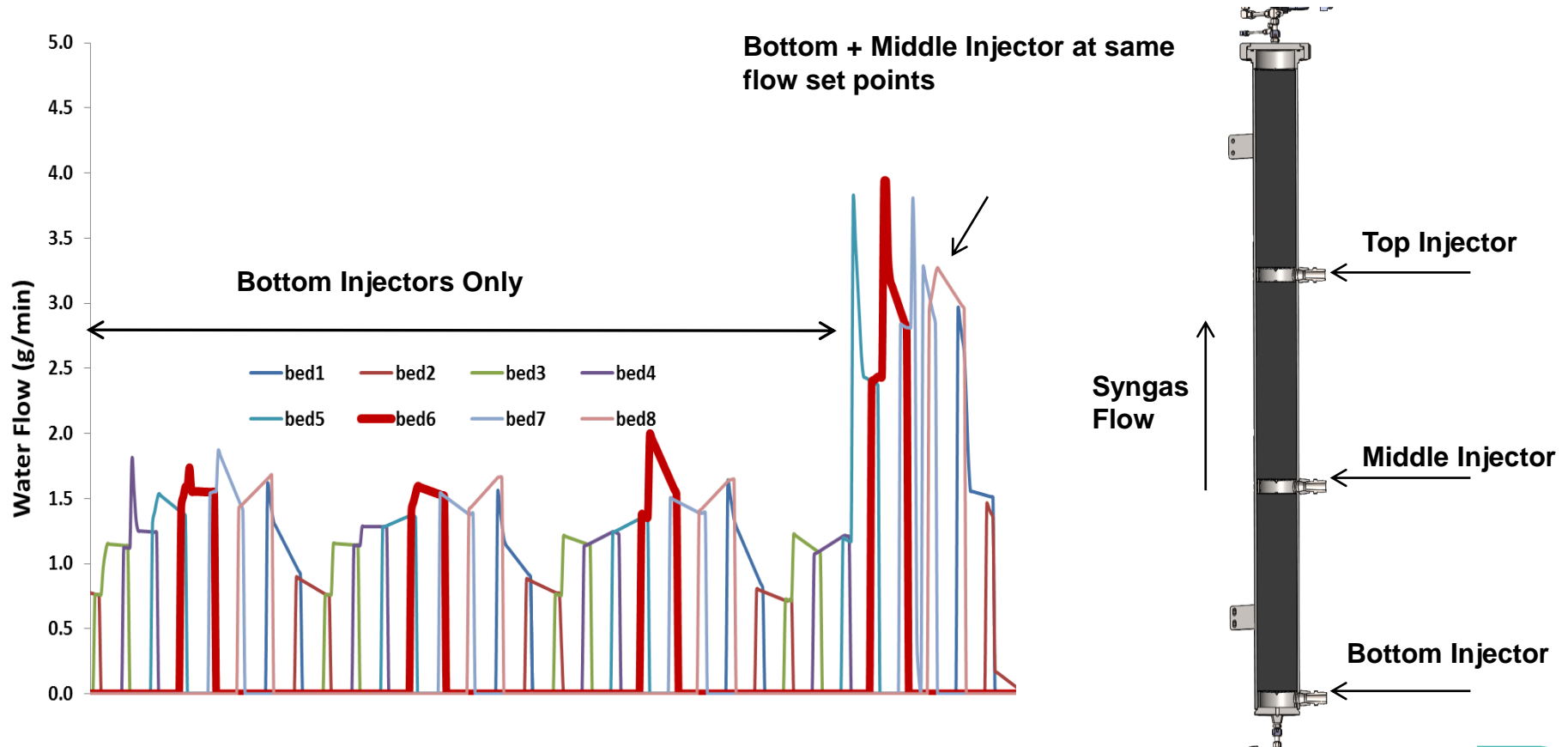


- Fabrication of the Prototype unit was completed in 2018 Q2 and installation at Praxair R&D Center (Tonawanda, NY) was completed in 2018 Q3
- First campaign is completed in Q2 2019



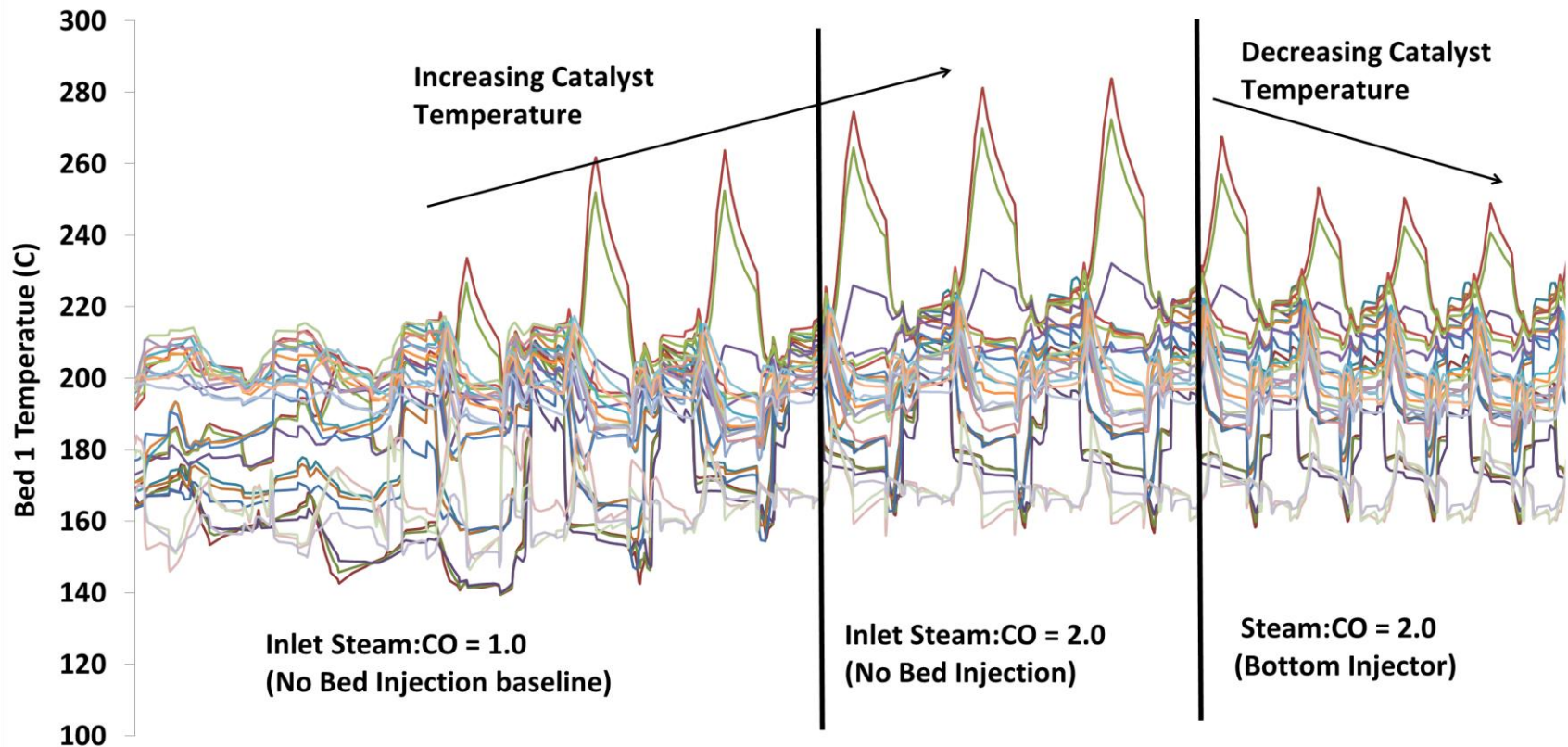
# Control of Water Injection

- We demonstrated that precise amounts of water can be injected and their individual flow rates can be controlled within tolerances of less than 0.5 g/min between injectors



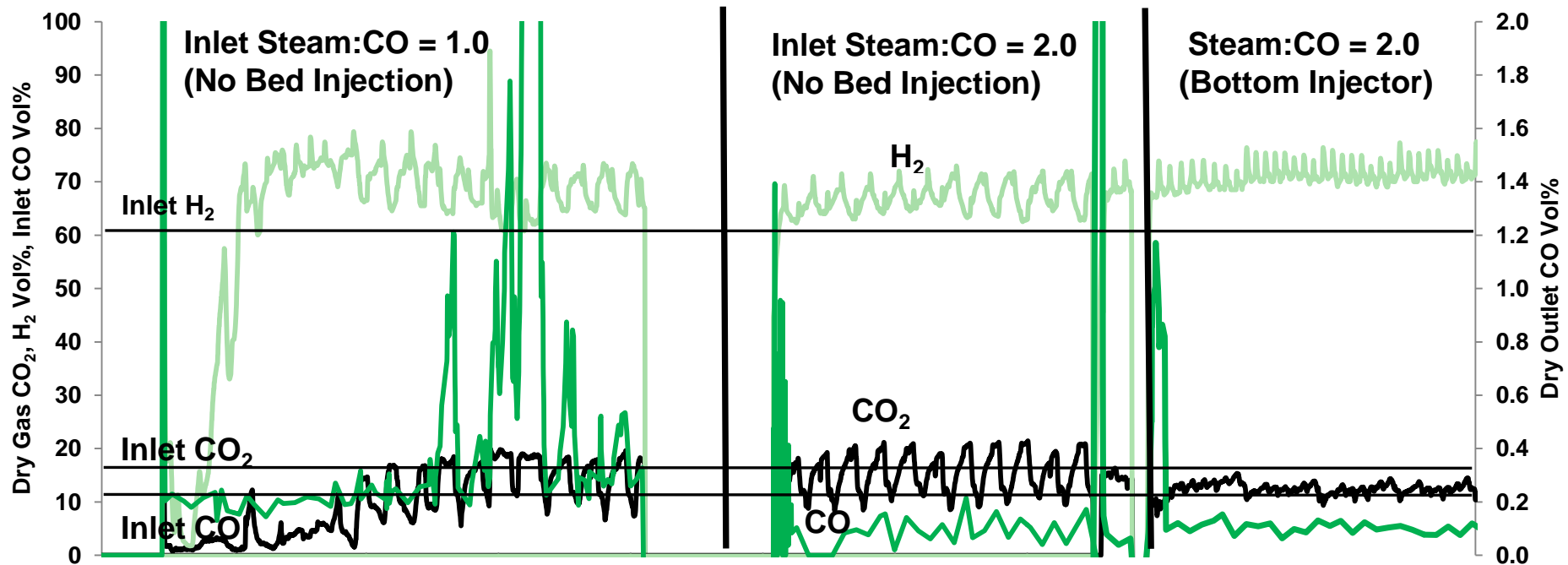
# Temperature Management via Water Injection

- We observed an increase in bed temperature by increasing the inlet steam:CO from 1 to 2
- Bed temperature was maintained at  $\sim 40^{\circ}\text{C}$  lower when injecting the same amount water directly into the beds



# Impact of Water Injection

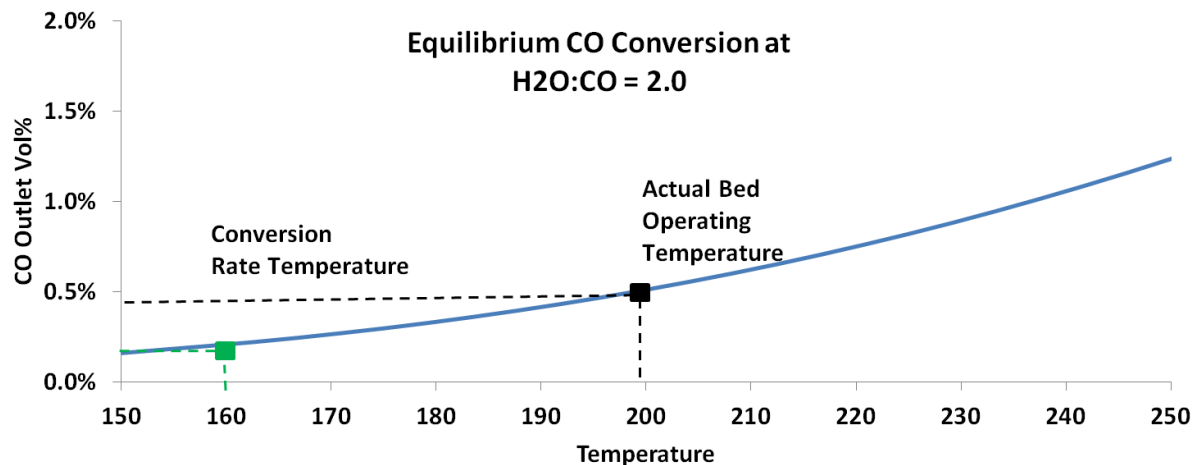
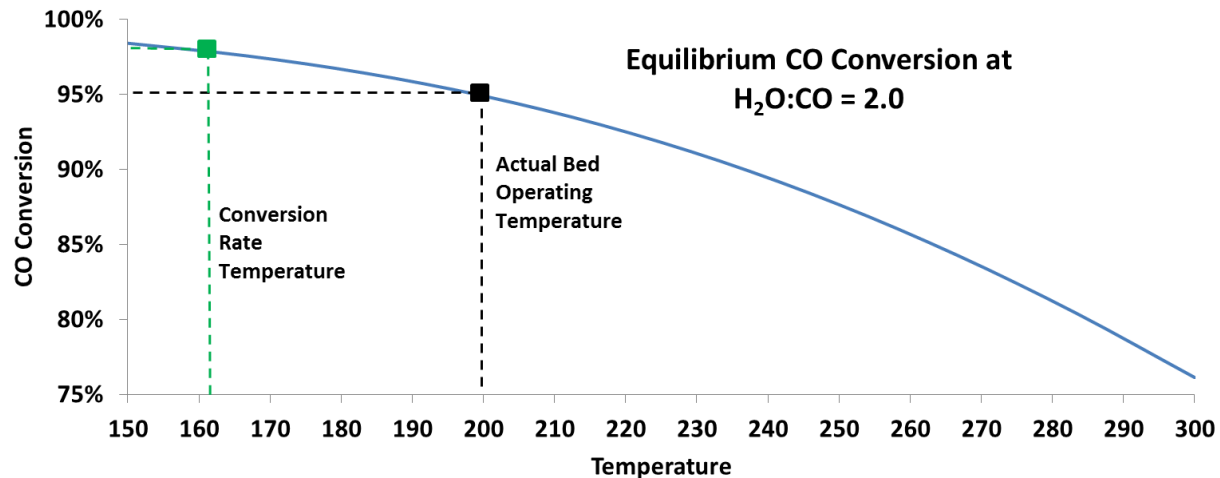
- An overall CO conversion >98% was achieved
- Cycle times were not yet optimized in this run therefore carbon capture was only at 60% (incoming CO<sub>2</sub> + CO<sub>2</sub> from shifted CO<sub>2</sub>)
- Optimization was planned for the test scheduled for the next campaign





# Effect on Equilibrium Conversion

- By coupling the WGS with the CO<sub>2</sub> sorbent and water injection, we were able to operate the beds at 200°C but achieve the equilibrium CO conversion of a 40°C cooler bed



# Integration with E-Gas™ Gasifier

| Gasifier Type/Make                         | E-Gas                        |   |   |
|--|------------------------------|---|---|
| Case                                       | 1                            | 2   | 2* (WGS/CO <sub>2</sub> )                         |
| CO <sub>2</sub> Capture Technology         | Cold Gas Cleanup<br>Selexol™ | Warm Gas Cleanup<br>TDA's CO <sub>2</sub> Sorbent | Warm Gas Cleanup<br>TDA's CO <sub>2</sub> Sorbent |
| CO <sub>2</sub> Capture, %                 | 90                           | 90  | 90  |
| Gross Power Generated, kW                  | 710,789                      | 670,056   | 693,542   |
| Gas Turbine Power                          | 464,000                      | 425,605   | 427,980   |
| Steam Turbine Power                        | 246,789                      | 244,450   | 265,562   |
| Syngas Expander Power                      | -                            | -   | -   |
| Auxiliary Load, kW                         | 194,473                      | 124,138   | 138,741   |
| Net Power, kW                              | 516,316                      | 545,917   | 554,801   |
| Net Plant Efficiency, % HHV                | 31.0                         | 34.1  | 34.7  |
| Coal Feed Rate, kg/h                       | 220,549                      | 212,265   | 212,265   |
| Raw Water Usage, GPM/MW                    | 10.9                         | 10.3  | 10.0  |
| Total Plant Cost, \$/kW                    | 3,464                        | 3,042   | 2,990   |
| COE without CO <sub>2</sub> TS&M, \$/MWh   | 136.8                        | 120.5   | 118.8   |
| COE with CO <sub>2</sub> TS&M, \$/MWh      | 145.7                        | 128.6   | 126.7   |
| Cost of CO <sub>2</sub> Captured, \$/tonne | 53.2                         | 37.4  | 35.8  |

- IGCC plant efficiency is estimated as 34.7% with TDA's WGS/CO<sub>2</sub> system
- Cost of CO<sub>2</sub> capture is estimated as less than \$26/tonne (including TS&M less than \$35.8/tonne)



# Process Economic Analysis - CTL

|  |                            |  |
|--|----------------------------|--|
| Gasifier   | Shell                      |  |
| Coal   | Bituminous                 |  |
| Case   | 9                          | 10A  |
| CO <sub>2</sub> Capture Technology                                     | Cold Gas Cleanup Rectisol™ | Warm Gas Cleanup TDA's CO <sub>2</sub> Sorbent |
| CO <sub>2</sub> Capture, %   | 90                         | 90   |
| Gross Power Generated, kW  | 462,568                    | 458,830  |
| Gas Turbine Power  | 130,283                    | 130,519  |
| Steam Turbine Power  | 332,285                    | 328,311  |
| Syngas Expander Power  | -                          | -  |
| Auxiliary Load, kW   | 397,803                    | 365,956  |
| Net Power, kW  | 64,764                     | 92,875   |
| Net Plant Efficiency, % HHV  | 1.08                       | 1.55   |
| Naphtha Production rate, ST/D  | 1,803                      | 1,722  |
| Diesel Production rate, ST/D   | 4,789                      | 4,933  |
| Coal Feed Rate, kg/h   | 793,864                    | 793,864  |
| Raw Water Usage, GPM   | 14,032.6                   | 12,394.0                                       |
| Total Plant Cost, \$/kg/D  | 949.87                     | 864.94   |
| NAPHTHA  |                            |  |
| 1st year Required Selling Price (RSP) w/o CO <sub>2</sub> TS&M, \$/bbl | 107.0                      | 100.0  |
| DIESEL   |                            |  |
| 1st year Required Selling Price (RSP) w/o CO <sub>2</sub> TS&M, \$/bbl | 153.0                      | 143.0  |

- Integrated WGS with CO<sub>2</sub> capture reduced the required selling price for Naphtha to \$100 per bbl compared to \$107 per bbl for a CTL plant with Rectisol
- Integrated WGS with CO<sub>2</sub> capture reduced the required selling price for Diesel to \$143 per bbl compared to \$153 per bbl for a CTL plant with Rectisol

# Acknowledgement

---

- **NETL, Project Manager, Diane Revay Madden**
- **Chuck Shistla, GTI**
- **Sean Kelly, Juan Li, Praxair**
- **Frank Morton, NCCC**
- **Ashok Rao, UCI**

Disclaimer: "This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof."