Techno-Economic Analyses for Direct Air Capture (DAC)

Overview



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February 24, 2021



Presentation Outline



- Techno-Economic Analysis (TEA) Process
- QGESS Description/Location
- Bituminous Baseline Study Overview/Example



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Tecno-Economic Analysis Tools

Right tool for TRL level



• Low TRL Analysis

- Mass and Energy Balances
- Preliminary Spreadsheet Models Post Combustion Tool, Compression Tool
- Cost correlations

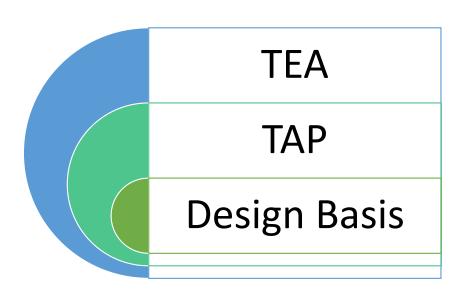
• Mid to High TRL (for NETL projects)

- Process Simulation Software
 - Aspen Plus
 - CHEMCAD
 - Thermoflow
 - Others



Steps to Performing TEA





- 1. Form a Technology Analysis Plan
- 2. Create a Performance Model
- 3. Cost Estimating BSP
- 4. Reporting Requirements



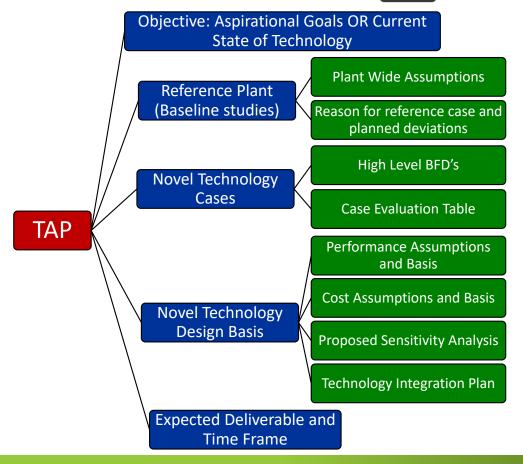
Technology Analysis Plan (TAP)

What is a TAP?

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- A TAP discusses the approach and methodology required to conduct the TEA
- Presented to stakeholders prior to starting the TEA
 - Document assumptions
 - Ensure valuable product
- Updated as the TEA is performed changes should be noted in a final document

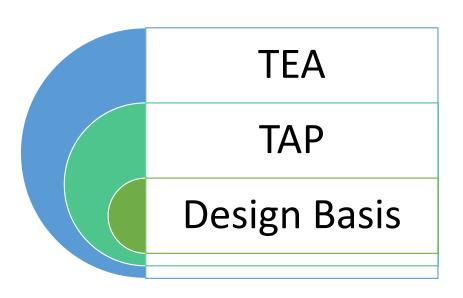
Case	Baseline	Case Study							
Case	(Reference)	Case 1	Case 2	Case 2A					
Technology Combinations									
CO ₂ Removal	Selexol	Novel Capture Tech.							
Enabling Tech.	Std. Te	Std. Tech. Enabled Tech.							
CO ₂ Purification		Yes							





Steps to Performing a TEA





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Performance Model Results for Reporting



• Build a performance model

- Frequently completed in ASPEN, CHEMCAD, Thermoflow, etc.
- When applying novel technology:
 - Balance of plant equipment NOT affected by research area will be scaled (RR)
 - Changes in operating parameters and other assumptions that are different than those QGESS must be justified in the TEA document (RR)

• Detailed Process Flow Diagram (RR)





Performance Modeling Inconsistencies



- Items that are often varied between the reference and novel cases without justification:
 - Condenser pressure
 - Steam cycle conditions (e.g. reheat temperature)
 - Combustion turbine conditions (e.g. turbine inlet temperature)
 - Cooling water temperature
 - ASU performance and oxygen quality
 - Emissions levels
 - Equipment selection

These variations without justification may require further communication or resubmission of report

Performance variations <u>NOT</u> related to the novel technology between the reference and novel cases should thoroughly explained



Performance Model Results for Reporting



- Material and Energy Balances (RR)
 - Consistent with the level of detail found in the Baseline reports. Material balance should include
 - All inputs feedstock, catalyst, limestone, etc.
 - All outputs such as stack gas, waste water, solid waste disposal
 - Stream compositions
 - Energy Balance should include
 - Thermal energy input from fuel
 - Major auxiliary loads
 - Detailed loads for new technology



Model Results

B5B (GEE Radiant Capture)

- Total power from turbines (RR)
- New auxiliary loads (RR)
- Net Power (RR)
- Heat rate, efficiencies, etc. (RR)

HHV Commonly used for NETL reporting purposes

• Water withdraw, consumption, and discharge (RR)

If new technology creates impurities in water discharge, this must be documented

- CO₂ product composition (RR)
- Air emissions
- Equipment and auxiliary loads NOT affected by novel technology will be scaled appropriately

Power Summary	Rev4-PO	Rev4
Combustion Turbine Power, MWe	464	464
Sweet Gas Expander Power, MWe	3	3
Steam Turbine Power, MWe	276	274
Total Gross Power, kWe	743	741
Auxiliary Load S	ummary	
Acid Gas Removal, kWe	11,490	11,550
Air Separation Unit Auxiliaries, kWe	1,000	1,000
Air Separation Unit Main Air Compressor, kWe	70,920	71,280
Air Separation Unit Booster Compressor, kWe	5,580	5,610
Ammonia Wash Pumps, kWe	90	90
Circulating Water Pumps, kWe	4,740	4,850
Claus Plant TG Recycle Compressor, kWe	60	1,080
Claus Plant/TGTU Auxiliaries, kWe	250	250
CO ₂ Compression, kWe	29,000	31,670
Coal Dryer Air Compressor, kWe	0	0
Coal Handling, kWe	470	470
Coal Milling, kWe	2,240	2,250
Combustion Turbine Auxiliaries, kWe	1,000	1,000
Condensate Pumps, kWe	260	270
Cooling Tower Fans, kWe	2,450	2,510
Feedwater Pumps, kWe	3,810	3,840
Gasifier Water Pump, kWe	0	0
Ground Water Pumps, kWe	490	500
Miscellaneous Balance of Plant ^A , kWe	3,000	3,000
Nitrogen Compressors, kWe	35,460	36,580
Nitrogen Humidification Pump, kWe	0	0
Oxygen Pump, kWe	480	480



Auxiliary Load Summary								
Quench Water Pump, kWe	400	400						
Shift Steam Pump, kWe	210	210						
Slag Handling, kWe	1,150	1,150						
Slag Reclaim Water Recycle Pump, kWe	0	0						
Slurry Water Pump, kWe	190	190						
Sour Gas Compressors, kWe	0	0						
Sour Water Recycle Pumps, kWe	10	10						
Steam Turbine Auxiliaries, kWe	100	200						
Syngas Recycle Compressor, kWe	0	0						
Syngas Scrubber Pumps, kWe	140	140						
Process Water Treatment Auxiliaries, kWe	1,670	1,320						
Transformer Losses, kWe	2,860	2,870						
Total Auxiliaries, MWe	180	185						
Net Power, MWe	564	556						



Reporting Novel Equipment

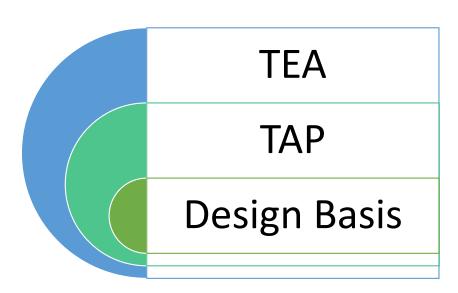


- Novel equipment should be reported at a greater level of detail than found in the Baseline study
- Items to include (RR):
 - Design equations (if developed)
 - Scaling methodology and equations
 - Design basis (kinetics, volumetric throughput, etc.)
 - How was the data for the above collected (TGA, lab scale bubbling bed, etc.)



Steps to Performing TEA



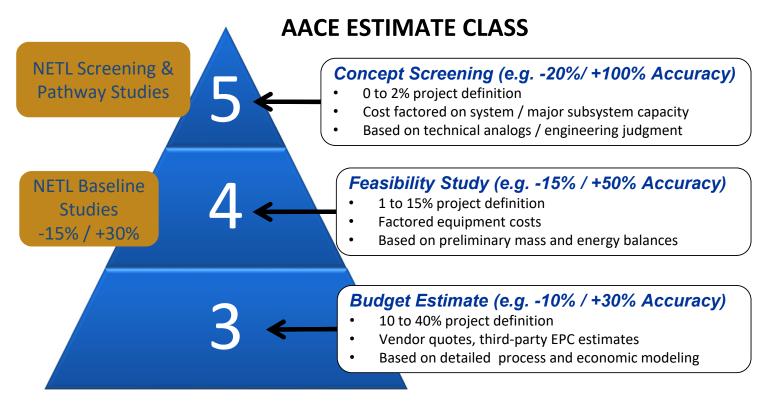


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Classes of NETL Cost Estimates





Process flow diagrams (PFDs) and piping and instrument diagrams (P&IDs) are the primary documents that define project scope. Association for the Advancement of Cost Engineering International (AACE) Recommended Practice No. 18R-97 describes the AACE cost estimate classification system.



QGESS: Cost Estimation Methodology



Capital Cost Breakdown

- Estimate Class
- Contingency Guidelines
- Owner's Cost Recommendations
- Estimate Scope
- Project Scope

Economic Analysis

- Global Economic Assumptions
- Recommended Financing Structures
- Estimation of BSP

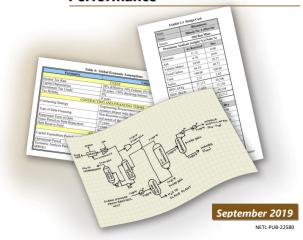


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QUALITY GUIDELINES FOR ENERGY SYSTEM STUDIES

Cost Estimation Methodology for NETL Assessments of Power Plant

Performance



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https://netl.doe.gov/projects/files/QGESSCostEstMethodforNETLAssessmentsofPowerPlantPerformance 090119.pdf



Economic Analysis – Breakeven CO₂ Sales Price

Cost of Capture



- Breakeven CO₂ Sales Price (BSP) is the minimum revenue a power plant must receive for the CO₂ captured and sent to storage in order to cover cost and stated IRROE
 - Determining involves a complex set of financial assumptions
 - To simplify the calculation, a Fixed Charge Rate (for capital) has been developed.
 - Simplifies and unifies common financial terms and assumptions
 - Annualizes the capital cost over the life of the plant
- A simplified equation can be utilized to determine the BSP to unify assumptions

$$BSP = \frac{Annualized}{capital\ charge} + fixed\ operating + variable\ operating}{costs} \\ annual\ CO_2\ captured\ and} \\ sent\ to\ storage$$



Economic Analysis - BSP

(RR)

$$BSP = \frac{FCR \cdot TASC + OC_{FIX} + CF \cdot OC_{VAR} + CF \cdot FP}{CF \cdot FCO_2}$$

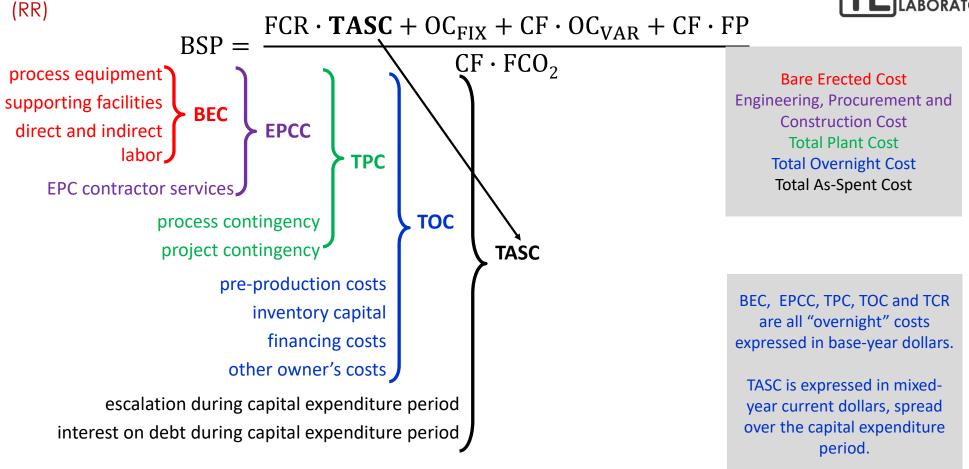
- The **FCR** takes into account the financial aspects of the plant and represents them in a single factor that can then be used to annualize the capital over the life of the plant. Greater detail can be found in the QGESS documents.
- The **FCO₂** parameter is the annual flow of CO₂ from the plant (at 100% CF);
 - NET removal = is the net CO₂ removed from the atmosphere
 - GROSS = is the gross CO₂ removed from the atmosphere by the DAC system
 - PLANT GROSS = gross DAC removal plus and other CO₂ product flow from the overall plant including power generation
- The **CF** parameter Capacity Factor, which is assumed to be equal to the availability
- The **FP** is the sum of annual fuel costs (if in plant boundary)

Fixed Operating Costs (OC _{FIX})	Variable Operating Costs (OC _{VAR})
Annual Operating Labor Cost	Maintenance Material Cost
Maintenance Labor Cost	Other Consumables
Administrative & Support Labor	Waste Disposal
Property Taxes and Insurance	Emission Costs
Additional OC _{Fix} for new technology	Byproduct Revenues
	Additional OC _{Var} for new technology
	*Energy Costs, if outside plant



Economic Analysis – Capital Costs







Capital Cost Basis of Novel Equipment



- Capital costs (projected commercial costs) for unique equipment may be calculated by several methods: (RR)
 - Scaled: The equipment can be scaled if analogous equipment is available either in an NETL baseline study or otherwise
 - Bottom-up: Build cost from metal and manufacturing cost estimates
 - If neither a scaled approach or a bottom-up estimate can be produced research goals or bearable costs can be estimated
 - This approach is occasionally used at laboratory scale projects
 - Report what the basis is for cost (experimental scale)
- The methodology, reference equipment, and sources of data should be documented in detail within the TEA
- Balance of plant will be directly used or scaled from the Baseline reports



Contingency Estimation



- Contingency is to cover the known-unknowns or costs that will likely occur based on past experience due to incomplete engineering design
 - Example: early in the design phase, the plant will have high contingencies, future plants should have lower contingencies, but more known costs
- Two types of contingencies are used:
 - Project Contingency: AACE 16R-90 states that project contingency for a "budget-type" estimate (AACE Class 4 or 5) should be 15 percent to 30 percent of the sum of BEC, EPC fees and process contingency.
 - Process Contingency: intended to compensate for uncertainty in cost estimates caused by performance uncertainties associated with the development status of a technology.

• Each "process" in the TEA is assigned a contingency

	Process
Technology Status	Contingency
New Concept – limited data	40+%
Concept with bench scale data	30-70%
Small Pilot scale data	20-35%
Full sized modules tested	5-20%
Commercial process	0-10%



Contingency Estimation



- Generally, novel technology should have a <u>higher contingency</u> than those in the Baseline studies
- Level of Contingency used should be relative to the development level and engineering completeness of the cost estimate for the novel technology.
- If R&D cost targets, if applicable, contingency might be inclusive
 - When assessing progress towards R&D targets, appropriate contingencies should be included

- Contingency is not:
 - To cover poor engineering or poor estimates
 - Accuracy
 - Cover a scope change
 - Account for delays
 - Unexpected cost escalation
 - Plant performance after startup

Process contingencies range between 2-5% of overall TPC

Process Contingency	
Slurry prep and Feed pump	5%
Gasifier and syngas cooler	15%
Two stage Selexol	20%
Mercury Removal	5%
CO ₂ removal (PC & NGCC)	20%
Combustion Turbine	5%
AHT in IGCC	10%
Instrumentation and controls	5%



Economic Analysis - BSP

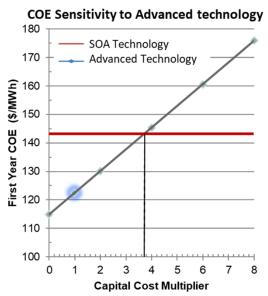


Once BSP has been calculated:

- Compared to reference to novel cases(RR)
- Sensitivity analysis can be conducted to guide research or suggest future goals (RR)

Examples include:

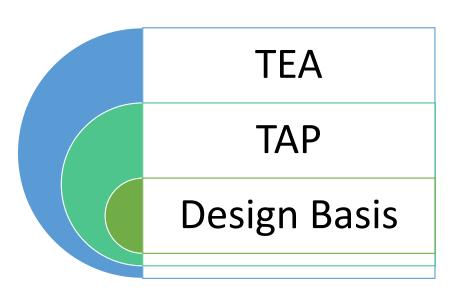
- Capital cost,
- changes in kinetics
- reduced pressure drop,
- reduced heat of reaction to reduce regeneration duties
- This information can be utilized to determine if a parameter is critical.
- Warning: Do not compare BSP from different developer TEA's. BSP's should only be compared when from the same TEA with the same assumptions and basis





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Reporting Requirements



- TAP share with stakeholders
 - State Design and Cost Assumptions and Basis

Stakeholders

- Updated TAP
- Performance Modeling
 - Block Flow diagram
 - Detailed Simulation Model
 - Material and Energy Balance
- Cost Estimating Capital Cost and Breakeven CO₂
 Sales Price (\$/tonne)
 - Detailed TOC cost estimates
 - Sensitivity Studies
 - Breakeven Sales Price
 - Focus on \$/tonne NET
 - May also calculate on GROSS or PLANT GROSS basis

• The TEA report should:

- Provide reasoning for new equipment design basis
 experimental data is preferred
- Have a level a detail equal or greater than that outlined in the Bituminous Baseline (particularly for novel equipment)
- Provide a basis for both design and costing of novel equipment

• Remember to:

- Justify any variations from the QGESS/Baseline outside of the new technology
- Provide enough detail to reproduce stated number
- Once complete, use the information to guide research



Presentation Outline



- TEA Process
- QGESS Description/Location
- Bituminous Baseline Study Overview/Example



NETL Quality Guidelines for Energy System Studies



QGESS

Title	Description
Detailed Coal Specifications	Provides detailed specifications for seven coals commonly used with detailed production information
Specifications for Selected Feedstocks	Provides recommended specifications for natural gas and coal that are commonly found in NETL energy system studies.
Process Modeling Design Parameters	Documents the process modeling assumptions most commonly used in systems analysis studies and the basis for those assumptions. The large number of assumptions required for a systems analysis makes it impractical to document the entire set in each report. This document serves as a comprehensive reference for these assumptions as well as their justification.
CO ₂ Impurity Design Parameters	Summarizes the impurity limits for CO_2 stream components for use in carbon steel pipelines, enhanced oil recovery (EOR), saline formation sequestration, and co-sequestration of CO_2 and H_2S in saline formations.
Capital Cost Scaling Methodology	Provides a standard basis for scaling capital costs, with specific emphasis on scaling exponents. This document contains a listing of frequently used pieces of equipment and their corresponding scaling exponent for various plant types, along with their ranges of applicability.
Cost Estimation Methodology	Summarizes the cost estimation methodology employed by NETL in its assessment of power plant performance.
Estimating Carbon Dioxide Transport and Storage Costs	Addresses the cost of CO_2 transport and storage (T&S) in a deep saline formation with respect to plant location and region-specific aquifers.
Fuel Prices for Selected Feedstocks	Provides an estimate of the market price delivered to specific end-use areas of four coals that are commonly used as feedstocks in the energy system studies sponsored by NETL. Also includes the estimated market price for natural gas delivered to three different regions.



Examples of Information Used in TEA

QGESS Documents Frequently Referenced



- QGESS on Process Modeling Design
 - Site Conditions
 - Steam Cycle Conditions
 - Coal Combustion Parameters
 - Gasifier Performance
 - Syngas Processing
 - Sulfur Processing
 - Equations of State
 - Cooling Water Parameters

- FeedstockSpecification QGESS
 - Natural Gas Composition
 - Coal Compositions by type
 - Limestone Analysis
 - Lime Analysis
 - LHV and HHV

• QGESS on CO₂ Impurities

- CO₂ Delivery Pressure
- Individual Contaminate Concentration Limits
- CO₂ minimum concentration
- Specifications for intended use (Saline, EOR, etc.)
- Venting concerns



Energy Analysis Website NETL Webpage: Library: Energy Analysis



ABOUT ENERGY ANALYSIS

NETL conducts a variety of energy analyses to identify and evaluate promising research and development (R&D) opportunities in order to provide balanced solutions in support of economic sustainability, energy supply security, mitigation of global climate change, and improved enrichmental partnershape.

NETL-conducted studies require a multi-disciplinary approach to the assessment of large, complex energy systems encompassing energy production, distribution, and use. Strategic assessments and planning efforts also incorporate the evaluation of current status, near-term trends, and futurities cenarios.

KEY ANALYSIS AREAS

TECHNOLOGY ANALYSIS

Technology analyses estimate and assess the performance and cost of current, state-of-the-art as well as future energy technologies and systems that result from successful NETL RD&D. Example energy technologies and systems include advanced carbon capture



BENEFITS ANALYSIS

Focuses on quantifying both prospective and retrospective benefits of energy R&D programs using economic models. These studies deliver an understanding of the potential economic competitiveness of advanced energy technologies being developed at NETL, both in the near term and over the next several decades.

The extent to which benefits are realized is a function of several factors, including:

- Success at meeting R&D goals
- Competition with other technologies
- Future energy prices
- Future regulatory action

Since the future of markets and regulations is uncertain, alternative scenarios must be considered. NETL analysts use economic models to forecast the market penetration of advanced energy systems for a variety of possible futures. Impacts are evaluated and associated benefits quantified across three areas: economic, environmental, and energy security.

INTEGRATED ELECTRIC POWER SYSTEMS INFRASTRUCTURE EVALUATION

Studies involve analyzing the interdependencies of electric power systems with other critical infrastructures, such as transportation networks and water infrastructure. Analyses evaluate options for generation, transmission, distribution, and consumption of electricity considering the value of electric power to industry, consumers, and society.

ENERGY DATA AND TRENDS ANALYSIS

Energy analyses include assessments of near- and long-term trends within the U.S. and world energy industries that may impact energy price, availability, and security while influencing the choice of fuels and energy production technologies.

LIFE CYCLE ASSESSMENT

Life Cycle Analysis (LCA) is a comprehensive form of analysis that utilizes the principles of Life Cycle Assessment, Life Cycle Cost Analysis, and various other methods to evaluate the environmental, economic, and social attributes of energy systems ranging from the extraction of raw materials from the ground to the use of the energy carrier to perform work (commonly referred to as the "life cycle" of a product). Results are used to inform research at NETL and evaluate energy options from a National perspective.













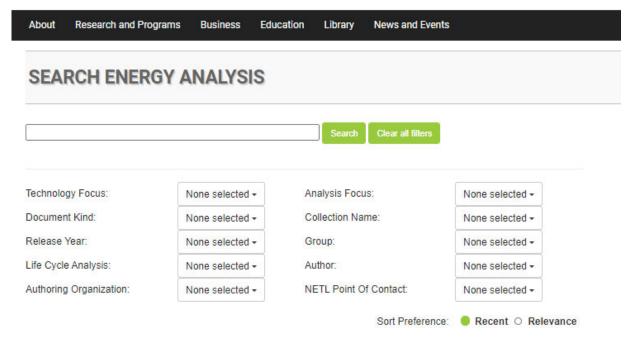
https://netl.doe.gov/ea/about



Energy Analysis Website Search Energy Analysis







https://netl.doe.gov/energy-analysis/search



QGESS Examples

Site Characteristics



Site Characteristics

Parameter	Value
Location	Greenfield, Midwestern U.S.
Topography	Level
Size (PC), acres	300
Size (NGCC), acres	100
Transportation	Rail or Highway
Ash Disposal	Off-Site
Water	50% Municipal and 50% Ground Water

Site Ambient Conditions

Parameter	Value		
Elevation, m (ft)	0 (0)		
Barometric Pressure, MPa (psia)	0.101 (14.696)		
Average Ambient Dry Bulb Temperature, °C (°F)	15 (59)		
Average Ambient Wet Bulb Temperature, °C (°F)	10.8 (51.5)		
Design Ambient Relative Humidity, %	60		
Cooling Water Temperature, °C (°F) ^A	15.6 (60)		
Air composition based on published psychrometr	ic data, mass %		
N ₂	75.055		
O ₂	22.998		
Ar	1.280		
H ₂ O	0.616		
CO ₂	0.050		
Total	100.00		



QGESS Examples

Fuel Specification

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Coal Specifications

coar specimentions										
	Volume 1a and	Volume 1b Rev3	Volume 1 Rev4							
Rank	Bitum	ninous	Bituminous							
Seam	Illinois No.	. 6 (Herrin)	Illinois	No. 6						
Source	Old Be	n Mine		-						
	Proxi	mate Analysis (weight	%) ^A							
	As Received	Dry	As Received	Dry						
Moisture	11.12	0.00	11.12	0.00						
Ash	9.70	10.91	9.70	10.91						
Volatile Matter	34.99	39.37	34.99	39.37						
Fixed Carbon	44.19	49.72	44.19	49.72						
Total	100.00	100.00	100.00	100.00						
Sulfur	2.51	2.82	2.51 2.82							
HHV, kJ/kg (Btu/lb)	27,113 (11,666)	30,506 (13,126)	27,113 (11,666) 30,506 (13,120							
LHV, Btu/lb (Btu/lb)	26,151 (11,252)	29,544 (12,712)	26,151 (11,252) 29,544 (12,71)							
	Ultim	ate Analysis (weight	%)							
	As Received	Dry	As Received	Dry						
Moisture	11.12	0.00	11.12	0.00						
Carbon	63.75	71.72	63.75	71.72						
Hydrogen	4.50	5.06	4.50	5.06						
Nitrogen	1.25	1.41	1.25	1.41						
Chlorine	0.29	0.33	0.15	0.17						
Sulfur	2.51	2.82	2.51	2.82						
Ash	9.70	10.91	9.70	10.91						
Oxygen ^B	6.88	7.75	7.02	7.91						
Total	100.00	100.00	100.00	100.00						

Natural Gas Specification

	Volume	1a Rev3	Volume 1 Rev4					
Component	Volume P	ercentage	Volume Percentage					
Basis	QG	SESS	Aspen: QVAL (Aspen: QVAL GRS/NET @ 25C				
Methane	93	3.1	9	3.1				
Ethane	3	.2	3	3.2				
Propane	0	.7	0.7					
n-Butane	0	.4	0.4					
Carbon Dioxide	1	0	1.0					
Nitrogen	1	.6	1.6					
Methanethiol ^A	5.75	x10 ⁻⁶	5.75	5x10 ⁻⁶				
Total	100	0.00	100.00					
	LHV	HHV	LHV	HHV				
1-1 /1 (Dt.: /11-)	47,454	52,581	47,201	52,295				
kJ/kg (Btu/lb)	(20,410)	(22,600)	(20,293) (22,483)					
MJ/scm (Btu/scf)	34.71 (932)	38.46 (1,032)	34.52 (927) 38.25 (1,02					



Presentation Outline

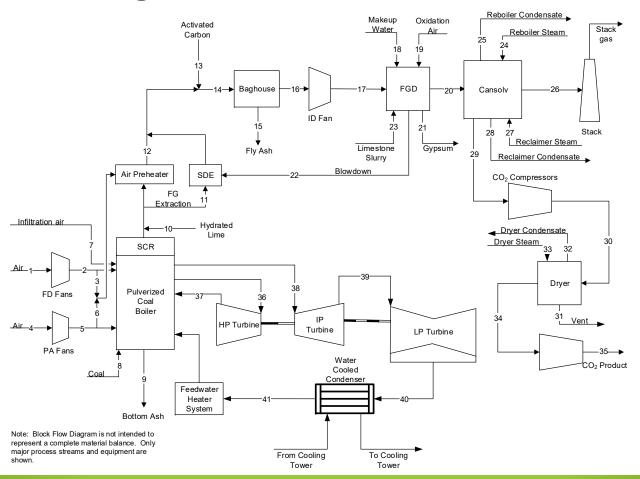


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 - Type of content to include
 - DAC baseline not available yet



Final Block Flow Diagram – B12B







B31B NGCC Stream Tables



-6,801.2

61.977

	1	2	3	4	5	6	7	8	9	10	11	12					- 1		ABORA	TORY
V-L Mole Fraction																				
Ar	0.0092	0.0000	0.0089	0.0089	0.000	0.0000	0.0000	0.0098	0.0000	0.000	0.0000	0.0000								
CH ₄	0.0000	0.9310	0.0000	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0.0000								
CH ₄ S	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0.0000								
C₂H ₆	0.0000	0.0320	0.0000	0.0000	0.000	- 1			1				_							
C₃H ₈	0.0000	0.0070	0.0000	0.0000	0.000					13	14	15	16	17	18	19	20	21	22	23
C ₄ H ₁₀	0.0000	0.0040	0.0000	0.0000	0.000	V-L Mole Frac	tion													
CO ₂	0.0003	0.0100	0.0408	0.0408	0.000	Ar	Ar			0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H₂O	0.0099	0.0000	0.0875	0.0875	1.000	CH ₄				0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
N ₂	0.7732	0.0160	0.7428	0.7428	0.000	CH ₄ S			$\overline{}$	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
O ₂	0.2074	0.0000	0.1200	0.1200	0.000															
SO ₂	0.0000	0.0000	0.0000	0.0000	0.000	C ₂ H ₆			-	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	1.0000	1.0000	1.0000	1.0000	1.000	C ₃ H ₈			$\overline{}$	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
V 1 51	400.007	5.000	400 405	400 400	44.00	C ₄ H ₁₀			(0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
V-L Flowrate (kgmol/hr)	132,867	5,383	138,406	138,406	14,39	CO ₂			(0.0000	0.9995	0.0500	0.9995	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
V-L Flowrate (kg/hr)	3,834,126	93,272	3,927,398	3,927,398	259,2 0	H₂O				1.0000	0.0005	0.9500	0.0005	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Solids Flowrate (kg/hr)	-	U	0	0	0	N ₂				0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Temperature (°C)	15	27	625	111	308	O ₂			_	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Pressure (MPa, abs)	0.10	2.96	0.11	0.10	0.51	SO ₂	_			0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Steam Table Enthalpy (kJ/kg) ^A	30.23	22.04	832.66	255.52	3,080				$\overline{}$	$\overline{}$										
AspenPlus Enthalpy (kJ/kg) ^B	-97.58	-4,487.18	-644.47	-1,221.61	-12,900	Total				1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Density (kg/m³)	1.2	22.1	0.4	0.9	1.9															
V-L Molecular Weight	28.857	17.328	28.376	28.376	18.01	V-L Flowrate (kg _{mol} /hr)			7	5,089	18	5,089	26,991	26,991	31,036	31,036	4,030	20,674	35,246
						V-L Flowrate (kg/hr)			133	223,888	353	223,888	486,242	486,242	559,118	559,118	72,598	372,443	634,975
V-L Flowrate (Ib _{mol} /hr)	292,921	11,867	305,132	305,132	31,77	Solids Flowrat	e (kg/hr)			0	0	0	0	0	0	0	0	0	0	0
V-L Flowrate (lb/hr)	8,452,800	205,630	8,658,430	8,658,430	571,5		(0, 7													
Solids Flowrate (lb/hr)	0	0	0	0	0	Temperature	(°C)			203	29	29	30	585	356	584	308	281	38	38
7 (05)			4.450	224	586	Pressure (MPa	. ,			1.64	2.90	3.04	15.27	16.50	3.74	3.51	0.52	0.51	0.01	0.01
Temperature (°F)	59 14.7	80 430.0	1,156 15.5	231 14.8	73.5	Steam Table E	<u> </u>	1/ka\A		863.65	-6.32	137.79	-231.09	3,528.08	3,112.11	3,642.67	3,080.20	3,024.62	2,376.09	160.78
Pressure (psia) Steam Table Enthalpy (Btu/lb) ^A	13.0	9.5	358.0	109.9	_			. 0,						,	,		-			
AspenPlus Enthalpy (Btu/lb) ^B	-42.0	-1,929.1	-277.1	-525.2	1,324 -5,546	AspenPlus Ent		(g)°	$\overline{}$	5,116.65	-8,969.87	-15,225.37	-9,194.65	-12,452.22	-12,868.18	-12,337.62	-12,900.10	-12,955.67	-13,604.20	-15,819.51
Density (lb/ft³)	0.076	1.380	0.025	0.057	0.11	Density (kg/m	3)			861.8	60.1	375.2	630.1	45.6	13.8	9.0	2.0	2.0	0.1	992.8
Density (ID/It-)	0.076	1.300	0.023	0.037	0.11	V-L Molecular	Weight			18.015	43.997	19.315	43.997	18.015	18.015	18.015	18.015	18.015	18.015	18.015
						V-L Flowrate (lb _{mol} /hr)			16	11,219	40	11,219	59,504	59,504	68,422	68,422	8,884	45,578	77,705
						V-L Flowrate (V-L Flowrate (lb/hr)			294	493,588	777	493,588	1,071,980	1,071,980	1,232,645	1,232,645	160,051	821,097	1,399,880
						Solids Flowrate (lb/hr)			0	0	0	0	0	0	0	0	0	0	0	
						Temperature	(°F)			397	85	85	86	1,085	672	1,084	587	538	101	101
						Pressure (psia)			237.4	421.1	441.1	2,214.7	2,393.1	542.3	508.6	75.0	73.5	1.0	1.0
						Steam Table E	nthalpy (B	tu/lb)A	i	371.3	-2.7	59.2	-99.4	1.516.8	1.338.0	1.566.1	1.324.2	1.300.4	1.021.5	69.1



-6,499.0

AspenPlus Enthalpy (Btu/lb)^B

Density (lb/ft3)

-6,545.7

-3,953.0

-5,353.5

-5,532.3

-5,304.2

-5,546.0

-5,569.9

-5,848.8

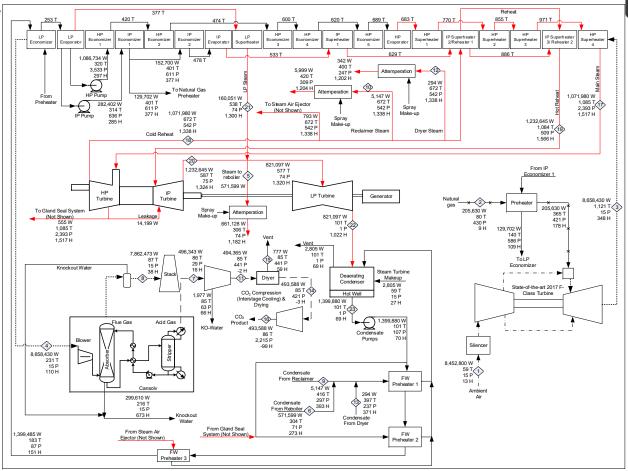
-3,856.4

ASteam table reference conditions are 32.02°F & 0.089 psia

⁸Aspen thermodynamic reference state is the component's constituent elements in an ideal gas state at 25°C and 1 atm

B31B (NGCC Capture)

Heat & Mass Balance





B12B (SC PC Capture)

Performance Summary

Power Summary	Rev4 - 650 MW
Steam Turbine Power, MWe	770
Total Gross Power, MWe	770
Auxiliary Load Summary	
Activated Carbon Injection, kWe	40
Ash Handling, kWe	880
Baghouse, kWe	120
Circulating Water Pumps, kWe	9,610
CO ₂ Capture/Removal Auxiliaries, kWe	27,300
CO ₂ Compression, kWe	44,380
Coal Handling and Conveying, kWe	530
Condensate Pumps, kWe	790
Cooling Tower Fans, kWe	4,970
Dry Sorbent Injection, kWe	80
Flue Gas Desulfurizer, kWe	4,230
Forced Draft Fans, kWe	2,560
Ground Water Pumps, kWe	900
Induced Draft Fans, kWe	10,440
Miscellaneous Balance of Plant ^{A,B} , kWe	2,250
Primary Air Fans, kWe	2,010
Pulverizers, kWe	4,100
SCR, kWe	50
Sorbent Handling & Reagent Preparation, kWe	1,280
Spray Dryer Evaporator, kWe	300
Steam Turbine Auxiliaries, kWe	500
Transformer Losses, kWe	2,680
Total Auxiliaries, MWe	120
Net Power, MWe	650



Performance Summary	Rev4 – 650 MW
Total Gross Power, MWe	770
CO ₂ Capture/Removal Auxiliaries, kWe	27,300
CO ₂ Compression, kWe	44,380
Balance of Plant, kWe	48,320
Total Auxiliaries, MWe	120
Net Power, MWe	650
HHV Net Plant Efficiency, %	31.5%
HHV Net Plant Heat Rate, kJ/kWh (Btu/kWh)	11,430 (10,834)
LHV Net Plant Efficiency, %	32.7%
LHV Net Plant Heat Rate, kJ/kWh (Btu/kWh)	11,024 (10,449)
HHV Boiler Efficiency, %	88.1%
LHV Boiler Efficiency, %	91.3%
Steam Turbine Cycle Efficiency, %	57.5%
Steam Turbine Heat Rate, kJ/kWh (Btu/kWh)	6,256 (5,930)
Condenser Duty, GJ/hr (MMBtu/hr)	2,127 (2,016)
AGR Duty, GJ/hr (MMBtu/hr)	2,344 (2,222)
As-Received Coal Feed, kg/hr (lb/hr)	273,628 (603,246)
Limestone Sorbent Feed, kg/hr (lb/hr)	26,469 (58,354)
HHV Thermal Input, kWt	2,062,478
LHV Thermal Input, kWt	1,989,286
Raw Water Withdrawal, (m³/min)/MW _{net} (gpm/MW _{net})	0.058 (15.3)
Raw Water Consumption, (m³/min)/MW _{net} (gpm/MW _{net})	0.041 (10.8)
Excess Air, %	20.3%

Rev4 Footnotes:

^ABoiler feed pumps are turbine driven ^BIncludes plant control systems, lighting, HVAC, and miscellaneous low voltage loads



B12B Equipment Summaries

Equipment No.	Description	Туре	Design Condition	Operating Qty.	Spares	
8	Vacuum Filter Belt	Horizontal belt	44 tonne/hr (49 tph) of 50 wt% slurry	2	1	
9	Filtrate Water Return Pumps	Horizontal centrifugal	850 lpm @ 13 m H₂O (220 gpm @ 40 ft H₂O)	1	1	
10	Filtrate Water Return Storage Tank	Vertical, lined	560,000 lpm (150,000 gal)	1	0	
11	Process Makeup Water Pumps	Horizontal centrifugal	1,990 lpm @ 21 m H₂O (530 gpm @ 70 ft H₂O)	1	1	
12	Activated Carbon Injectors		60 kg/hr (140 lb/hr)	1	0	
13	Hydrated Lime Injectors	777	1,660 kg/hr (3,650 lb/hr)	1	0	
14	Cansolv	Amine-based CO2 capture technology	3,724,000 kg/hr (8,211,000 lb/hr) 19.1 wt% CO₂ concentration	1	0	
15	Cansolv LP Condensate Pump	Centrifugal	1,287 lpm @ 1 m H₂O (340 gpm @ 4 ft H₂O)	1	1	
16	Cansolv IP Condensate Pump	Centrifugal	6 lpm @ 4.6 m H₂O (2 gpm @ 15 ft H₂O)	1	1	
17	CO₂ Dryer	Triethylene glycol	Inlet: 152 m³/min @ 3.0 MPa (5,381 acfm @ 441 psia) Outlet: 2.9 MPa (421 psia) Water Recovered: 487 kg/hr (1,074 lb/hr)	1	0	
18	CO₂ Compressor	Integrally geared, multi-stage centrifugal	8.0 m³/min @ 15.3 MPa, 80°C (299 acfm @ 2,217 psia, 176°F)	2	0	
19	CO₂ Aftercooler	Shell and tube heat exchanger	Outlet: 15.3 MPa, 30°C (2,215psia, 86°F) Duty: 88 MMkJ/hr (84 MMBtu/hr)	1	0	

Case B12B - Account 7: Ductwork and Stack

Equipment No.	Description	Туре	Design Condition	Operating Qty.	Spares
1	Stack	Reinforced concrete with FRP liner	152 m (500 ft) high x 6.0 m (20 ft) diameter	1	0

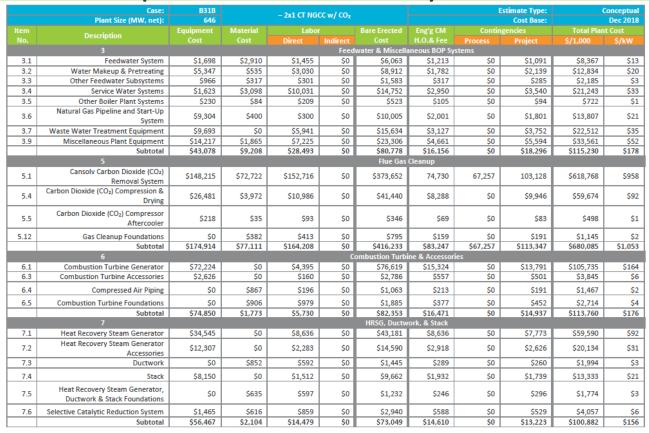
Case B12B - Account 8: Steam Turbine and Accessories

		Туре	Design Condition	Operating Qty.	Spares	
		Commercially available advanced steam turbine	798 MW 24.1 MPa/593°C/593°C (3500 psig/ 1100°F/1100°F)	1	0	
2	Steam Turbine Generator	Hydrogen cooled, static excitation	890 MVA @ 0.9 p.f., 24 kV, 60 Hz, 3- phase	1	0	
3	Surface Condenser	urface Single pass, divided 1,170 GJ/hr (2,220 MMBtu/hr),		1	0	





B12B Capital Cost Summary





Report Capital by Account and Sub Account

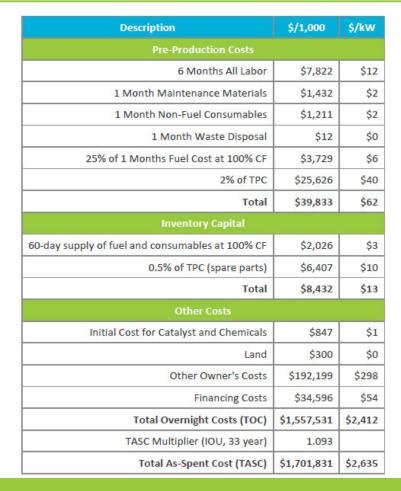
Additional Accounts in Baseline include:

- 8 Steam Turbine & Accessories
- 9 Cooling Water System
- 11 Accessory Electric Plant
- 12 Instrumentation & Controls
- 13 Improvements to Site
- 14 Buildings & Structures



Build up of Capital Costs

B31B Example







Fixed and Variable Operating Costs

B12B Example

Dec 2018	Cost Base:	− SC PC w/ CO ₂			B12B	Case:		
85	Capacity Factor (%):	10,834	Heat Rate-net (Btu/kWh):		650	Plant Size (MW, net):		
			ng & Maintenance La	Operati				
r Shift	Labor Requirements per	Operating			ating Labor	Oper		
2.0		Skilled Operator:	\$/hour	38.50		Operating Labor Rate (base):		
11.3		Operator:	% of base	30.00		Operating Labor Burden:		
1.0		Foreman:	% of labor	25.00		Labor O-H Charge Rate:		
2.0		Lab Techs, etc.:						
16.3		Total:						
			ed Operating Costs	Fi				
ost	Annual Co							
(\$/kW-net)	(\$)							
\$11.024	\$7,161,008					Annual Operating Labor:		
\$24.319	\$15,797,590					Maintenance Labor:		
\$8.836	\$5,739,649					Administrative & Support Labor:		
\$75.997	\$49,367,468					Property Taxes and Insurance:		
\$120.175	\$78,065,715					Total:		
\$120.17S	\$70,003,713		able Operating Costs	Vari		rotan		
- defense	-41		able Operating Costs	Val				
(\$/MWh-net)	(\$)							
\$4.89906	\$23,696,385		C			Maintenance Material:		
		a tata eta	Consumables		. tot a min			
		Initial Fill	Per Unit	Per Day	Initial Fill			
\$0.86967	\$4,206,523	\$0	\$1.90	7,136	0	Water (/1000 gallons):		
\$0.74992	\$3,627,291	\$0	\$550.00	21.3	0	Makeup and Waste Water Treatment		
\$0.15975	\$772,686	\$0	\$1,600.00	1.56	0	Chemicals (ton): Brominated Activated Carbon (ton):		
\$0.61349	\$2,967,412	\$0	\$240.00	39.9	0	Enhanced Hydrated Lime (ton):		
\$0.98814	\$4,779,570	\$0	\$240.00	700	0	Limestone (ton):		
\$1.32741	\$6,420,577	0.00	\$300.00	69.0	0.00	Ammonia (19 wt%, ton):		
\$0.15301	\$740,101	\$2,612,120	\$150.00	15.9	17,414	SCR Catalyst (ft ³):		
		\$2,612,120		15.9	17,414	CO ₂ Capture System Chemicals ^A		
\$1.90730 \$0.23720	\$9,225,455 \$1,147,315	\$0	Proprietary \$6.80	544	w/oguin	<u> </u>		
\$7.00589	\$33,886,930	\$2,612,120	\$0.00	344	w/equip.	Triethylene Glycol (gal): Subtotal:		
\$7.00589	\$33,880,930	\$2,612,120	Waste Disposal			Subtotal:		
\$1.60115	\$7,744,619	\$0	\$38.00	657	0	Fly Ash (ton)		
\$0.35568	\$1,720,404	\$0	\$38.00	146	0	Bottom Ash (ton)		
\$0.00255	\$1,720,404	\$0	\$2.50	16	0	SCR Catalyst (ft³):		
\$0.00233	\$59,053	\$0	\$0.35	544	-			
\$0.01221	\$59,055	\$0 \$0	\$38.00	3.51	0	Triethylene Glycol (gal): Thermal Reclaimer Unit Waste (ton)		
\$0.00856	\$41,395	\$0 \$0	\$38.00	52.1	0	Prescrubber Blowdown Waste (ton)		
	. ,		\$38.00	32.1	0			
Subtotal: \$0 \$10,192,273 \$2.10718 By-Products								
\$0,00000	SO I	\$0	S0.00	1064	0	Gypsum (ton)		
\$0.00000	\$0	\$0	\$0.00	1004	-	Subtotal:		
\$14.01213	\$67,775,588	\$2,612,120				Variable Operating Costs Total:		
\$14.01213	\$01,113,588	\$2,012,120	516			variable Operating Costs Total:		
			Fuel Cost					
\$24.12521	\$116,691,765	\$0	\$51.96	7,239	0	Illinois Number 6 (ton):		
\$24.12521	\$116,691,765	\$0				Total:		





Revision 4 Cost Estimate Results

PC and NGCC Cases



	PC				NGCC	
Case Name	PC Subcritical		PC Supercritical		State-of-the-art 2017 F-Class	
	B11A	B11B	B12A	B12B	B31A	B31B
	COST					
Total Plant Cost (2018\$/kW)	2,011	3,756	2,099	3,800	780	1,984
Bare Erected Cost	1,482	2,641	1,548	2,677	561	1,312
Home Office Expenses	259	462	271	469	112	262
Project Contingency	269	526	280	531	107	304
Process Contingency	0	127	0	123	0	105
Total Overnight Cost (2018\$M)	1,611	2,991	1,678	3,023	692	1,558
Total Overnight Cost (2018\$/kW)	2,478	4,604	2,582	4,654	952	2,412
Owner's Costs	467	848	484	854	172	428
Total As-Spent Cost (2018\$/kW)	2,860	5,314	2,980	5,371	1,040	2,635
LCOE (\$/MWh) (excluding T&S)	60.9	100.8	61.3	99.7	42.2	68.2
Capital Costs	24.2	45.0	25.2	45.4	8.8	22.3
Fixed Costs	9.1	16.0	9.5	16.1	3.6	8.6
Variable Costs	7.9	14.5	7.7	14.0	1.7	5.6
Fuel Costs	19.7	25.4	18.9	24.1	28.1	31.6
LCOE (\$/MWh) (including T&S)	60.9	110.2	61.3	108.7	42.2	71.6
CO ₂ T&S Costs	0.0	9.4	0.0	8.9	0.0	3.5
Breakeven CO ₂ Sales Price (ex. T&S), \$/tonne ^A	N/A	42.0	N/A	42.9	N/A	74.8
Breakeven CO ₂ Emissions Penalty (incl. T&S), \$/tonne ^A	N/A	72.7	N/A	69.9	N/A	96.7

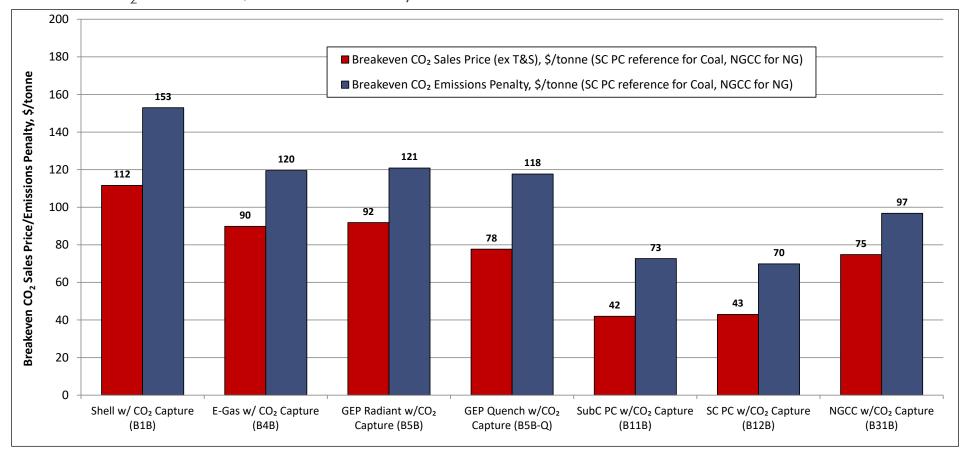
A Both the breakeven CO2 sales price and emissions penalty were calculated based on the non-capture SC PC Case B12A for all coal cases, and the non-capture NGCC Case B31A for natural gas cases



Revision 4 Cost Estimate Results

Breakeven CO₂ Sales Price/Emissions Penalty







Revision 4 Cost Estimate Results

Sensitivities – Capacity Factor



