



DOE Contract DE-FE0012829

Pilot Test of a Nanoporous, Super-hydrophobic Membrane Contactor Process for Post-combustion CO₂ Capture






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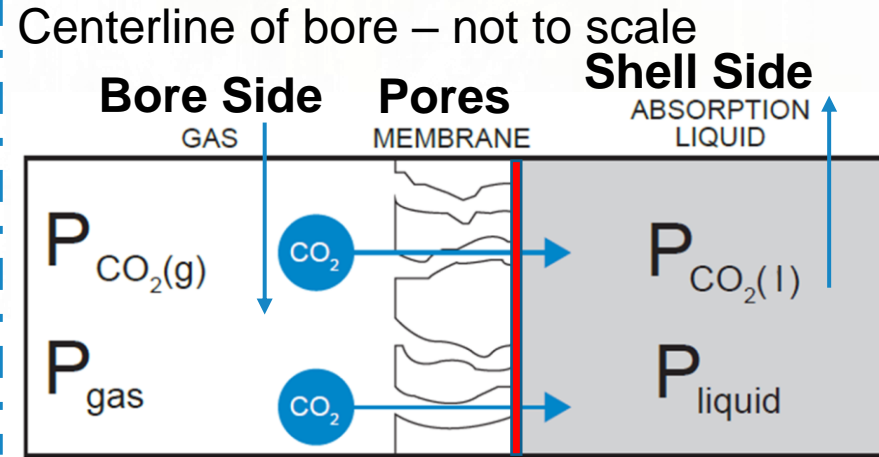
Project overview

- **Performance period**: October 1, 2013 – June 30, 2022
- **Total funding**: \$15.6MM (DOE: \$12.5MM, Cost share: \$3.1MM)
- **Objectives**:
 - Build and operate a 0.5 MW_e pilot-scale CO₂ capture system and conduct tests on coal flue gas at the National Carbon Capture Center (NCCC)
 - Demonstrate a continuous, steady-state operation for ≥ 2 months
- **Goal**: Achieve DOE's goal of $\geq 95\%$ CO₂ purity at a cost of $\leq \$40$ /tonne of CO₂ captured by 2025

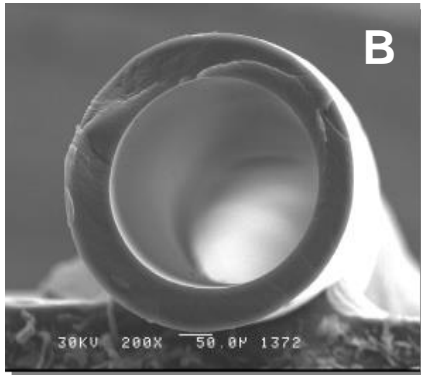
■ <u>Team</u> :	Member	Roles
		<ul style="list-style-type: none">• Project management and planning• Process design and testing
	 ALaS  	<ul style="list-style-type: none">• Membrane and module development
	 TRIMERIC CORPORATION	<ul style="list-style-type: none">• Techno-Economic Analyses (TEA)
	NCCC	<ul style="list-style-type: none">• Site host

Hollow Fiber Membrane Contactor (HFMC) technology

HFMC: high surface area device that facilitates mass transfer

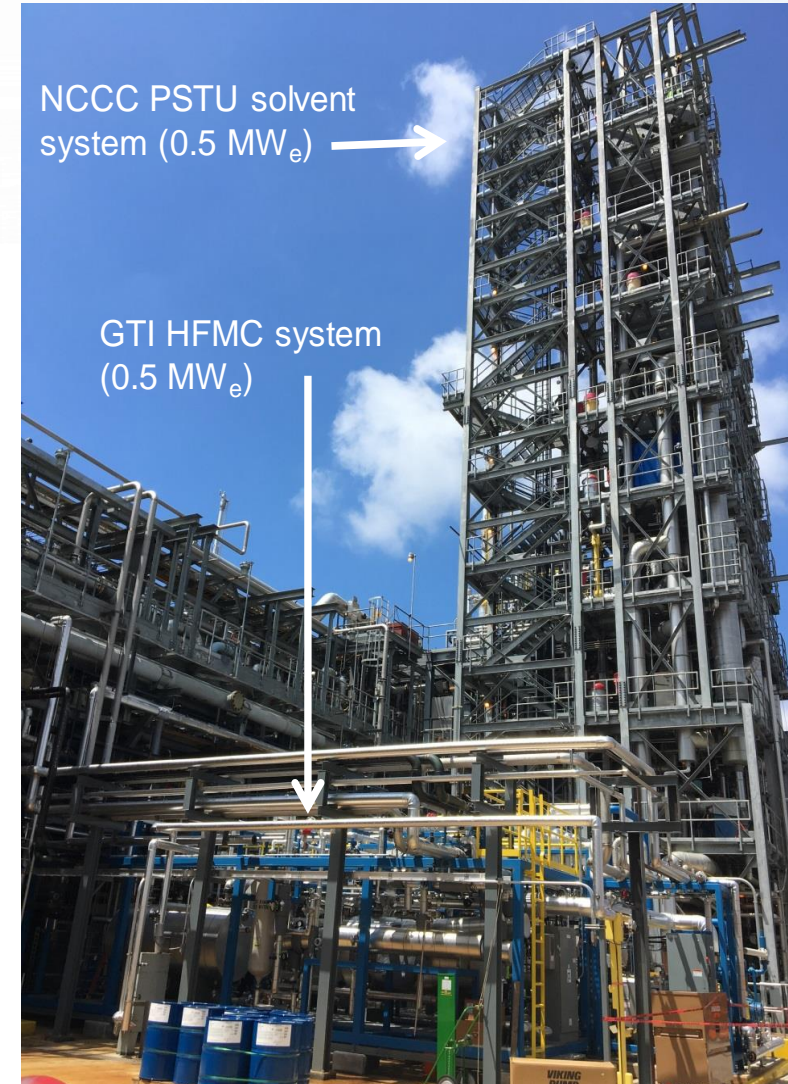


Hydrophobic coating layer to prevent wetting



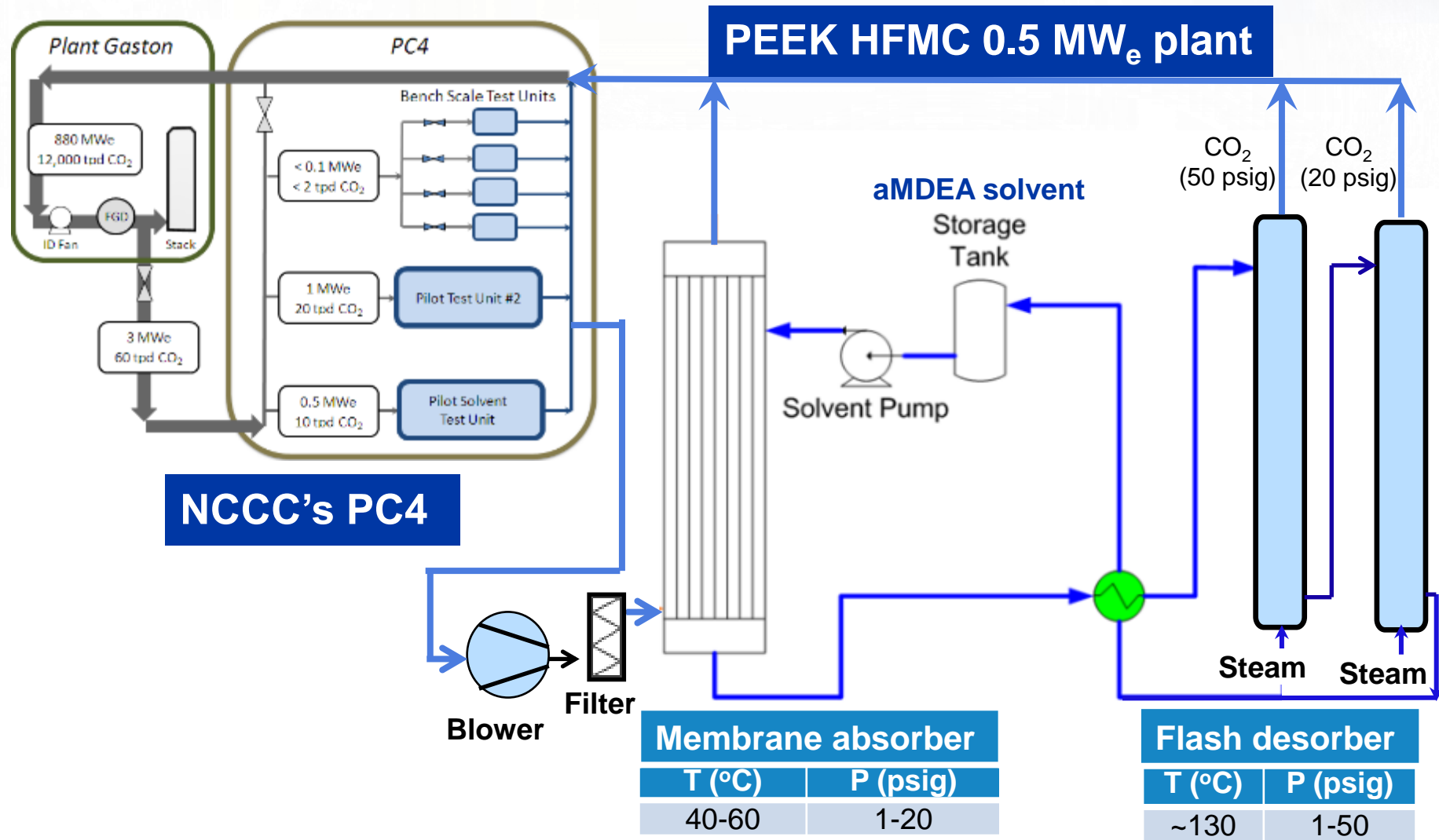
PEEK spun into high-packing density, hollow fibers

8-inch-diameter commercial cartridges with ~2,000 GPU intrinsic CO_2 permeance used in pilot scale testing

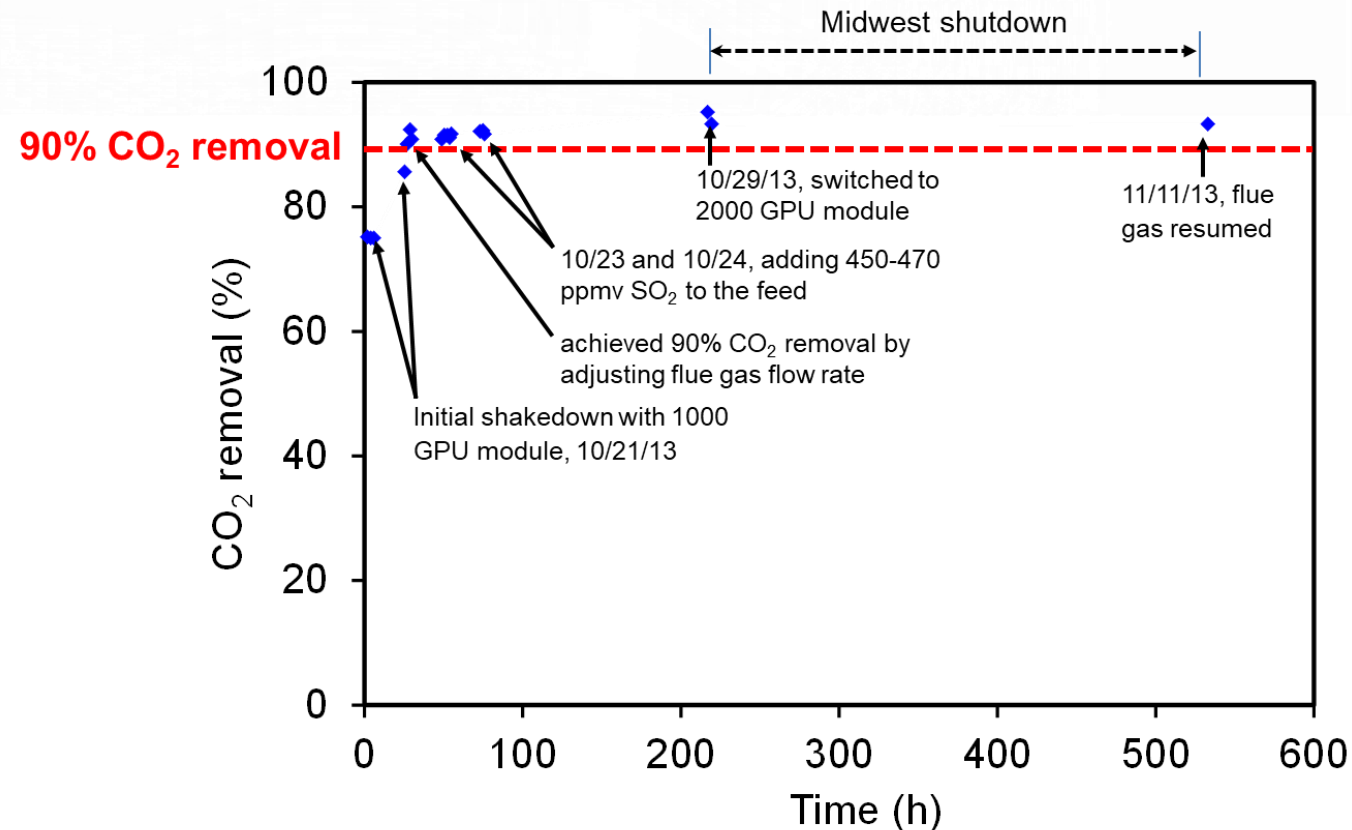
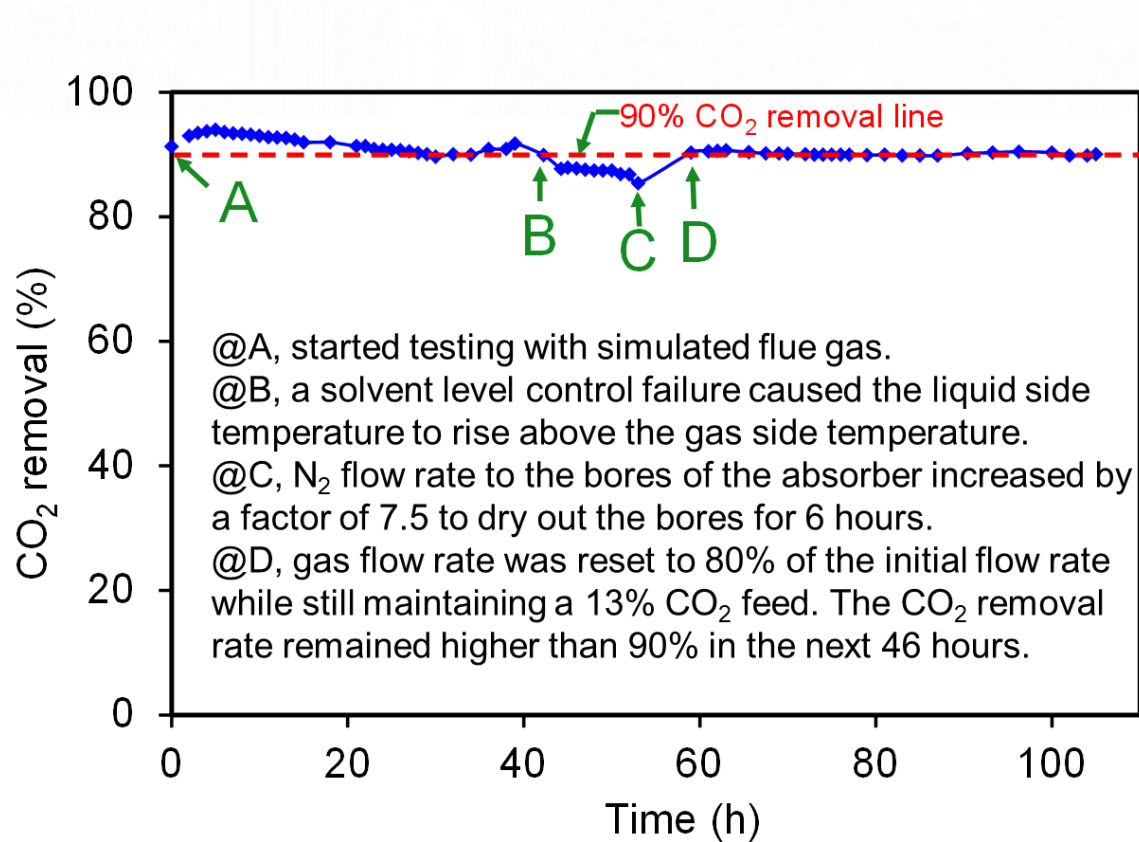


Pilot plant (10 ton/day) being tested at the National Carbon Capture Center (NCCC)

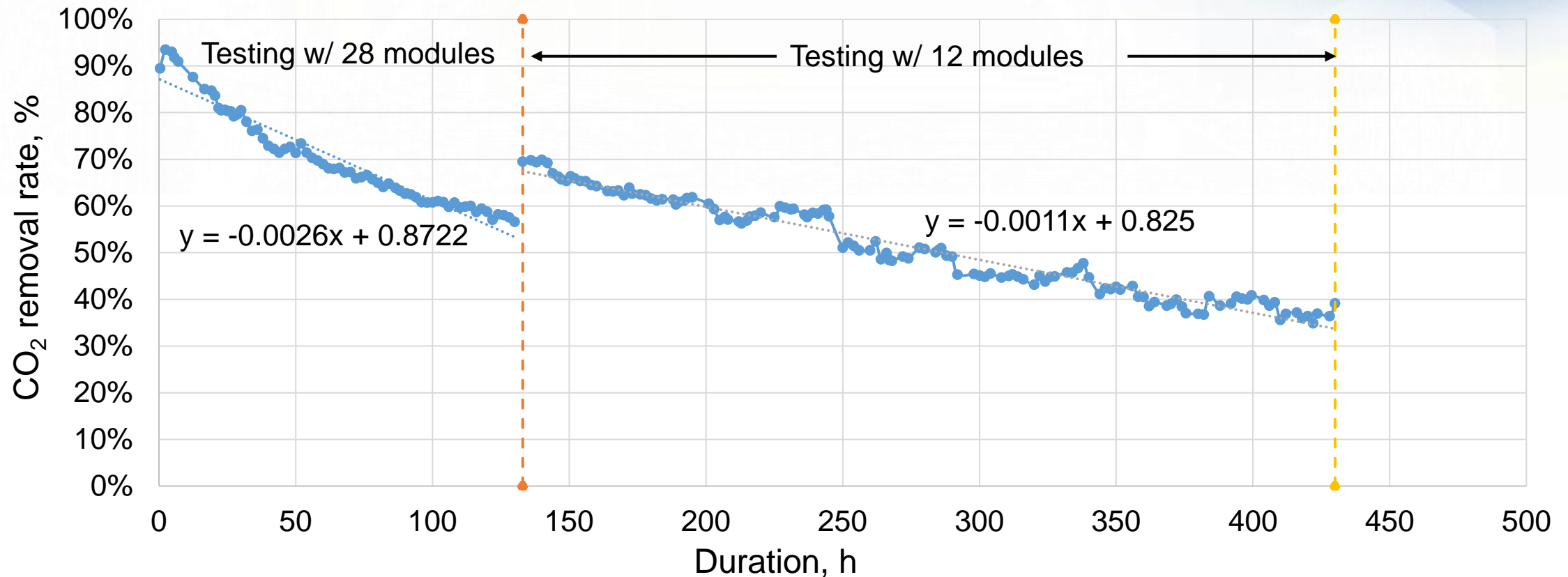
HFMC process at NCCC



Integrated testing in the previous lab and bench (coal flue gas) project showed performance and stability



2018's testing with 28 membrane modules



- **Observation**: Performance declined with time
- **Analysis**: Quantitative analysis indicated three causes: 1) contaminants (powder and rust particles); 2) vapor condensation in fiber bores; and 3) capillary condensation of vapor in PEEK pores
- **Decision made at that point**: Resolve issue of contaminants (powder and rust particles) first

Additional flue gas filters and pre-membrane mesh pads installed to protect the membrane; orifice plates installed to monitor if there is a flow maldistribution issue



Installed new filters

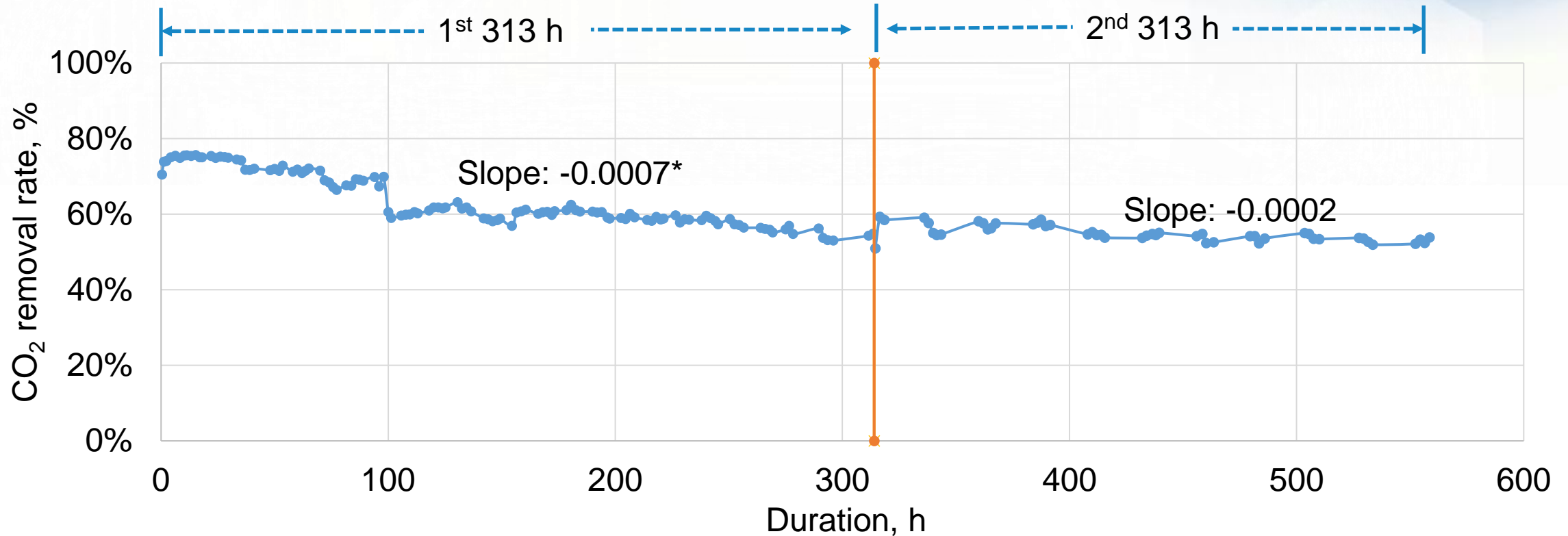


Pre-membrane mesh pad

Liquid side
Pressure
gauge →
Liquid side
orifice plate →
Gas side
orifice plate ↗
Gas side
Pressure gauge ↗

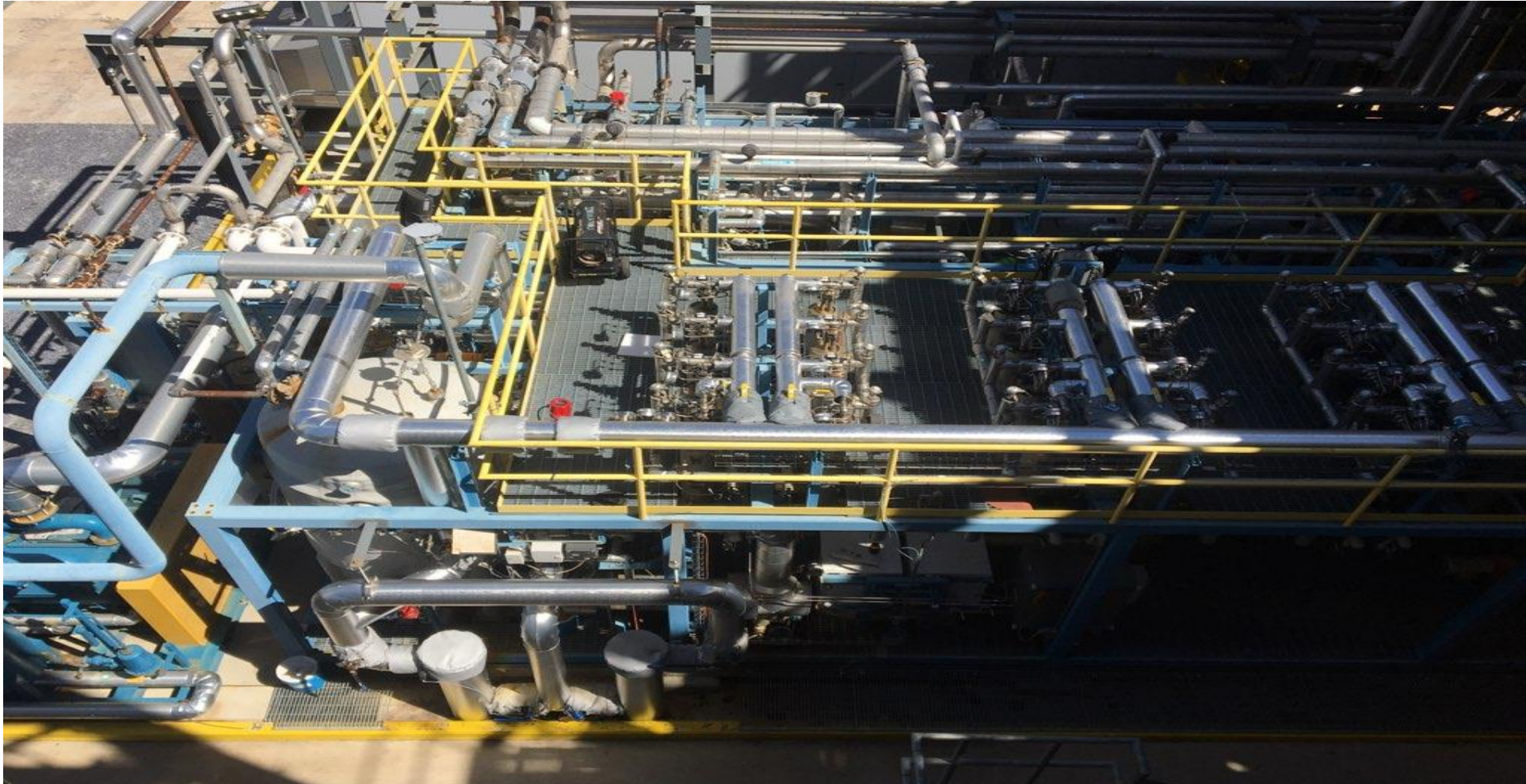


2019's testing with 8 modules (7 used and one new)



- **Observation:** stability improved, especially during the 2nd 313 h
- **Analysis:** 2% drop/100h during the 2nd 313h, might be because: 1) 7 used membranes (containing particles inside) were used, and 2) rusts from carbon steel piping; new membranes were expected to be stable
- **Decision made at that point:** move forward to fabricate 28 new membrane cartridges, replace carbon steel piping with stainless steel piping between filter and membrane header, and perform tests

Modified skid with stainless steel piping (February 2020)



2021's testing with 28 modules

- **January 17:** Started testing
- **January 21 (system operated for ~92h):** Shutdown due to power plant's shutdown
- **February 6:** Flue gas was back at NCCC, system brought back online
- **February 20 (system operated for ~347 total hours):** Observed CO₂ capture rate dropped from 90% to ~39%. The decision was made to shut down system and look into approaches to recover performance and improve stability
- **February 20 – March 26:** Investigated: 1) approaches to recover performance, and 2) approaches to improve stability and performance
- **March 26:** System shutdown due to power plant's shutdown
- **March 26 – April 12:** Data analysis and reporting

Inspection: Inlet mesh pads were clean after system improvements, no visible rust or particulates present on the mesh pads, indicating the issue of particles had been resolved

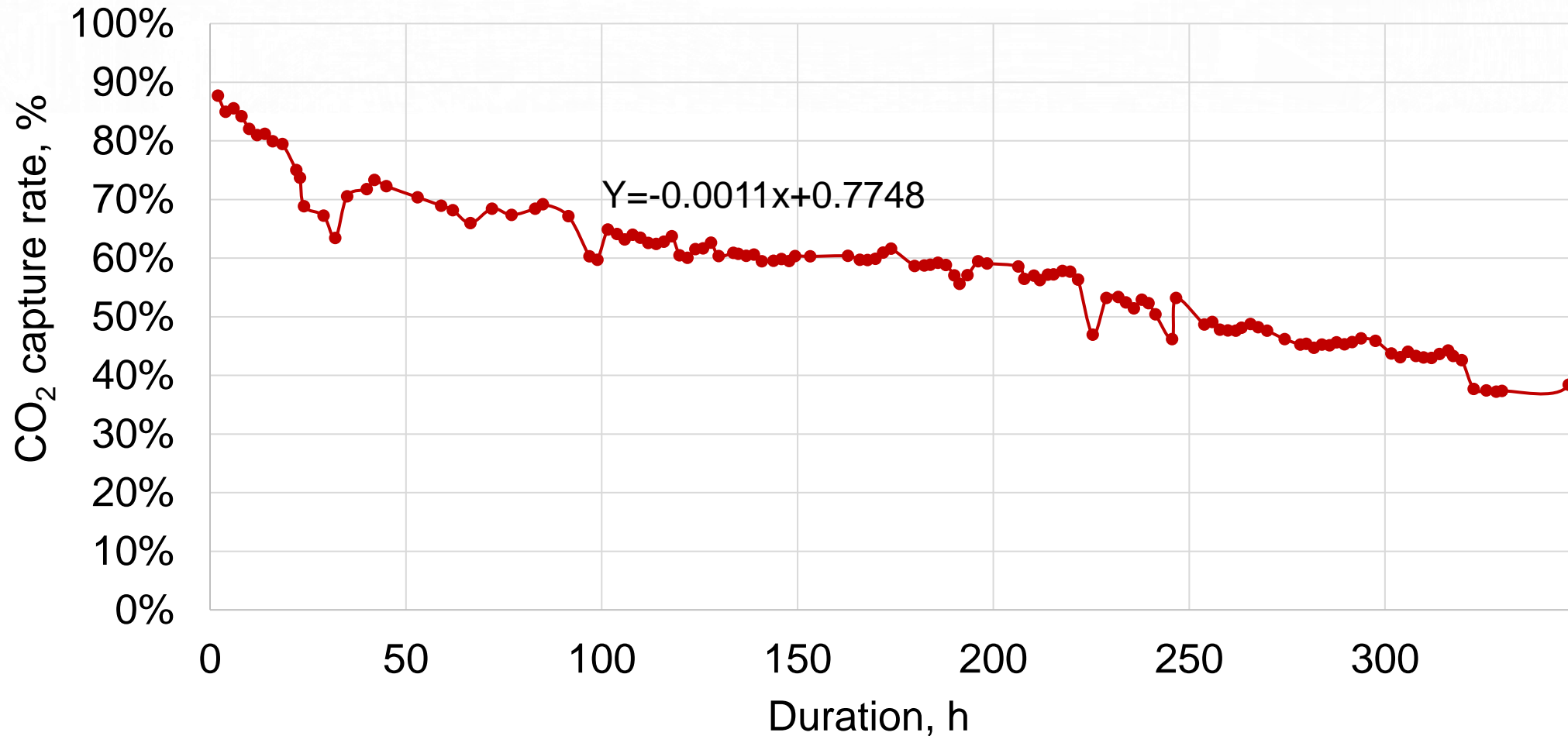


Used mesh pad top surface after March 2019 testing: rust particles observed because between filter and membrane header carbon steel piping was used at that time

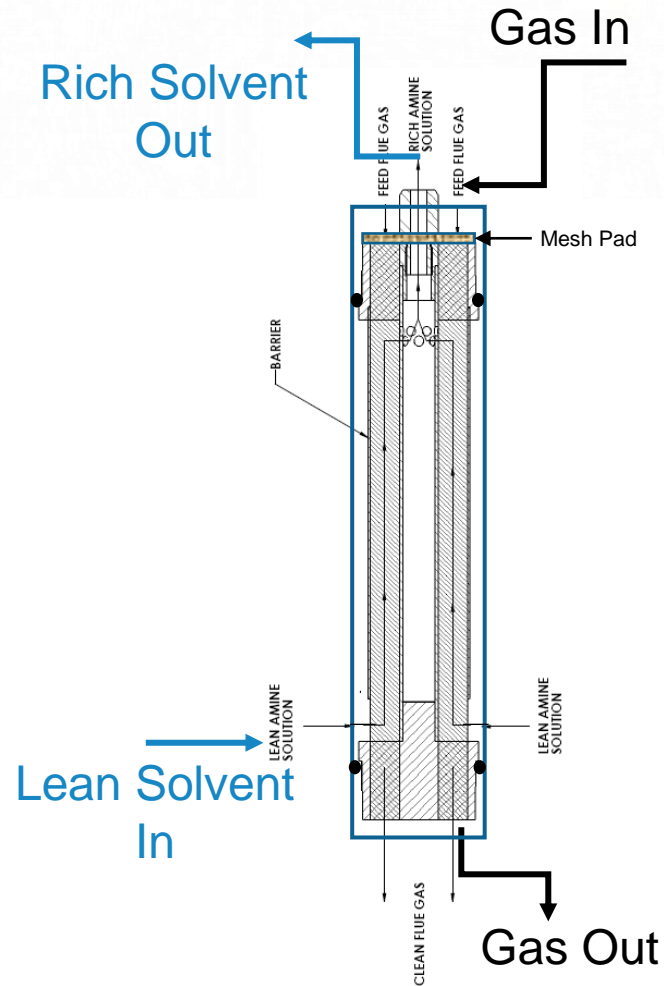


Used mesh pad top surface after 2021 testing: clean

2021's testing: Decline in performance observed for the 1st 347 hours with 28 modules

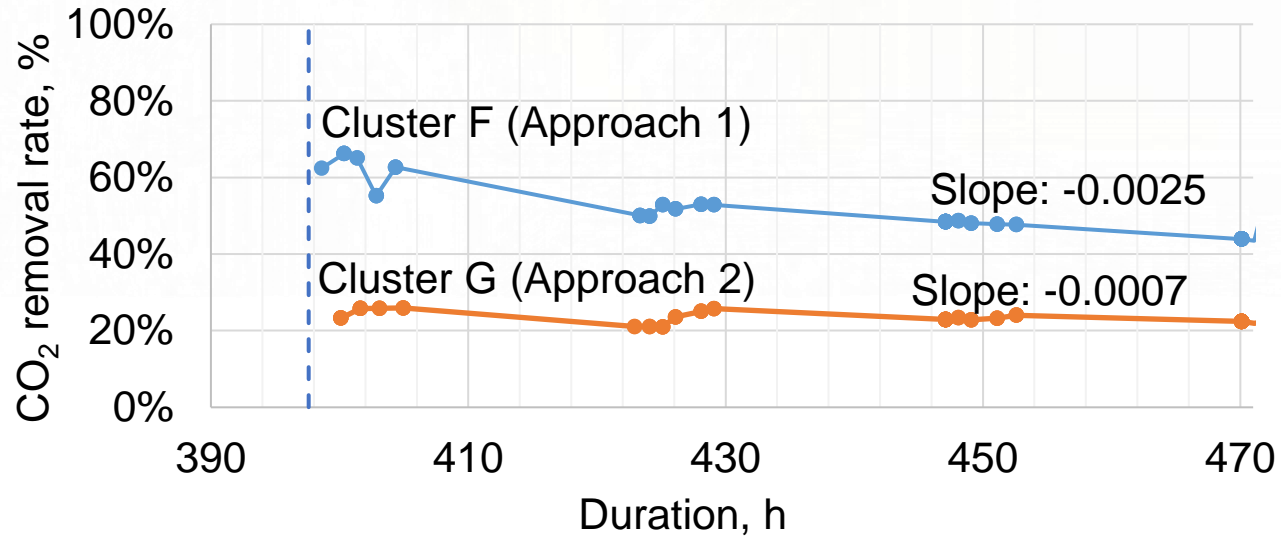


Approaches to recover membrane performance

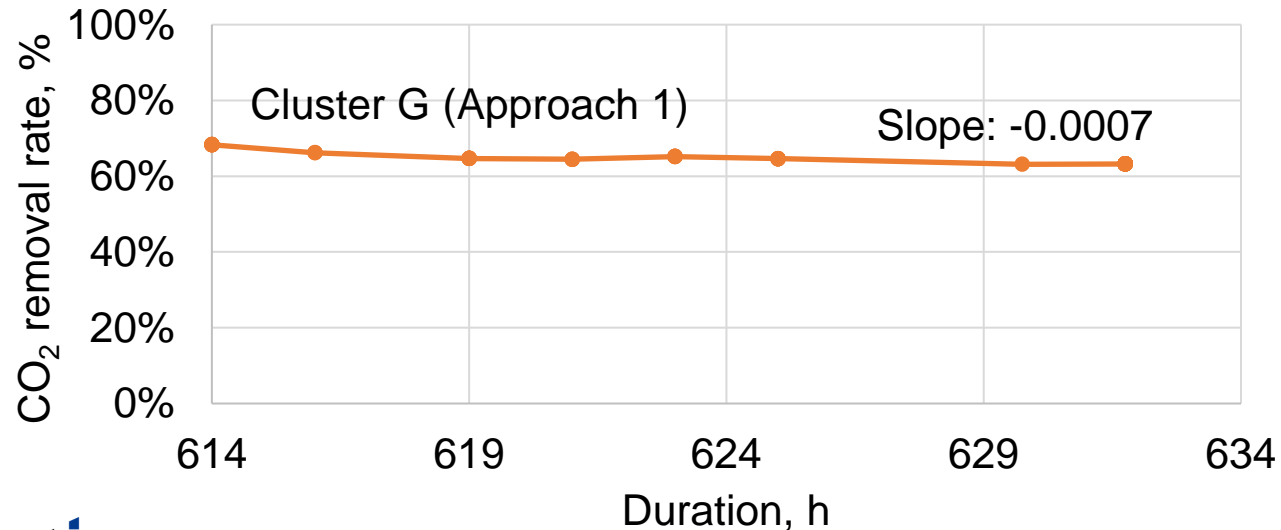


- **Approach 1**: Water wash followed by air dry
 1. Drain liquid from membrane shell side
 2. Remove inlet mesh pad
 3. Connect demineralized water to gas inlet, allow water to flow down to gas outlet
 4. Connect instrument air to the gas inlet, purge fibers with air
 5. Replace gas inlet mesh pad, bring membrane back online
- **Approach 2**: Air dry
 1. Drain liquid from membrane shell side
 2. Remove inlet mesh pad
 3. Connect instrument air to the gas inlet, purge fibers with air
 4. Replace gas inlet mesh pad, bring membrane back online

Performance can be recovered, but stability was not improved



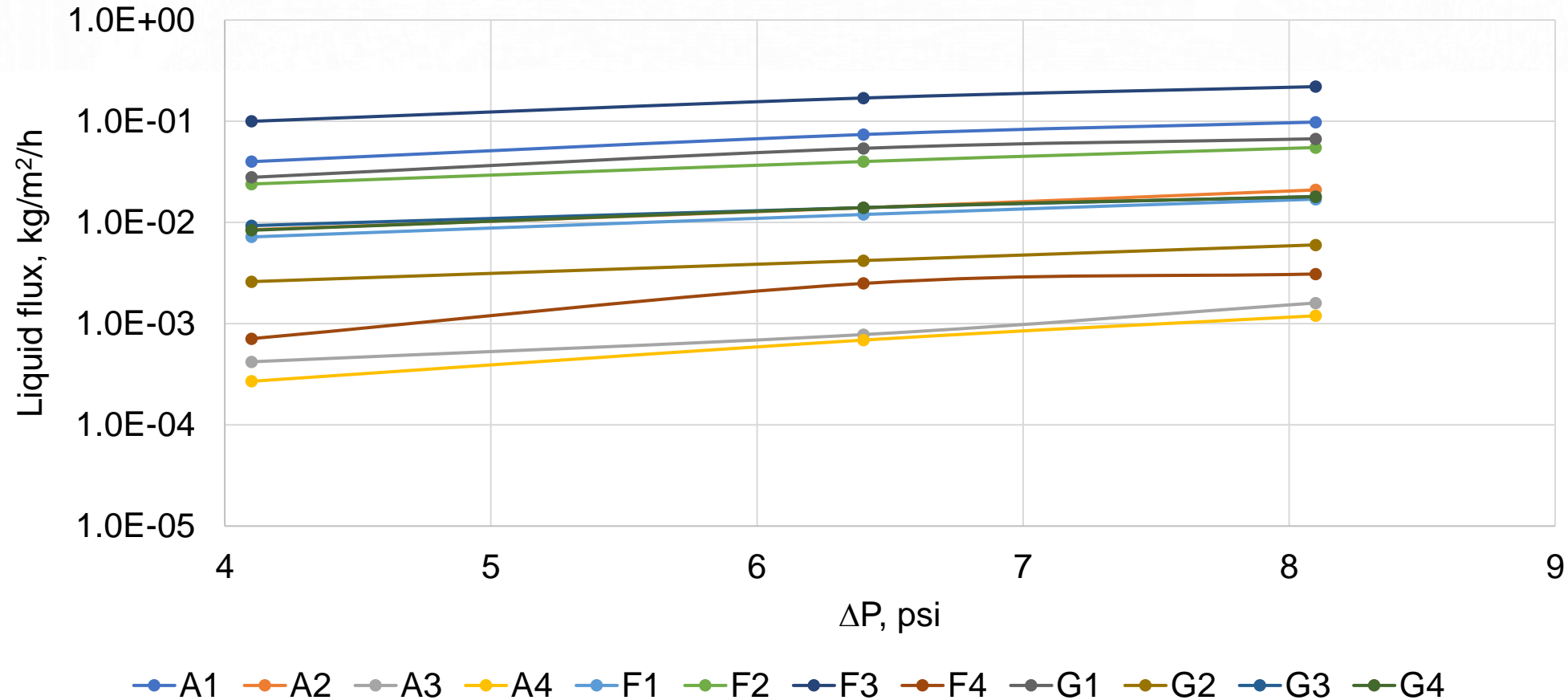
- Air purge alone was not sufficient in recovering performance
- Water wash + air purge can recover the performance but doesn't resolve continual decline issue



Performance degradation possible causes, actions and solutions

Cause #	Explanation	Sub-cause #	Explanation	Mitigating Information/Action Required to Resolve	Resolved?
1	Contaminants in the flue gas	A	Solids observed on inlet tubesheets and in bores	Replaced piping with stainless steel, installed filter, mesh pads in 2020	Yes
		B	Within bore or pore, water vapor condenses, blocking CO ₂ passage	Reduced flue gas dewpoint with no effect on degradation. Liquid found in bore is consistent with amine, NOT flue gas	Yes, verified not to be the cause
2	Liquid was observed from the bore side drain with amine concentration close to solvent	A	Poor membrane potting into epoxy tubesheet provides a path	ALaS developed an infusion technique to eliminate leak path in 2016	Yes, verified not to be the cause
		B	Broken fibers during operations provide a path for amine to get into the top tubesheet and into the bores	Solvent permeation test, single gas permeation tests, and cyclohexane permeation tests on used modules	Ongoing
		C	Defects of the membrane superhydrophobic layer coating during handling or operation	SEM and other characterizations, Solvent permeation test, single gas permeation tests, and cyclohexane permeation tests on used modules	Need action
		D	Membrane hydrophobicity change (especially surface contact angle) after long-term contact with liquid	ALaS: measure contact angle as a function of time in the presence of solvent	Need action
		E	Vapor phase permeation of the solvent through the membrane and then condensation in the pores and in the bore	GTI: V-L-E data for amine solution, amine and water permeances to calculate the amine concentration of the condensed liquid; ALaS: prepare PEEK with pores > 50 nm (current pores have average size of 13-16 nm).	Need action

Testing underway to verify the causes of instability; solvent permeation tests suggest quality of the hydrophobic coating layer needs to be improved to be impermeable to solvent



Summary

- Made modifications to skid – filters, stainless steel piping, mesh pads, 28 new membrane cartridges fabricated and installed
- Performed testing early 2021, solid issue resolved, decline in performance observed
- Developed an approach to recover performance, but stability was not improved
- Data analysis indicates most probable cause to instability: liquids in the pores
- Additional tests are ongoing to verify the causes of instability and resolve the issue

Acknowledgements

- Financial and technical support



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JIP Partners

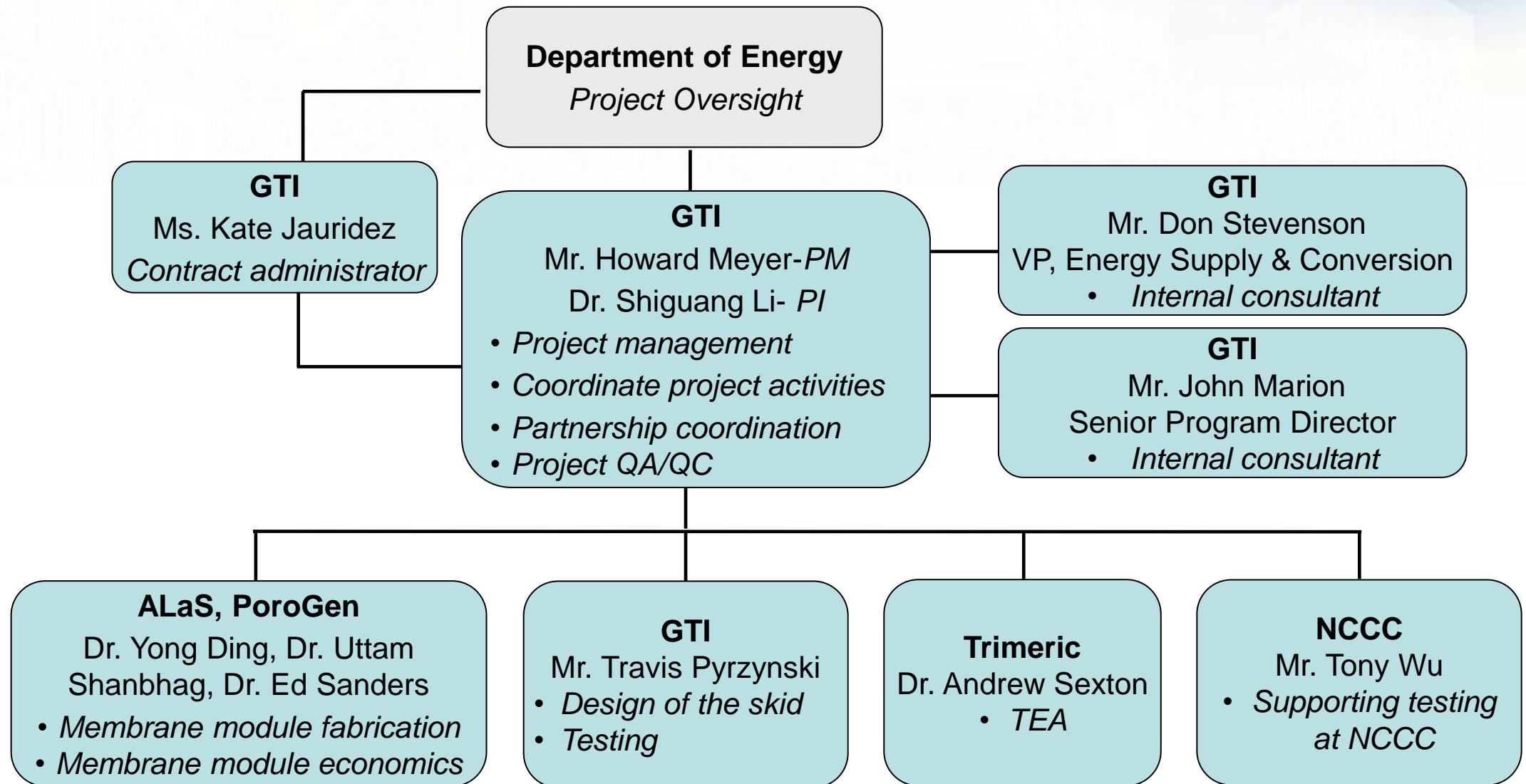


Air Liquide ALaS

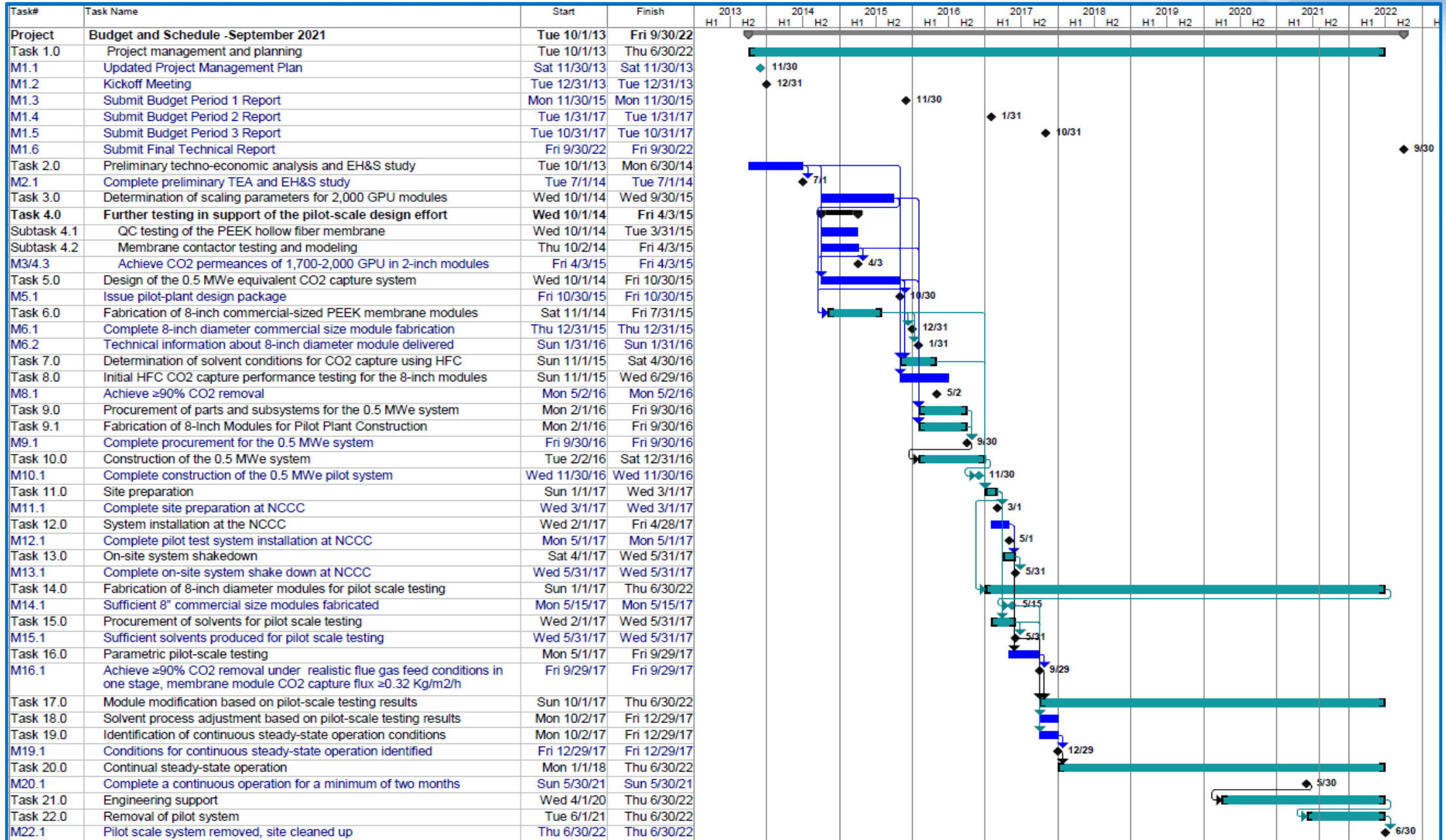


- NETL: Andrew O'Palko, Steven Mascaro, Dan Hancu, José Figueroa, and Lynn Brickett

Appendix – Organization Chart



Appendix – Gantt Chart



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