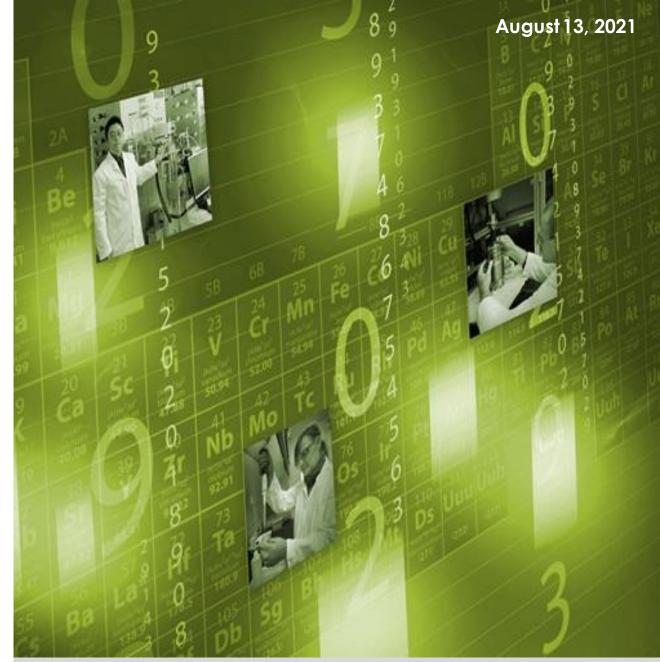
# Updated Costs for Carbon Capture Retrofits

Timothy Fout Strategic Systems Analysis & Engineering Directorate



**Preliminary Results – Subject to Revision** 





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## Agenda



### Natural Gas Retrofit Updates

- Design Basis
- Performance Results
- Cost Results
- Sensitivities





## **Design Basis**



## **Basis for Model and Cost Development**



- QGESS for Carbon Capture Retrofit (in process)
- QGESS for Capital Cost Estimation Methodology<sup>1</sup>
- Cost and Performance Baseline for Fossil Energy Plants Volume 1: Bituminous Coal (PC) and Natural Gas to Electricity (2019) – Rev 4<sup>2</sup>
  - Cases B31A/B (NGCC)
  - H-class supplement Cases B32A/B (in process)
- Aspen Plus v10
  - Previous revisions of the NGCC retrofit report were developed in GTPro
  - Development of F(retrofit)- and H-frame cases
    - 1 <u>https://netl.doe.gov/projects/files/QGESSCostEstMethodforNETLAssessmentsofPowerPlantPerformance\_022621.pdf</u>
    - 2 https://netl.doe.gov/projects/files/CostAndPerformanceBaselineForFossilEnergyPlantsVol1BitumCoalAndNGtoElectBBRRev4-1\_092419.pdf

### Site Characteristics



Parameter	Value				
Location	Greenfield, Midwestern U.S.				
Topography	Level				
Size (NGCC), acres	100				
Transportation	Rail or Highway				
Water	50% Municipal and 50% Ground Water				

Parameter	Value					
Elevation, m (ft)	0 (0)					
Barometric Pressure, MPa (psia)	0.101 (14.696)					
Average Ambient Dry Bulb Temperature, °C (°F)	15 (59)					
Average Ambient Wet Bulb Temperature, °C (°F)	10.8 (51.5)					
Design Ambient Relative Humidity, %	60					
Cooling Water Temperature, °C (°F) <sup>A</sup>	15.6 (60)					
Air composition based on published psychrometric data, mass %						
N <sub>2</sub>	75.055					
0 <sub>2</sub>	22.998					
Ar	1.280					
H <sub>2</sub> O	0.616					
CO <sub>2</sub>	0.050					
Total	100.00					

<sup>A</sup>The cooling water temperature is the cooling tower cooling water exit temperature. This is set to  $4.8^{\circ}$ C (8.5 °F) above ambient wet bulb conditions in ISO cases.



### **Fuel Characteristics**



Componen	t	Volume Percentage				
Methane	CH <sub>4</sub>		93.1			
Ethane	C <sub>2</sub> H <sub>6</sub>		3.2			
Propane	C₃H <sub>8</sub>	0.7 0.4				
<i>n</i> -Butane	$C_4H_{10}$					
Carbon Dioxide	CO <sub>2</sub>		1.0 1.6			
Nitrogen	N <sub>2</sub>					
Methanethiol <sup>A</sup>	CH <sub>4</sub> S		5.75x10 <sup>-6</sup>			
	Total		100.0			
	LHV		ННУ			
kJ/kg (Btu/lb)	47,201(20	),293)	52,295 (22,483)			
MJ/scm (Btu/scf)	34.52 (9	27)	38.25 (1,027)			

<sup>A</sup>The sulfur content of natural gas is primarily composed of added Mercaptan (methanethiol  $[CH_4S]$ ) with trace levels of hydrogen sulfide  $(H_2S)$ 



## **Emission Limits**



- Air Emissions: All cases are compliant with the current utility Mercury and Air Toxics Standards (MATS) and New Source Performance Standards (NSPS)
  - $\circ$  CO<sub>2</sub> emission limit for NGCC technology is 1,000 lb CO<sub>2</sub>/MWh-gross
  - $\circ$  B31A has a CO<sub>2</sub> emission rate of 741 lb/MWh-gross

Pollutant <sup>A</sup>	NGCC (lb/MWh-gross)				
SO <sub>2</sub>	0.90				
NOx	0.43				
PM (Filterable)	N/A				
Hg	N/A				
HCI	N/A				

<sup>A</sup> Carbon monoxide (CO) emissions will be reported as 1 ppm

- Water Emissions: Based on the global plant assumptions made for NGCC cases in Revision 4 of the Bituminous Baseline report, there were no water streams that required treatment to attain compliance with the effluent limitation guidelines
  - H-frame cases will apply the same set of plant assumptions, and thus, are compliant without additional treatment technology



### **Case List**



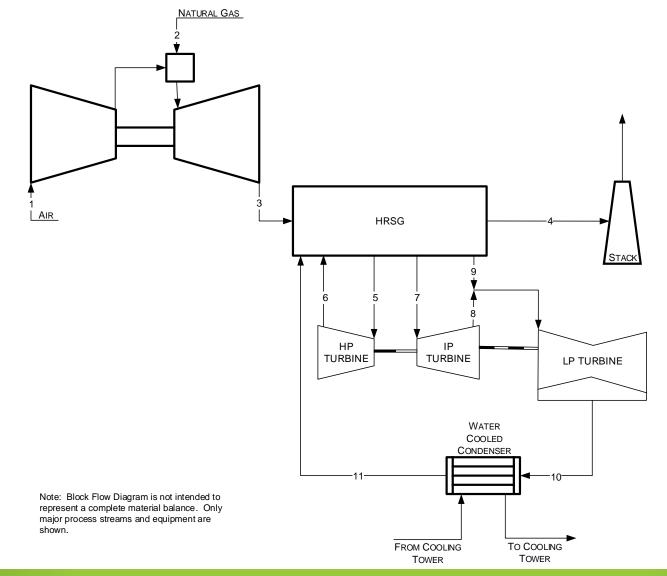
Case <sup>A</sup>	Unit Cycle	Steam Cycle, psig/°F/°F	Combustion Turbine	Heat Recovery	Oxidant	NOx Control	CO <sub>2</sub> Separation	Capture Rate	Plant Type	Process Water Treatment
<b>B31A</b>		2400/1085/1085	art 2017 F-Class	Heat Recovery Steam Generator Air (HRSG)	A :	Low NOx Burner and Selective	N/A	N/A	Greenfield	- -
B31B							Cansolv	90%	Greenfield	
B <b>31A-B</b> R							Cansolv	90%	Brownfield (retrofit)	
<b>B32A</b>	NGCC		2 x State of the		Catalytic Reduction	N/A	N/A	Greenfield	N/A	
B32B		2700/1085/1045				-	Cansolv	90%	Greenfield	
B32A-BR							Cansolv	90%	Brownfield (retrofit)	

<sup>A</sup> Natural Gas feed flow rate is the same amongst similar frames types.



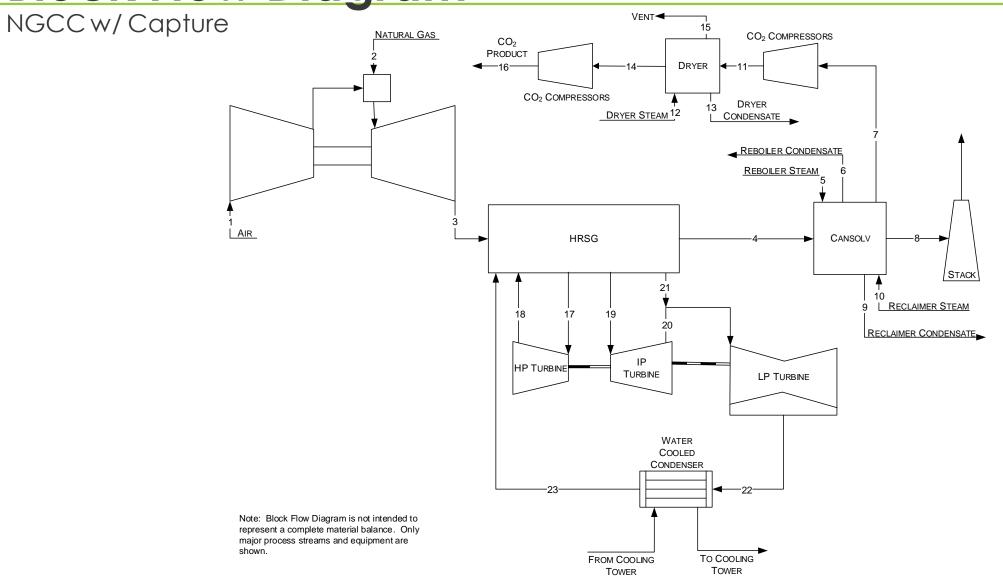
# Block Flow Diagram

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## **Block Flow Diagram**





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Retrofit plants are assumed to be capture ready

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- The IP/LP crossover pressure of 73.5 psia pre-retrofit is suitable for Cansolv applications
- In addition to the reduction in output from redirected steam flow prior to the LP turbine, additional derate due to off-design steam turbine flow was considered
- Derate calculations were performed in the Aspen Plus models
  - The derate is calculated as a ~2% decrease from the gross steam turbine power (reference study is Lucquiaud et al.)





### Assumptions for retrofit cases

- Existing units are assumed to be fully paid off
- The only capital outlays required are for the carbon capture processes (including the removal technology process equipment, a CO<sub>2</sub> compression train, and any modification to the existing plant required for the retrofitted technology)
- Ongoing fuel costs, as well as fixed and variable O&M, and additional consumables are included in the levelized cost of electricity calculations



### **Cost Estimation**



$$SC = RC * \left(\frac{SP}{RP}\right)^{Exp}$$

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$$SC - greenfield equivalent of the scaled cost for the retrofit technology
RC - item reference cost
SP - process scaling parameter for the retrofit equipment
RP - process reference parameter for the reference plant equipment
Exp - scaling exponent
RDF - retrofit difficulty factor
FRC - factored retrofit cost$$

### • The retrofit difficulty factor was applied at the total TPC level

- $\circ$  RDF = 1.09 for NGCC cases
- RDF varies from 1 to 1.3 depending on difficulty of retrofit, type of equipment and labor productivity
- Value use represents an overall average



### Financial Parameters

- The prior study/QGESS method had financial structures for low risk (NGCC w/o capture) and high risk (NGCC w/ capture); both were three-year construction periods.
  - -The updated QGESS\* only includes differentiators for three versus five-year construction periods.
- The existing three-year construction period timeframe/financial structure was used as is.
- A make-up power cost (MPC) of \$30/MWh was added to retrofit cases to bring to net plant power back to pre-retrofit levels

\*https://netl.doe.gov/projects/files/QGESSCostEstMethodforNETLAssessmentsofPowerPlantPerformance\_022621.pdf



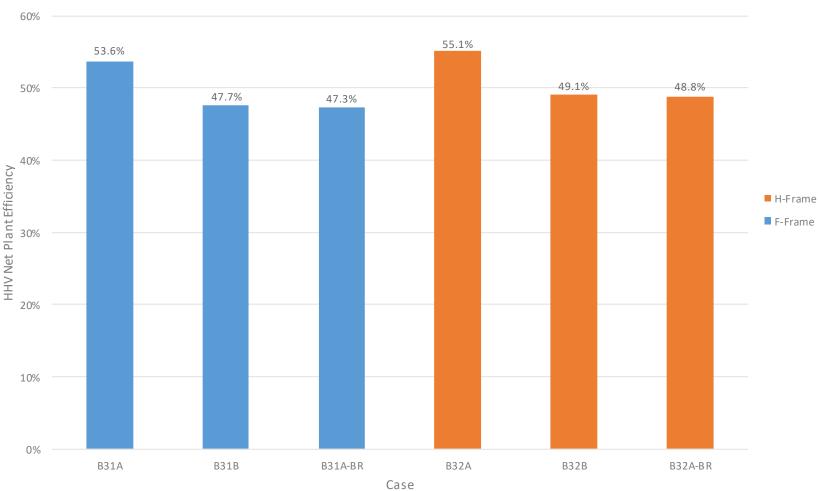


### **Performance Results**



## **Performance Summary**

#### HHV Net Plant Efficiency



HHV Net Plant Efficiency



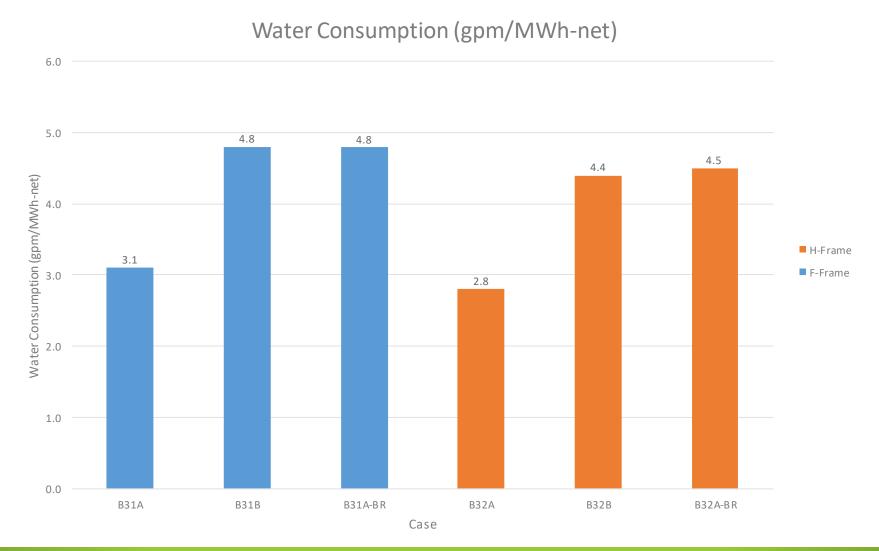
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### **Performance Summary**

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#### WaterUsage

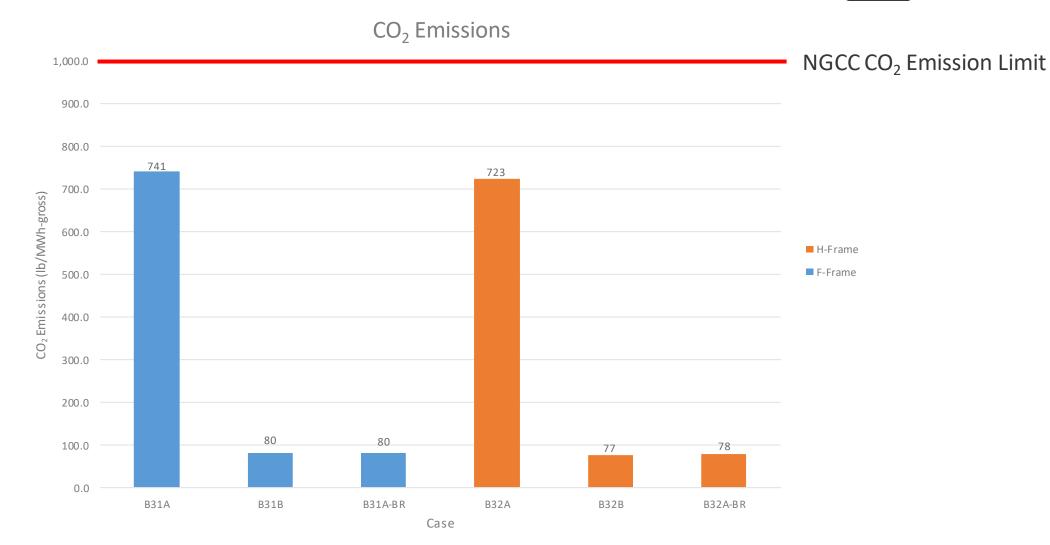




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### **Performance Summary** CO<sub>2</sub> Emissions

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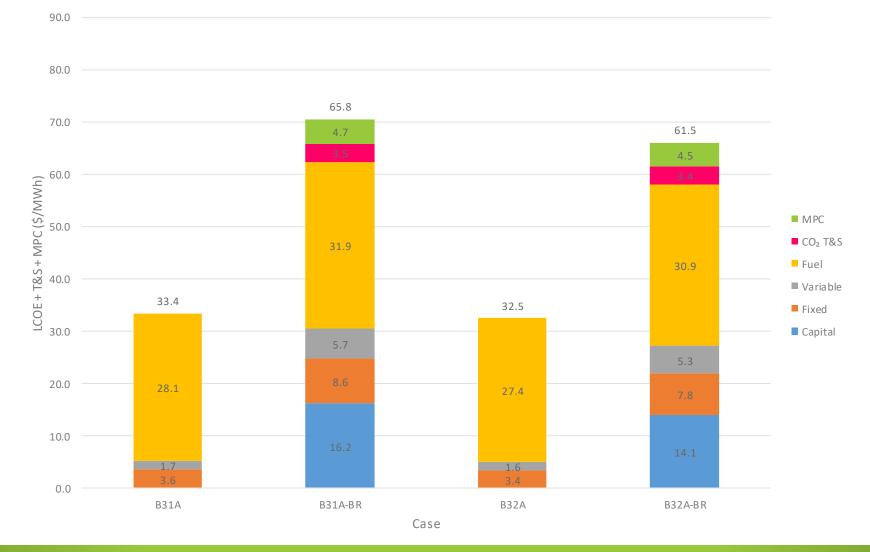
### **Cost Results**



### Levelized Cost of Electricity

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LCOE + T&S (\$/MWh)





## **CO<sub>2</sub> Breakeven Point**







### Price of Natural Gas

• \$1-10/MMBtu

### Capacity Factor

30 to 100 percent

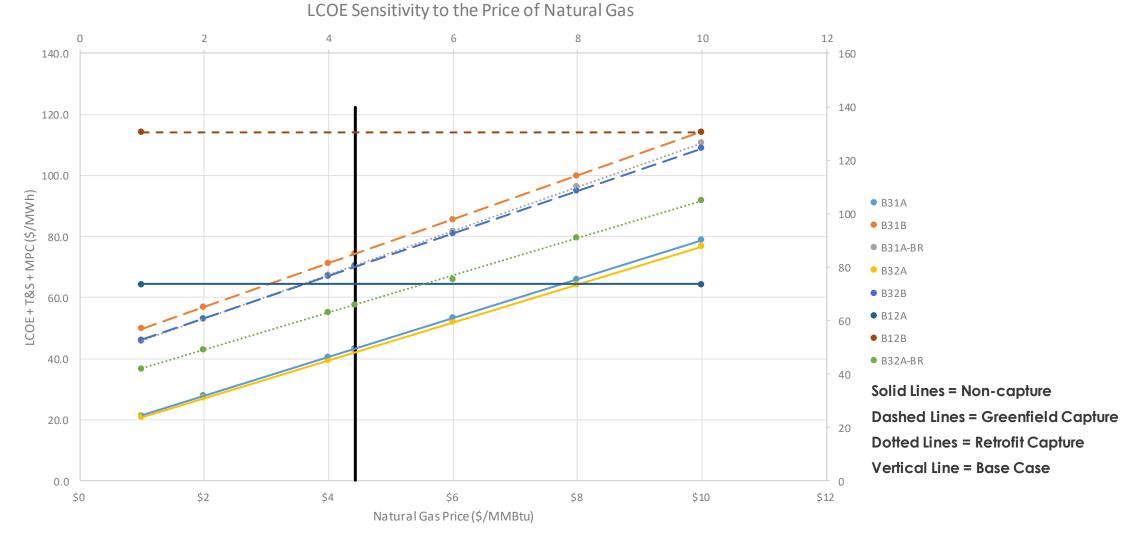
### Make-up Power Cost

• \$0/MWh - \$100/MWh



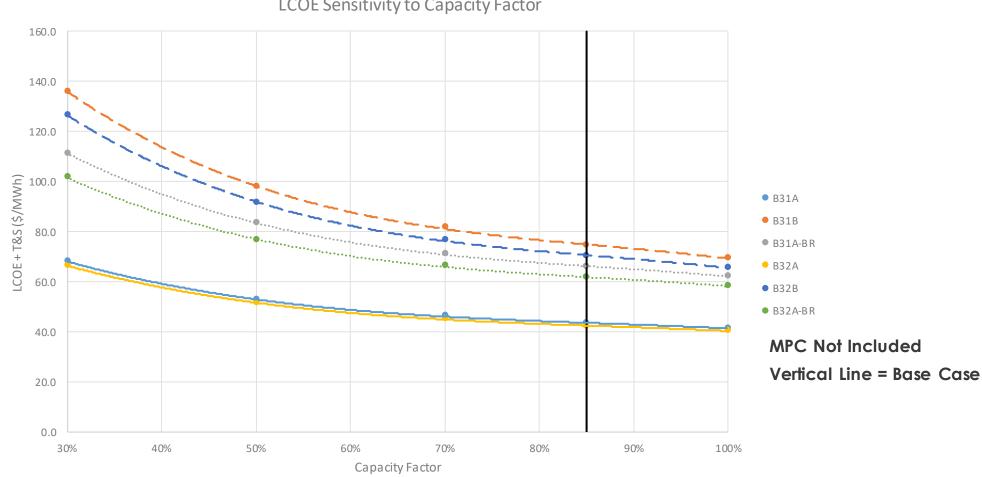
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#### Price of Natural Gas



#### Capacity Factor



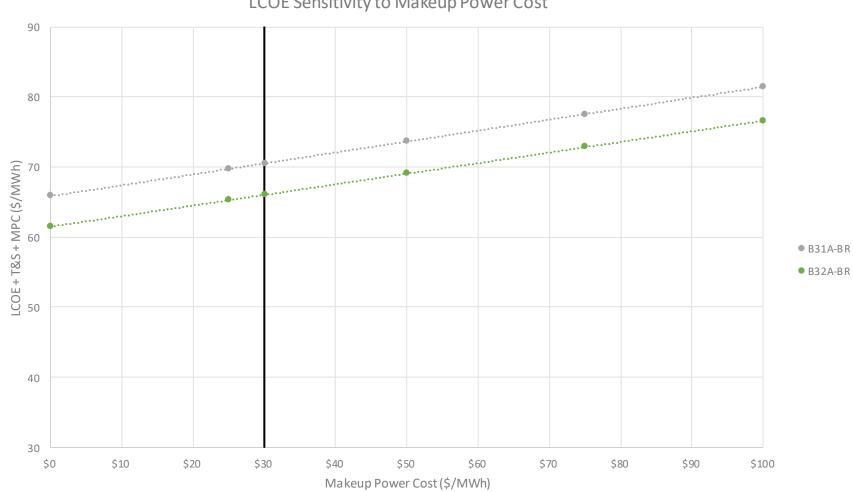


LCOE Sensitivity to Capacity Factor



#### Makeup Power Cost









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## Current work



- Updating Carbon Capture Retrofit Database to reflect this report
  - Incudes update to NGCC, PC and Industrial Database
- Analogous retrofit reports for Industrial and PC under review/development



## **Acknowledgements**



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