Development of Hybrid Polymer Membranes for Direct Air Capture of Carbon Dioxide

Project Number: DE-FE0031968

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Program Overview

- a. Funding: DOE \$799,985 and Cost Share \$200,001
- b. Overall Project Performance Dates: 01/01/2021 06/30/2022
- c. Project Participants: InnoSense LLC (Torrance, CA) and University of Utah (Salt Lake City, UT)
- d. Overall Project Objectives: Develop hybrid polymer membrane capable of direct air capture (DAC) CO₂ separating from ambient air at a low cost (low hundreds in \$) per metric tonne by 2030

Technology Background

- Carbon dioxide (CO₂), captured directly from ambient air, is a leading method for carbon management and reducing greenhouse gas emissions
- A recent study estimates that primary processes envisioned for large-scale CO₂ capture from ambient air can cost \$94–\$232 per metric tonne
- Current methods of DAC CO₂ separation from ambient air (~0.04%) are intrinsically inefficient due to:
 - Thermal energy losses
 - Large footprint
 - Degradation of sorbent materials
- Sorbents and solvents used in the DAC process have many disadvantages:
 - Need to build a very large structure
 - High cost and complexity of regenerative systems
 - Loss of moisture in dry environments

Technical Approach / Project Objectives

The overall objective of this project is to develop a disruptive DAC CO₂ separation system using a hybrid polymer membrane (HypoMem) from ambient air to reduce CO₂ separation costs and energy penalties.

Step-by-step processes for developing HypoMem



Project Technical Objectives

Objective 1. Formulation and Processing of Functional Polymer Materials for the Development of Hybrid Polymer Membrane (HypoMem).

Objective 2. Development and Characterization of HypoMem Samples for Determining their Physical, Morphological and Mechanical Properties.

Objective 3. Laboratory-Scale Testing and Evaluation of Flat and Stack HypoMem Sample Performance Under Simulated Air to Demonstrate Potential for DAC CO₂ Separation from Ambient Air at a Reduced Cost.

Technical Approach/Project Scope

Current project process of HypoMem based DAC CO₂ separation system



Technical Approach/Project Scope

An overall process of HypoMem based DAC CO₂ separation system



Team and Facilities

InnoSense LLC Team



Maksudul M. Alam, PhD Principal Investigator



Adrien Hosking, MS Design & Formulation Scientist



Thomas Saremi, BS **Research Engineer**

University of Utah Team



Professor Milind Deo, PhD Subaward Project Director

Differential Scanning Calorimetry (DSC)



Progress and Current Status of Project

Project Team working strategically towards Project Objectives

- Selected desired functional polymers that are selective toward CO₂
- Fabricated large flat and stacked HypoMem samples
- Characterized HypoMems through FT-IR and SEM analysis
- Constructed an on-site gas permeation testing set-up
- Measured the permeance, permeability, and CO₂/N₂ selectivity of HypoMem samples
- Began process simulation to model the HypoMem in application

Flow Diagram for Fabricating Flat and Stacked HypoMem Samples

Flow diagram shows the fabrication steps for large flat HypoMem samples



Preparation of Active Polymer Layer

Consistently fabricated active polymer layer for HypoMem samples



- 1. Disperse and dissolve PA and PBI polymers in *N*-methylpyrrolidone (NMP)
- 2. Add functionalized nanomaterials such as GO to increase permeability and selectivity of CO₂
- 3. Filter with syringe and cast onto large glass substrate. Generate polymer membrane layer with doctor blade. Dry and anneal under heat (~70 °C) to remove solvent.

Preparation of Epoxy Resin Support Layer





Submerge in Water



Lift off Membrane from Substrate





Fabrication of large flat HypoMem samples



Figure: Preparation of HypoMem films applying epoxy resin on large glass substrate: (**A**) Carbon veil placed on annealed active polymer membrane; (**B**) Epoxy resin formulation drop cast and diffused on the carbon veil; and (**C**) Fully annealed tri-layered polymer membrane showing support layer side.

- 1. Create epoxy resin support layer solution standardized based on carbon veil area with a targeted ratio of polyethylene glycol (PEG)200 to bisphenol A diglycidyl ether (BADGE) to methylene-bis(cyclohexylamine) (MBCa).
- 2. Place carbon veil onto dried active polymer layer and then drop cast epoxy resin layer onto carbon veil.
- 3. Dry under vacuum ($\sim 70^{\circ}$ C)



Figure: Schematic of support materials

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HypoMem Preparation & Characterization

Fabricated Large Flat HypoMems characterized by distinct peaks in FT-IR Analysis

- 1. After drying the epoxy resin solution, the trilayered membrane is fabricated.
- 2. Delaminate the tri-layered membrane from the glass substrate easily by submerging in water with the thin-film lift off method (T-FLO). Store in wet conditions.

3. Characterized by FT-IR and SEM Analysis



Figure: Thin-film lift off method (T-FLO) with HypoMem samples: (**A**) Submerged in water; and (**B**) Lifted off the large glass substrate.



SEM Analysis of HypoMem Samples





Constructed On-Site Gas Permeation Testing Setup

Gas permeation testing set up evaluates, permeability, permeance and CO₂ Selectivity



Components of Gas Permeation Cell and Method for Testing

Gas permeation method and cell designed for HypoMem performance testing

With this type of setup installed, the gas permeability was calculated using Eq. 1:

$$P = 10^{10} \times \frac{VL}{P_{Permeate}ART} \times \frac{dp(t)}{dt}$$
(1)

where, *P* is the gas permeability across the membranes (in Barrers) [1Barrer = 10^{-10} cm³ (STP) cm/cm² s cmHg], *P*_{Permeate} is the permeate pressure (in cmHg), *dp/dt* is the rate of the steady-state permeate side pressure increase (in cmHg/s), *V* is the standardized permeate volume (in cm³), *L* is the active layer thickness (in cm), *A* is the effective surface area of the membrane (in cm²), *T* is the experimental temperature (K), and *R* is the gas constant [0.278 cm³ cmHg/cm³ (STP) K]. Solving for permeance is a similar equation but does not factor in thickness of the sample *L*. Permeance *P*_{Permeance} is calculated using Eq. 2:

$$P_{Permeance} = 10^6 \times \frac{V}{P_{Permeate}ART} \times \frac{dp(t)}{dt}$$
 (2)

The ideal selectivity (α) was obtained from the ratio of permeability coefficients using Eq. 3:

$$\alpha_{A/B} = \frac{P_A}{P_B} \times \frac{P_{CO2}}{P_{N2}}$$
(3)

where, P_A and P_B are the permeability coefficients of the pure gases CO_2 and N_2 , respectively.



Figure: The component parts of the permeation cell at ISL: (A) Exploded view of the permeation cell; (B) Closed permeation cell; and (C) Open permeation cell showing components.

HypoMem's Membrane Performance: CO₂ Permeance



Test Conditions:

- Membrane diameter of 1 cm, active layer thickness of 9.0 μ m, and epoxy layer thickness ~ 225 μ m,
- Feed flow rate of 0.172 ml/s for both CO₂ and N₂ gases,
- Ambient temperature conditions and fixed upstream condition 75.9 cm Hg (101kPa),

Higher permeance value observed for CO_2 (6.83*10⁵) than N_2 (2.15*10⁵) for a pressure drop across the membrane of 70 cm Hg (~95 kPa)

HypoMem's Membrane Performance: CO₂ Selectivity



- Observed CO₂ selectivity value of 3.17 at permeance of 6,830 GPU for a pressure drop across the membrane of 70 cm Hg (~95 kPa)
- Determined CO₂ selectivity values by varying the permeance via different feed flow rates and active layer thicknesses
- Observed a trend of an increase in selectivity with a decrease permeance or permeability

Computer Simulation and Modeling on Direct Air Capture Membranes

Simulation of HypoMem membrane performance model will guide future work

- Material balances on species and permeance calculations were performed to establish the membrane outlet characteristics
- Given certain operational parameters, the permeate and the retentate compositions are fixed
- flow rates (volumetric and molar) for the species are dictated by their partial pressure differences between the outlet and the inlet
- The outlet concentration of CO₂ in the permeate is a function of the inlet concentration, the inlet and the outlet pressures, and the membrane selectivity
- The total throughput through the membrane is governed by its GPU and area.
- The parameters are adjusted so that the retentate CO₂ concentration is about the pre-industrial 300 ppm
- Reaching a selectivity of 10 at permeance of 10,000, a permeate CO₂ concentration of 7560 ppm can be achieved



Base Case CO₂ Separation Parameters Used for Illustrative Calculations

CO ₂ Separation Parameters	Value
Upstream Pressure (kPa)	100
Downstream Pressure (kPa)	2
Initial CO ₂ Concentration (mole fraction)	0.0004
Selectivty CO ₂ /(Other)	30
Membrane Permeance (GPU)	10000
Membrane Area (cm ²)	5

Characteristics of All the Streams for Base Case CO₂ Separation

Streams	Feed			Permeate			Retentate		
Species	Total	CO ₂	Other	Total	CO ₂	Other	Total	CO ₂	Other
Concentration (ppm)	1000000	400	999600	1000000	7560	992440	1000000	309	999691
Flow Rates (ml/s)	10	4.000E-03	9.996	0.125	9.480E-04	0.124	9.878	3.052E-03	9.875

Computer Simulation and Modeling on Direct Air Capture Membranes

Some Basic Considerations for HypoMem Simulation

- Since the starting concentration is low (~400 ppm), multistage separation is essential
- Each stage is operated under vacuum
- The process is usually designed to maintain a concentration of 300 ppm in the retentate (preindustrial concentration of CO₂)
- CO₂ purity of about 50% possible after three stages
- Permeate concentration dependence
 - Pressure ratio (upstream to downstream for each stage)
 - Selectivity
- Throughput
 - Combination of flowrate, GPU and membrane area



- In stage 1, increased selectivity has minimal impact on the permeate CO₂ concentration
- In stage 2, increased selectivity has a moderate impact on the permeate CO₂ concentration
- By stage 3, increased selectivity has a strong impact on the permeate CO₂ concentration

Plans for Future Development

- In this project
 - Continue developing HypoMem samples modifying composition, active layer thickness, and fabrication processes such as thin-film lift off (T-FLO).
 - Continue conducting gas permeation testing on HypoMem samples.
 - Optimize permeance, permeability, and CO₂ selectivity performance.
 - Perform basic level Techno-Economic Analysis (TEA), Technology Gap Analysis, and Environmental Health and Safety Risk (EH&S) Assessment.
- After this project
 - Optimize fabrication processes for large size membrane and scaleup production.
 - Prototype development and field level testing for DAC CO₂ separation from ambient air.

Summary

- Formulated and fabricated hybrid polymer HypoMem samples with reasonably large size (~8 by 12 cm).
- Verified consistent thicknesses and morphologies of both active polymer layer and epoxy support layer by SEM.
- Constructed an on-site gas permeation testing set-up utilizing a standard constant-volume/variable-pressure test method.
- Observed higher permeance values: 6.83*10⁵ GPU for CO₂ and 2.15*10⁵ GPU for N₂ at a pressure drop across the membrane of 70 cm Hg (~95 kPa).
- Observed CO₂ selectivity value of 3.17 at permeance of 6,830 GPU at a pressure drop across the membrane of 70 cm Hg (~95 kPa)
- Observed a trend of an increase in selectivity with a decrease permeance or permeability
- Computer simulation suggested that multi-stage process is required to achieve the desired CO₂ permeate concentration for successful
 DAC CO₂ separation









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