



# Damage Accumulations Predictions For Boiler Components Via Microstructurally Informed Material Models

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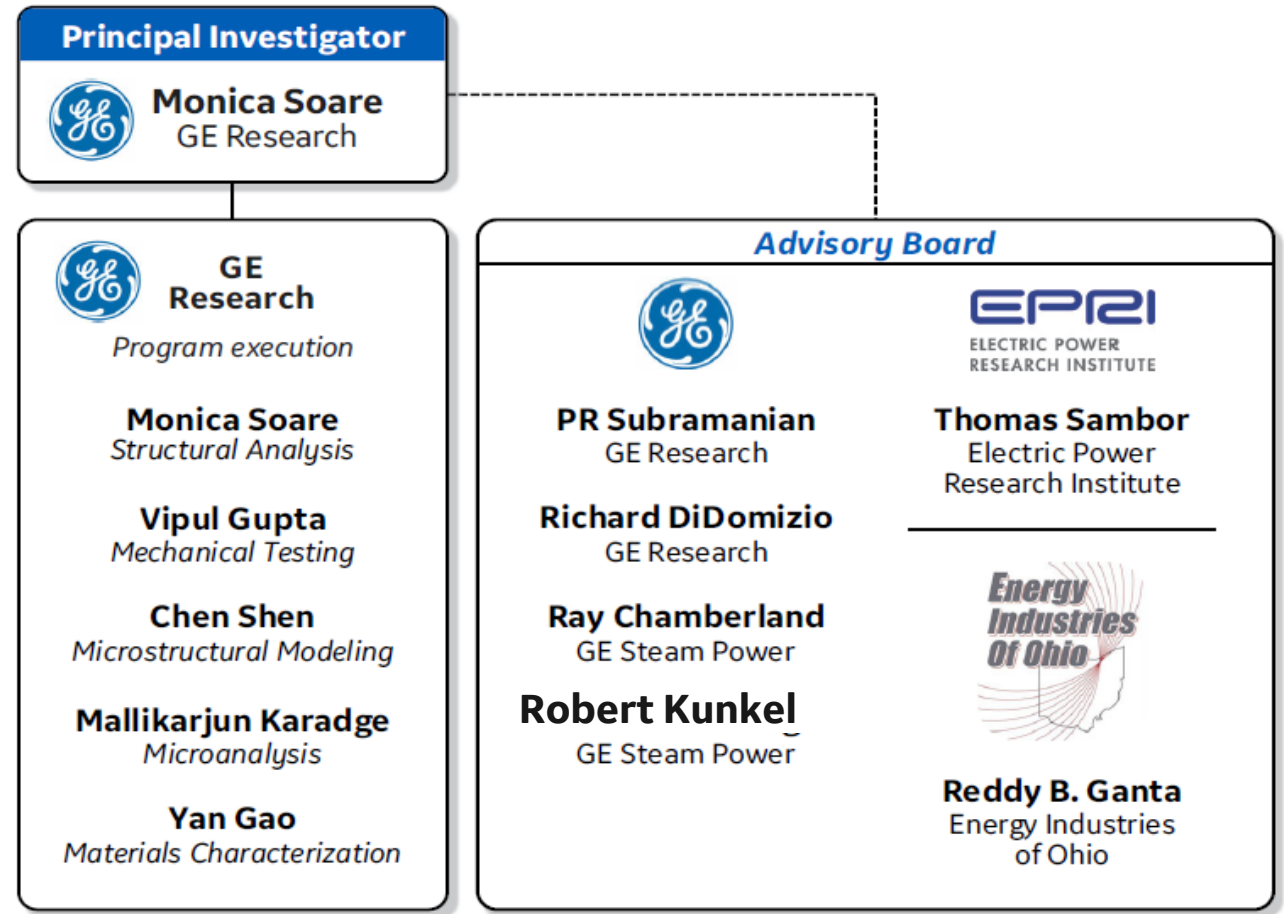
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# Summary

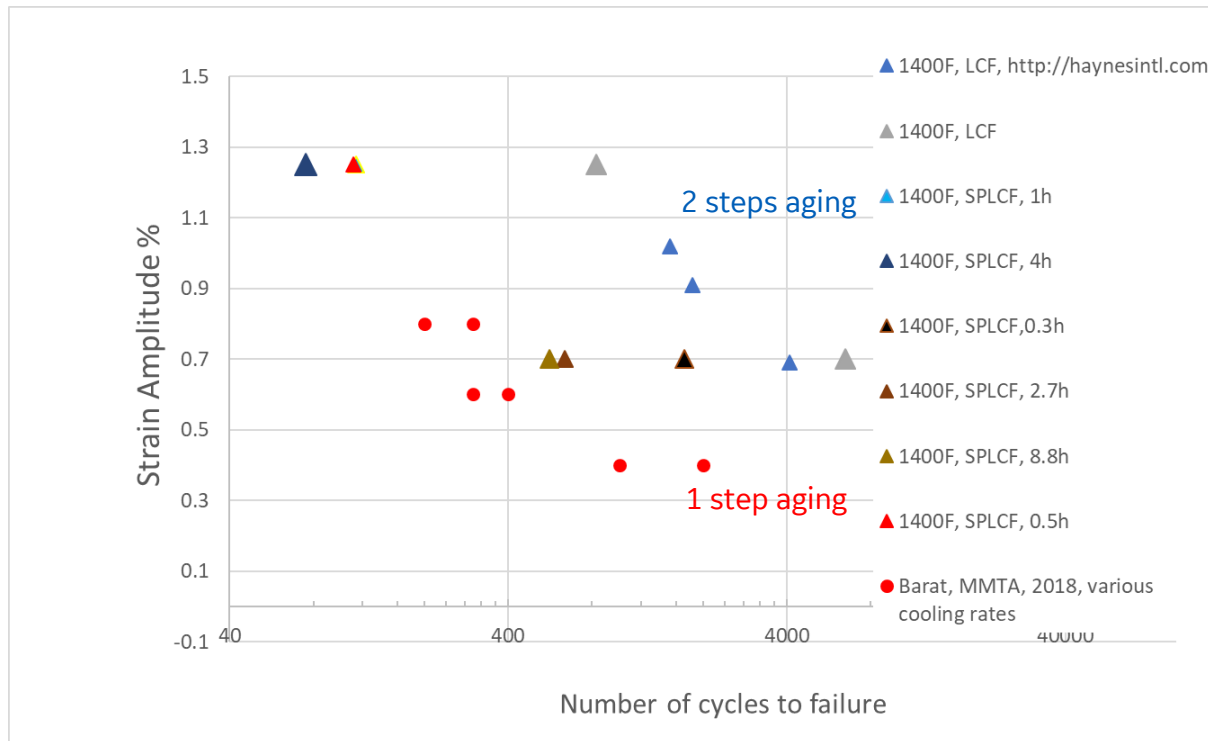
- ❑ Technical background of the project
- ❑ Potential significance of the results of the work
- ❑ Statement of project objectives
- ❑ Technical approach to achieving the project goals
- ❑ Conclusions and next steps



# Technical background of the project

Develop physically informed models to capture degradation and predict durability of Nickel-based superalloys during cyclic operations in fossil energy (FE) USC and A-USC power plants components where thermo-mechanical fatigue and creep damage are occurring at the same time. 300,000h operation

- 1100 °F to 1400 °F/ Haynes 282/ Boiler headers



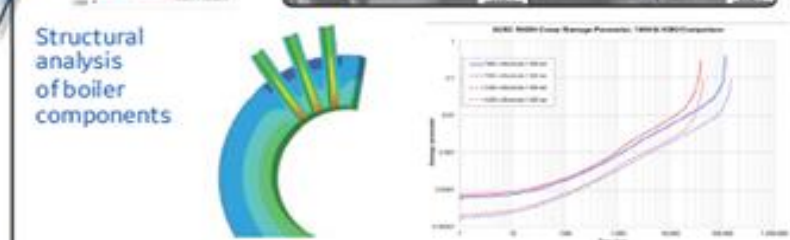
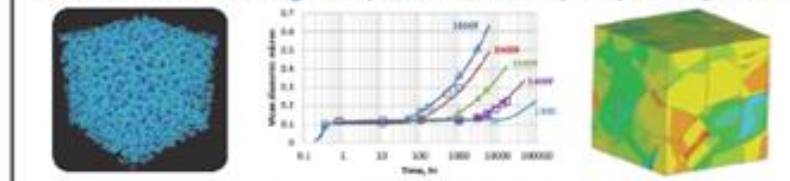
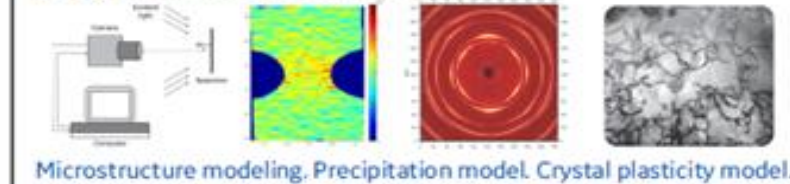
## Relevant Prior Work

- DOE modeling creep-fatigue-environment interactions for A-USC steam turbine rotor materials
- DOE modeling long-term creep performance of welded Ni-based superalloy structures for power generation systems
- DOE modeling creep behavior of ComTest-AUSC thick-walled header
- GE microstructure based lifing technology
- GE materials design acceleration tools

## A 3-Year, \$937,500 Program to Develop Damage Accumulation Predictions for Boiler Components via Microstructurally Informed Material Models

**Program Objective:** Develop High Fidelity Materials Models for Ni-based Alloys under cyclic and longterm creep loadings

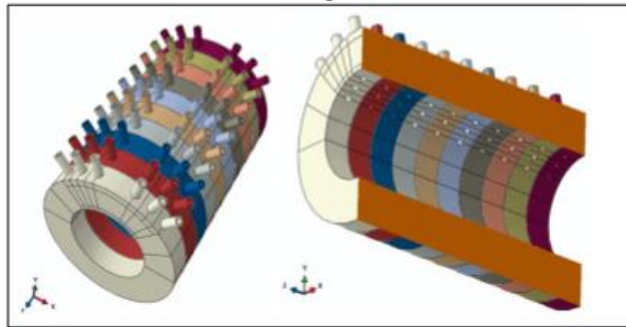
State-of-the-art experimental methods: strain mapping, diffraction patterns using high energy synchrotron, dislocation activity captured using transmission electron microscopy.



# Potential significance of the results of the work. Boiler Applications



Shingledecker et al, 2013



Schrecengost, 2017

Boiler headers	USC	A-USC
Max T/P	1100F/25-30MPa	1400F/35MPa
Challenge	LCF	LCF & Creep
Selected material	9-12%Cr Steel, Ni-based superalloy may allow thinner designs	Ni-based superalloy

- Estimate remaining life & durability predictions for boiler components (USC and A-USC power plants)
- Accelerate the qualification of new materials for boiler and steam components (A-USC power plants – higher efficiency, carbon reduction)
- Enabling thinner designs (USC power plants)
- Enable more flexible conditions – more frequent cycles (USC Power plants)
- Model transferrable to other superalloys – 740H, N105

# Statement of project objectives

- Provide physically informed models, capturing the microstructural changes taking place in the industrial components under cyclic loading and exposure to high stress and temperature for long operating life

## Task 2. 2020-2121

### Develop Quantitative Understanding of Microstructure Evolution, Deformation and Damage Mechanisms of H282

- 2.1. Perform High Temperature Tensile and Isothermal Low Cycle Creep-Fatigue Tests
- 2.2 Perform Cycling Loading Tests at the Advanced Photon Source (APS)
- 2.3. Perform Thermo-Mechanical Fatigue Tests
- 2.4. Characterize Microstructures of Test Specimens from Sub-Tasks 2.1, 2.2 and 2.3

## Task 3. 2020

### Perform Microscale Modeling of Microstructure and Strain Evolution

- 3.1. Perform Modeling of the Rate of Precipitation and Growth of Gamma Prime Particles in the Haynes 282 Microstructure
- 3.2. Perform three (3) Dimensional Crystal Plasticity (CP) Modeling of Haynes 282

## Task 4. 2020-2021

### Develop Continuum Damage Mechanics (CDM) Model of Haynes 282

- 4.1. Develop CDM Model Framework
- 4.2. Calibrate, Validate and Document the CDM Model Framework
- 4.3. Integrate CDM Model Framework into Finite Element Analysis Software
- 4.4. Couple Transient Thermal Analysis to CDM Model Framework in Finite Element Analysis Software

## Task 5. 2021-2022

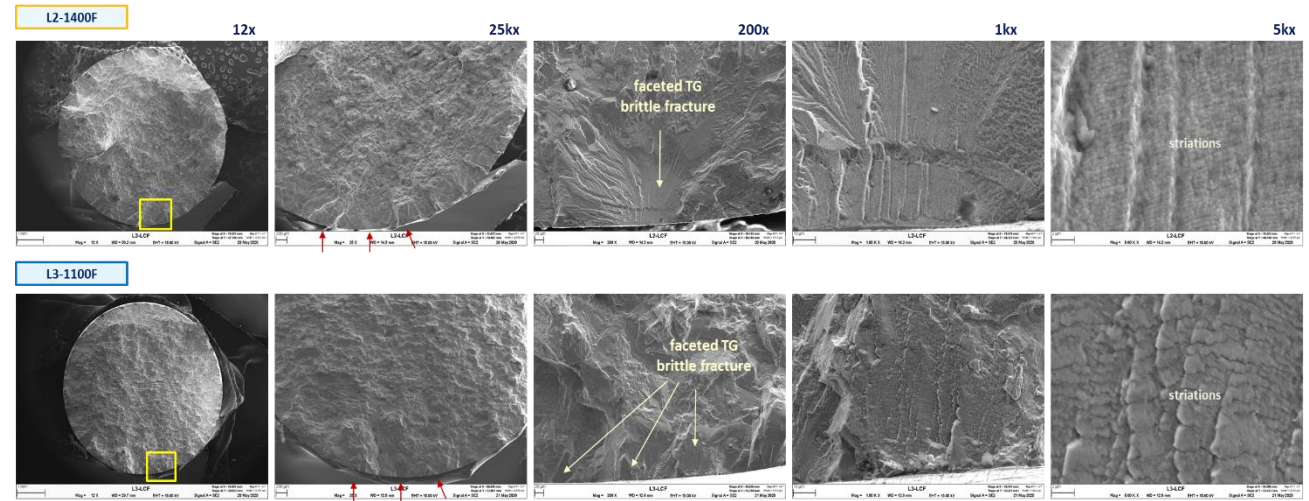
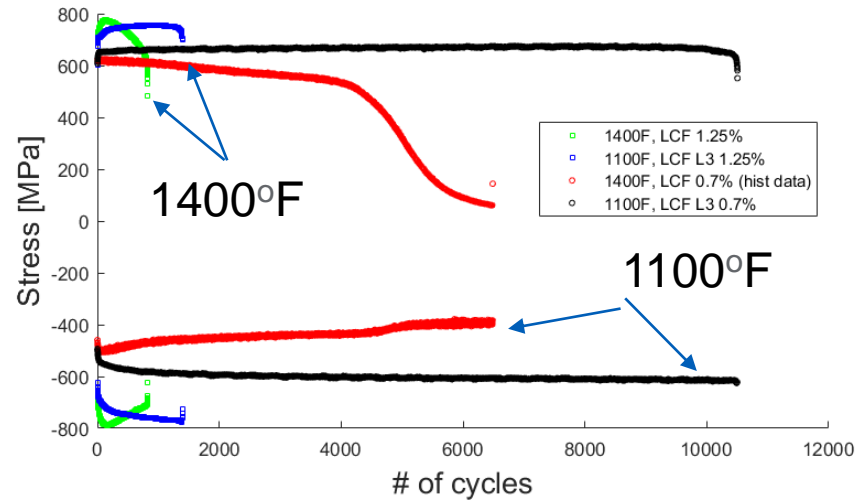
### Perform Structural Modeling of a Thick Wall Boiler Component

- 5.1 Perform Baseline CDM Analyses of a Thick Wall Boiler Component
- 5.2. Perform Damage Sensitivity Studies on a Thick Wall Boiler Component



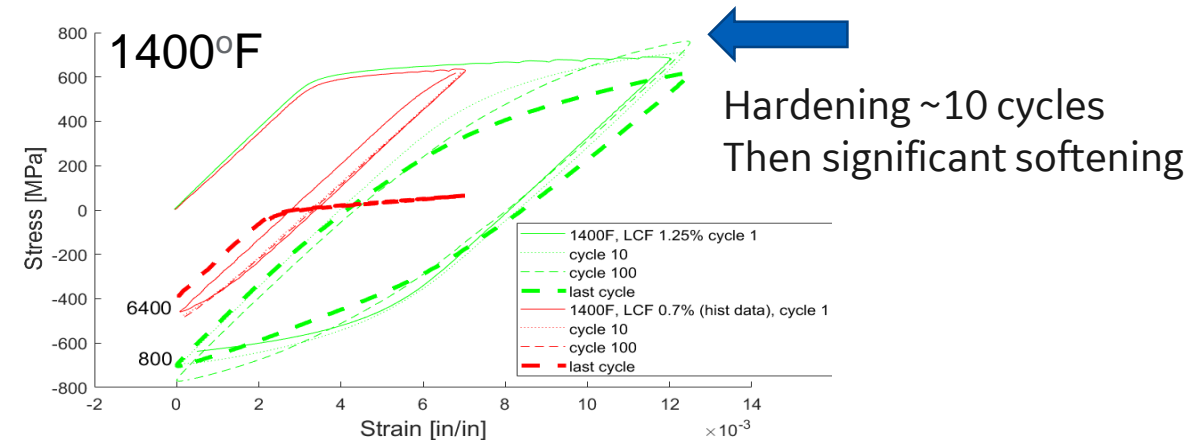
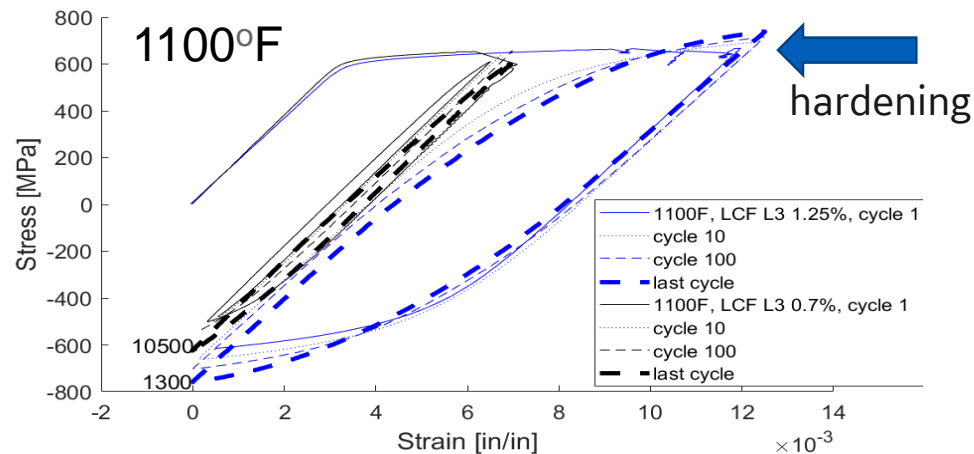
## Task 2. Mechanical Testing

LCF tests at 1100°F and 1400°F. 1.25% strain amplitude vs 0.7% strain amplitude



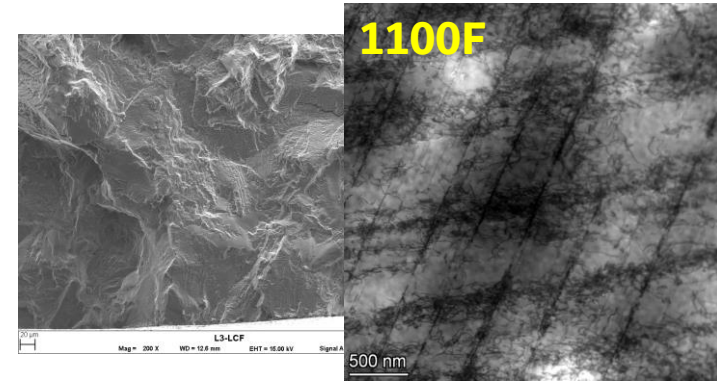
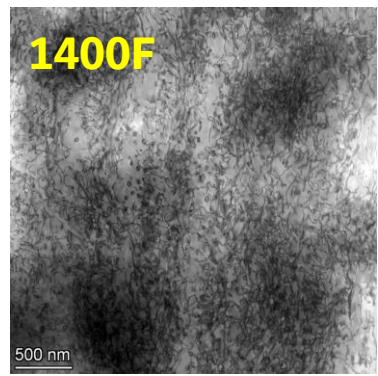
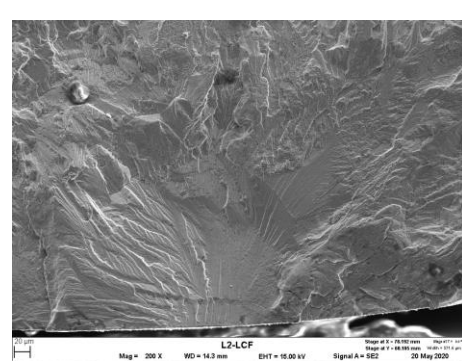
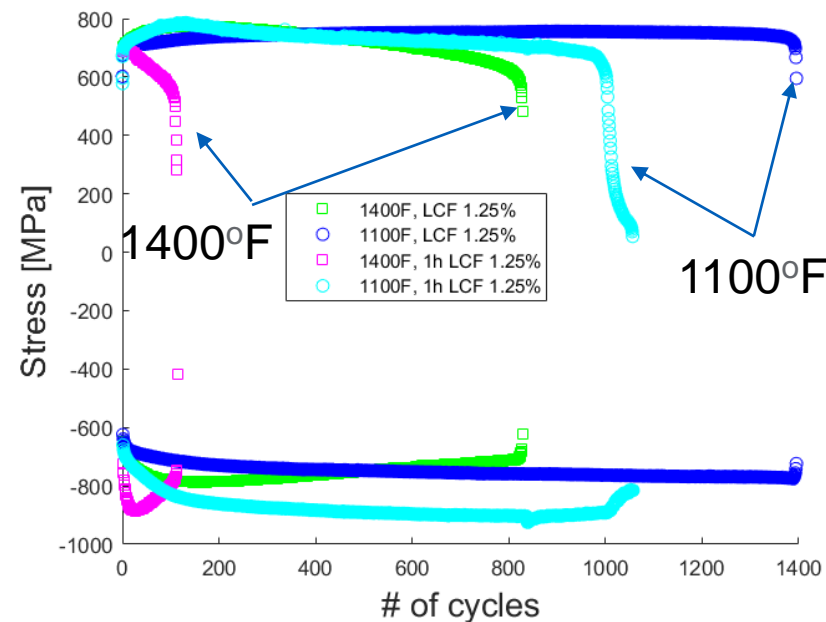
At 1.25% strain – crack propagation time – very small compared with crack initiation time

First, 10<sup>th</sup>, 100<sup>th</sup> and last stress-strain cycles at 0.7% and 1.25% strain amplitudes



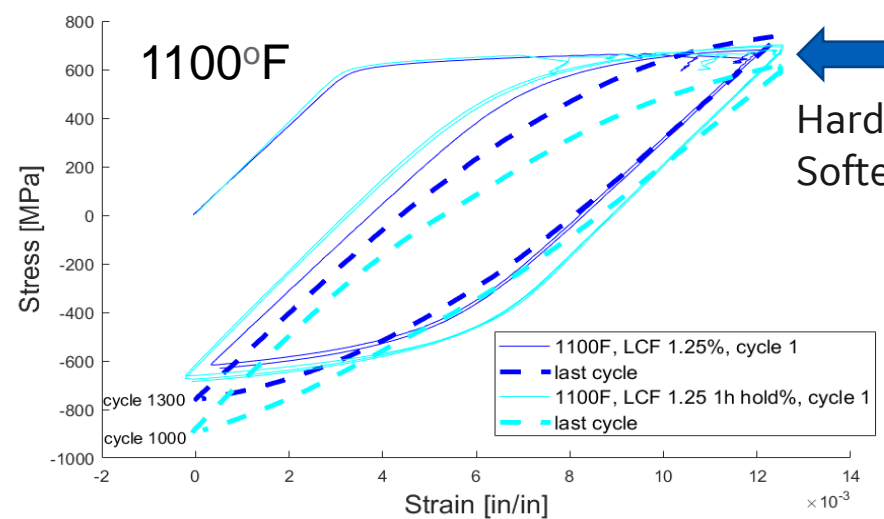
# Task 2. Mechanical Testing

Pure LCF tests compared with 1-hour SPLCF at the maximum strain at 1100°F and 1400°F

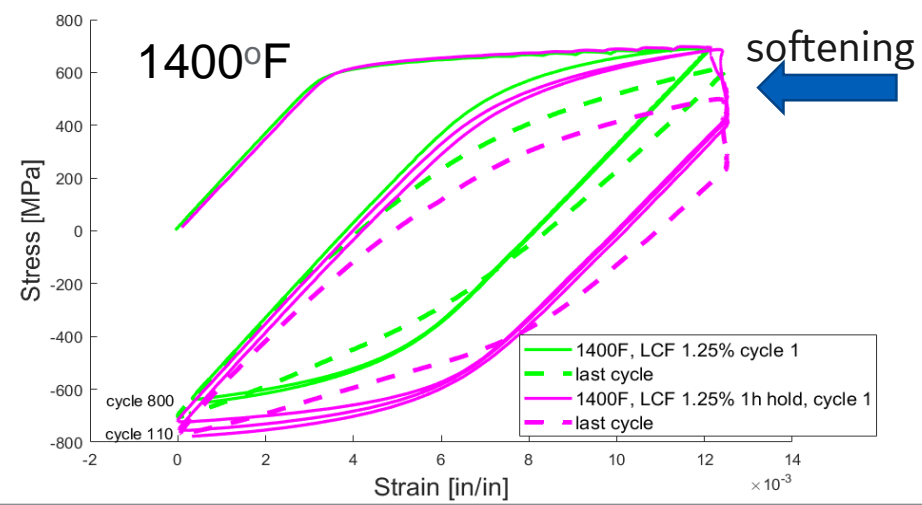


Homogeneous deformation  
Faceted crack initiation

Localized deformation  
Faceted crack initiation

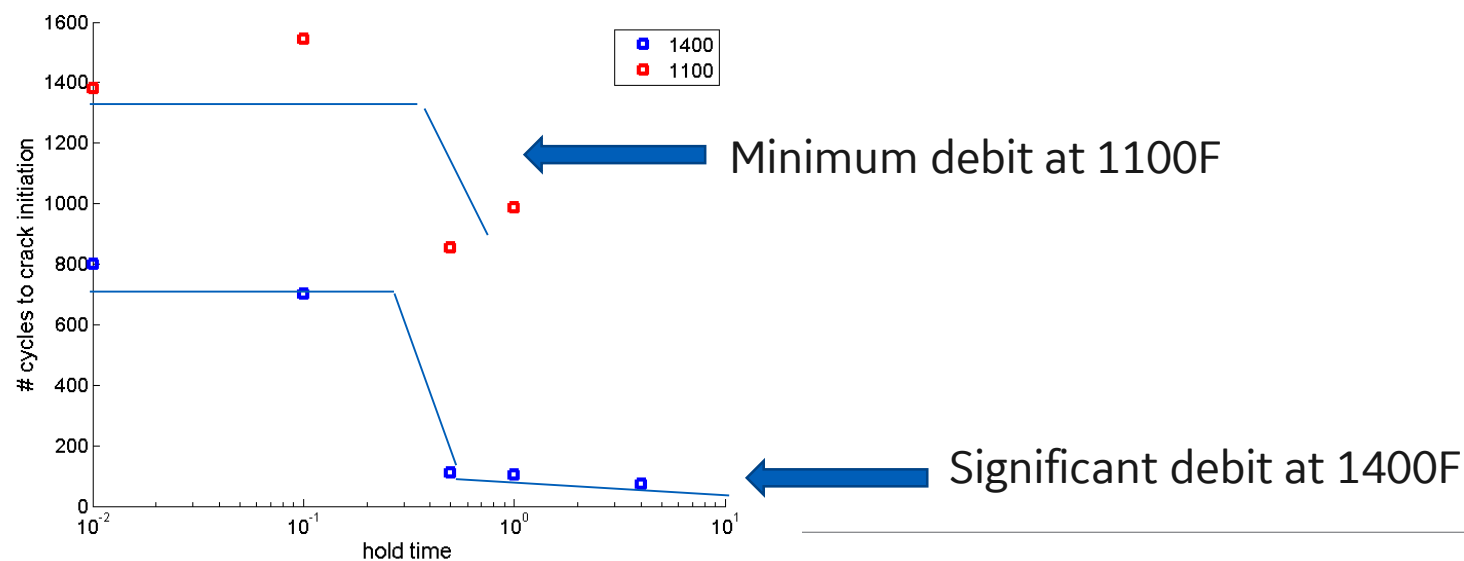
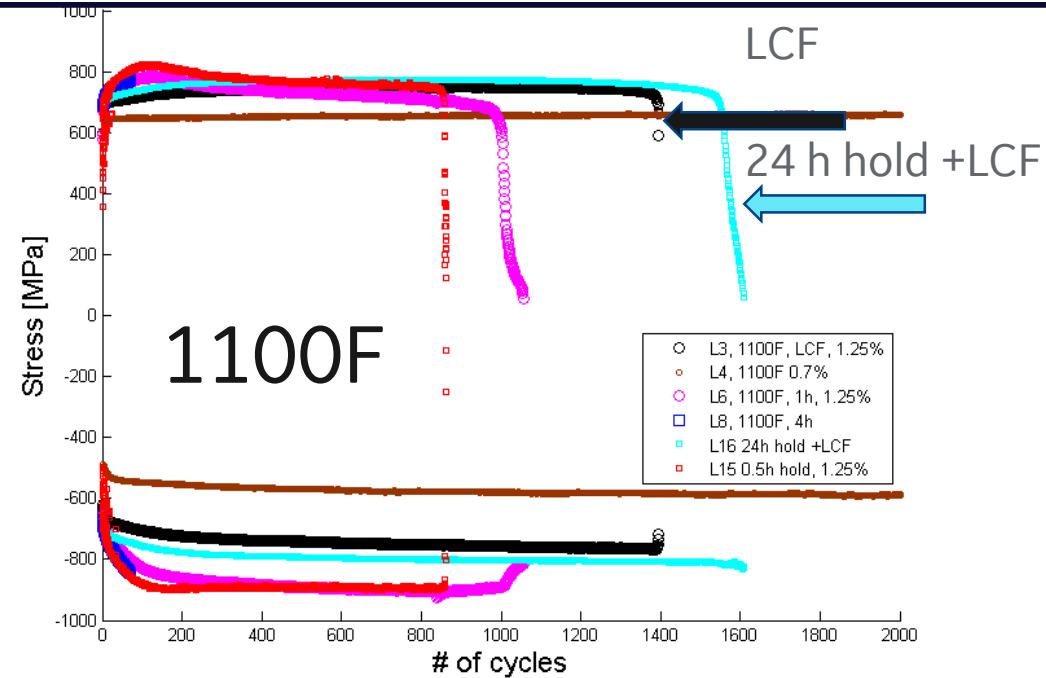
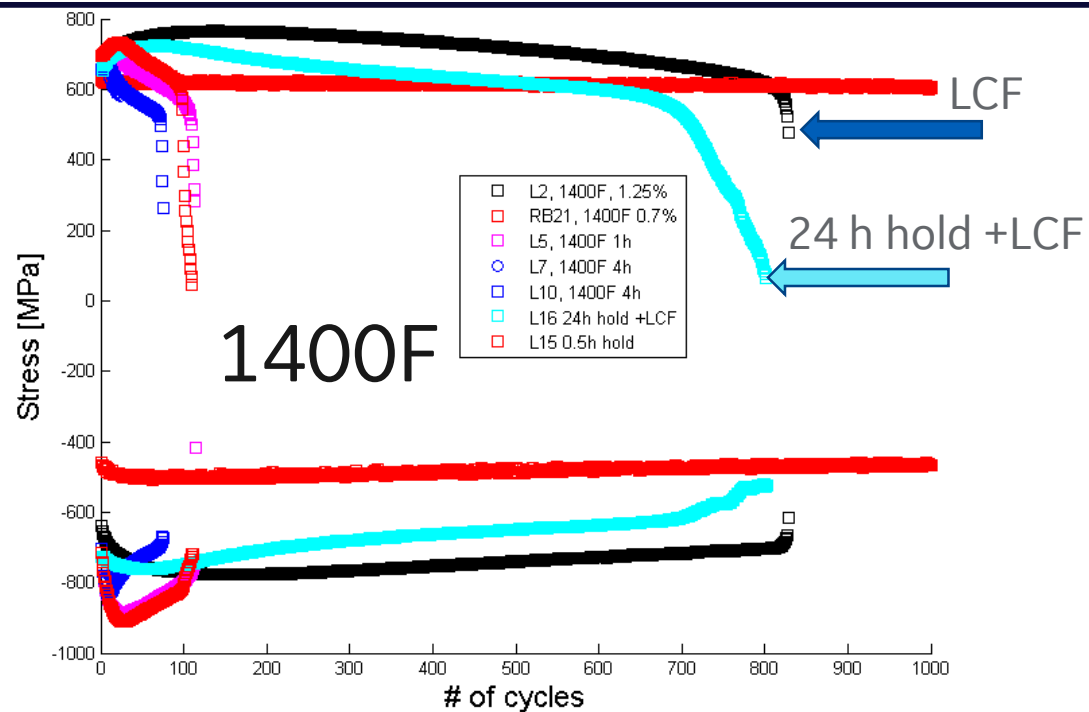


Hardening @ pure LCF  
Softening @ hold time LCF



## Task 2. Mechanical Testing

### Effect of hold time on number of cycles to crack initiation

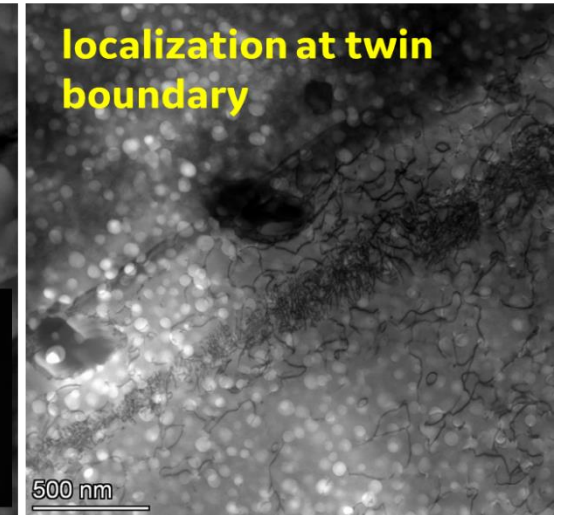
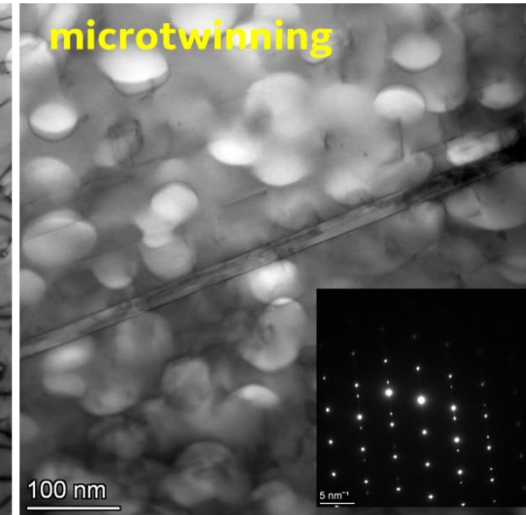
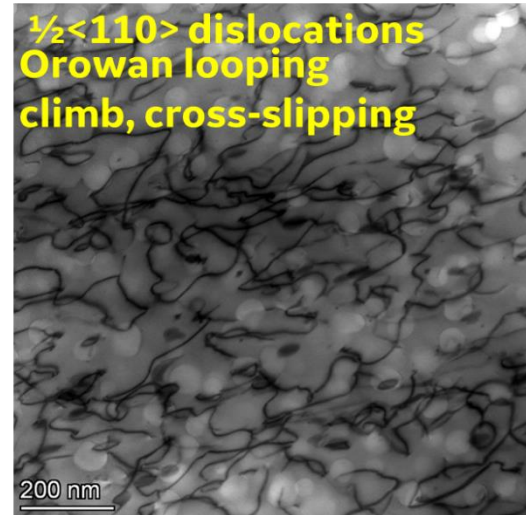


## Task 2. Mechanical Testing

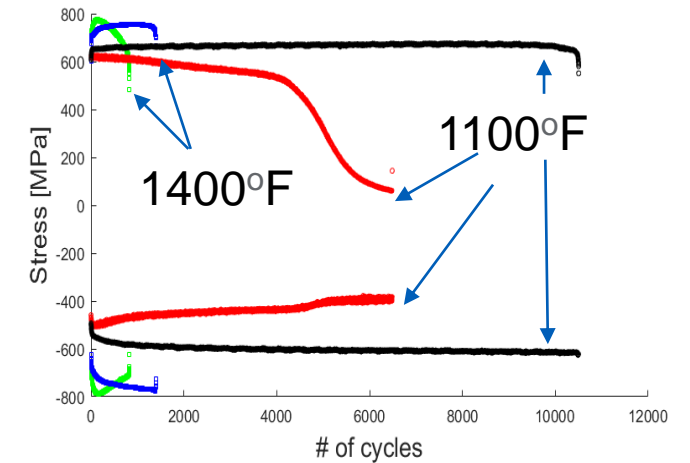
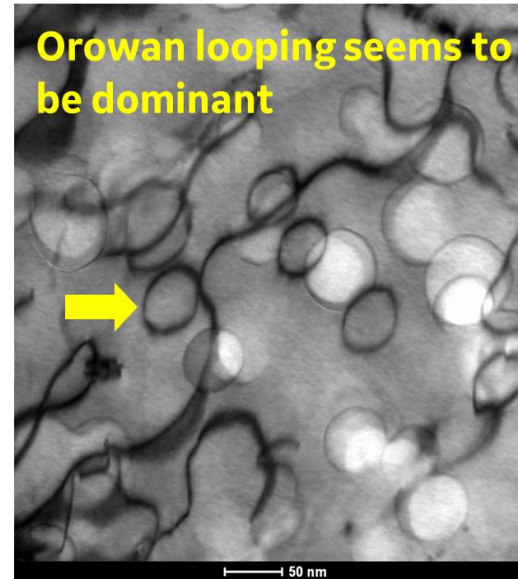
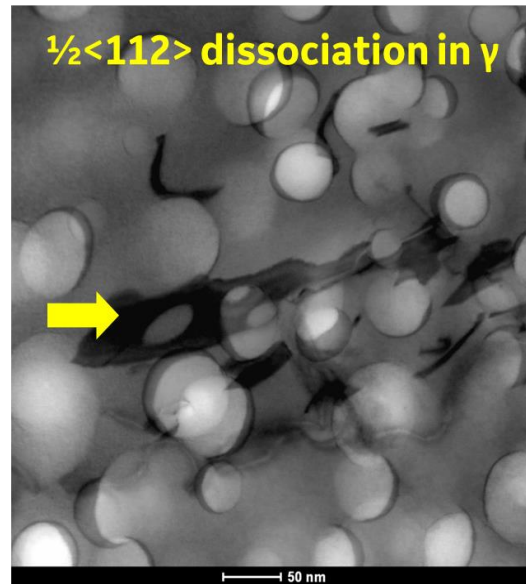
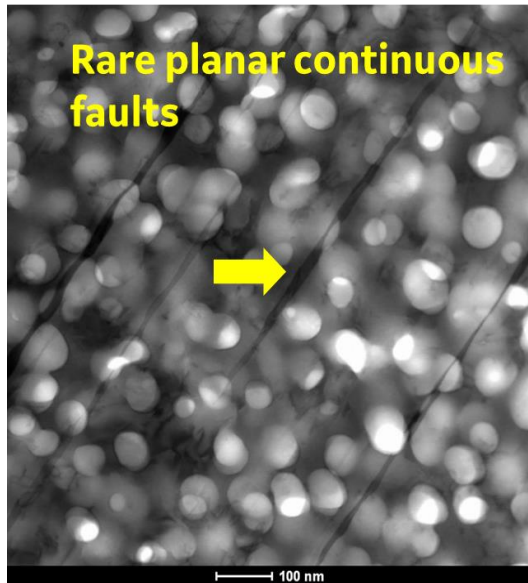
### 1400F SPLCF-1h, 1.25%max/114 life hours

Deformation mechanisms understanding

- Dislocation-dislocation
- Dislocation-precipitate interactions



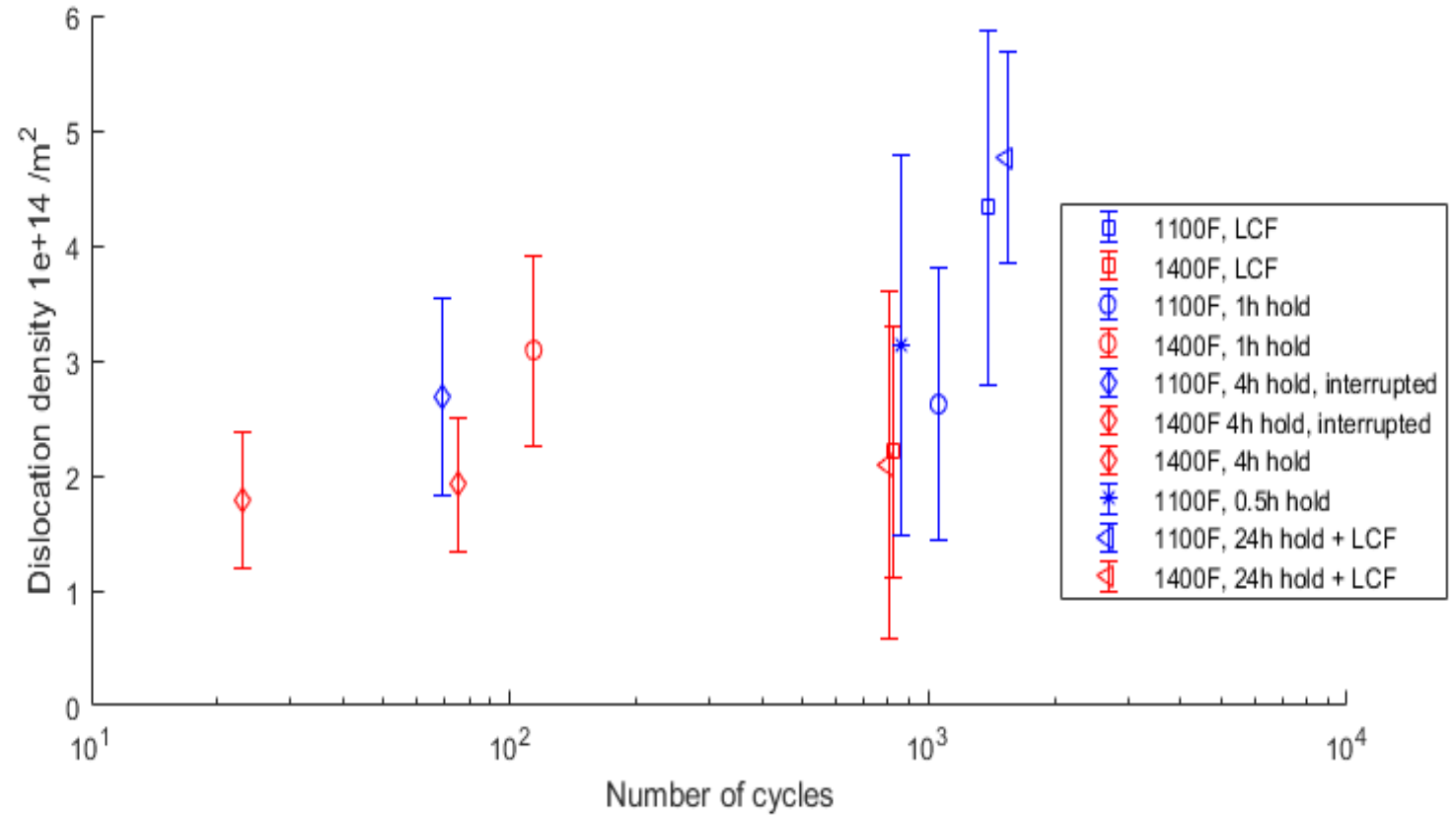
### 1100F SPLCF-1h, 1.25%max/1056 life hours



## Task 2. Mechanical Testing

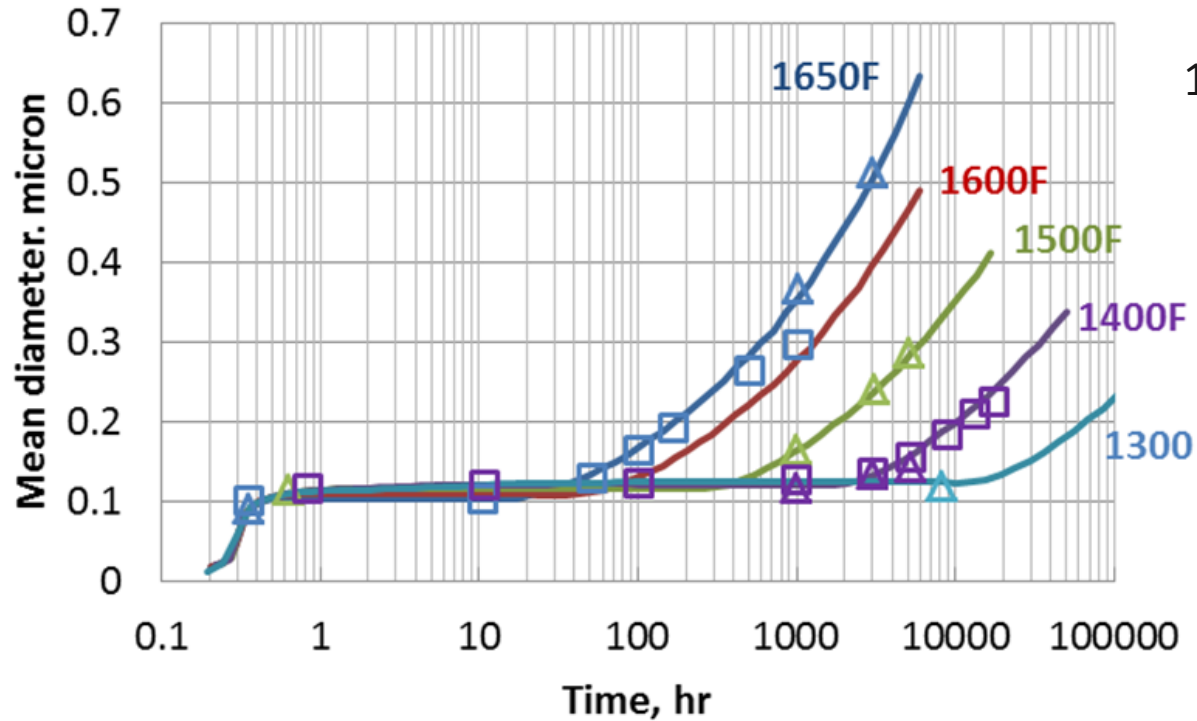
### Dislocation Density Measurement

Specimen Number	Type of test	Temperature F	Max Strain %
L2	LCF	1400	1.25
L3	LCF	1100	1.25
L5	SPLCF, 1h	1400	1.25
L6	SPLCF, 1h	1100	1.25
L7	SPLCF, 4h	1400	1.25
L8	SPLCF, 4h	1100	1.25
L10	SPLCF, 4h	1400	1.25
L13	SPLCF, 0.5h	1100	1.25
L16	24h hold, LCF	1400	1.25
L17	24h hold, LCF	1100	1.25



# Task 3. Microscale modeling

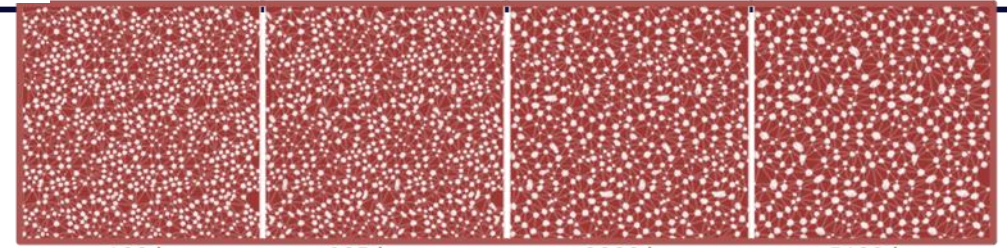
## Rate of Precipitation and Growth of Gamma Prime Particles in the Haynes 282 Microstructure



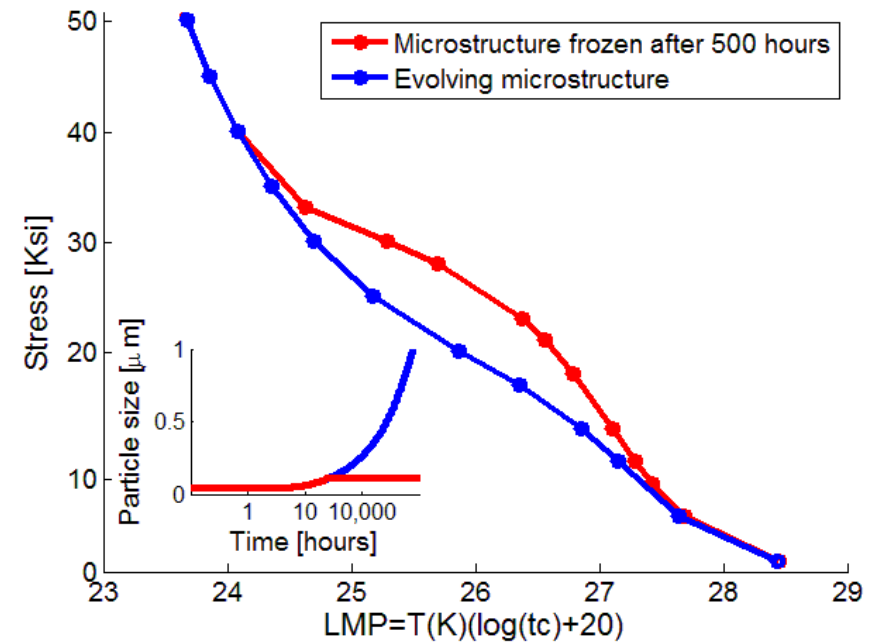
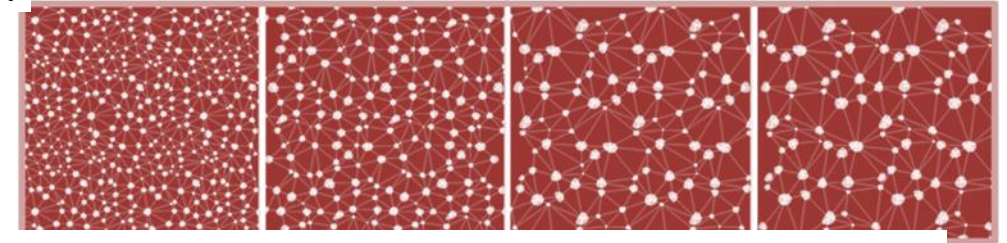
$$D^3(t) - D_0^3(t_0) = K(T)(t - t_0)$$

$$K = K_0 \exp(-Q/R_g T)$$

1400F

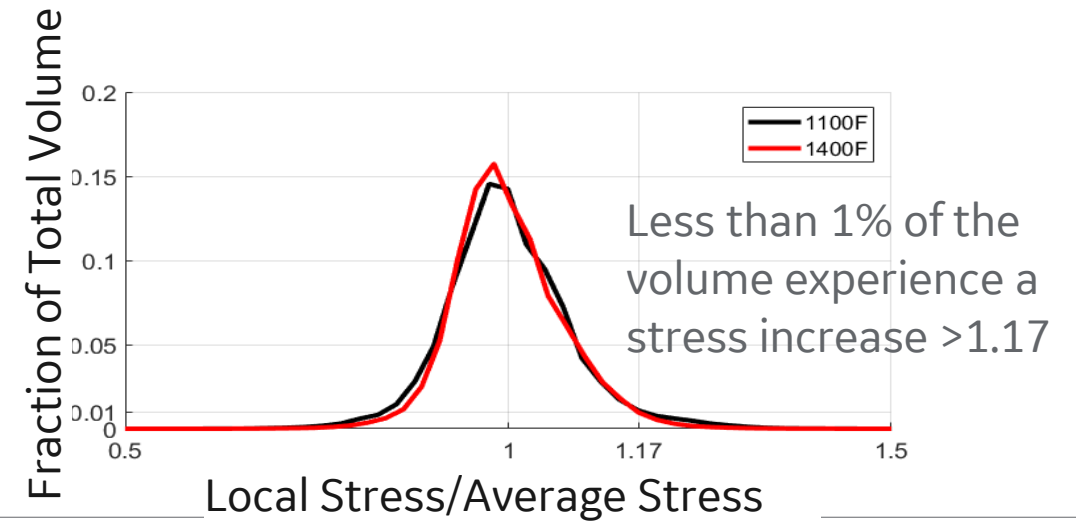
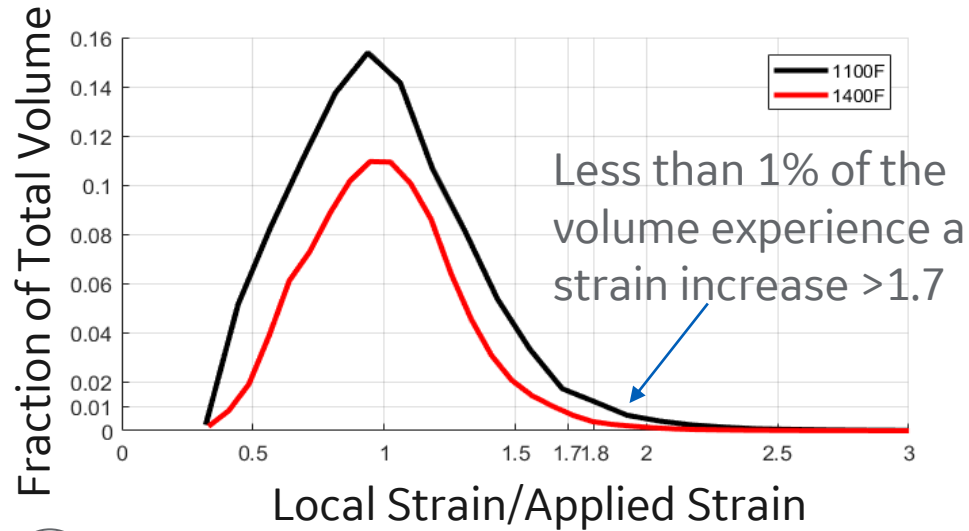
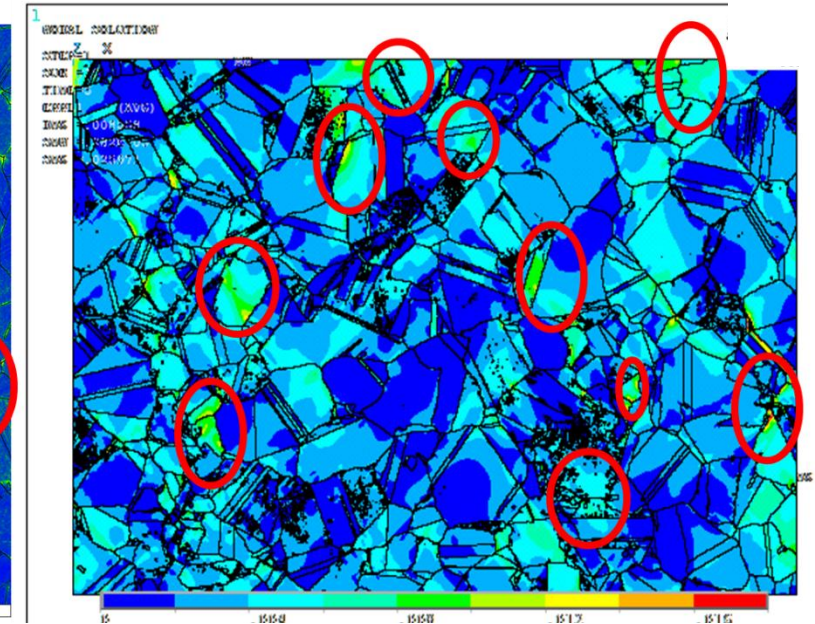
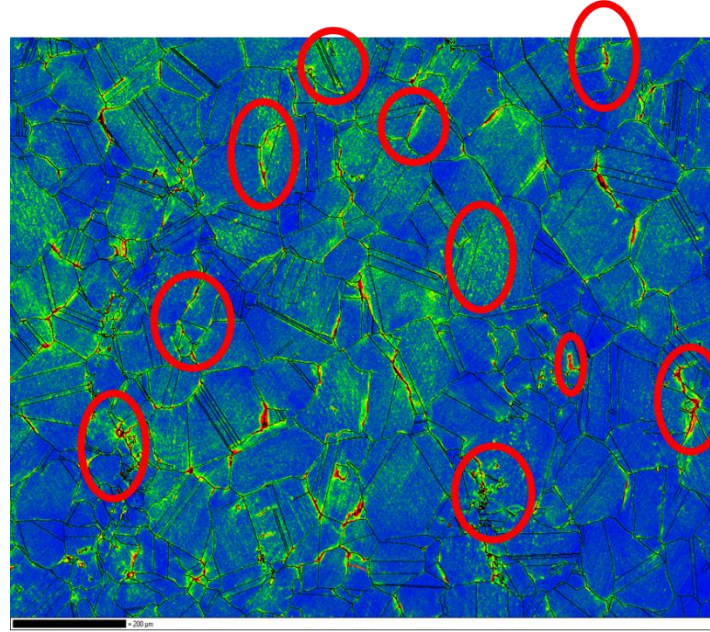
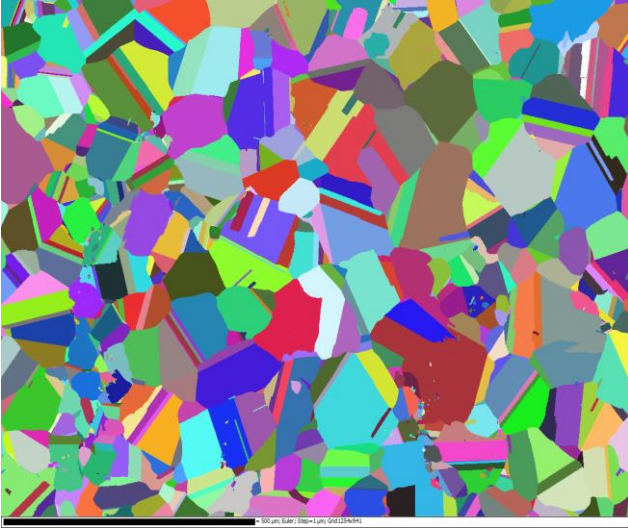


1600F



# Task 3. Microscale modeling

## Crystal Plasticity Modeling



# Task 4. Continuum Damage Mechanics (CDM)

## Creep

$$\epsilon_{cr} = \epsilon_{cr}^{eq} S^{eff}$$

Flow rule

Effective deviatoric stress

$$S_{climb} = S_0 + S_1 S^{eff-eq} (1 - \exp(-S_2 E \epsilon_{disloc}^{eq} / S^{eff-eq}))$$

Back stress due dislocation-precipitates interaction

$$\frac{d\epsilon_{cr}^{eq}}{dt} = \frac{d\epsilon_{disloc}^{eq}}{dt} + \frac{d\epsilon_{diff}^{eq}}{dt} \quad \text{Creep strain rate}$$

$$\frac{d\epsilon_{disloc}^{eq}}{dt} = A(\rho, f) \sinh \left\langle \lambda b^2 \frac{S^{eff-eq} - S_{climb}}{MkT} \right\rangle \quad \text{Dislocation strain rate}$$

$$\frac{d\epsilon_{diff}^{eq}}{dt} = f(\sigma^{eq}, D_{diff}) \quad \text{Diffusion strain rate}$$

$$D_{cr} = D_{disloc} + D_{diff} \quad \text{Dislocation + diffusion damage}$$

## Plasticity

$$\epsilon_{plastic} = \epsilon_{plastic}^{eq} S^{eff} \quad \text{Flow rule}$$

$$S^{eff} = S / (1 - D) \quad \text{Effective deviatoric stress}$$

$$\frac{d\epsilon_t^{eq}}{dt} = \frac{d\epsilon_{cr}^{eq}}{dt} + \frac{d\epsilon_{plastic}^{eq}}{dt} \quad \text{Total strain rate}$$

$$\frac{d\epsilon_{plastic}^{eq}}{dt} = \left\langle \frac{|S^{eff} - \sigma_p| - \sigma_o}{K} \right\rangle^{\frac{1}{m}} \quad \text{plastic component}$$

$\sigma_p$  - kinematic back stress

$\sigma_o$  - isotropic back stress

$$D = D_{cr} + D_{plastic} \quad \text{Total damage variable}$$

Micro structural parameters/  
Material properties: E, b, f,  $\lambda$ ...

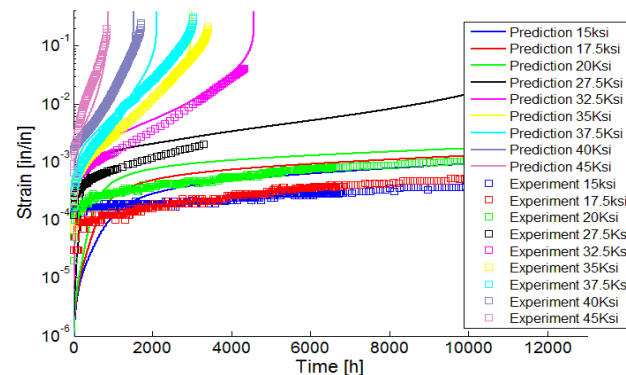
Fitted parameters

$S_0, S_1, S_2, A, K, m$ ...

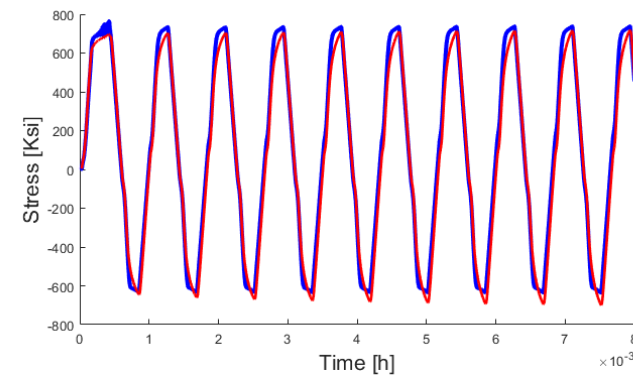
Internal variables

$\epsilon_{cr}^{eq}, \rho, D, D_{disloc}, D_{diff}, \epsilon_{plastic}^{eq}$ ...

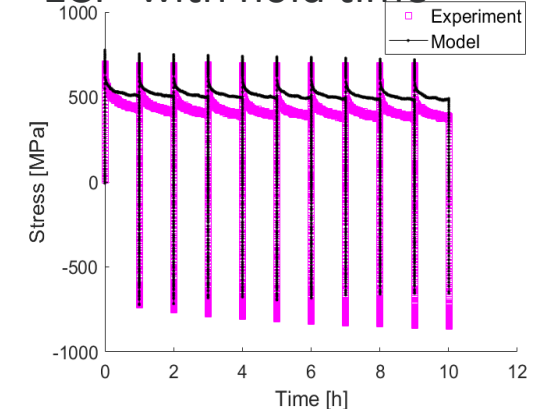
Pure creep



LCF



LCF with hold time



# Task 5. Structural Modeling of a Boiler Component

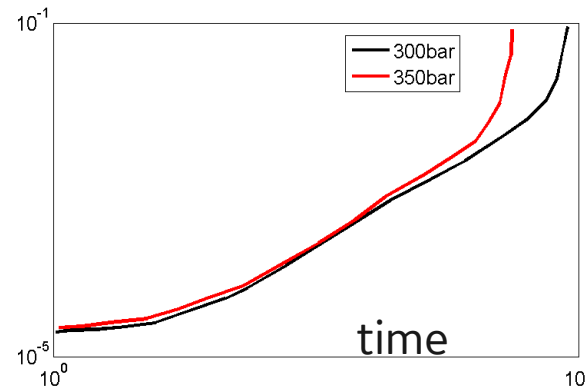
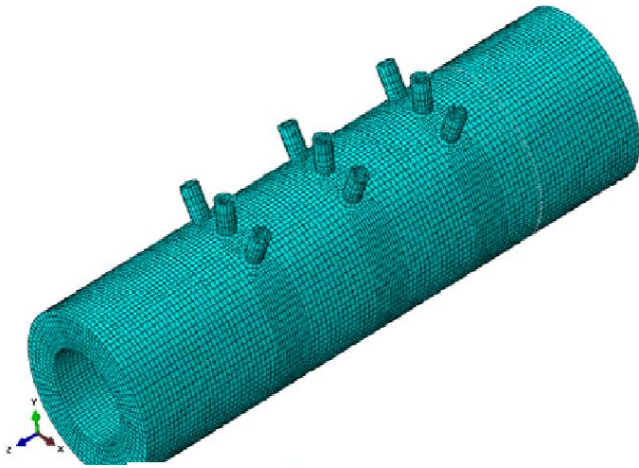
Task 4 outcome – a material model able to predict mechanical response under various loadings: pure cyclic, relaxation, creep, hold time fatigue.  
Provide limits of the damage parameters defining the failure

## ☐ Perform Baseline CDM Analyses of a Thick Wall Boiler Component

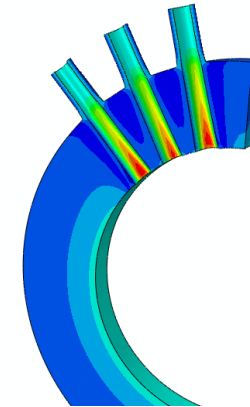
1100F (USC conditions) - benchmark configuration = Steel outlet header

1400F (AUSC conditions) –H282 alloy header

## ☐ Perform Damage Sensitivity Studies on a Thick Wall Boiler Component



Damage variable evolution and time/cycles to failure in high strain location



## Concluding Remarks

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- Performed Mechanical uniaxial tests for deformation mechanisms understanding, model development and calibration for Haynes 282 alloy (tensile, LCF, SPLCF, Relaxation, TMF)
- Characterized tested specimens for key damage mechanisms identification (TEM, EBSD, SEM)
- Performed small scale modeling (crystal plasticity finite element modeling) for estimating the local stress, strain variations and classify sources of variation.
- Developed preliminary – framework for continuum damage model coupling creep and cyclic plasticity

## Next Steps

- Finalize CDM model calibration
- Validate model on uniaxial and multiaxial stress tests
- Perform Baseline CDM Analyses of a Thick Wall Boiler Component
- Perform Damage Sensitivity Studies on a Thick Wall Boiler Component

