### ADVANCED STRUCTURED ADSORBENT ARCHITECTURES FOR TRANSFORMATIVE CARBON DIOXIDE CAPTURE PERFORMANCE

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# **Program Overview**

- Total Funding: \$3,774,983
  - Federal Funds: \$2,999,904
  - Cost Share: \$775,079
- Project PoP: May 2019 July 2021
- Overall Project Objectives:
  - 1. Demonstrate energy reduction potential from Advanced Structure Adsorbent with greater than 30% reduction in Steam injection per MT of  $CO_2$ .
  - 2. Preserve other KPIs of RC-TSA\* process and update TEA for new structure.

# **Program Overview**



### **Project Participants:**

- Electricore, Inc. Prime Contractor and Program Manager
- Svante, Inc. Technical subrecipient, leader in large-scale CO<sub>2</sub> capture responsible for structured sorbent bed development and testing.



**Svante** 

 DNV GL USA Inc. - Technical subrecipient, responsible for identification, development and updating critical documents including TMP and EH&S. DNV will also perform process modeling and simulations.



Susteon, Inc. - Technical subrecipient, leading the technoeconomic analysis (TEA).

# **Technology Background**



- High bed productivity 10 Tonnes of  $CO_2$  per m<sup>3</sup> of sorbent per day range
- Strong Capex advantage for contactor (RAM) at intermediate capture scale.
- Some energy penalty with difficult to recover heat stored in solids.

# **Technology Background**

- Prior to program: demonstrated RC-TSA RAM technology with amines doped silica sorbent materials at 0.5 Tonnes / day scale.
- Identified potential MOF for RC-TSA with very good stability to moisture swing.

#### **Fundamental performance enablers:**

- > Very fast kinetics with contact time < 1s, 50-80s total cycle time.
- > Contactor with very high surface area
- **>** Low flow resistance of parallel channel structure.
- > Low heat capacity relative to adsorption capacity.

#### **Significant challenges:**

- Sorbent lifetime needs to be years (3-5 yrs.)
- Cost of sorbent structure have to be modest (20-30 \$/kg)
- > Energy intensity of process needs to be minimized

# **Technical Approach**

- Use new engineering design to create an advanced structure adsorbent for RC-TSA to:
- Optimize thermal management in Moisture Swing Adsorption
  - Enable synergistic design and reduced amount of steam injection
- Create two different regeneration environments
  - Potential for increased capacity with high capacity sorbent material with fast regeneration.
- Expand the material choice to non-steam stable adsorption material (ex. MOF)
  - Part of the sorbent can have lower heat of desorption and use the heat generated in the other sorbent w/o using hot steam as a carrier gas

### Structured Bed with Heat Exchange



Step 3 (A desorp/B desorp)

### Project Scope – BP1 Complete

Task/Subtask Number	SOPO Task/ Subtask Title	Completion Date
1.0	Project Management and Planning	04/30/21
2.0	Technology Maturation Plan	04/30/21
3.0	Adsorbent Selection, Characterization and Synthesis (Phase I)	04/30/20
3.1	Finalize candidate adsorbent materials for Bi-Layer program	07/30/19
3.2	Thermodynamic equilibrium measurements of candidate adsorbents	04/30/20
3.3	Dynamic characterization of kinetic behavior of adsorbents	04/30/20
3.4	Flue gas compatibility study – contaminants, composition, and condition	04/30/20
3.5	Adsorbent Down-Selection and Production	04/30/20
4.0	Bi-Layer Laminated Structures Development (Phase I)	04/15/20
4.1	Barrier material selection and optimization	04/15/20
4.2	Bi-Layer coating development	04/15/20
4.3	Bi-Layer spacer and flow-path control printing	04/15/20
4.4	Bi-Layer laminate structure development	04/15/20
5.0	Bi-Layer Structured Adsorbent Bed Development and Design	05/31/20
5.1	Bi-Layer structures packaging development	04/30/20
5.2	Bi-Layer Bed fluid distribution analysis for independent process streams	12/31/19
5.3	Bi-Layer Bed Design	05/31/20
6.0	VTS Modifications for Bi-Layer Bed Testing	05/31/20
7.0	Bi-layer Bed Bench-Scale Testing (Phase I)	07/31/20
8.0	Computational Modeling and Process Simulation (Phase I)	07/31/20

### **Solid Sorbent Selection**

#### • Subtask 3.1 - Finalize candidate adsorbent materials for Bi-Layer

- Down selection of the first set of sorbent material for Gen-0 Bi-layer bed design was based on the following criteria:
  - Critical Technology Element (CTE) criteria 1A and 1B,
  - Material availability, and
  - Prior demonstration of ability to form a laminate structure with the sorbent with minimal loss of adsorption capacity.
- The list of down selected sorbent is provided below.

Side A sorbent	Water tolerance	Heat of CO <sub>2</sub> adsorption	Available at Kg scale	Laminate process
S4+ Doped silica	Very Good	about 90 kJ/mol	Yes	Yes
PNP-1 Porous polymer	Excellent	about 90 kJ/mol	Yes	To be optimized
S4 Doped silica	Vapor only	about 95 kJ/mol	Yes	Yes
Side B sorbent	Water tolerance	Heat of CO <sub>2</sub>	Available at Kg	Laminate process
		adsorption	scale	
MOF-1	Excellent	about 35 kJ/mol	Yes	Yes
MOF-2 (aminated)	Poor	about 56 kJ/mol	Yes	Yes

### Solid Sorbent Stability

S4+ and MOF-1 showed good O<sub>2</sub> resistance in accelerated tests



# RC-TSA – Single Layer KPIs

#### Subtask 3.3 - Dynamic characterization of kinetic behavior of adsorbents



Veloxotherm Testing Station II - picture -0.5 to 1L adsorbent beds

- Multiple VTS testing beds were manufactured and optimized (structure sorbent and cycle) to match cycle times between the both sides of the bi-layered.
- Cycle time need to be short <60sec to minimize water pickup form the feed on MOF-1

10% CO <sub>2</sub> , 5% H <sub>2</sub> O in Feed	S4+ (PEIDS) bed	
Total Cycle time [Sec]	50	Fast Cycle
Productivity [CO2 T/m3 day]	14.1	Very high productivit
Recovery [%]	81	
Prod. Purity [%]	85.5	
17% CO2, 5% H2O in Feed	MOF-1 bed	
Total Cycle time [Sec]	50	Fast Cycle
Productivity [CO2 T/m3 day]	9.6	High productivity
Recovery [%]	85	
Prod. Purity [%]	94.3	11

# Material Scale Up

#### **Subtask 3.5 - Adsorbent Down-Selection and Production**

- Out of the five adsorbent candidates selected two were chosen
  - $\Box$  Side A: S4+
    - Relatively high heat of adsorption, water and steam resistant, fast cycle, high productivity, better oxidation resistance
    - Slurry and coating optimization still needs to be done for large scale
  - □ Side B: MOF-1
    - Low HOA, water and steam resistant, low temperature (RT) and low pressure (1 ATM) synthesis using commercially available raw materials (easily scalable), high oxidation resistance
- The adsorbent and coating processes necessary for proof of concept for the Bilayer bed design are complete.
- > 200kg of the MOF-1 have been produced at Svante with evaluation of multiple suppliers leading to successful reduction in raw material and processing costs.

### Sorbent Process Model

#### **Dynamic Computational Modeling and Process Simulation – single layer**

- Single layer models for the preferred adsorbent layers have been developed and validated using VTS data. Objectives included:
  - Model the individual adsorbent layers to closely understand the dynamics of each layer during the process steps
  - Evaluate and validate modeling results in detail using test data under the same process condition
  - Deliver modeling inputs for the software capable of handling the Bi-layer modeling dynamics

Highlevel	High level model vernication results of two adsorbent candidates for bi-layer project										
	S4/S4 <sup>+</sup> - cycl	e without Reflux	Calf20 - cycle with Reflux								
KPI	Test results	Dynamic model results	Test results	Dynamic model results							
Recovery [%Out/In]	84%	85%	88%	91%	•						
Purity [vol% CO <sub>2</sub> ]	88.5%	89%	89%	90%							
Steam Ratio [wt H <sub>2</sub> 0/wt CO <sub>2</sub> ]	1.98	1.9	2.1	2.09							

- Successfully modelled dynamic behavior and cycle KPIs using measured sorbent isotherms
- Provide greater insight in coupling of heat generation and desorption of CO<sub>2</sub> induced by H<sub>2</sub>O adsorption and competitive CO<sub>2</sub>, H<sub>2</sub>O adsorption.

# Modelling of Heat Released and Transferred Through the Barrier

Use transient adsorption model from single layer to compute heat duties to simulate bi-layer dynamic temperature profiles.



Modeling of 2D temperature profile through laminate (DNV-GL)

Down selected Aluminized Polymer-1 for process scale up to VTS bed size (m<sup>2</sup> scale)

Barrier thin enough for this application (~10um).

### **Bed Design and Assembly**

#### **Bi-Layer Bed fluid distribution analysis for independent process streams**

• Built multiple 0.75L test beds with about 0.8m<sup>2</sup> of heat exchange surface and about 200g of active sorbent.





Inlet of 1.16m long bed



**Bi-layer bed assembly** 

Illustration of flow arrangement (DNV-GL)

# **Process Testing**

#### Task 7 - Bi-layer Bed Bench-Scale Testing

• The VTS 2 test station was used to test the single layer beds and commission the unit with its increased feed gas configuration flexibility. New connectors were built to distribute gas connections to channel A and B individually.



### Testing – Heat Exchange Through the Barrier

Thermal transfer performance verified experimentally. Almost no lag in temperature rise between layers across the barrier material.



Temperature in A and B channels VS time during BT test

 $CO_2$  injected on one side only (S4+ side)

### Cyclic Process Testing – Product Flows



Comparison on Product flows for different steam injection strategies

- Desorption of CO<sub>2</sub> has large spike after 2s, followed by complex decay.
- Indirect heat fast desorption demonstrated.

### **Process KPIs for Bilayer Beds**

Steam	SR ratio (relative)	<b>TPD / m3</b>	Purity	S4 CO2/ Total CO2	
Both side	1	3.4	77%	64%	
S4+ side	0.85	2.7	80.4%	80%	
Steam	SR ratio (relative)	TPD / m3	Purity	S4 CO2/ Total CO2	
Both side	1	5	73.3%	55%	
S4+ side	0.64	2.8	87.2%	85%	$\Leftarrow$
	Steam Both side S4+ side Steam Both side S4+ side	SteamSR ratio (relative)Both side1S4+ side0.85SteamSR ratio (relative)Both side1S4+ side0.64	SteamSR ratio (relative)TPD / m3Both side13.4S4+ side0.852.7SteamSR ratio (relative)Both side15S4+ side0.642.8	SteamSR ratio (relative)TPD / m3PurityBoth side13.477%S4+ side0.852.780.4%SteamSR ratio (relative)Both side1573.3%S4+ side0.642.887.2%	Steam         SR ratio (relative)         TPD / m3         Purity         S4 CO2/ Total CO2           Both side         1         3.4         77%         64%           S4 + side         0.85         2.7         80.4%         80%           Steam         SR ratio (relative)         TPD / m3         Purity         S4 CO2/ Total CO2           Steam         SR ratio (relative)         TPD / m3         Purity         S4 CO2/ Total CO2           Both side         1         5         73.3%         55%           S4 + side         0.64         2.8         87.2%         85%

#### Steam Ratio reduction successfully demonstrated twice.

- Steam Ratio dropped 15% and 35% respectively related to dual side steam injection.
  - Meets the end of year 1 success criteria for SR reduction.
- MOF-1 indirect regeneration demonstrated
  - Need flush gas or better vacuum to increase productivity
- Productivity, recovery need to improve.
  - Optimization of coating thickness and process

### Summary

Development and initial testing of two very interesting  $CO_2$  capture materials that could be important for  $CO_2$  capture for carbon reduction/removal (Direct air capture, cement and SMR).

Built first successful dual channel parallel film heat exchanger with adsorbent with extremely low mass flow separator.

Demonstrated the manufacturability of device, as well as, effectiveness of heat transport between A and B sides.

Demonstrated fast indirect regeneration of sorbent across barrier layer and found a significant reduction (~35%) in the Steam Ratio by avoiding excess steam addition [In phase operation].

# **Budget Period 2 Goals**

- Bi-layered optimization and testing of the optimized layers
  - Cycle development and optimization
  - Optimization of bed design (parallel vs alternative design)
  - Modelling energy balance
- Optimization of each layers in terms of material and process
  - MOF-1 and S4+
    - Scale-up efforts for MOF-1 (up to 1,000 Kg)
    - Optimized MOF-1 for lower SR
    - Long term field testing (Lafarge Cement site in Richmond BC, Canada, ~ 1TPD)
    - Long term testing of S4+ (synthetic flue gas composition (NG boiler) at external site, 0.1 TPD)
    - Slurry and Laminate optimization
    - Cycle optimization

# Appendix

### **Organization Chart**



- Electricore will serve as PRIME contractor and Project Director.
- Svante serves as the main technical point of contact for this project and technology provider.
- Susteon is leading the TEA.
- DNV is responsible for identification, development and updating critical documents for natural gas transmission stations and will perform process modeling and simulations.

### Gantt Chart – BP1

	2019	Qtr 2			2019 Qtr	3		2019 Qtr 4			2020 Qtr 1			2020 Qtr 2			2020 Qtr 3
Task Name 👻	Ар	r	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul
▲ 1.2.2 DOE Bi-layer																	
Task 3 - Adsorbent Selection Phase 1																	
3.1 - Finalize candidate adsorbent materials for Bi-Layer program	1					07-30											
3.2 -Thermodynamic equilibrium measurements of candidate adsorbents	1																
3.3 - Dynamic characterization of kinetic behavior of adsorbents	1																
3.4 - Flue gas compatibility study - contaminants, composition, and condition																	
3.5 - Adsorbent Down-Selection and Production																	
<ul> <li>Task 4 - Bi-Layer Laminated Structures</li> <li>Development (Phase 1)</li> </ul>	1																
4.1 - Barrier material selection and optimization																	
4.2 - Bi-Layer coating development																	
4.3 - Bi-Layer spacer and flow-path control printing	3																
4.4 - Bi-Layer laminate structure development - sheet stacking or pleating																	
Task 5 - Bi-Layer Structured Adsorbent Bed Development and Design	1																
5.1 - Bi-Layer structures packaging development	1																
5.2 - Bi-Layer Bed fluid distribution analysis for independent process streams	1																
5.3 - Bi-Layer Bed Design	1																
Task 6 - VTS Modifications for Bi-Layer Bed Testing																	
Task 7 - Bi-Layer Bed Bench-Scale Testing (Phase 1)																	
Task 8 - Computational Modeling and Process Simulation (Phase I)																	

### Gantt Chart – BP2

Task Name 👻	Aug Sep	2020 Qtr 4 Oct	Nov Dec	2021 Qtr 1 Jan F	eb Mar	2021 Qtr 2 Apr May	2021 Qtr 3 Jun Jul
<ul> <li>Task 9 - Adsorbent Selection, Characterization and Synthesis (Phase II)</li> </ul>							1
9.1 - Thermodynamic equilibrium measurements of candidate adsorbents							
9.2 - Dynamic characterization of kinetic behavior of adsorbents							
9.3 Adsorbent lifetime on PDU and 1 TDP unit							
9.4 - Flue gas compatibility study -Contaminants							
9.5 - Synthesis and Production of candidate adsorbents							
MS 9.1 - Final specification of down-selected adsorbents for Gen-1 Mk-II Bi-layer Architecture					<b>♦</b> 02-26		
MS 9.2 - Lifetime of Adsorbent estimate report from on stream and bench data							♦ 05-31
Task 10 - Proof of Scalability beyond Kg scale for novel adsorbent							
MS 10 - >50kg adsorbent produced in one batch with						04-30	
MOF price projection update							
<ul> <li>Task 11 - Bi-Layer Laminated Structures Development (Phase II)</li> </ul>							
11.1 - Bi-Layer coating development	l						
11.2 - Bi-Layer spacer and flow-path control printing							
11.3 - Bi-Layer laminate structure development - sheet stacking and pleating				•			
MS 11.1 - Final Gen-1 Mk-II Bi-Layer laminate structure production for bench scale bed testing		<b>↓</b> 1	10-31				