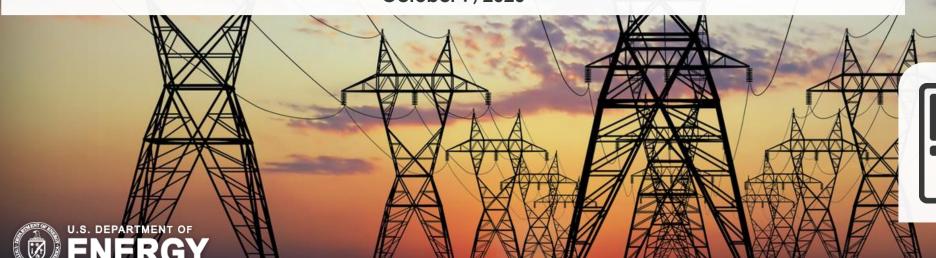
# Plant and Process Level Carbon Capture Techno-Economic Analysis at NETL

Timothy Fout

October 7, 2020





## Systems Engineering & Analysis

Associate Director, Acting Peter C. Balash, Ph.D.



Senior Fellow David Miller, Ph.D.

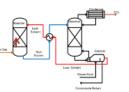




#### **Energy Process Analysis**

Energy Process Design, Analysis, and Cost Estimation

- Plant-level modeling, performance assessment
- Cost estimation for plant-level systems
- General plant-level technology evaluation and support



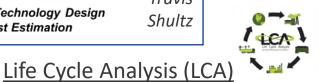
& Cost Estimation

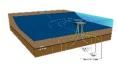
Advanced Technology Design

## **Energy Systems Analysis**

Resource Availability and Cost Modeling

- CO<sub>2</sub> storage (saline and EOR)
- Fossil fuel extraction
- Rare earth elements
- General subsurface technology evaluation and support







Luciane Cunha, Ph.D.

Balash, Acting

#### **Energy Markets Analysis**

Travis

Shultz

**Energy Economy Modeling and Impact Assessment** 

- Enhanced fossil energy representation
- Multi-model scenario/policy analysis
- Grid, infrastructure, energy-water



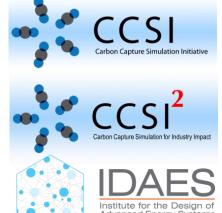
- Economic impact assessment
- General regulatory, market and financial expertise

### **Process Systems Engineering Research**

- Process synthesis, design, optimization, intensification
- Steady state and dynamic process model development
- Uncertainty quantification
- Advanced process control



Anthony Burgard, Ph.D.





#### Overview



## BECCS Study (includes LCA)

- Design Basis Review
- Performance Results
- Economic Results
- Ongoing Updates
- Questions

#### **BECCS Key Research Questions:**

- 1. Can co-firing biomass with coal reduce greenhouse gas (GHG) emissions on a life cycle basis?
- 2. Will adding biomass to coal-fired power plants increase or decrease the cost of electricity?
- 3. What is the optimal combination of coal and biomass to achieve low-carbon electricity and low costs?



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### **Site Characteristics**



 Site characteristics and ambient conditions are consistent with Revision 4 of the Bituminous Baseline Study

#### **Site Characteristics**

Parameter	Value			
Location	Greenfield, Midwestern U.S.			
Topography	Level			
Size (pulverized coal), acres	300			
Size (natural gas combined cycle), acres	100			
Transportation	Rail or Highway			
Ash Disposal	Off-Site			
Water	50% Municipal and 50% Ground Water			

https://netl.doe.gov/projects/files/QualityGuidelinesforEnergySystemStudiesProcessModelingDesignParameters 062819.pdf

#### **Site Ambient Conditions**

Parameter	Value	
Elevation, m (ft)	0 (0)	
Barometric Pressure, MPa (psia)	0.101 (14.696)	
Average Ambient Dry Bulb Temperature, °C (°F)	15 (59)	
Average Ambient Wet Bulb Temperature, °C (°F)	10.8 (51.5)	
Design Ambient Relative Humidity, %	60	
Cooling Water Temperature, °C (°F) <sup>A</sup>	15.6 (60)	
Air composition based on published psychrometric	c data, mass %	
$N_2$	75.055	
02	22.998	
Ar	1.280	
H <sub>2</sub> O	0.616	
CO <sub>2</sub>	0.050	
Total	100.00	

<sup>&</sup>lt;sup>A</sup>The cooling water temperature is the cooling tower cooling water exit temperature; this is set to 8.5°F above ambient wet bulb conditions in International Organization for Standardization (ISO) cases



<sup>-</sup> Quality Guidelines for Energy Systems Studies: Process Modeling Design Parameters, June 2019, NETL-PUB 22478

#### **Fuel Characteristics**



- The coal analysis is consistent with the Bituminous Baseline Rev4 analysis
- Biomass characteristics consistent with prior NETL report

Hybrid Poplar <sup>1</sup>					
Ultimate Analysis (weight %)					
	As Received	Dry			
Moisture	50.00	0.00			
Carbon	26.18	52.36			
Hydrogen	2.80	5.60			
Nitrogen	0.19	0.37			
Chlorine	0.00	0.00			
Sulfur	0.02	0.03			
Ash	0.74	1.48			
Oxygen <sup>B</sup>	20.08	40.16			
Total	100.0	100.00			
HHV, kJ/kg (Btu/lb)	9,813 (4,219)	19,627 (8,438)			
LHV, kJ/kg (Btu/lb)	9,232 (3,969)	18,464 (7,938)			

	LABORA	
Volume 1 Rev 4		
Bituminous		
Illinois No. 6 <sup>2</sup>		
	-	
mate Analysis (weight	: %) <sup>A</sup>	
As Received	Dry	
11.12	0.00	
9.70	10.91	
34.99	39.37	
44.19	49.72	
100.00	100.00	
2.51	2.82	
27,113 (11,666)	30,506 (13,126)	
26,151 (11,252)	29,544 (12,712)	
nate Analysis (weight s	%)	
As Received	Dry	
11.12	0.00	
63.75	71.72	
4.50	5.06	
1.25	1.41	
0.15	0.17	
2.51	2.82	
9.70	10.91	
7.02	7.91	
100.00	100.00	
	## Pitum Illinois  mate Analysis (weight  ## As Received  11.12  9.70  34.99  44.19  100.00  2.51  27,113 (11,666)  26,151 (11,252)  mate Analysis (weight 9  ## As Received  11.12  63.75  4.50  1.25  0.15  2.51  9.70  7.02	

<sup>&</sup>lt;sup>A</sup>The proximate analysis assumes sulfur as volatile matter



<sup>&</sup>lt;sup>B</sup> By difference

#### **MATS and NSPS Limits**



 The utility Mercury and Air Toxics Standards (MATS) and New Source Performance Standards (NSPS) limits for pulverized coal (PC) plants considered in the Bituminous Baseline Rev4 is adhered to

MATS and NSPS Emission Limits for PM, HCl, SO <sub>2</sub> , NOx, and Hg					
Pollutant <sup>A</sup>	PC (lb/MWh-gross)				
SO <sub>2</sub>	1.00				
NOx	0.70				
PM (Filterable)	0.09				
Hg	3x10 <sup>-6</sup>				
HCI	0.010				

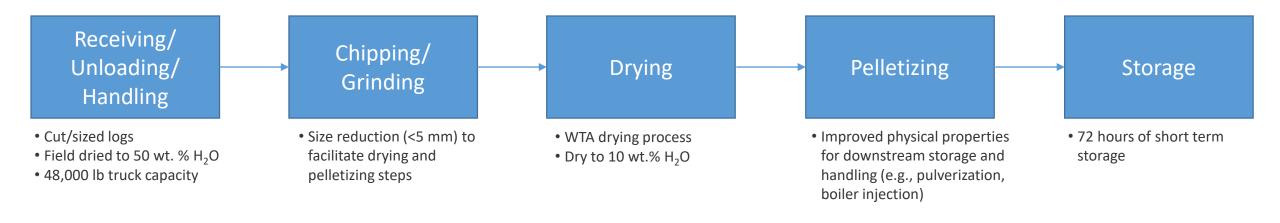
<sup>&</sup>lt;sup>A</sup>CO emissions were not considered, or reported, in BBR Rev 4



## **Biomass Pre-Processing**



- The current and prior studies assume that cut and sized hybrid poplar logs are received at the plant site by truck
- The logs are then pre-processed to improve the energy density, handling characteristics, and combustion efficiency of the hybrid poplar, as depicted below





## **Design Assumptions**

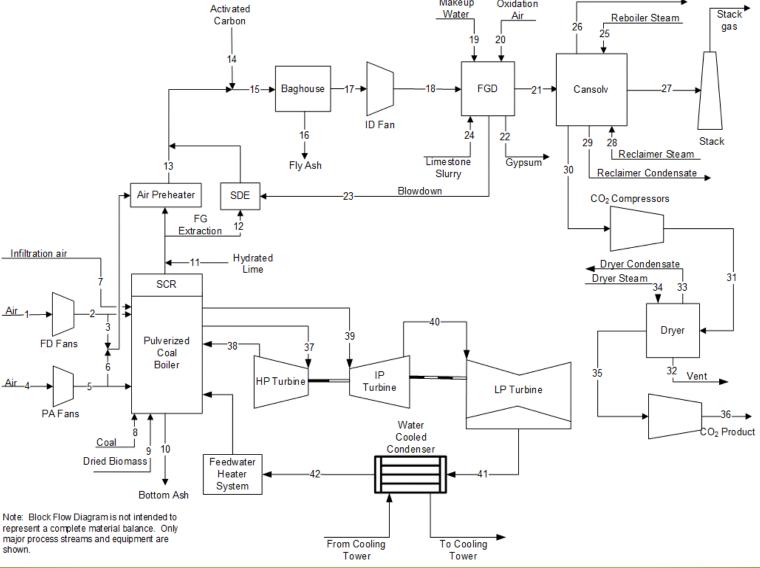


- Biomass is available in the quantity, type, frequency, and at the cost assumed in the study
- Biomass co-firing does not effect performance/cost of the carbon capture system
- Product CO<sub>2</sub> must meet requirements of NETL QGESS on CO<sub>2</sub> product purity<sup>1</sup>
- Facility Capacity Factor = Availability = 85% for all cases
- Capital Cost Uncertainty Range -15%/+30% (AACE Class 4)<sup>2</sup>
- Use mature plant costing methodology<sup>2</sup>
  - Initial plants will likely have higher costs when incorporating CCS and cofiring



## Plant Configuration with CO<sub>2</sub> Capture







### Case Matrix



 The following case matrix was considered part of this study update

Case	Biomass Type	Plant Type	% Biomass in Feed	CO <sub>2</sub> Capture %	Capture Strategy	
PN1			20			
PN2			35	0	N/A	
PN3	Lludavial Davalav	Greenfield	49			
PA1	Hybrid Poplar	Supercritical	20			
PA2			35	90	Amine (Cansolv)	
PA3			49			

- 20 wt%
  - Lower end of co-firing
  - Represents the majority of currently in practice co-firing rates
  - Boiler efficiency impacts not statistically significant
- 35 wt%
  - Mid-range of feasible co-firing
  - Close to the potential net-zero greenhouse gas emissions point (with capture)
  - —If the desired result is for a net-zero LCA, this co-fire rate could be changed
- 49 wt%
  - Current potential maximum rate of co-firing based on logistical supply constraints
  - Maintains coal with biomass co-firing idea
- Case nomenclature: P poplar, N non-capture, A amine, numericals case designation



#### Overview



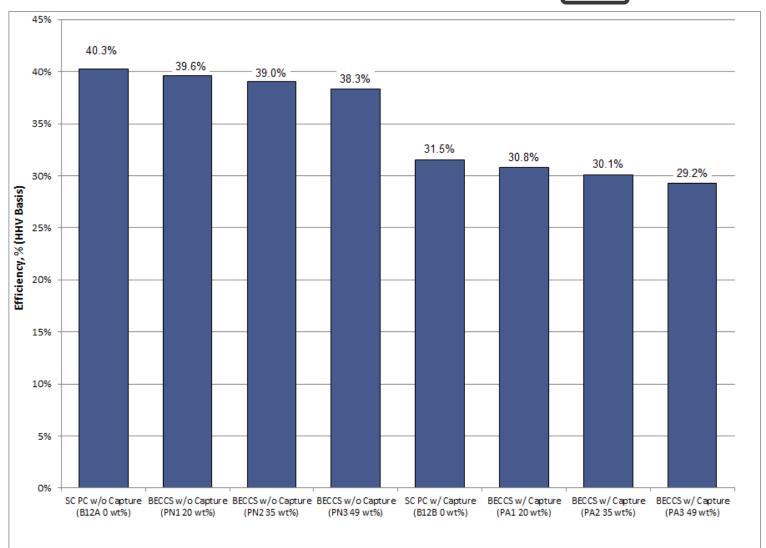
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## **Net Plant Efficiency**



- Plant efficiency is reduced as co-firing percentages increase primarily due to two factors:
  - Hybrid poplar has a lower heating value compared to coal leading to a higher overall fuel consumption rate and lower efficiency
  - Increased auxiliary loads due to pelletization and drying biomass from 50 wt% down to 10 wt% moisture

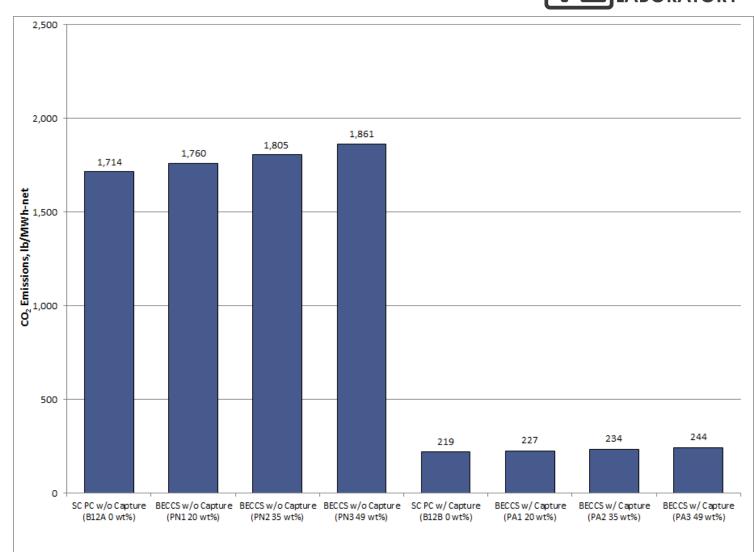




## Gross Plant CO<sub>2</sub> Emissions



- Carbon dioxide emissions within the plant boundary increase as co-fire rates increase again due in part to lower biomass fuel heating value and increased auxiliary load requirements
- This does not include the carbon dioxide captured during the biomass growth cycle





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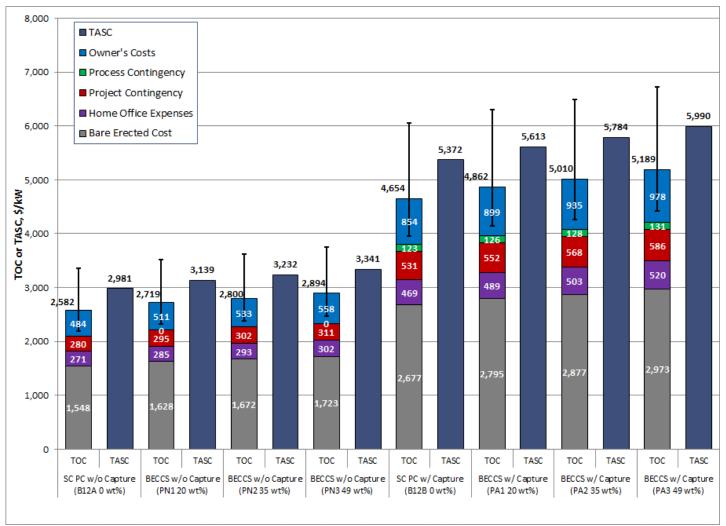


# Total Overnight Cost/Total As Spent Cost (TOC/TASC)



 Total costs impacted as overall plant efficiency decreases with the co-fire rate increase

wt% Biomass	% Increase TOC					
-	w/o Capture	w/ Capture				
20	5.3%	4.5%				
35	8.4%	7.7%				
49	12.1%	11.5%				



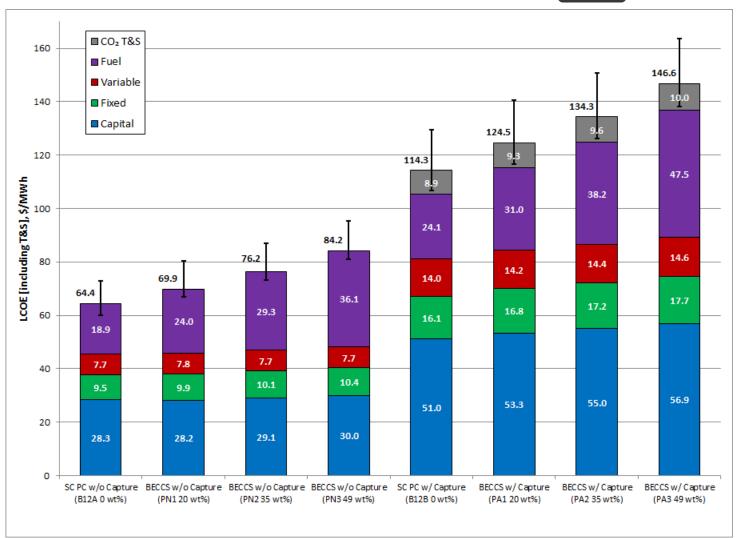


## Levelized Cost of Electricity (LCOE)



 Levelized cost of electricity increases dominated by increased biomass fuel costs

wt% Biomass	% Increase LCOE				
-	w/o Capture	w/ Capture			
20	8.5%	9.0%			
35	18.4%	17.5%			
49	30.7%	28.3%			

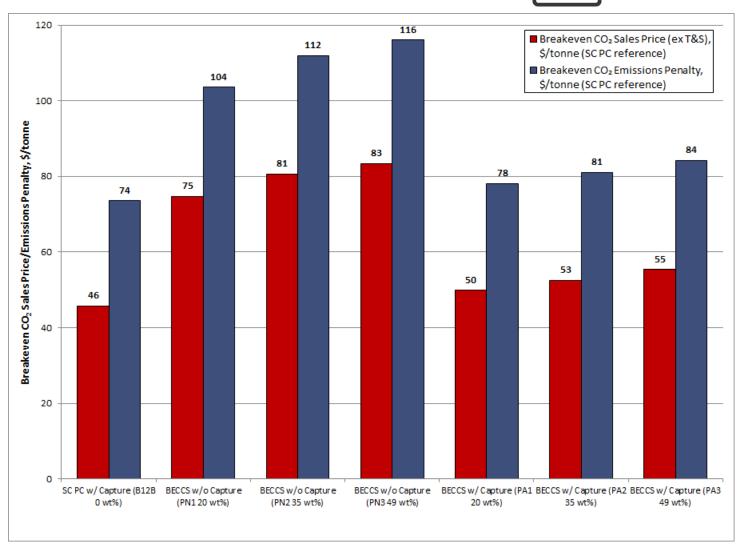




## Breakeven CO<sub>2</sub> Sales Price/Penalty



- High biomass costs drive the breakeven sales price/penalty above that of Case B12B
- Including the Cansolv unit with cofiring reduces the marginal increases
- Cases presented do not consider lifecycle emissions





#### **BECCS TEA Conclusions**



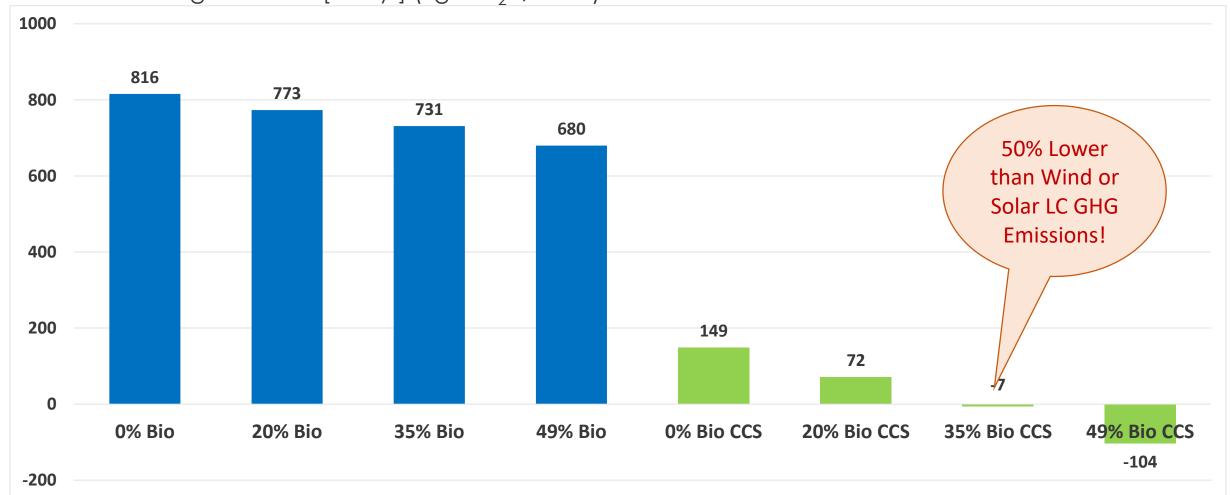
- PC with CCS, 0% biomass, offers lowest breakeven CO<sub>2</sub> cost option
- High cost of carbon emissions or desire for carbon negative systems makes co-firing with biomass plus CCS attractive
- Carbon-neutral or –negative coal-fired electricity can be achieved by adding both biomass and CCS to PC systems
  - Neutrality occurs near 35% Biomass with 90% CCS



## Life Cycle GHG Emissions per MWh, busbar



Global Warming Potential [100-yr] (kg CO<sub>2</sub>e/MWh)





Higher Biomass rates = larger land use requirements, can be reduced through application of higher capture rates (i.e. 95% capture with amines or CFB with oxy-combustion, etc.)

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#### NGCC with EGR

Updating Exhaust Gas Recycle Reports



- NETL has examined the use of EGR to increase the CO<sub>2</sub> concentration in NGCC flue gas to enable lower cost postcombustion capture of CO<sub>2</sub>
  - Current and Future Technologies for NGCC Power Plants, 2013 DOE/NETL-341-061013
  - Carbon Capture Approaches for NGCC Systems, Revision 2, 2010 DOE/NETL-2011-1470
- Developing baseline cases for NGCC with EGR and CCS
  - Focusing on parallel cases with B31B F Class turbine
  - Evaluating interim results w.r.t recent EPRI report<sup>1</sup>
- Will develop an H-Class EGR with CCS case as well



## NGCC Retrofit Study

Updating NGCC Retrofit Report



- Will update NGCC retrofit report<sup>1</sup> and Carbon Capture Retrofit Database (CCRD)<sup>2</sup>
  - Align with financial assumptions and performance updates of Rev 4 of Fossil Energy Baseline
  - Calculate costs and performance based on retrofit design
    - Retrofit difficulty factors applied to capital cost
    - Derate energy cost accounted
  - Will include F and H class cases
  - Sensitivities
  - Serves as basis for scaling factors used in CCRD for NGCC
- Also will be examining greater than 90% capture for NGCC (separate report)
- Update to PC retrofit report<sup>3</sup> and CCRD<sup>4</sup> to follow
  - 1. Cost and Performance of Retrofitting NGCC Units for Carbon Capture, November 2013, DOE/NETL-2018/1896 https://netl.doe.gov/projects/files/CostPerformanceRetrofittingNGCCforCarbonCapture 040119.pdf
  - 2. NGCC CCRD, April 2019 https://netl.doe.gov/energy-analysis/details?id=086796fb-e0d9-4d1d-831f-c2e986a7072e
  - 3. Eliminating the Derate of Carbon Capture Retrofits, September 2011, DOE/NETL-401/091211 https://netl.doe.gov/projects/files/FliminatingtheDerateofCarbonCaptureRetrofits, 091211.pdf
  - 4. PC CCRD, April 2019 https://netl.doe.gov/energy-analysis/details?id=69db8281-593f-4b2e-ac68-061b17574fb8



## Industrial CO<sub>2</sub> Capture Report<sup>1</sup> Update



- Cases model capture and compression of a CO<sub>2</sub> source from Industry type
  - Do not model the Industrial Facility
  - Capture/Compression not integrated with Industrial Facility
- Updating report to reflect Fossil Baseline Rev 4 assumptions
  - Updated Financial Assumptions
  - Updated Equipment Quotes
    - -Alignment of CO<sub>2</sub> Capture Systems used
- Utilized as a basis for Industrial Capture goals
- Reference for Carbon Capture Retrofit Database
  - Will update CCRD<sup>2</sup> as well



## Industrial Source CO<sub>2</sub> Capture (2014)



Industrial Process	Reference Plant Capacity	CO₂ Source Stream	CO <sub>2</sub> to Product Ratio (tonne CO <sub>2</sub> /tonne Product)	Source Stream CO <sub>2</sub> Concentra- tion (mol%)	Source Stream CO <sub>2</sub> Partial Pressure (psia)	Сар	ilable for ture CO₂/year) All U.S. sources	Breakeven Cost of Capturing CO <sub>2</sub> (\$/tonne CO <sub>2</sub> )
			Himb Dunite	, ,	(psia)	Fiant	Sources	CO2)
			High Purity	Sources			1	<u> </u>
Ethanol	50 M gal/year	Distillation gas	0.96	100	18.4	0.14	40	30
Ammonia	907,000 tonnes/year	Stripping vent	1.9	99	22.8	0.458	6	27
Natural Gas Processing	500 MMscf/d	CO <sub>2</sub> vent	N/A <sup>1</sup>	99	23.3	0.649	27	18
Ethylene Oxide	364,500 tonnes/year	AGR product stream	0.33	100	43.5	0.122	1	25
Coal-to-Liquids (CTL)	50,000 bbl/d	AGR product stream	N/A <sup>2</sup>	100	265	8.74	-	9
Gas-to-Liquids (GTL)	50,000 bbl/d	AGR product stream	N/A <sup>2</sup>	100	265	1.86	-	9
			Low Purity	Sources				
Refinery Hydrogen	59,000 tonnes/year	PSA tail gas	10.5	44.5	8.9	0.274	68	118
Iron/Steel	2.54 M tonnes/year	Plant Total COG PPS COG/BFG <sup>3</sup>	2.2	N/A 23.2 26.4	N/A 3.4 3.9	3.9 2.75 1.16	49	99 99 101
Cement SCR/FGD Sensitivity	992,500 tonnes/year	Kiln Off-gas	1.2	22.4	3.3	1.14	80	100 127
Coal-fired power plants	550 MW	Flue Gas	NA	13.5	2.0	4.13	2,545 <sup>4</sup>	77 <sup>56</sup>



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