

Integrated TBC/EBC for SiC Fiber Reinforced SiC Matrix Composites for Next Generation Gas Turbines

DoE UTSR DEFE0031281 (10/2017 – 09/2021)

Annual Review Meeting

Program Manager: Matthew Adams

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Research conducted by Drs. Quan Li, Sanat Chandra Maiti, and Zhao Zhang

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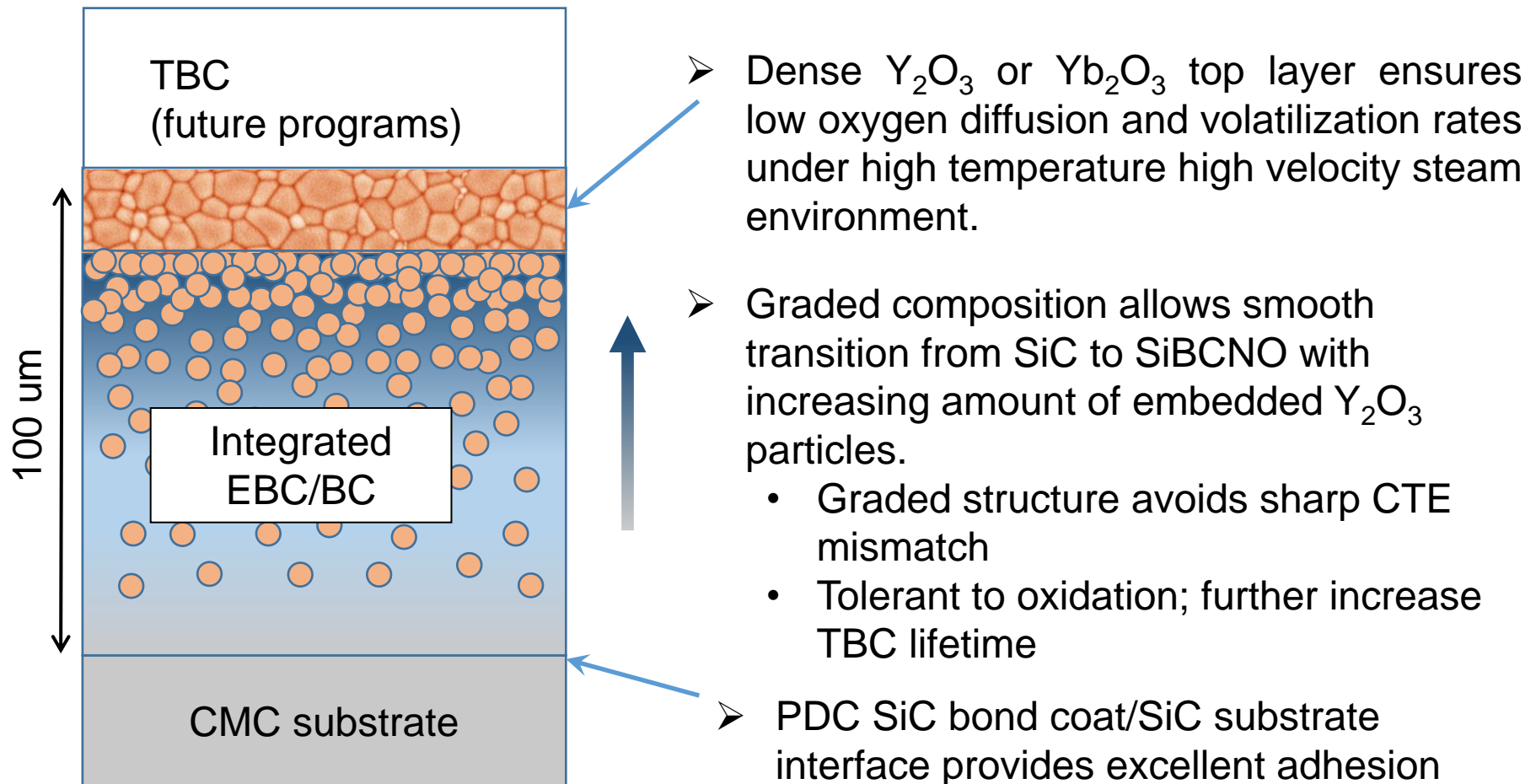
Clemson University

In Collaboration with GE Power Team led by John Delvaux

Outlines

- 1. The concept of integrated TBC/EBC/BC**
- 2. Overall Goals**
- 3. Objectives**
- 4. Project Tasks**
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- 6. Project Short Term Plans**

1. The concept of integrated TBC/EBC/BC



2. Overall Goals

- Develop an integrated and graded EBC/BC that is:
 - Good bonding with CMC;
 - Graded compositions without sharp interfaces to mitigate thermal stresses from CTE mismatch;
 - Low oxygen transport rate, low oxidation rate and low volatility in high temperature, high velocity steam environment;
 - Tolerant to certain degree of oxidation thereby preventing catastrophic failure;
 - Chemically stable and compatible with CMC and TBC

- Create a strong collaborative team with complementary expertise and state-of-the-art facilities
 - The Clemson University team of Drs. Bordia and Peng.
 - The GE team, led by John Delvaux

3. Objectives

- Investigate the effect of **composite stoichiometry** (*i.e.* Si/B/C/N ratio in the precursor and the ratio of the Si-based precursor to yttrium oxide (Y_2O_3) (or ytterbium oxide (Yb_2O_3)) particle filler and processing conditions on the size of the resultant phases and nanostructure of the composite ceramics.
- Investigate the effect of the **composition and nanostructure on the thermal properties and oxidation and volatilization behavior** in oxidizing and high velocity steam environments. The control parameters are the stoichiometry of the precursor (*e.g.* Si/B/C/N ratio) and the volume fraction of the oxide particles Y_2O_3 (or Yb_2O_3) and range of microstructures produced as part of the first objective

3. Objectives (contd.)

- Process the graded Y_2O_3 (or Yb_2O_3) particulate /silicon boron carbon nitride (SiBCN) matrix composite coating and investigate the phase and microstructure stability during high velocity steam exposure at temperatures up to 1500°C.
- Develop a method to create Y_2O_3 (or Yb_2O_3) and SiBCN powders with predetermined compositions suitable for atmospheric plasma spraying (APS). The powders will be provided to the industrial collaborators for the fabrication of integrated environmental barrier coating/bond coating (EBC/BC) using APS.
- Evaluate the performance of integrated BC/EBCs from APS under high velocity steam environments at temperatures up to 1500°C.

4. Project Tasks

- **Task 1:** Project management and planning
- **Task 2:** Processing and stability of $\text{Y}_2\text{O}_3\text{-Si-C-N}$ and $\text{Yb}_2\text{O}_3\text{-Si-C-N}$ composites
- **Task 3:** Thermal and oxidation response of $\text{Y}_2\text{O}_3\text{-Si-C-N}$ and $\text{Yb}_2\text{O}_3\text{-Si-C-N}$ composites
- **Task 4:** Processing and performance of graded coatings processed using cold spray and pyrolysis
- **Task 5:** Processing and performance of graded coatings processed using atmospheric plasma spraying (APS)

5. Project Progress -Task 1

Task 1.0: Project management and planning

- ❖ Kickoff meeting 10/27/17
- ❖ A poster at the 2017 UTSR review meeting
- ❖ Recruitment of UG students and post doc to work on the project
- ❖ A talk and a poster at the 2018 UTSR review meeting
- ❖ A talk at 2019 UTSR review meeting.
- ❖ Request for a one year no-cost extension (approved)
- ❖ Regular periodic review meetings with DoE Program Manager and GE team throughout the project

5. Project Progress - Task 2:

Task 2: Processing and stability of $\text{Y}_2\text{O}_3\text{-Si-C-N}$ and $\text{Yb}_2\text{O}_3\text{-Si-C-N}$ composites

Sub-task 2.1: Determine the effect of composition and processing temperature on the phase and microstructure of composites

Part of this task (~ 20%) completed in year 1 and rest of the part is completed in year 2

Sub-task 2.2: Investigate the effect of temperatures on the phase stability phase and microstructure of composites during oxidation at temperatures up to 1600°C .

Completed in year 2.

5. Project Progress - Task 3

Task 3: Thermal and oxidation response of Y_2O_3 -Si-C-N and Yb_2O_3 -Si-C-N composites (90% complete)

Sub-task 3.1: Determine the effect of composition and microstructure of composites on thermal expansion coefficient, elastic modulus and thermal conductivity (80 % completed)

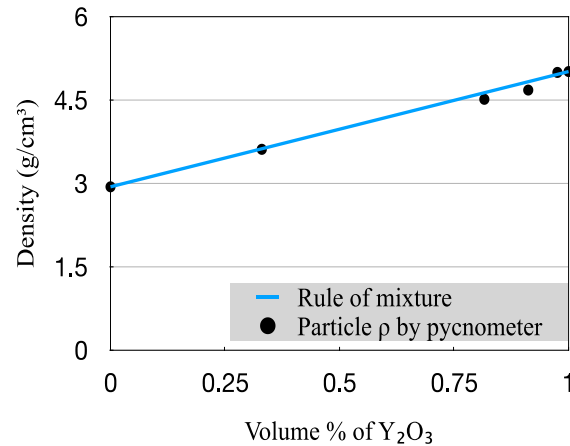
In year 2, we have completed this sub-task around 40 %. Accomplished the following:

- Measured the heat capacity and thermal conductivity of the Y_2O_3 - SiO_2 composites
- Developed and validated a technique for high temperature elastic modulus of ceramics

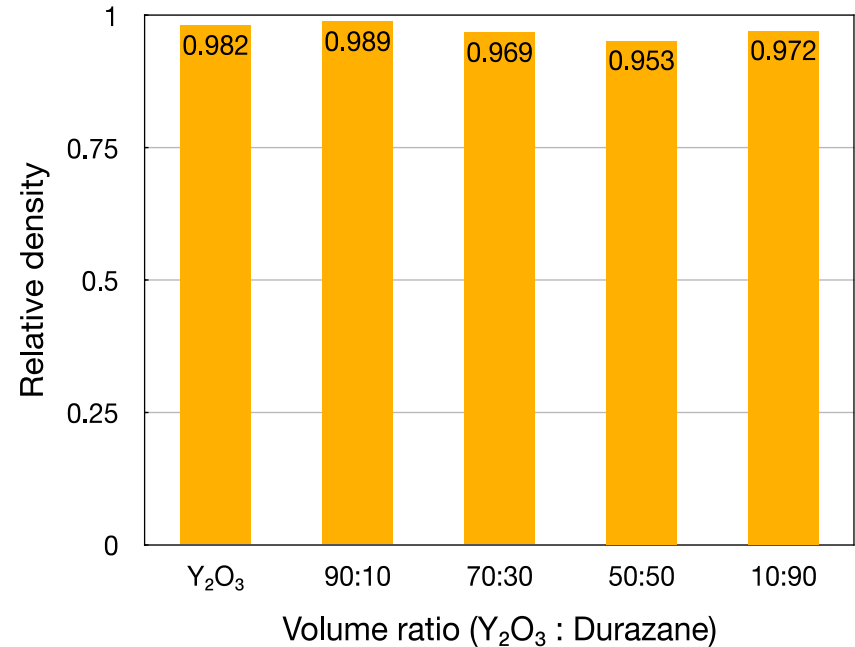
In year 3, we have completed 80 % of the sub-task. Accomplished the following:

- Made high density Y_2O_3 -SiCN composites using field assisted sintering (FAST)
- Measured the coefficients of thermal expansion for Y_2O_3 -SiCN, Y_2O_3 - SiO_2 , and Yb_2O_3 - SiO_2 composites
- Measured the elastic modulus of Y_2O_3 -SiCN composites as a function of temperature
- Measured the heat capacity of Yb_2O_3 - SiO_2 composites

5. Task 3 - High Density Y_2O_3 -SiCN Composites



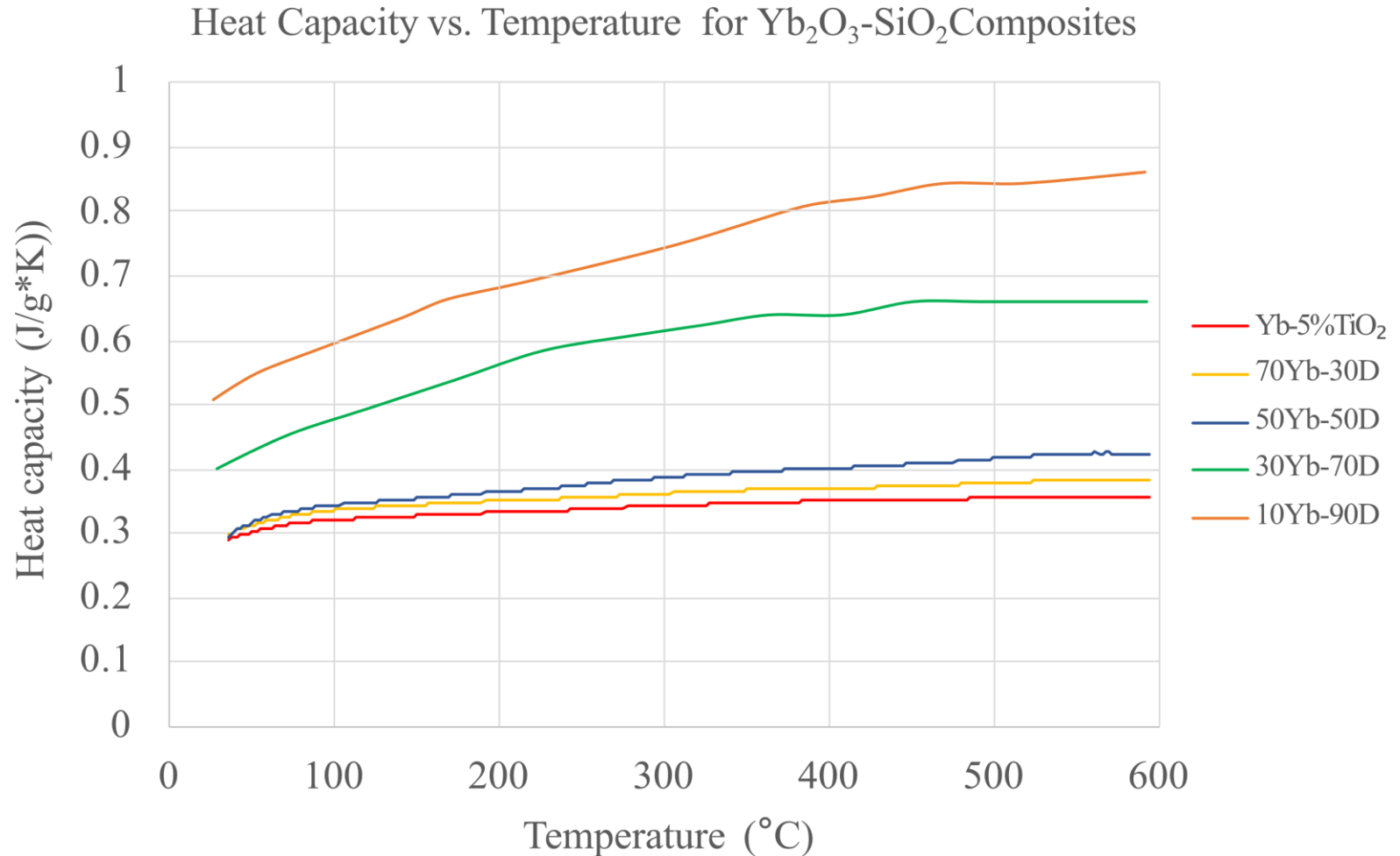
Sample	After heat treatment	
	Volume % of Y_2O_3	Volume % of SiCN
Y_2O_3	100	0
9Y-1D	98	2
7Y-3D	91	9
5Y-5D	82	18
1Y-9D	33	67
Durazane	0.00	100



Relative density of FAST samples processed at 1350°C for 5 mins under vacuum

Processing protocols to make high density Y_2O_3 -SiCN composites using FAST (needed for thermomechanical property measurement)

5. Task 3 - Heat Capacity of Yb_2O_3 - SiO_2 Composites



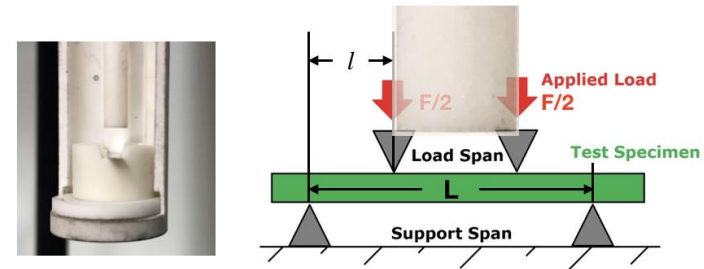
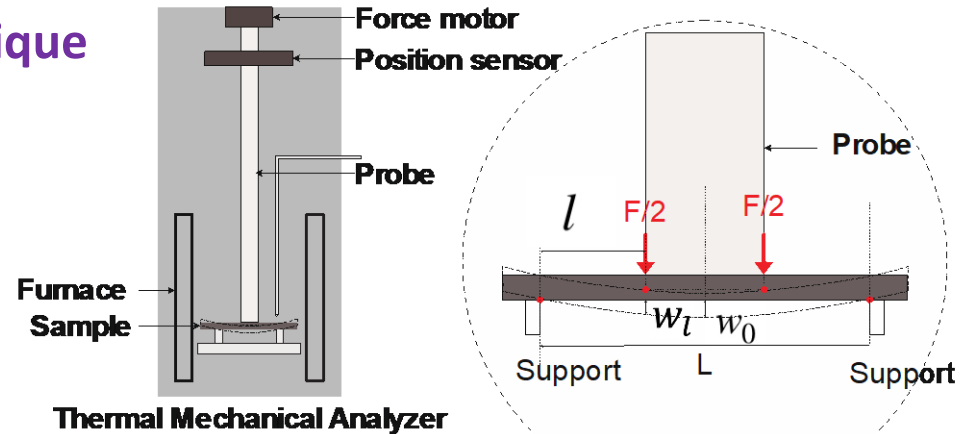
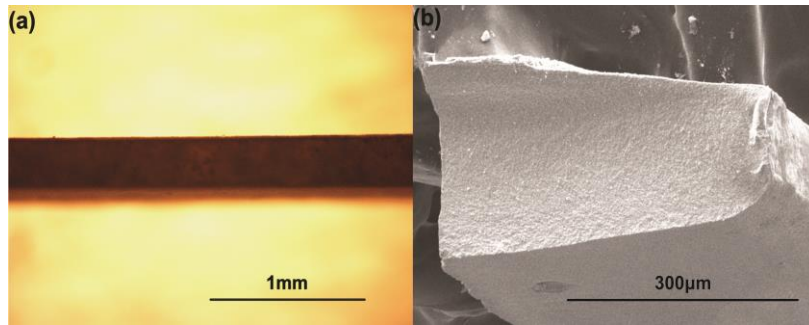
As expected, the higher Yb_2O_3 content, the lower heat capacity.

5. Task 3 - Elastic Modulus of Y_2O_3 -SiCN Composites

Developed Technique

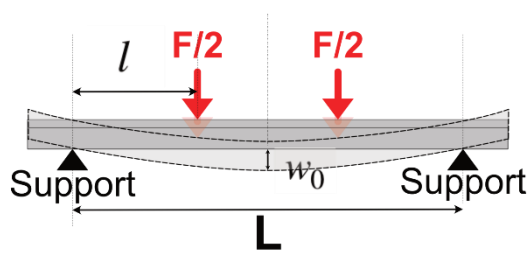


Thermo Mechanical Analyzer (SS6000)

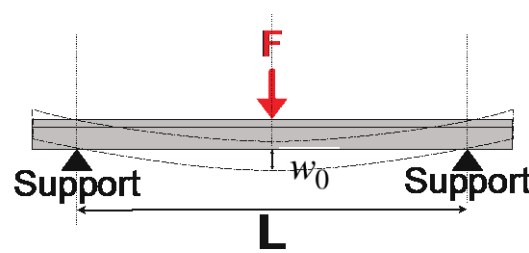
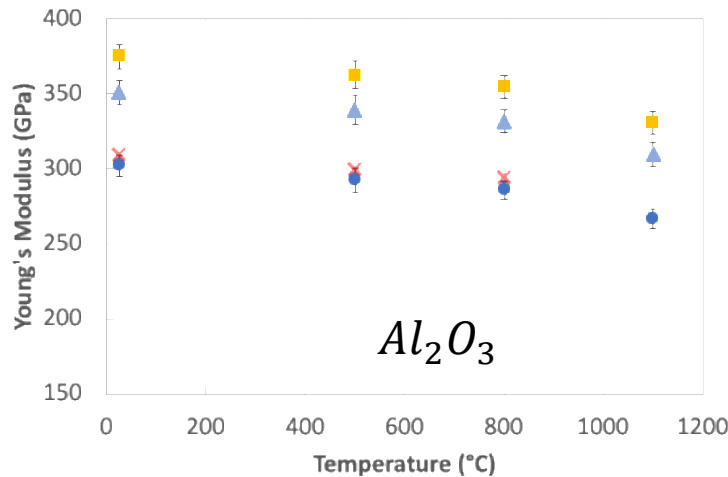


- ❖ Sample fabricated using laser machining
- ❖ Analysis uses the tapered sample cross-section

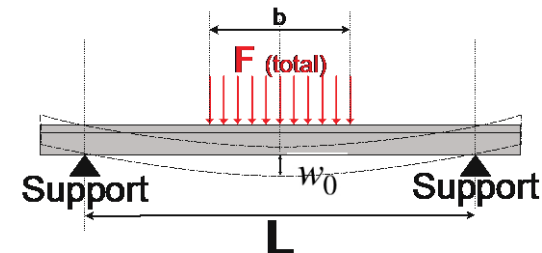
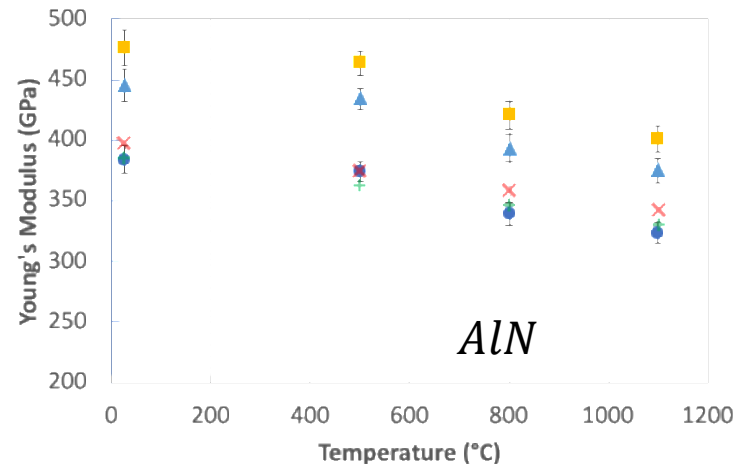
5. Task 3 – Elastic Modulus Technique Development



$$E = \frac{Fl(3L^2 - 4l^2)}{48Iw}$$



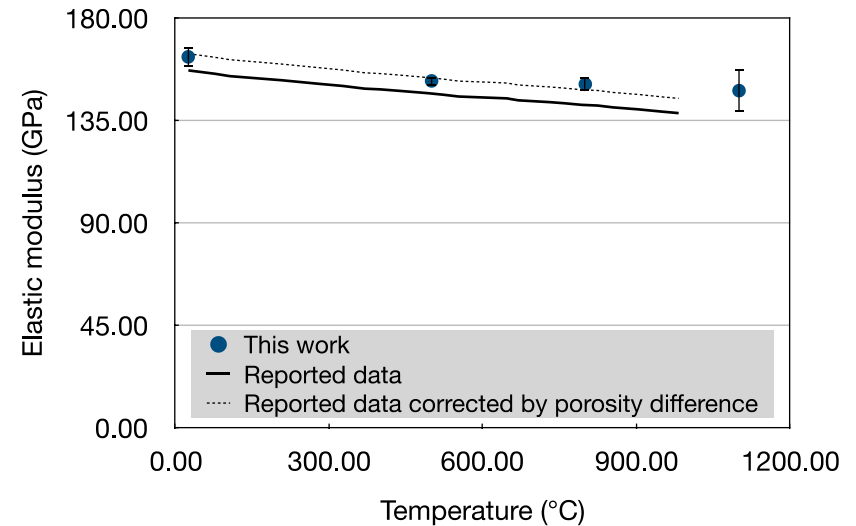
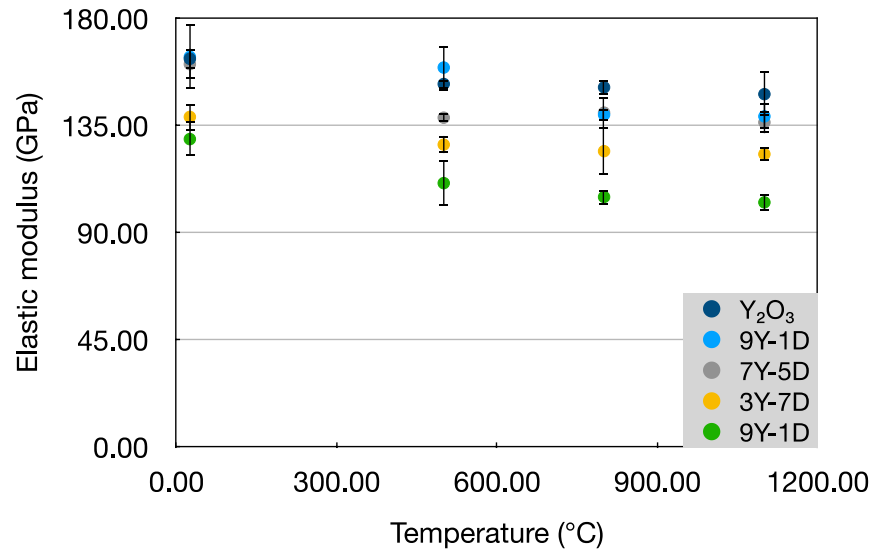
$$E = \frac{FL^3}{48Iw}$$



$$E = \frac{F(8L^3 - 4b^2L + b^3)}{384Iw}$$

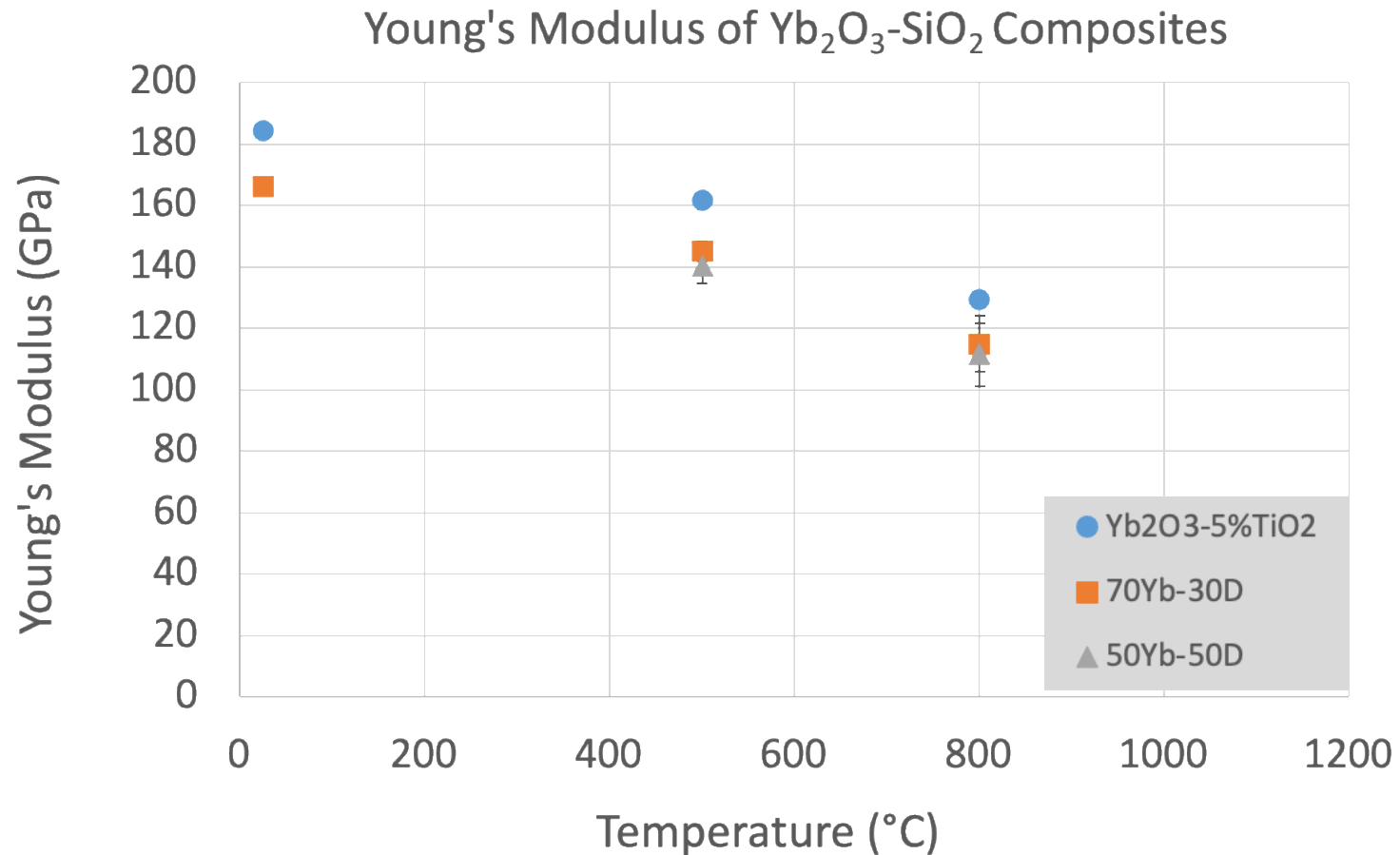
- ❖ 4-point model best since the modulus is measured at the start of the unloading process.
- ❖ The measured results match value the reported values for Al₂O₃ and AlN

5. Task 3 - Elastic Modulus of Y_2O_3 -SiCN Composites



- ❖ Elastic modulus of Y_2O_3 -SiCN composites decreased with temperature and the content of amorphous silicate phase.
- ❖ The temperature dependence of pure Y_2O_3 samples matches well with reported results.

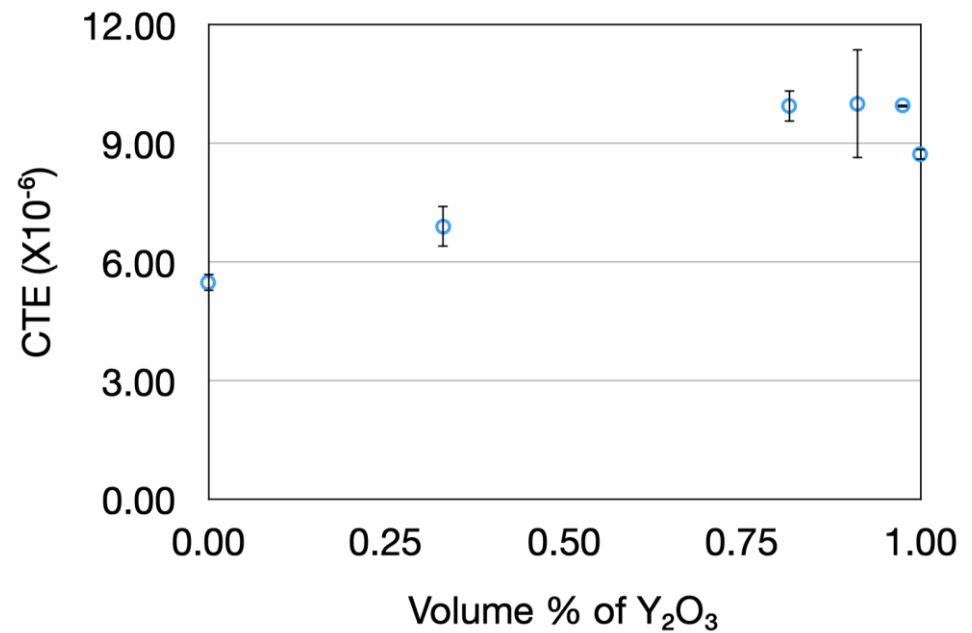
5. Task 3 - Elastic Modulus of Y_2O_3 - SiO_2 composites



❖ Elastic modulus of Y_2O_3 - SiO_2 composites decreased with temperature and SiO_2 content.

5. Task 3 - Coefficient of Thermal Expansion of Y_2O_3 -SiCN Composites

	CTE ($\times 10^{-6}/^\circ\text{C}$)
Y_2O_3	8.73
90Y-10D	9.97
70Y-30D	10
50Y-50D	9.95
10Y-90D	6.9
Durazane	5.49



- ❖ Pure Durazane derived ceramics have the lowest value
- ❖ Y_2O_3 value similar to reported data.
- ❖ The higher values for some composites maybe be due to oxidation during the CTE measurement.

5. Task 3 - Coefficient of Thermal Expansion of $\text{Y}_2\text{O}_3\text{-SiO}_2$ and $\text{Yb}_2\text{O}_3\text{-SiO}_2$ Composites

	CTE ($\times 10^{-6}/^\circ\text{C}$)
$\text{Y}_2\text{O}_3\text{-5TiO}_2$	8.46
90Y-10D	8.24
70Y-30D	7.67
50Y-50D	6.89
30Y-70D	4.64
10Y-90D	

	CTE ($\times 10^{-6}/^\circ\text{C}$)
$\text{Yb}_2\text{O}_3\text{-5TiO}_2$	8.07
90Yb-10D	8.14
70Yb-30D	8.11
50Yb-50D	7.66
30Yb-70D	5.80
10Yb-90D	3.26

- ❖ The CTEs of $\text{Y}_2\text{O}_3\text{-SiO}_2$ composites and $\text{Yb}_2\text{O}_3\text{-SiO}_2$ composites both decrease as the content of SiO_2 increases.

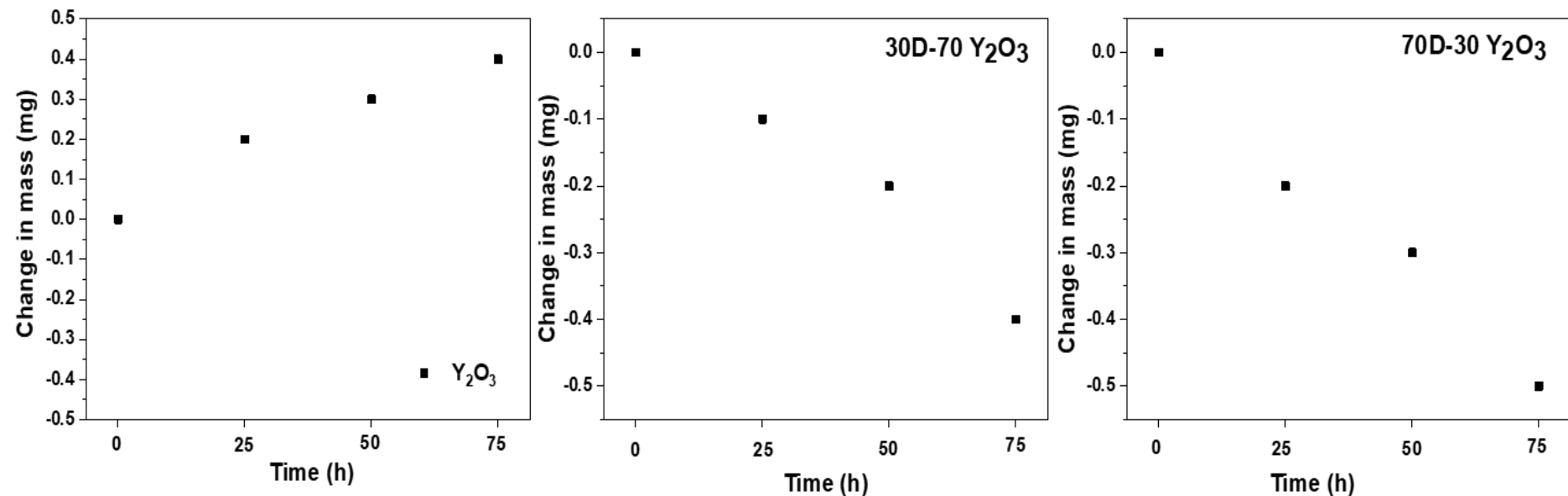
5. Project Progress - Task 3

Sub-task 3.2: Determine the effect of composition and microstructure of composites on oxidation and volatilization during exposure to high velocity steam at temperatures up to 1350°C.

- Significant work has been done and analysed in year 1 and 2.
- In the year 3, we have modified our steam oxidation set up by introducing zirconia holder and sapphire tube instead of alumina holder and tube to reduce the contamination
- In addition, we have modified the set up to introduce flushing inert gas to reduce contamination
- In consultation with GE, it was decided to focus only on Y_2O_3 and its composites.

This sub-task is 100 % complete

5. Task 3 - Steam oxidation behavior of Y_2O_3 and its composite



- ❖ Small increase in mass with time for the Y_2O_3 sample - due to the deposition of alumina contamination
- ❖ Composite material shows linear mass loss with time
- ❖ 70D-30 Y_2O_3 composite material shows higher mass loss compared to 30D-70 Y_2O_3 due to the presence of higher amount of silica-rich phase.

As postulated in the proposal, Y_2O_3 and high Y_2O_3 low SiO_2 composites are more resistant to high velocity stream oxidation and volatilization

5. Project Progress - Task 4

Task 4: Graded composition coatings using cold spray followed by heat treatment (30 % completed)

- **Sub-task 4.1:** Design and processing of the optimized composition graded coatings (60 % completed)

In the year 2, we have completed the following goals:

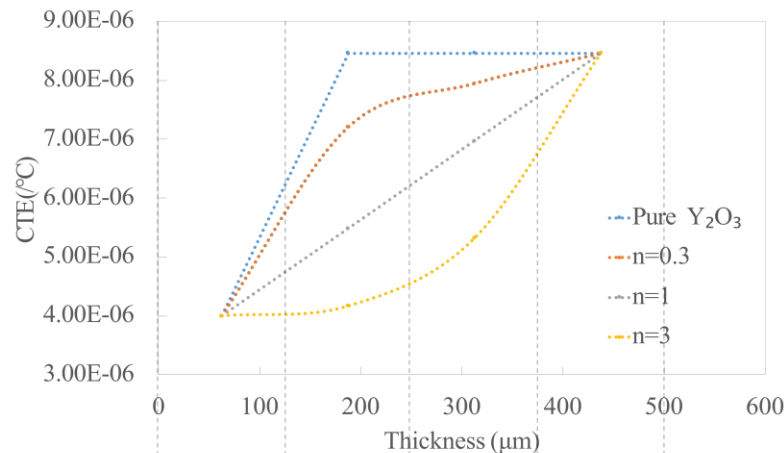
- The cold spray system to make coatings has been assembled
- Developed the protocol of the Y_2O_3 -SiCN submicrometer suspension
- Studied the microstructure uniformity of Y_2O_3 -SiCN composite film from dip-coating

In this year 3, we have focused on the following aspects:

- Determined the optimal composition profile for the graded coatings through COMSOL simulation

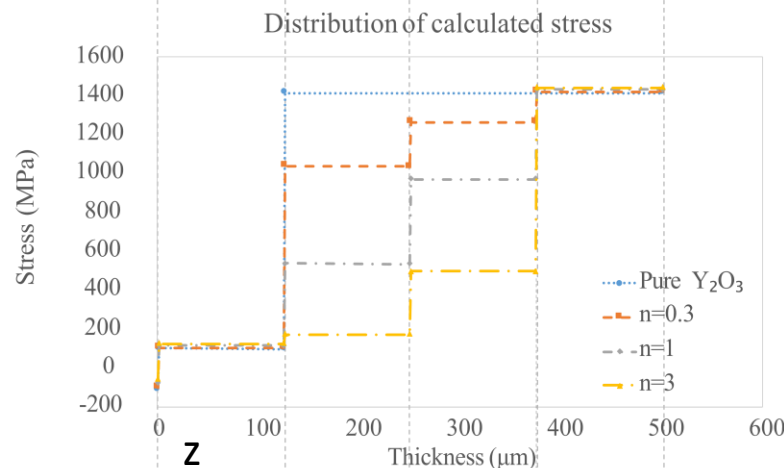
5. Task 4 - Optimal Composition Profile for the Graded Coatings

Design of CTE change vs position z by variation of n value



Assume CTE of the composites follows the rule of mixture.

- ❖ The thermal stress in the top coating remains almost constant.
- ❖ The thermal stress in the intermediate layers have the lowest thermal stress with the compositional profile when $n=3$ ($CTE_1=5.32 \times 10^{-6}/^{\circ}C$, $CTE_2=4.16 \times 10^{-6}/^{\circ}C$).

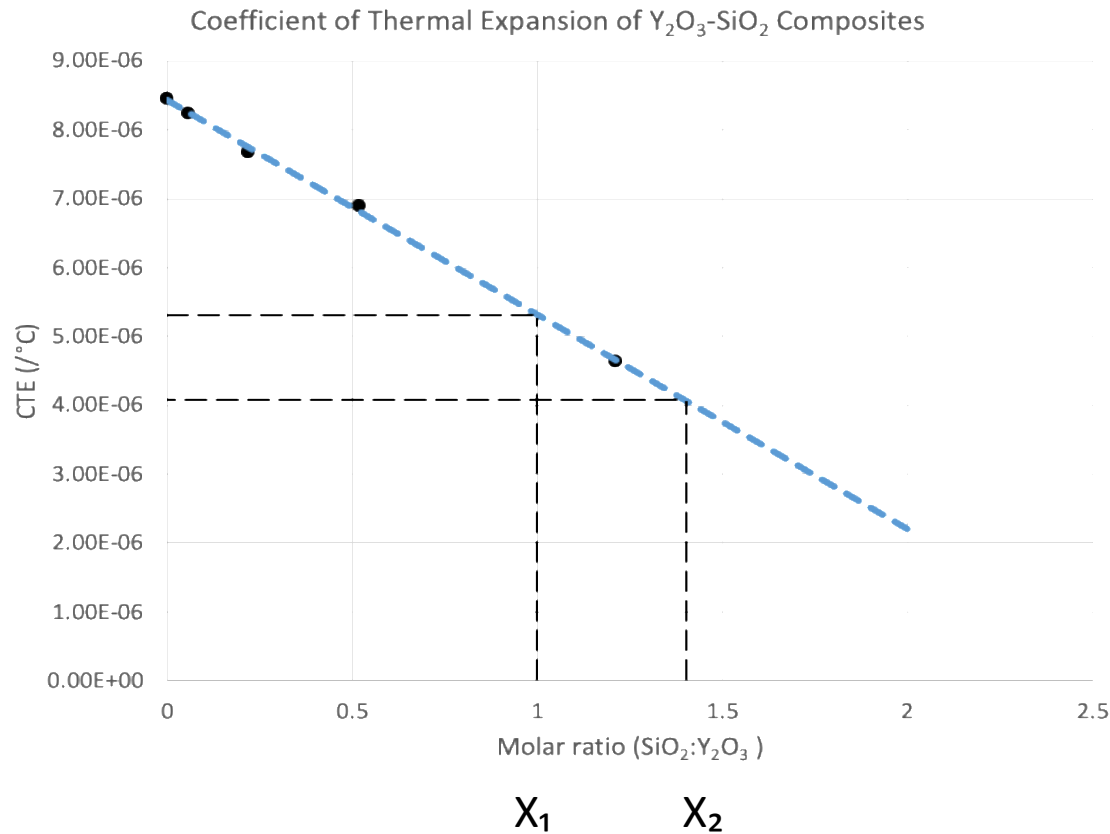


$$V_{Y_2O_3}(z) = \left(\frac{z}{h}\right)^n$$

5. Task 4 - Optimal Composition Profile for the Graded Coatings (Contd.)

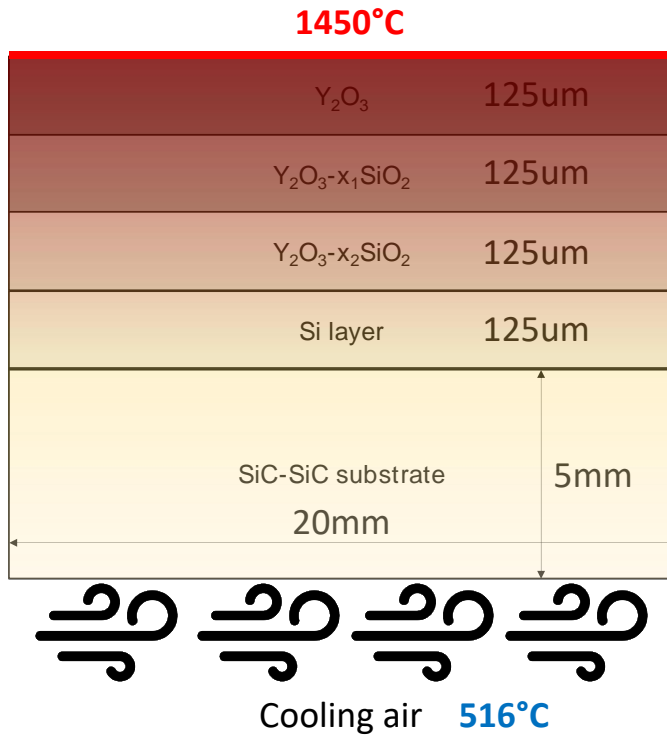
$$\text{CTE} = 5.32 \times 10^{-6} / ^\circ\text{C}$$

$$\text{CTE} = 4.16 \times 10^{-6} / ^\circ\text{C}$$



- ❖ Based on the required CTE values ($5.32\text{E-}6$ and $4.16\text{E-}6$) when $n=3$, we can determine the required compositions of the intermediate layers (x_1, x_2)

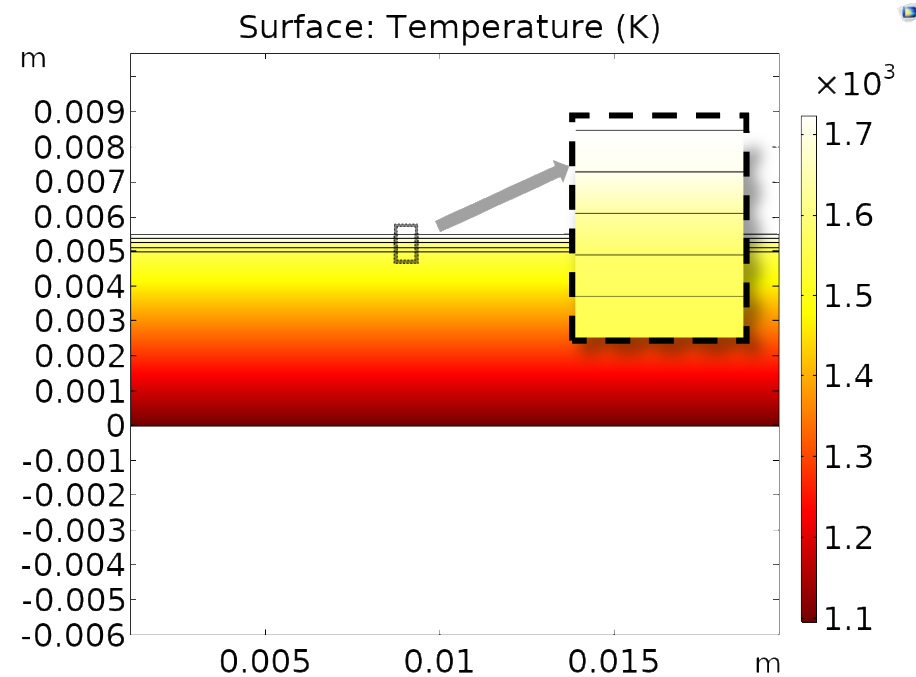
5. Task 4 - Temperature Profile Simulation Set Up



Parameter	Value
Thermal conductivity (Y_2O_3)	7 W/(m·K)
Thermal conductivity ($\text{Y}_2\text{O}_3\text{-x}_1\text{SiO}_2$) ^[1]	1.4 W/(m·K)
Thermal conductivity ($\text{Y}_2\text{O}_3\text{-x}_2\text{SiO}_2$)	2 W/(m·K)
Thermal conductivity (Si) ^[2]	25 W/(m·K)
Thermal conductivity (SiC/SiC) ^[3]	15 W/(m·K)
Heat transfer coefficient (cooling air) ^[4]	3000 W/(m ² ·K)
Temperature (Top surface of Y_2O_3 layer)	1450° C
Temperature (Cooling air) ^[4]	516° C

Boundary conditions in consultation with GE

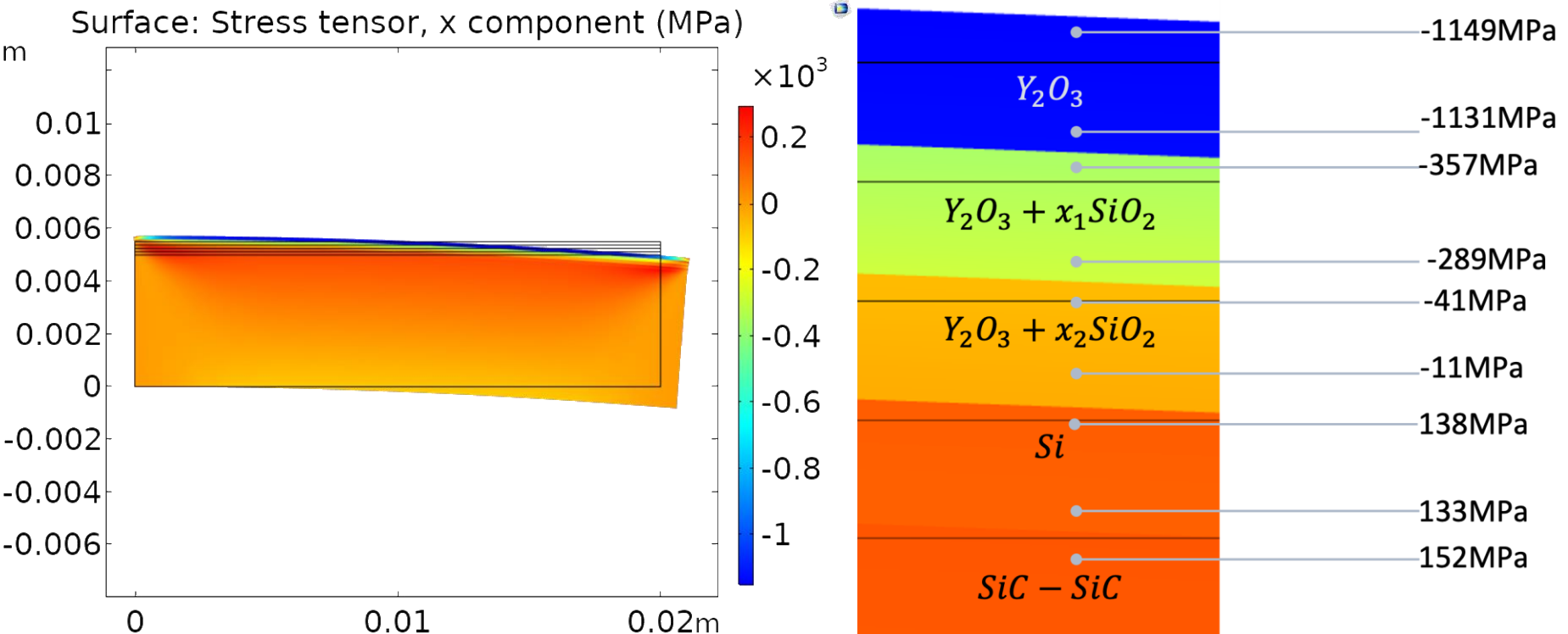
5. Task 4 - Simulated Temperature Profile by COMSOL (on changing gas temperature from 25°C to 1450°C)



Location	Initial T (°C)	Final T (°C)
Top surface of Y_2O_3 layer	25	1450
Y_2O_3 and $\text{Y}_2\text{O}_3\text{-x}_1\text{SiO}_2$ interface	25	1419
$\text{Y}_2\text{O}_3\text{-x}_1\text{SiO}_2$ and $\text{Y}_2\text{O}_3\text{-x}_2\text{SiO}_2$ interface	25	1337
$\text{Y}_2\text{O}_3\text{-x}_2\text{SiO}_2$ and Si interface	25	1266
Si and SiC/SiC interface	25	1261
Bottom surface of SiC/SiC	25	891

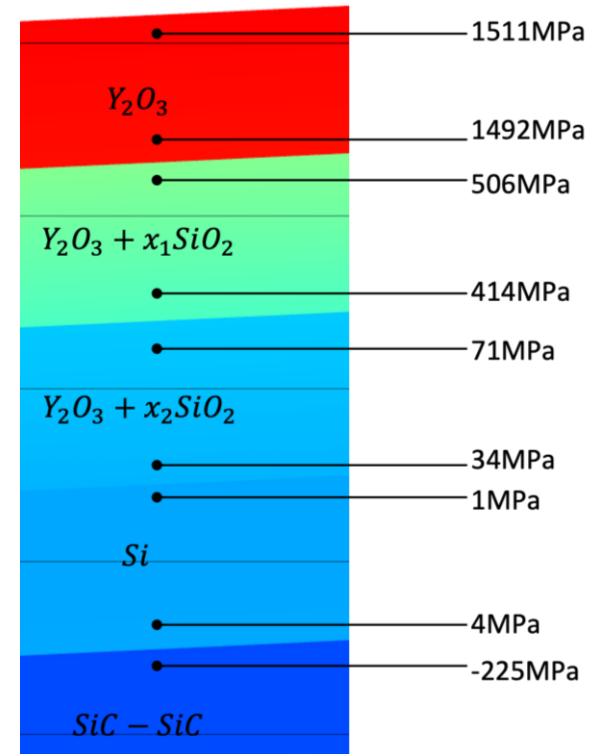
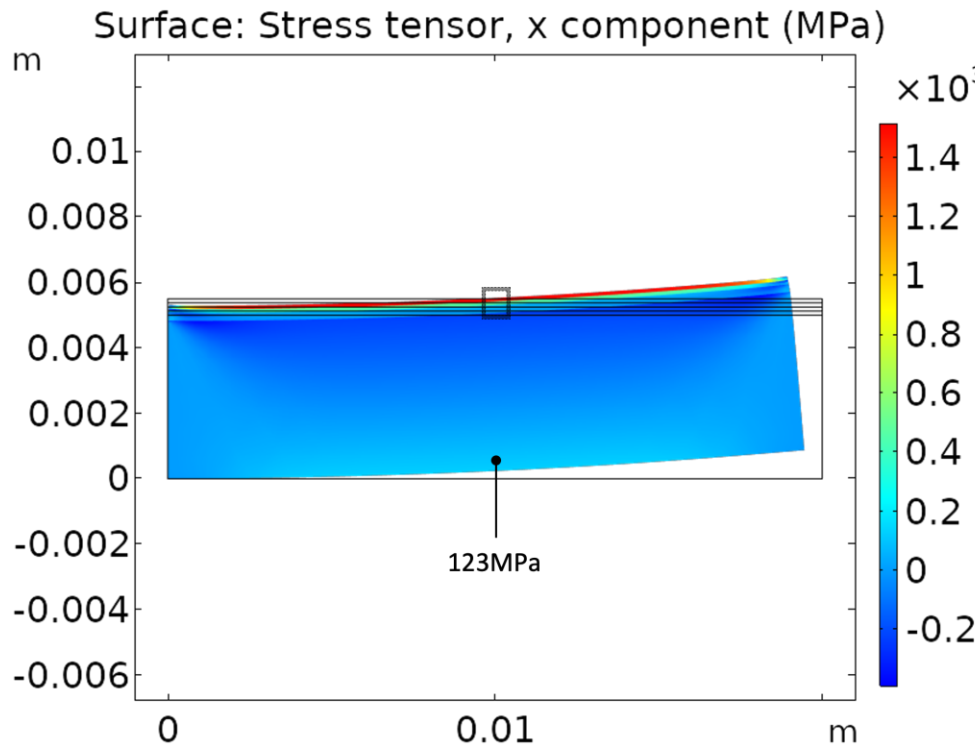
❖ Steady state temperatures obtained in each layer

5. Task 4 - Simulated Thermal Stress Profile 25°C (stress free) → 1450°C



- ❖ EBC layers are under tension. The stress in the top layer (Y_2O_3) is high due to significant CTE mismatch.
- ❖ The stresses in the intermediate layers are much lower – advantage of graded coating

5. Task 4 - Simulated Thermal Stress Profile 1450°C (stress free) → 25°C



- ❖ EBC layers are under compression. The stress in the top layer (Y_2O_3) is high due to significant CTE mismatch.
- ❖ The stresses in the intermediate layers are much lower – advantage of graded coating

5. Project Progress - Task 4

- **Sub-task 4.2:** Characterization of the oxidation and volatilization during exposure to high velocity steam at temperatures up to 1500°C and performance in burner rig. (20 % completed)

In the year 2 and 3, we have developed the steam oxidation set up for coated samples.

- **Sub-task 4.3:** Thermal cycling investigation of the coatings

We have not started sub-task

5. Project Progress - Task 5

Task 5: Processing and performance of graded coatings processed using atmospheric plasma spraying (APS) (50% completed)

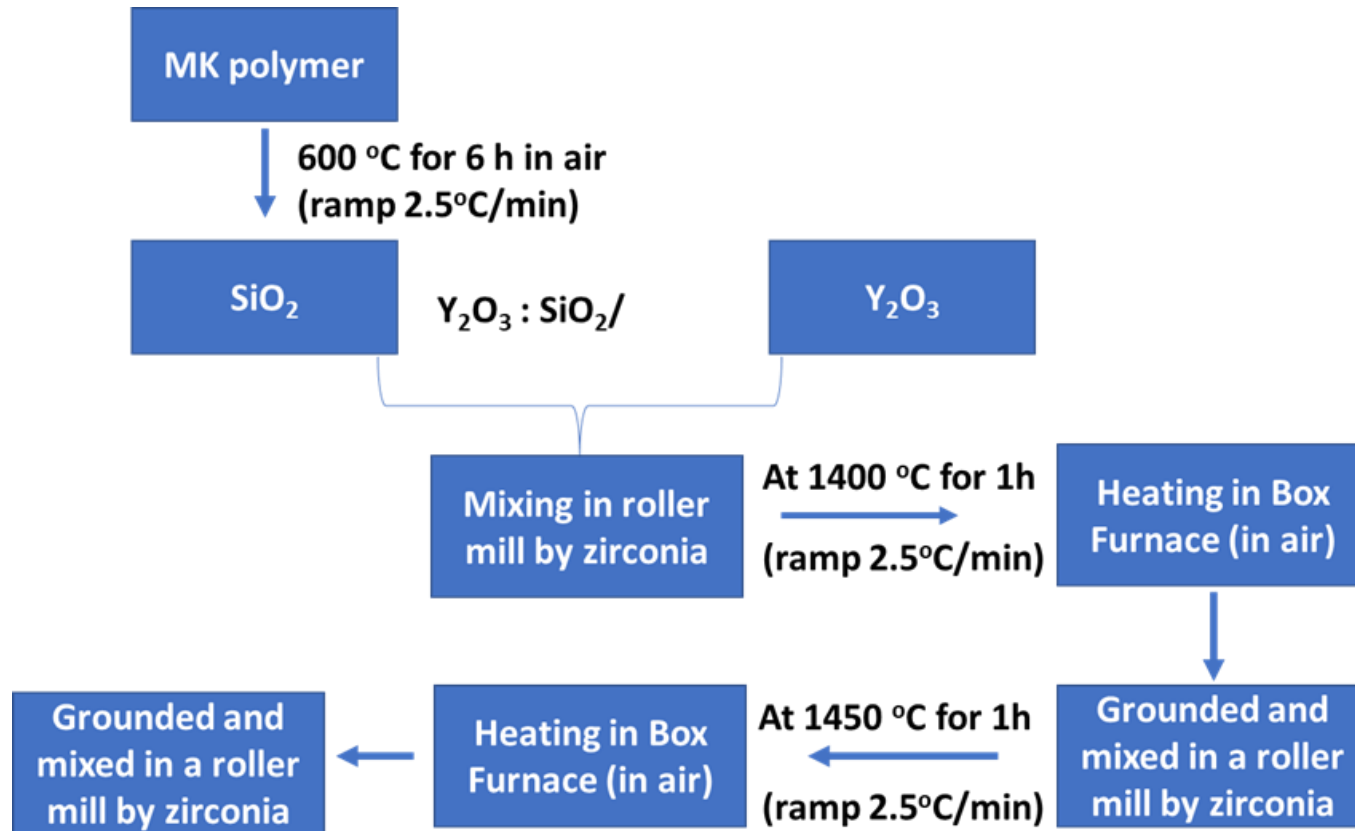
- **Sub-task 5.1: Processing of powders suitable for APS (100% completed)**

We initiated this sub-task in year 2 (about 10%).

In this year, we have done significant work and completed this sub-task.

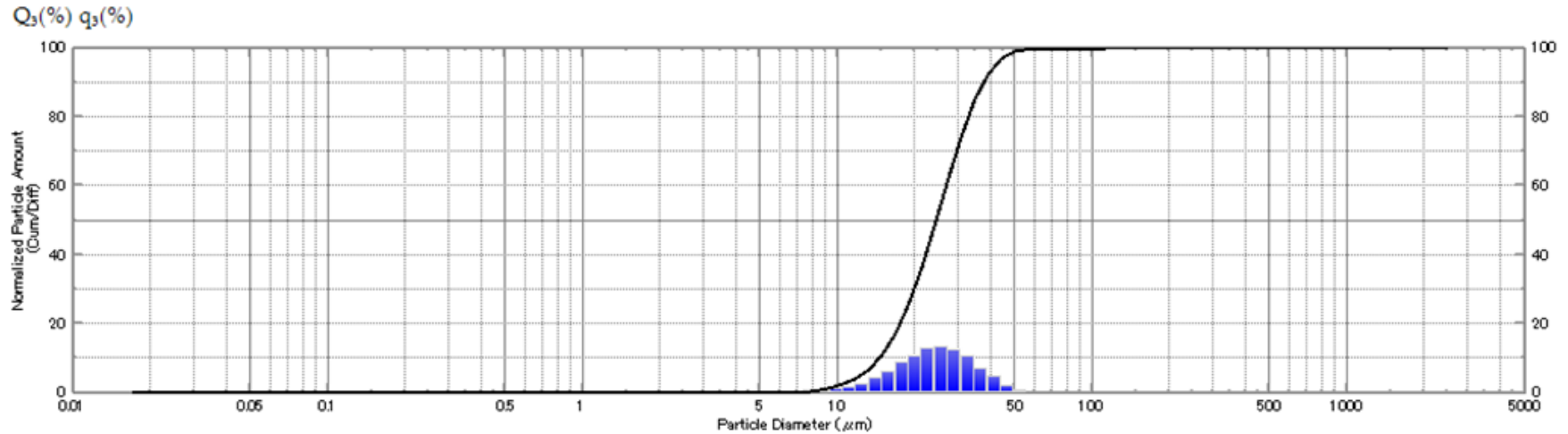
1. Determined the optimal composition for graded coating through COMSOL simulation.
2. Subsequently, we have synthesized large quantity of optimized composite sample (~6.5 lb)
3. Analyze the particle size suitable for APS.
4. We have sent composite sample along with pure Y_2O_3 sample to GE

5. Task 5 - Processing of Powders Suitable for APS



Complete protocol for large scale synthesis of composite powders

5. Task 5: Particle size analysis



❖ Average particle size of the composite powder ~ 24 micron

5. Project Progress - Task 5

- **Sub-task 5.2:** Processing of graded coatings using APS

This sub-task will be done by GE in Quarter 13

- **Sub-task 5.3:** Characterization of the oxidation and volatilization of APS coatings during exposure to high velocity steam at temperatures up to 1500°C and performance in burner rig.

This sub-task will start in Quarter 14

- **Sub-task 5.4:** Thermal cycling investigation of the APS coatings.

This sub-task will start in Quarter 14

6. Project Short Term Plans

- ❖ Complete sub-task 3.1 (10% remaining)
- ❖ Fabricate graded coating using the cold spray method and characterize the microstructure (sub-Task 4.1).
- ❖ Steam oxidation behavior of coated sample (sub-tasks 4.2 and 4.3)

Milestones

The milestones remained the same as in the original Statement of Work. Due to the one-year no-cost extension, the completion date was modified and approved by DoE.

Year 1

- ❖ M1: Selection of polymers and acquisition of the needed materials. Planned completion: end of Q1 (12/17) (Status: Completed).
- ❖ M2: Establish the effect of composition and processing temperature on the phase and microstructure of $\text{Y}_2\text{O}_3\text{-Si-B-C-N}$ and $\text{Yb}_2\text{O}_3\text{-Si-B-C-N}$ composites Planned completion: end of Q3 (6/18) (Status: Completed).
- ❖ M3: Design and fabrication of the cold spray processing of coatings and high velocity steam oxidation equipment Planned completion: end of Q3 (6/18) (Status: Completed).
- ❖ M4: Establish the effect of temperatures on the phase stability during oxidation at temperatures up to 1500°C . Planned completion: end of Q4 (9/18) (Status: Completed).

Milestones (Contd.)

Year 2

No Milestones planned for completion in Year 2

Year 3

- M5: Determine thermal expansion coefficient, elastic modulus and thermal conductivity for select composite coating compositions **Planned completion: end of Q12 (9/20) (Status: 90 % Completed)**
- M6: Determine the effect of composition on oxidation and volatilization during exposure to high velocity steam at temperatures up to 1500°C. **Planned completion: end of Q12 (9/20) (Status: 100% completed).**

Milestones (Contd.)

Year 4

- ❖ M7: Processing of composition graded coatings using cold-spray and pyrolysis. Planned completion: end of Q15 (6/21) (Status: 50% completed).
- ❖ M8: Determine the effect of exposure to high velocity steam at temperatures up to 1500°C on graded coatings made using cold spray and pyrolysis Planned completion: end of Q15 (6/21) (Status: 0 % complete)
- ❖ M9: Investigate the effect of thermal cycling and steam oxidation on graded coatings made using cold spray and pyrolysis Planned completion: end of Q13 (12/20) (Status: 0 % complete) .
- ❖ M10: Supply powders for APS to GE Power (Clemson) Planned completion end of Q13 (12/20) (Status: 100 % Completed)

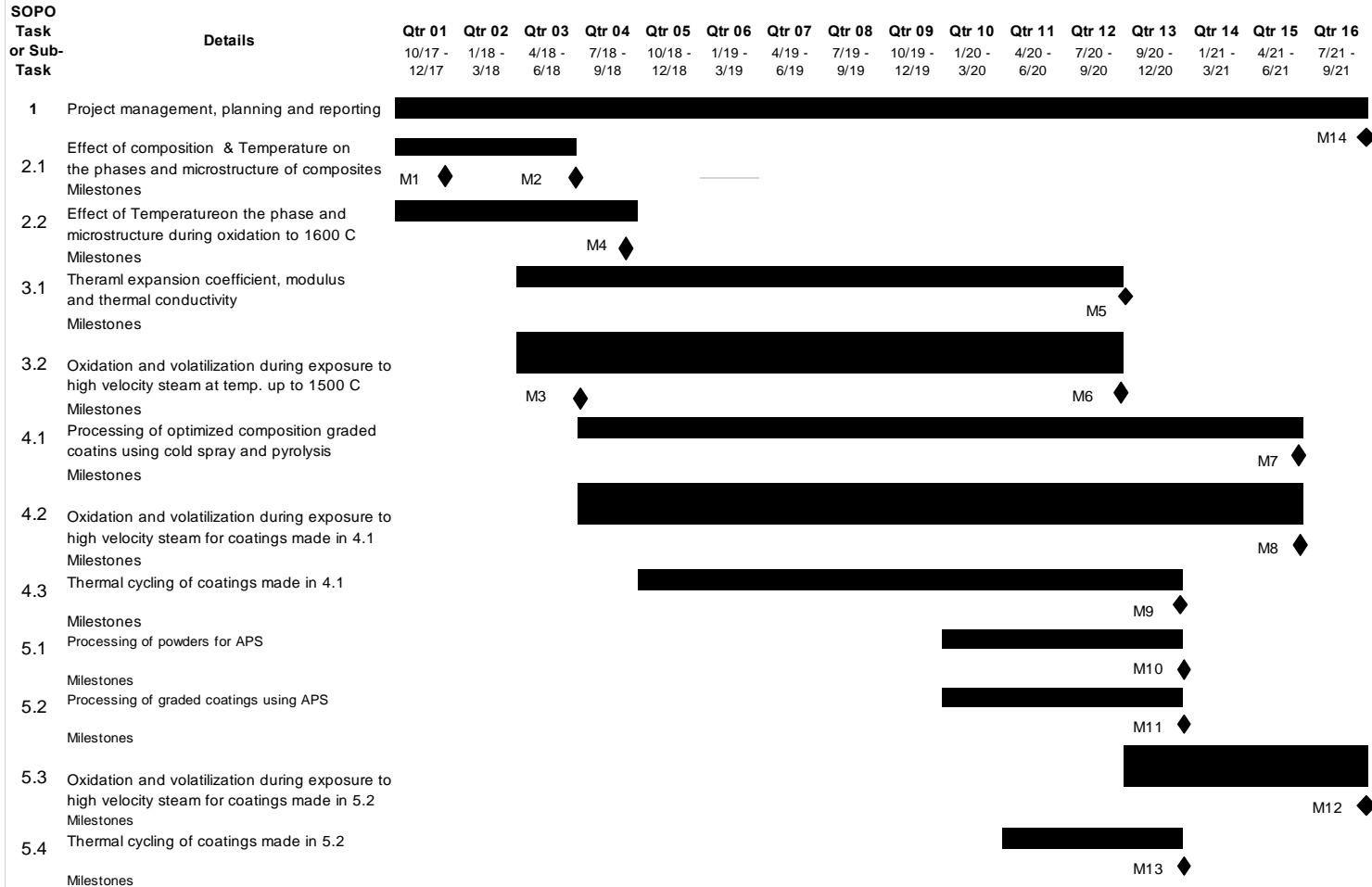
Milestones (Contd.)

Year 4 (Contd.)

- ❖ M11: Complete Fabrication of graded coatings using APS Planned completion: end of Q13 (12/20) (Status: 0 % completed)
- ❖ M12: Establish the effect of exposure to high velocity steam at temperatures up to 1500°C on graded coatings made by APS Planned completion: end of Q16 (9/21) (Status: 0 % completed)
- ❖ M13: Investigate the effect of thermal cycling on graded coatings made by APS Planned completion: end of Q13 (12/20) (Status: 0 % completed)
- ❖ M14: Phase 1 completion including final report Planned completion: end of Q16 (9/21) Status: Ongoing

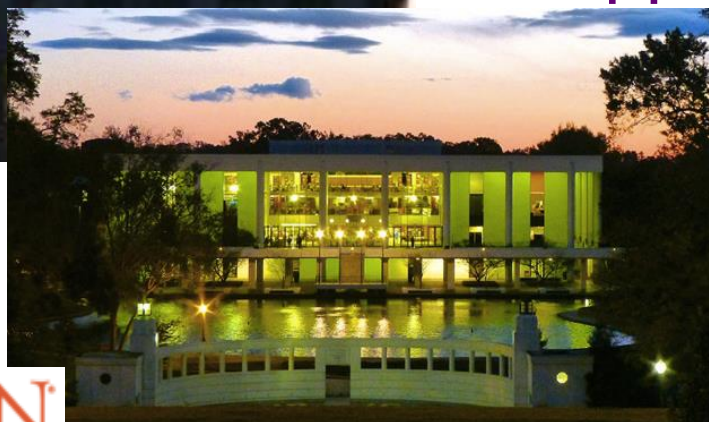
Current Version of Timeline

TA[3] Integrated TBC/EBC for Next Generation Gas Turbines (Clemson col. with GE Power)





Thank you very much
for your attention and
support



Rajendra K. Bordia and Fei Peng