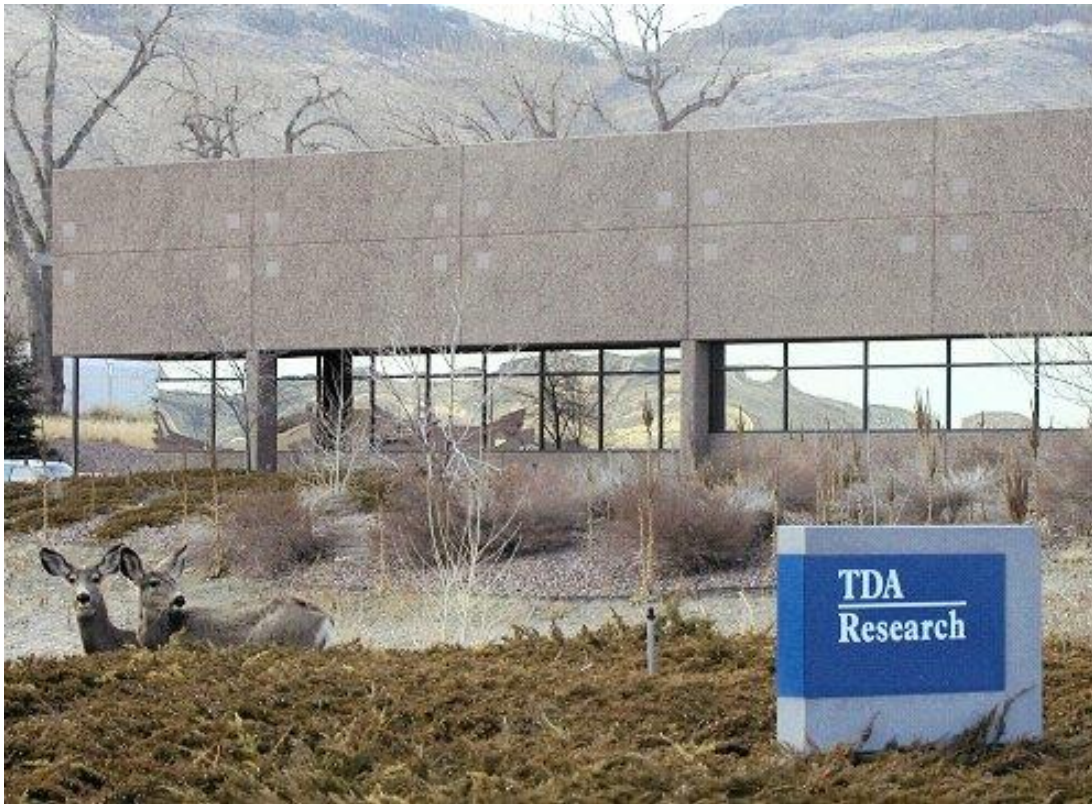


Integrated Water-Gas-Shift Pre-Combustion Carbon Capture Process (Contract No. DE-FE0023684)



**Gökhan Alptekin, PhD
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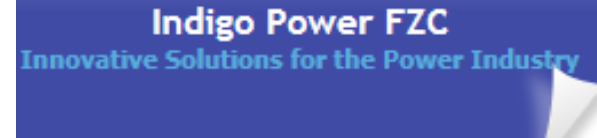
**2020 Gasification Systems
Project Review**

September 3, 2020

Project Objectives

- **The project objective is to demonstrate techno-economic viability of an integrated WGS catalyst/CO₂ removal system for IGCC power plants and CTL plants**
 - A high temperature PSA adsorbent is used for CO₂ removal above the dew point of the synthesis gas
 - A commercial low temperature catalyst is used for water-gas-shift
 - An effective heat management system is developed
- **Project Tasks**
 - Design a fully-equipped slipstream test unit with 10 SCFM raw synthesis gas treatment capacity
 - Design and fabricate CFD optimized reactors capable of managing the WGS exotherm while maintaining energy efficiency
 - Demonstrate critical design parameters including sorbent capacity, CO₂ removal efficiency, extent of WGS conversion as well as H₂ recovery using coal synthesis gas
 - Complete a high fidelity process design and economic analysis

Project Partners



Project Duration

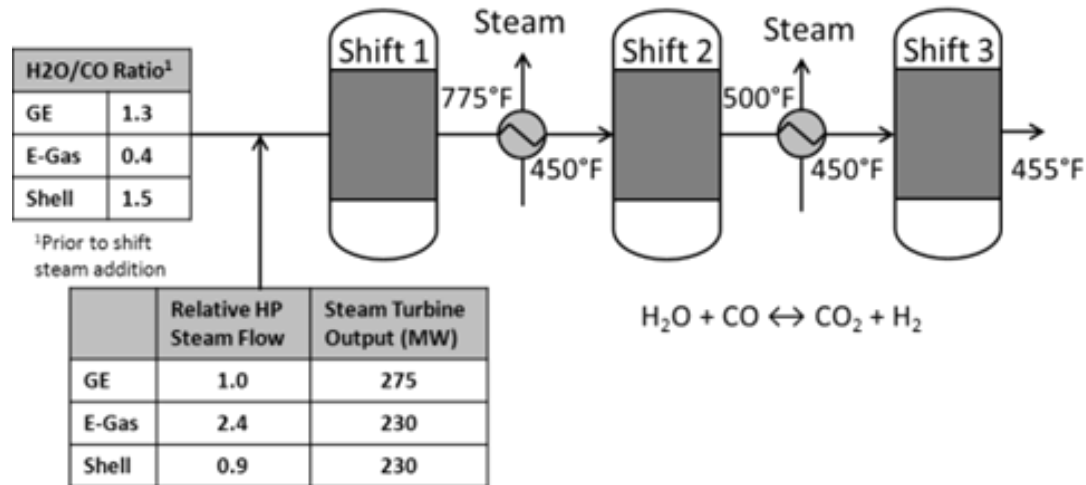
- Start Date = October 1, 2014
- End Date = September 30, 2020

Budget

- Project Cost = \$5,632,619
- DOE Share = \$4,506,719
- TDA and its partners = \$1,125,900

TDA's Approach

- Conventional IGCC plants use multi-stage WGS with inter-stage cooling
 - WGS is an equilibrium-limited exothermic reaction
- Water is supplied at concentrations well above required by the reaction stoichiometry to completely shift the CO to CO₂

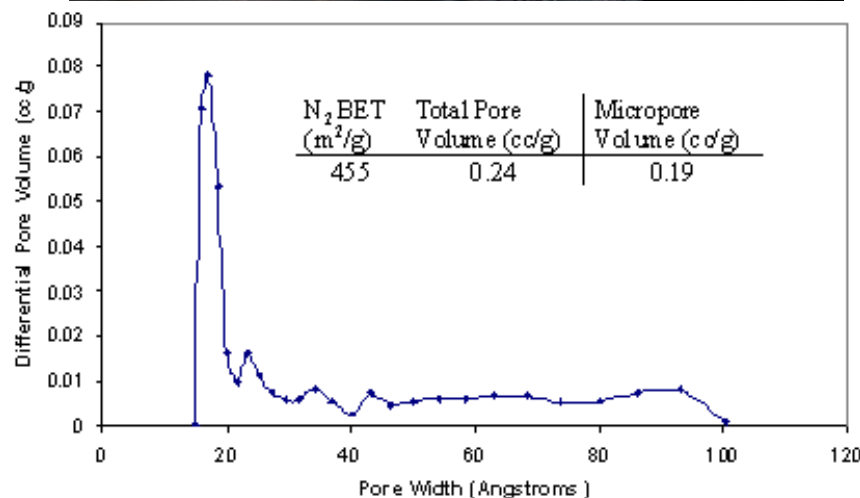


3-stage WGS unit as described in the DOE/NETL-2007/1281

- In our process, the WGS catalyst is combined with a high temperature CO₂ adsorbent to achieve high CO conversion at low steam:carbon ratios
- Reduced water addition increases process efficiency

TDA's Sorbent

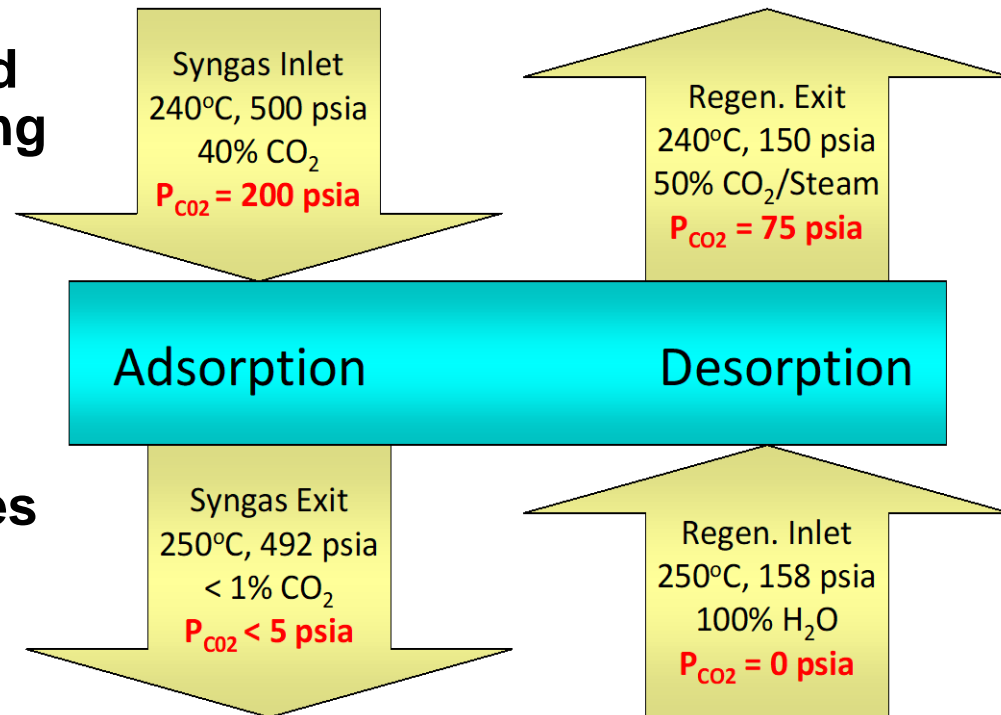
- TDA's uses a mesoporous carbon with surface functional groups that remove CO₂ via strong physical adsorption
 - CO₂-surface interaction is strong enough to allow operation at elevated temperatures
 - Because CO₂ is not bonded via a covalent bond, energy input for regeneration is low
- Heat of CO₂ adsorption is **4.9 kcal/mol** for TDA sorbent
 - Net energy loss in sorbent regeneration is similar to Selexol; much higher IGCC efficiency can be achieved due to high temperature CO₂ capture
- Favorable material properties
 - Pore size is tuned to 10 to 100 Å
 - Mesopores eliminates diffusion limitations



US Patent 9,120,079, Dietz, Alptekin, Jayaraman "High Capacity Carbon Dioxide Sorbent", US 6,297,293; 6,737,445; 7,167,354
US Pat. Appl. 61790193, Alptekin, Jayaraman, Copeland "Pre-combustion CO₂ Capture System Using a Regenerable Sorbent"

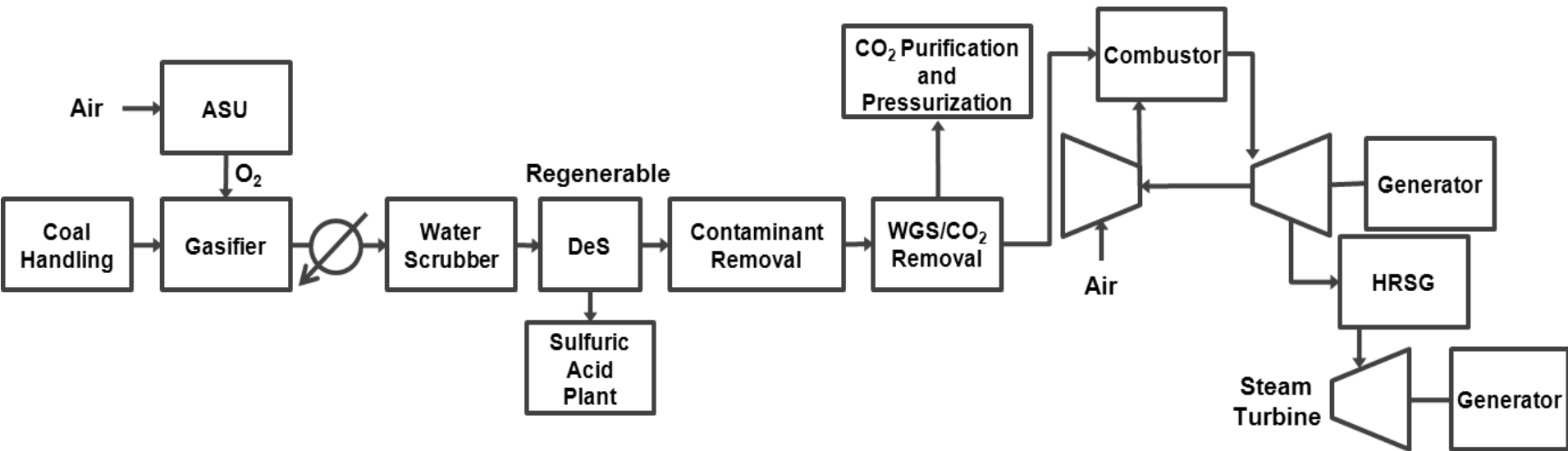
Operating Conditions

- **CO₂ is recovered via combined pressure & concentration swing**
 - CO₂ recovery at ~150 psia reduces energy need for CO₂ compression
 - Small steam purge ensures high product purity
- **Isothermal operation eliminates heat/cool transitions**
 - Rapid cycles reduces cycle time and increases sorbent utilization
- **Similar PSA systems are used in commercial H₂ plants and air separation plants**
- **The WGS catalyst was subjected to the same cycle**



Source: Honeywell/UOP

Integrated WGS/CO₂ Capture System

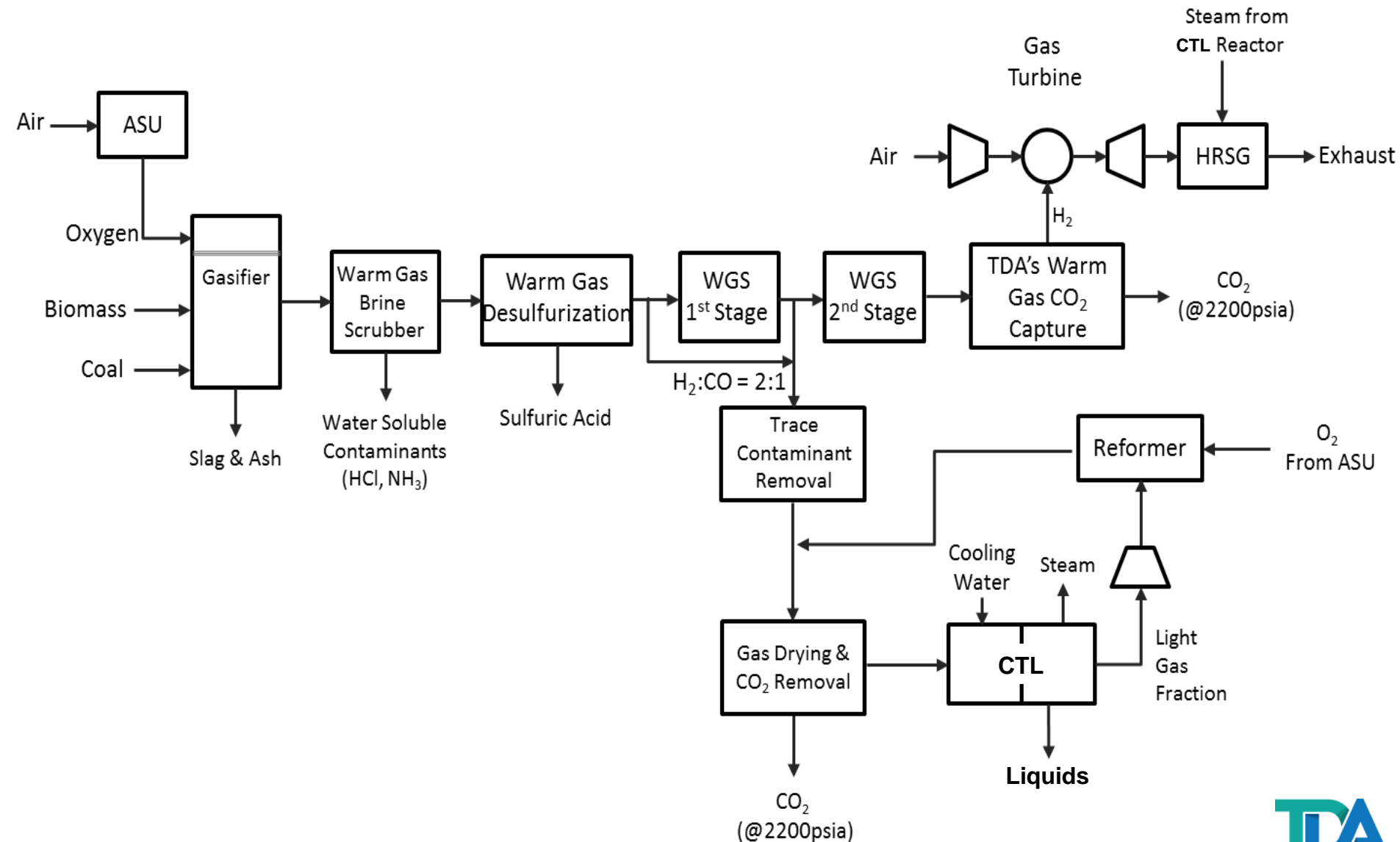


- **Reducing the use of excess steam improves power cycle efficiency**
 - Lower energy consumption to raise the steam
- **Process intensification could potentially reduce the number of hardware components and cost**

Sorbent's point of view:

- **Less dilution with water increases CO₂ partial pressure and in turn improves sorbent's working capacity**

Application of the Technology to CTL



Sorbent Development Work



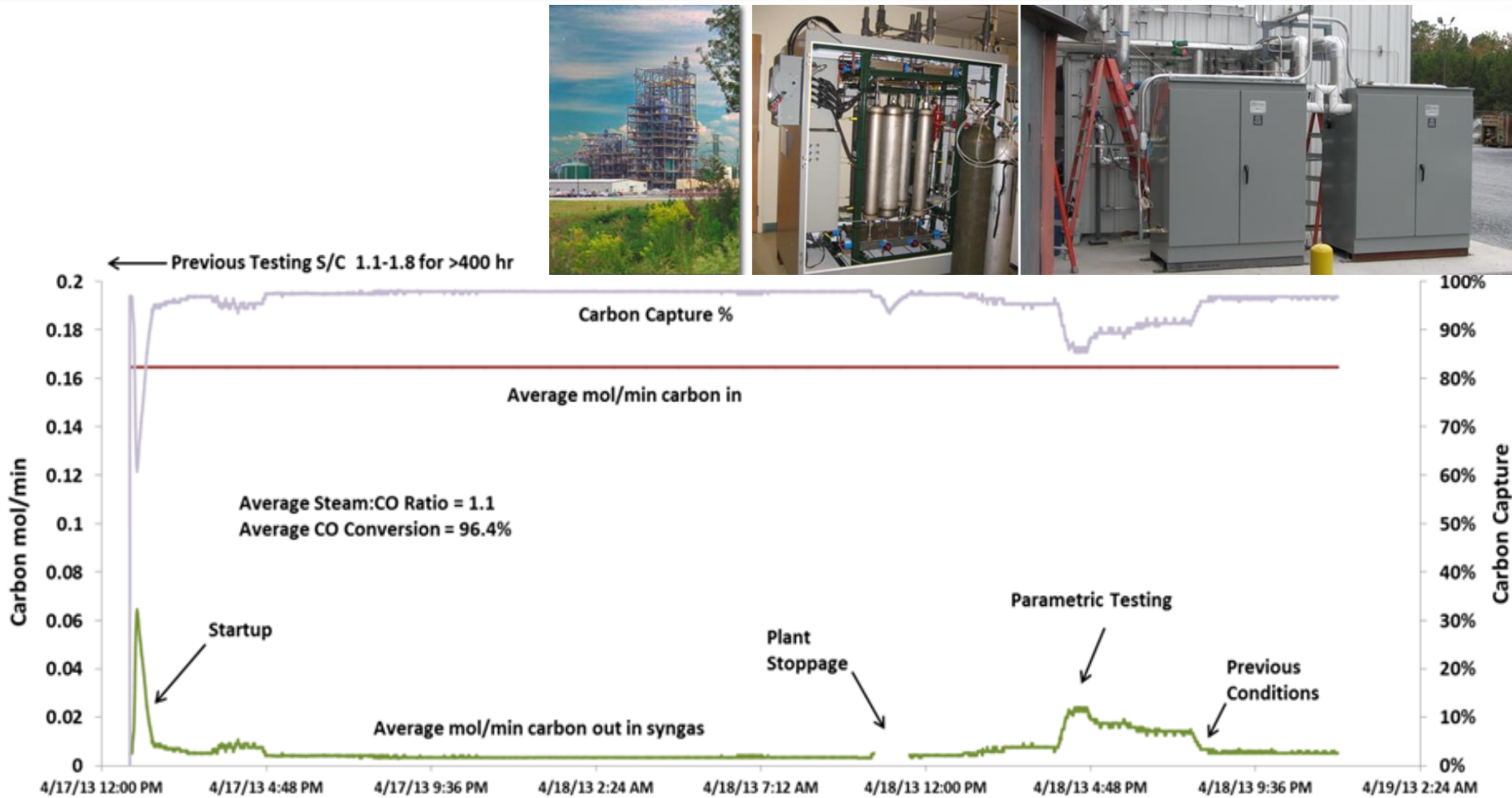
TDA 0.1 MW pre-combustion carbon capture unit installed at the National Carbon Capture Center

- **0.1 MW_e test in a world class IGCC plant to demonstrate full benefits of the technology**
 - Field Test #1 at NCCC
 - Field Test #2 at Sinopec Yangtzi Petrochemical Plant, Nanjing, Jiangsu Province, China
- **Full operation scheme**
 - 8 reactors and all accumulators
 - Utilize product/inert gas purges
 - H₂ recovery/CO₂ purity



Yangtzi Petro-chemical Plant

NCCC Field Test – Early Work

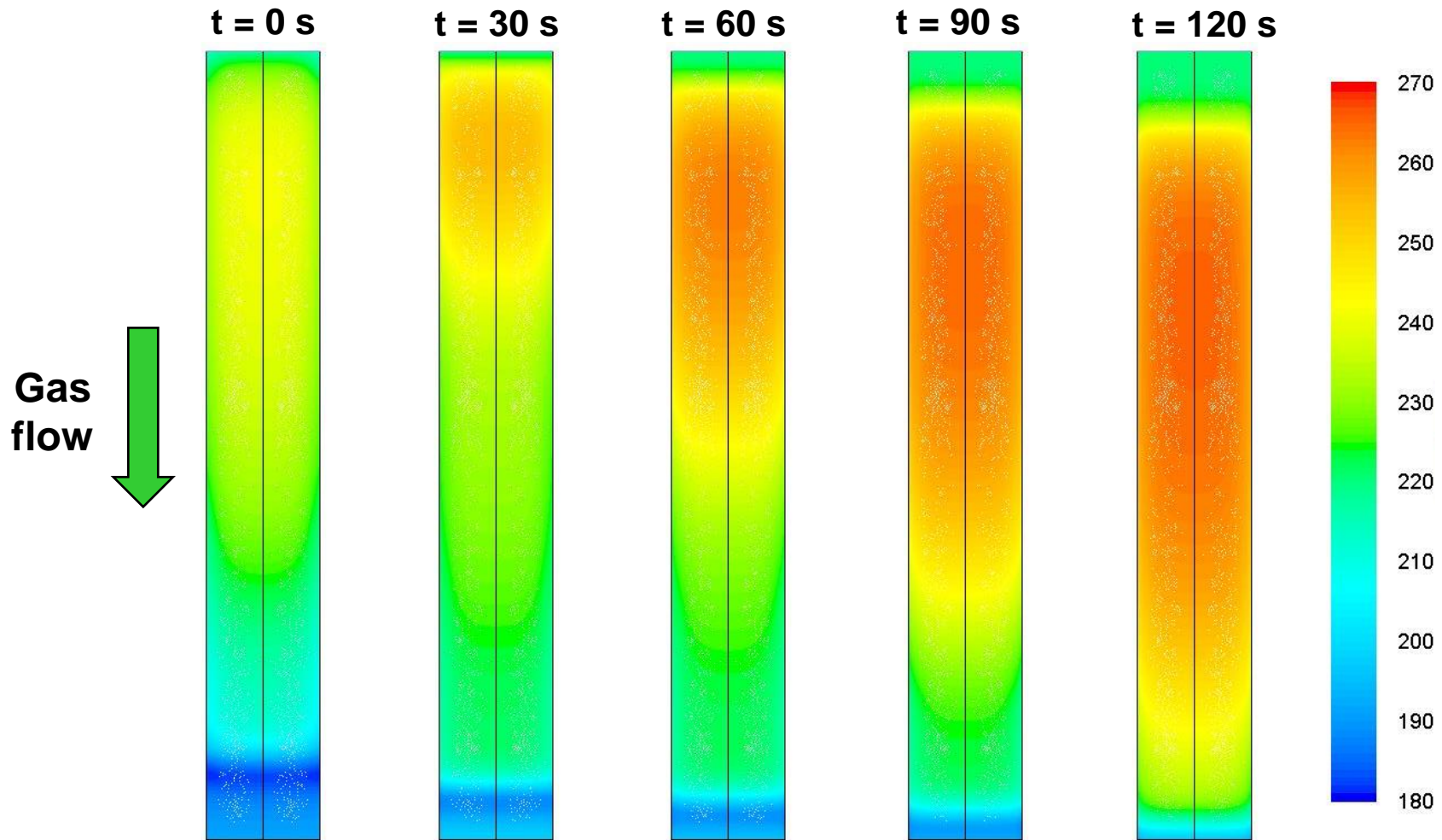


- 90+% capture at steam:CO ratio= 1:1.1 with average 96.4% CO conversion
- All objectives met (no coking etc.) but high reactor T was observed

Technology Status/R&D Needs

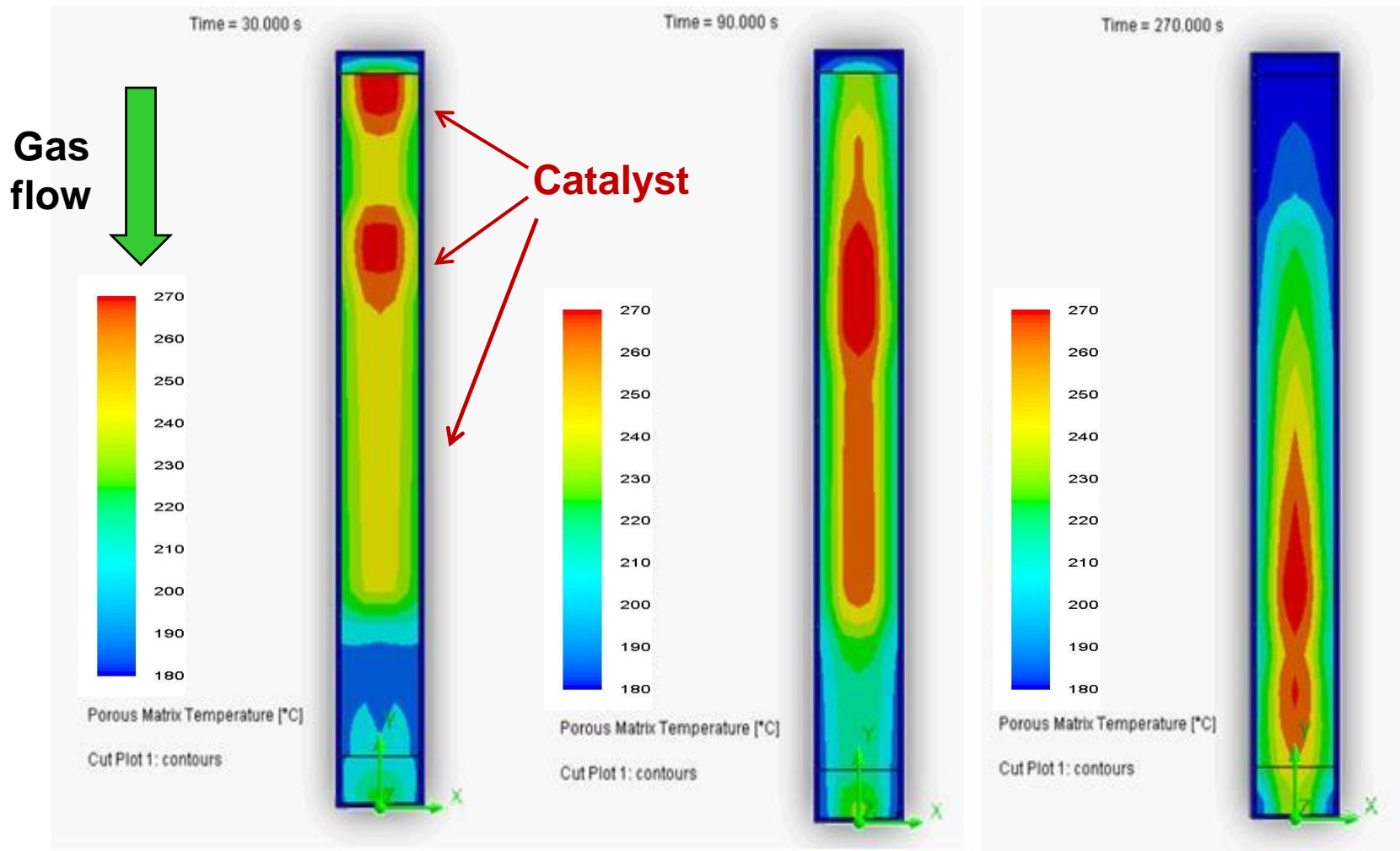
- **Sorbent is developed under a separate DOE project (DE-FE0000469)**
- **WGS catalyst is commercially available mature technology**
- **Early-stage concept demonstration has already been completed (DE-FE0007966 and DE-FE0012048)**
 - Integrated sorbent/catalyst operation
 - Pointed out the need to incorporate effective heat management
 - Implemented the heat management scheme in a 4-bed PSA system using coal derived synthesis gas at 1 kg/hr CO₂ removal
- **Key R&D need is the design/development of a high fidelity prototype to fully demonstrate the concept using actual coal-derived synthesis gas**
 - Reactor design to address the heat management needs
 - A 10 kg/hr CO₂ removal is being developed
 - Testing of the high fidelity system will be carried out at Praxair

T Profiles - During CO₂ Capture Only



- Heat generated during adsorption is removed during regeneration
 - Near isothermal operation through the cycle

Heat Wave WGS & CO₂ Capture

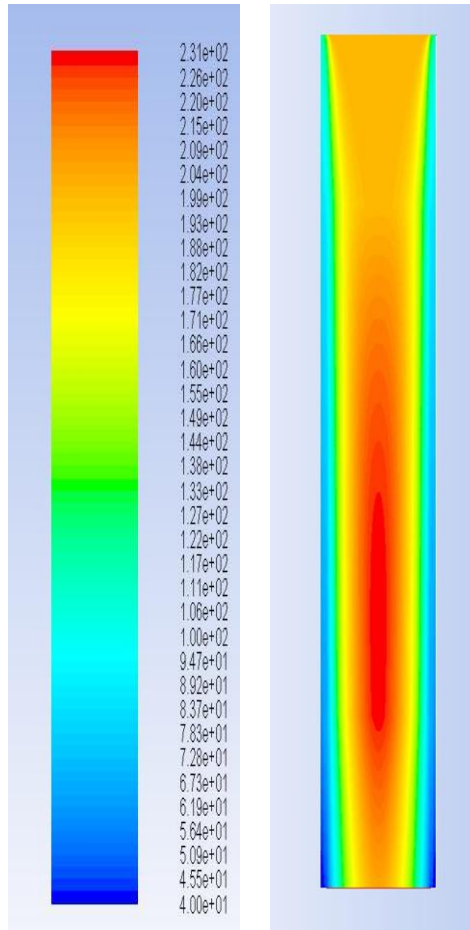


- Integrated WGS & CO₂ capture results in higher ΔT
- Not ideal for CO₂ capture (the WGS heat accumulates in the beds)

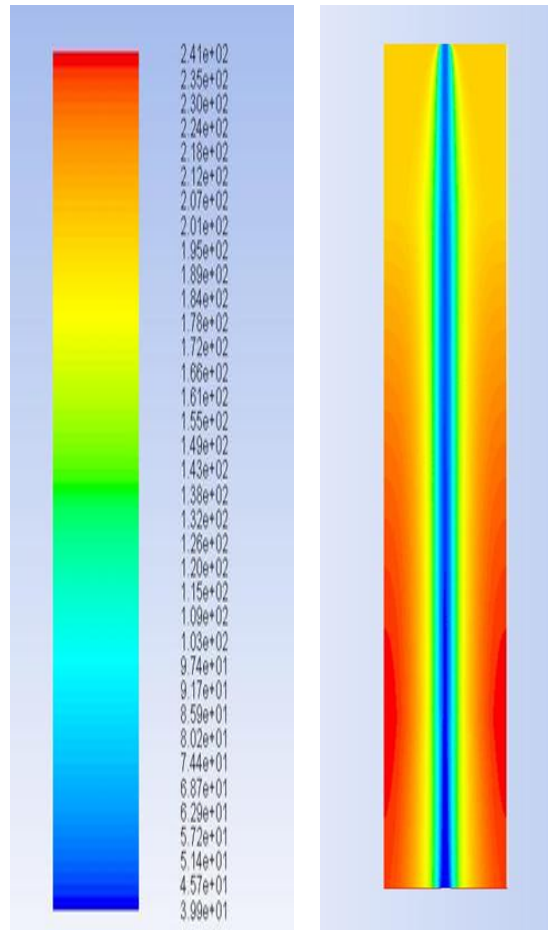
Conventional Heat Management Options

10 kg/hr CO₂ Removal Pilot Test System – 6" reactors

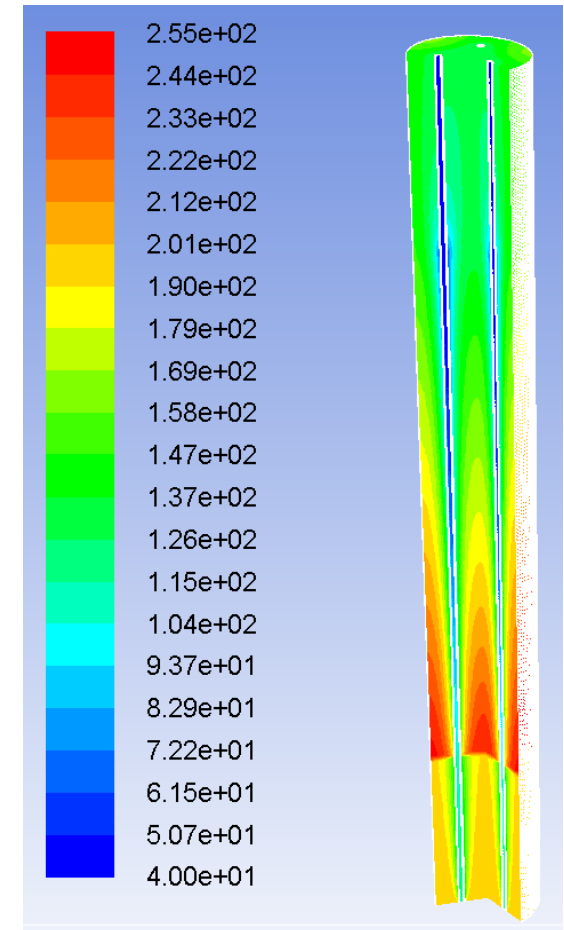
Cooling Jacket



Immersed Tube (1)



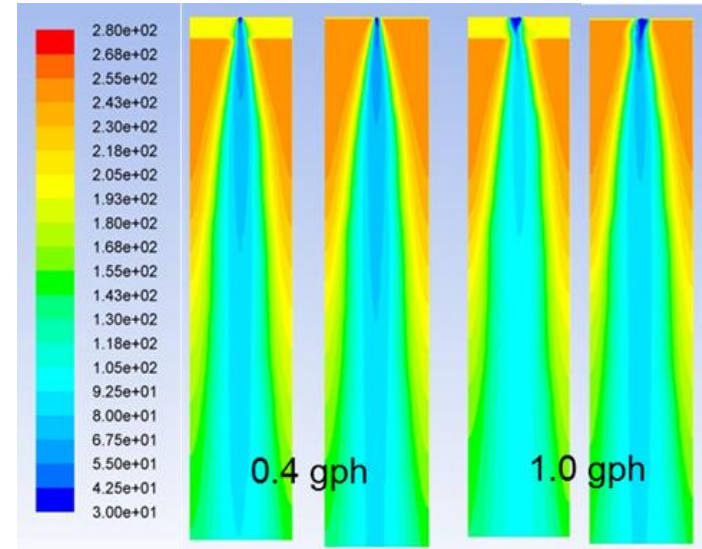
Immersed Tubes (3)



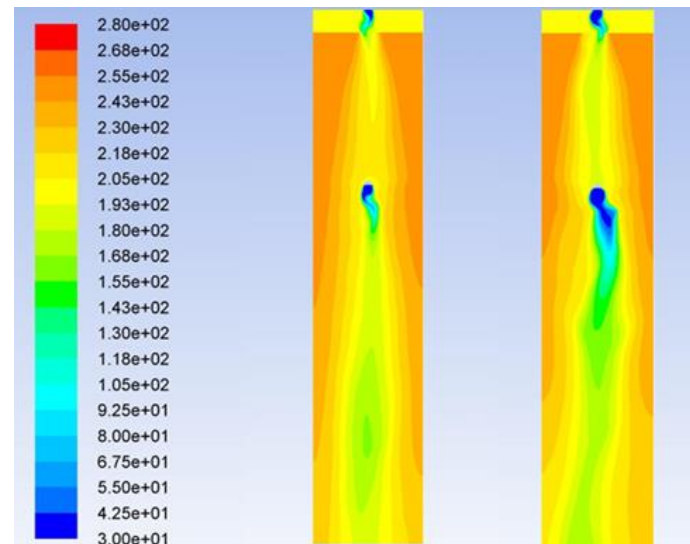
Heat Integrated WGS & CO₂ Capture

- **Advanced heat management concept based on direct water injection has proven to achieve much better temperature control**
 - Also much better heating efficiency (i.e., kJ heat removed per kg water)
- **Objective is to achieve a more uniform cooling without having hot or cold spots**
- **The temperature rise is optimal when the catalyst is distributed into two layers with water injections before each layer**

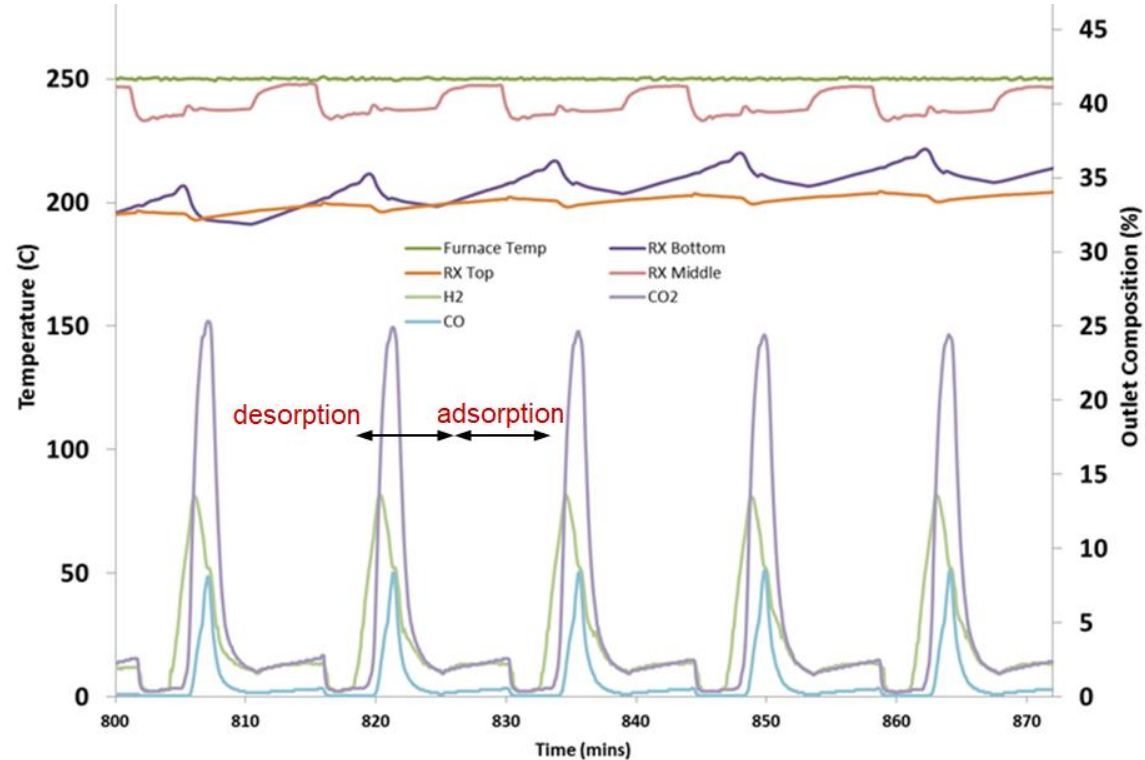
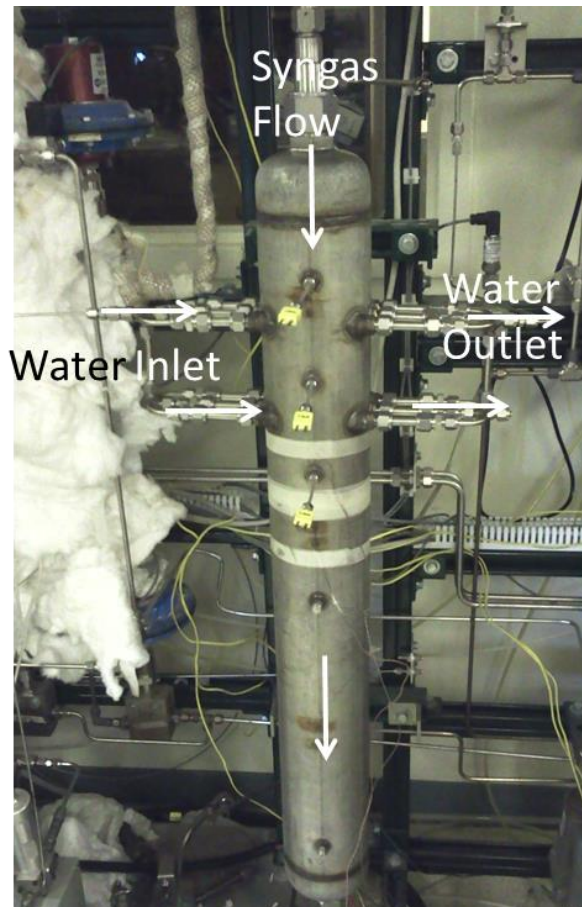
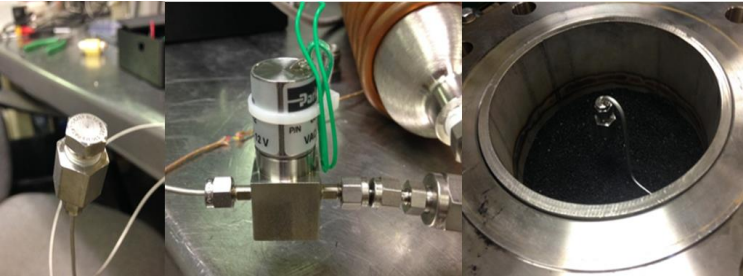
T Contours (°C) Single Injection Layer



T Contours (°C) Multiple Injection Layers

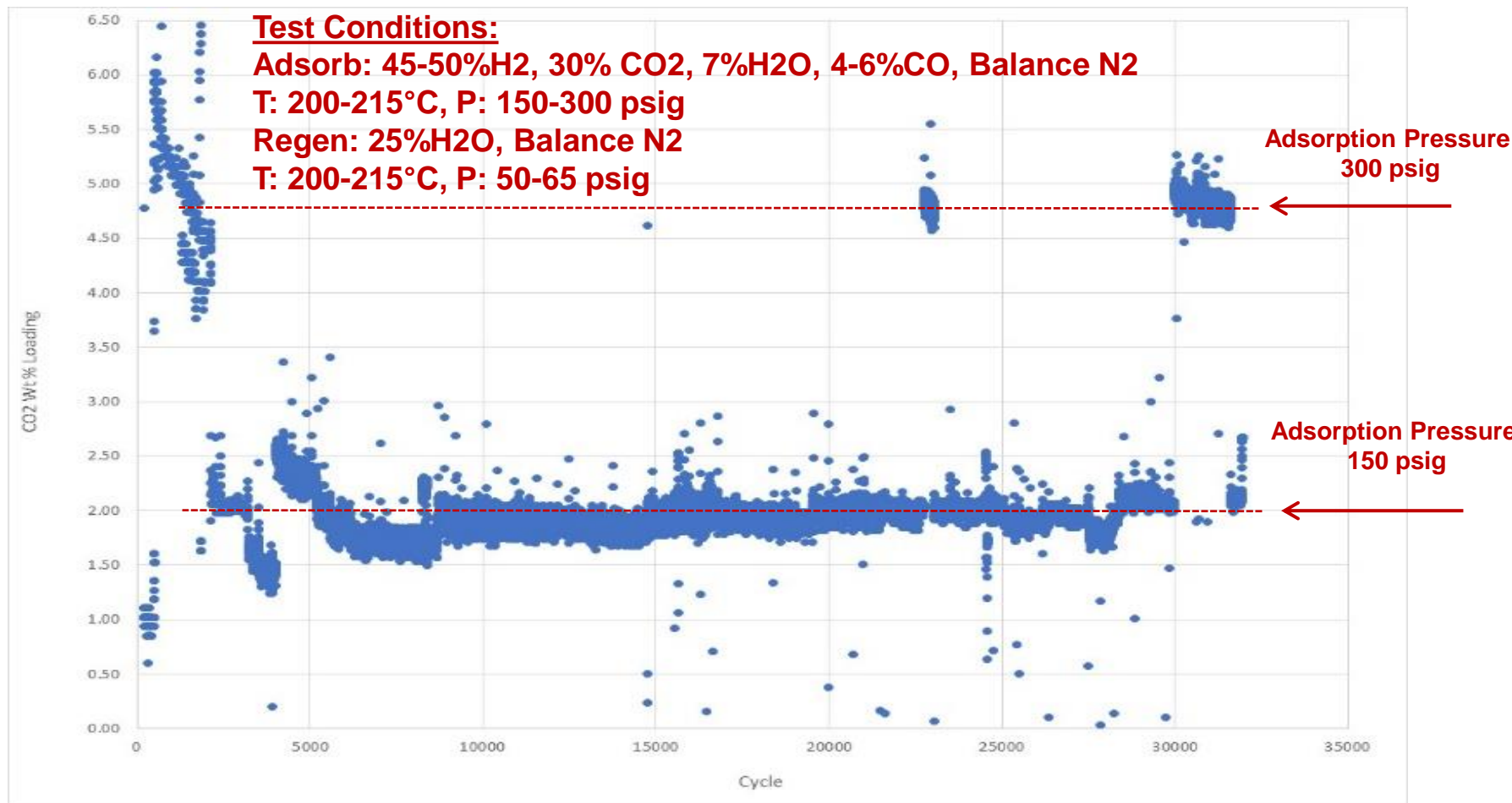


Bench-Scale Evaluations



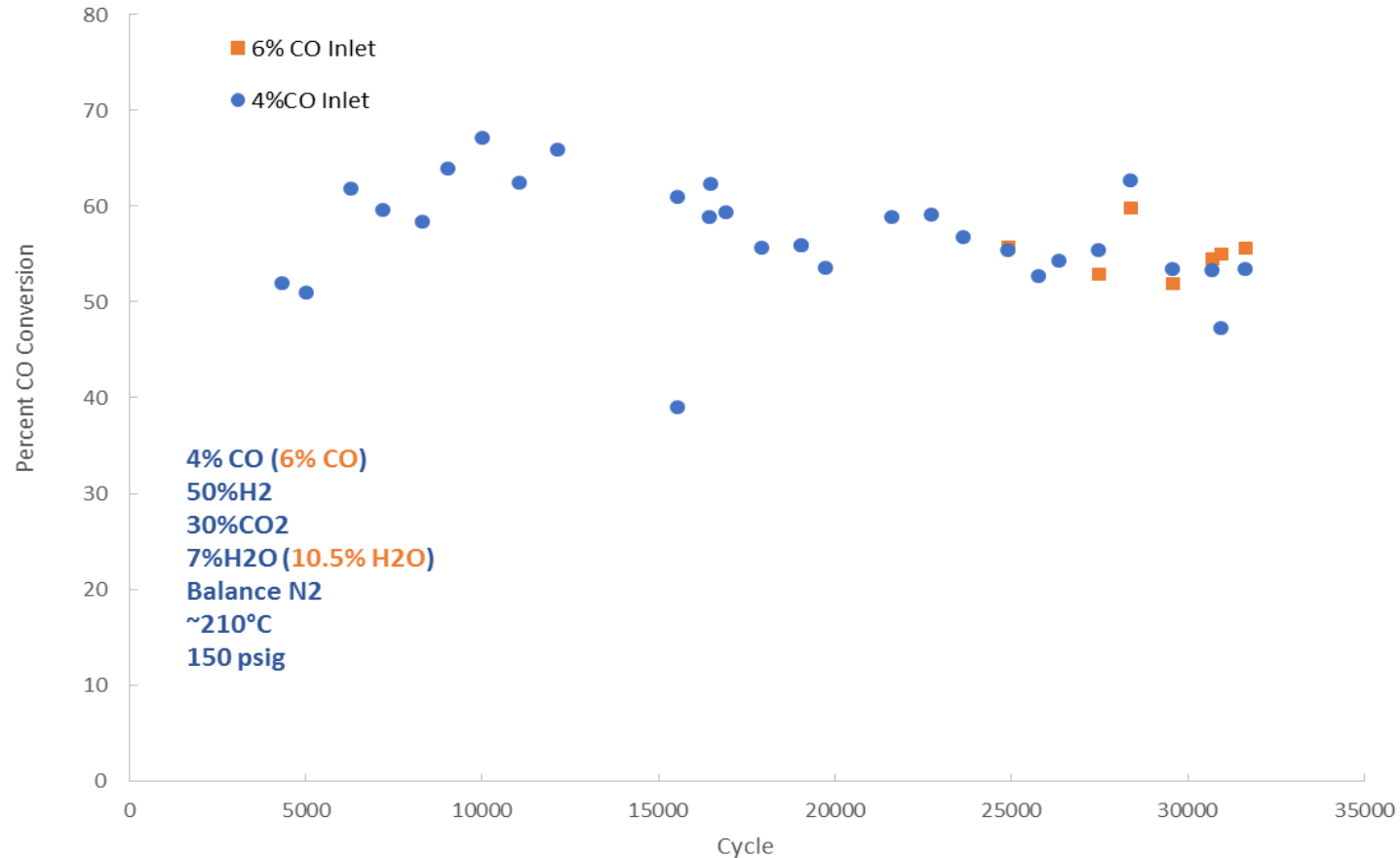
- 8L reactors were modified with water injectors
- Successful proof-of-concept demonstrations have been completed
- $\Delta T < 10^\circ\text{C}$ was maintained over extended cycling (much lower than those in early field tests)

Life Tests – Sorbent Activity



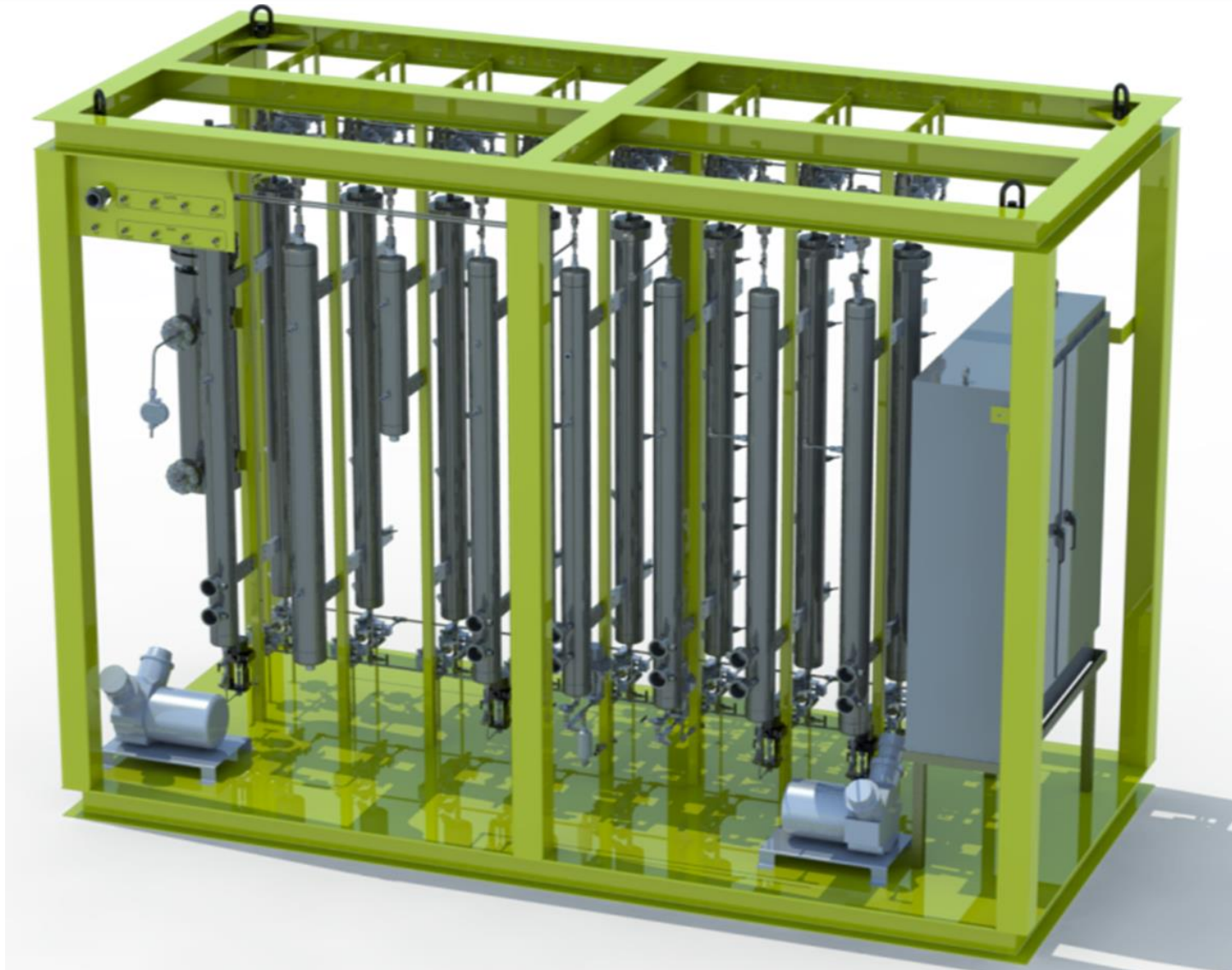
- We completed 32,000 cycles showing stable performance for the WGS catalyst and CO₂ sorbent

Life Tests – Catalyst Activity



- By evaluating continuous catalytic activity (alone) we showed that cycling between reducing and oxidizing conditions (i.e., steam exposure) had no adverse effect on the WGS catalyst

Integrated WGS/CO₂ Capture System



Fabrication of the Prototype



Installation at Praxair

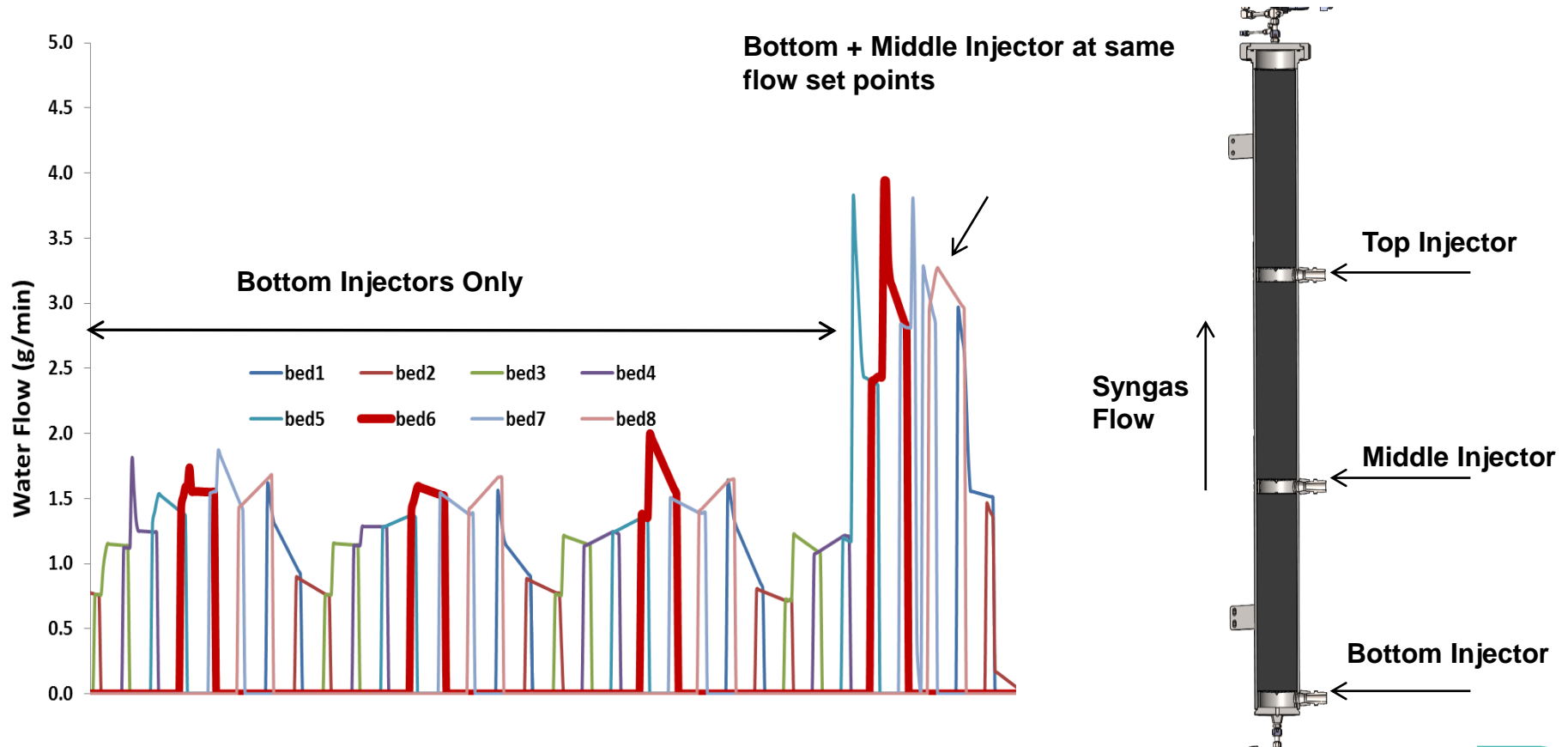


- Fabrication of the Prototype unit was completed in 2018 Q2 and installation at Praxair R&D Center (Tonawanda, NY) was completed in 2018 Q3
- First campaign is completed in Q2 2019



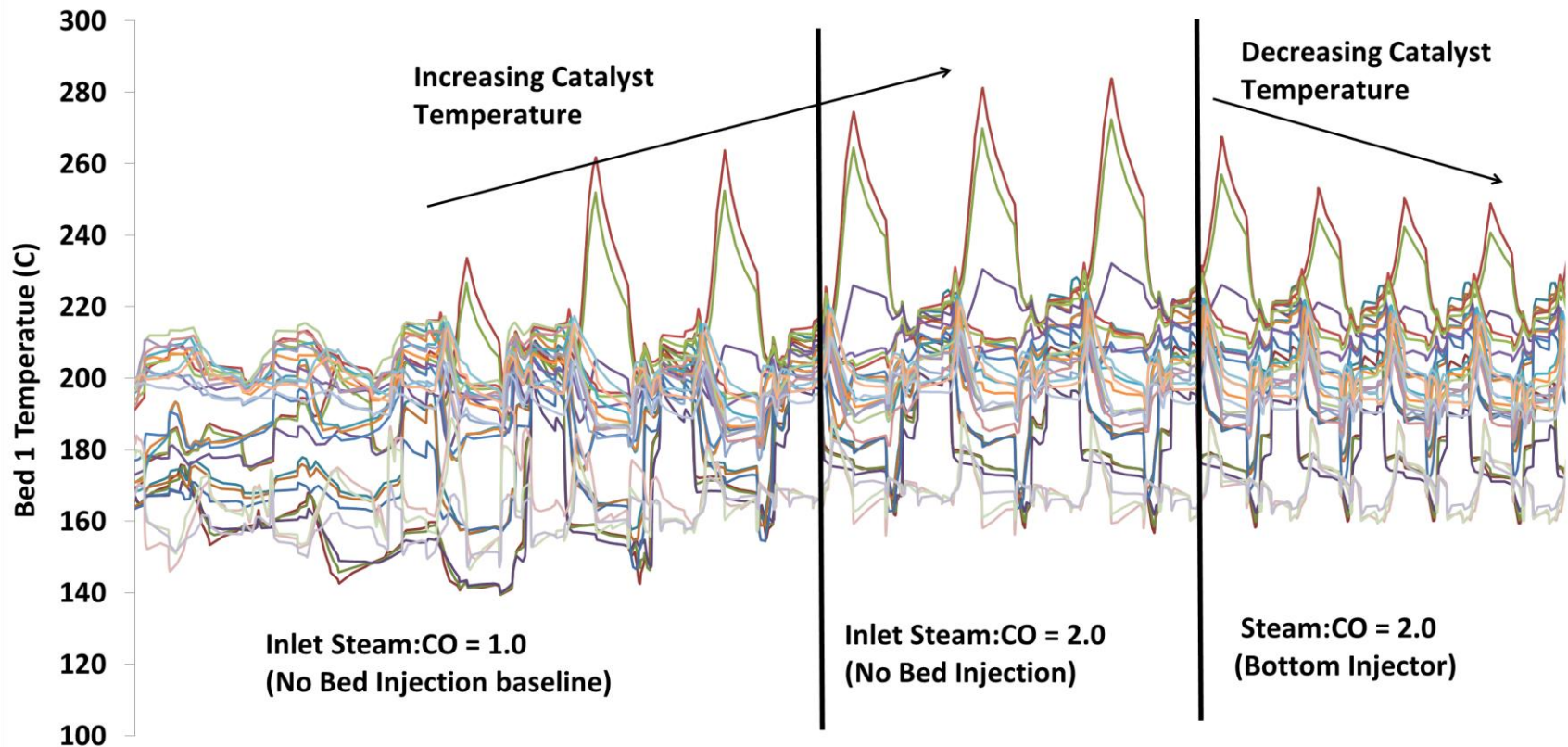
Control of Water Injection

- We demonstrated that precise amounts of water can be injected and their individual flow rates can be controlled within tolerances of less than 0.5 g/min between injectors



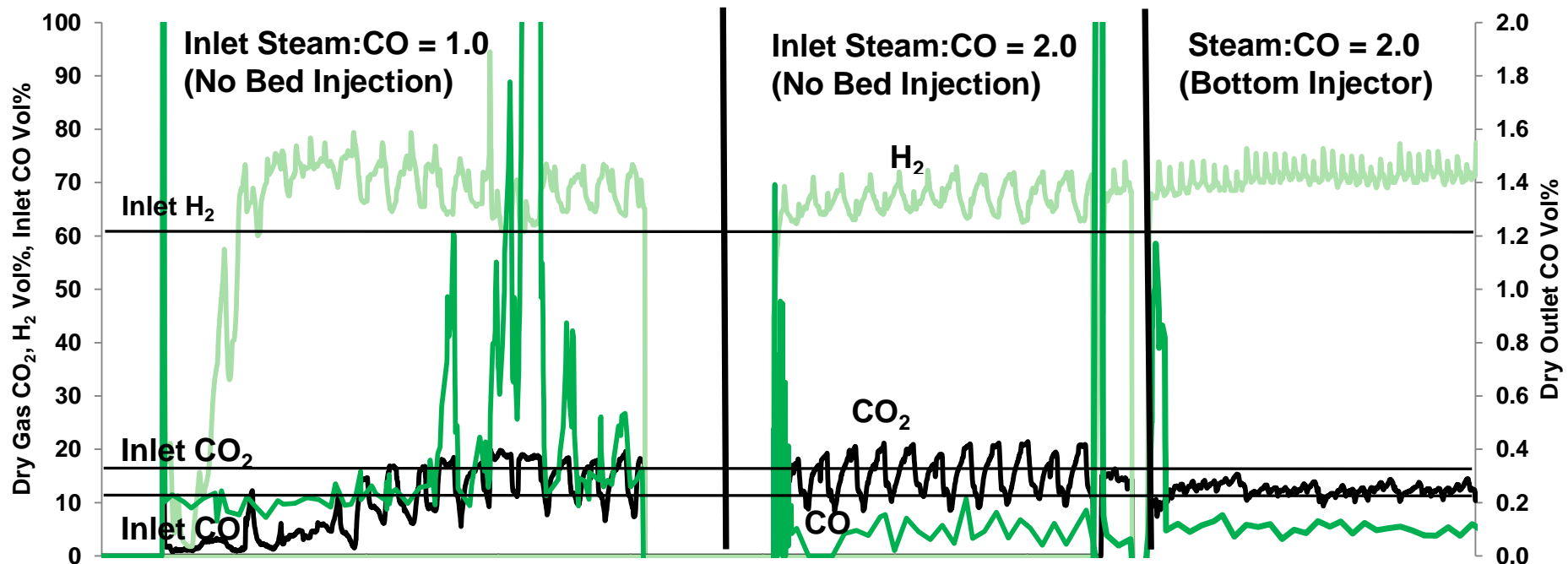
Temperature Management via Water Injection

- We observed an increase in bed temperature by increasing the inlet steam:CO from 1 to 2
- Bed temperature was maintained at $\sim 40^{\circ}\text{C}$ lower when injecting the same amount water directly into the beds



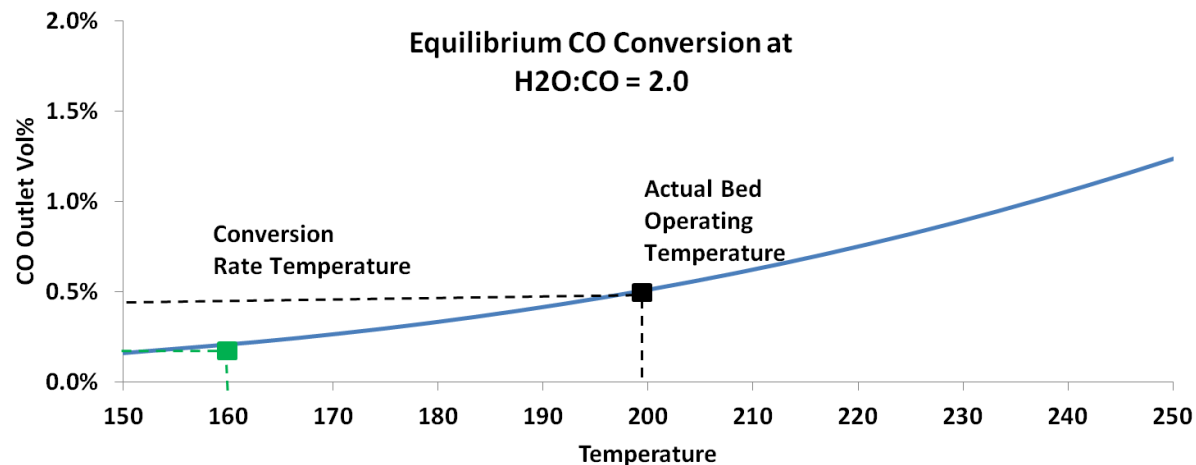
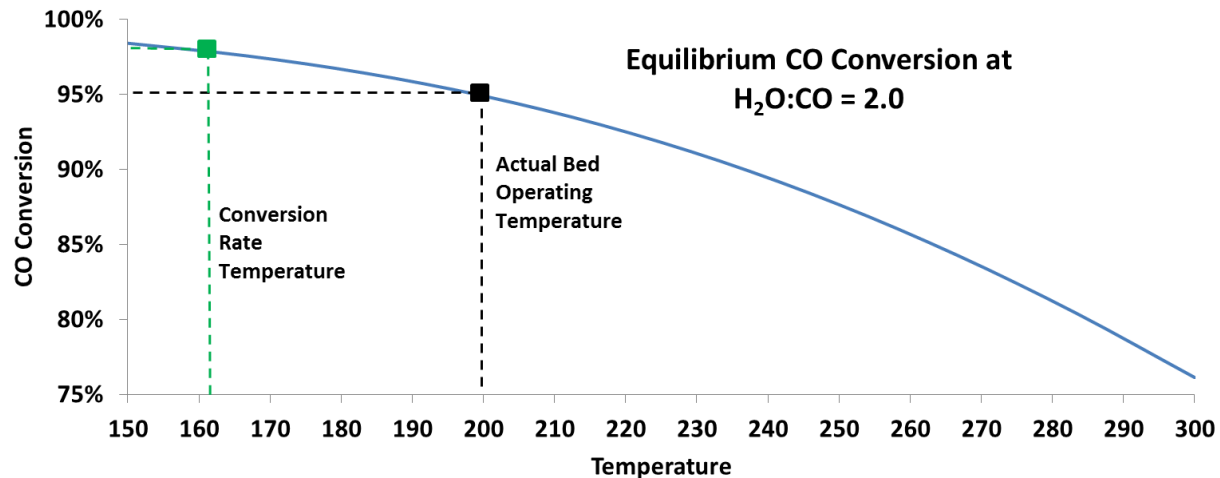
Impact of Water Injection

- An overall CO conversion >98% was achieved
- Cycle times were not yet optimized in this run therefore carbon capture was only at 60% (incoming CO₂ + CO₂ from shifted CO₂)
- Optimization was planned for the test scheduled for the next campaign



Effect on Equilibrium Conversion

- By coupling the WGS with the CO₂ sorbent and water injection, we were able to operate the beds at 200°C but achieve the equilibrium CO conversion of a 40°C cooler bed



Modifications After the First Campaign

- The damaged compressor (due to debris in the lines) were repaired
 - The broken outlet valve and the piston rings
- The smaller tee style filters that clogged so quickly were replaced with the larger filter housings for longer periods of sustained operation
- The compressor was turned on and it successfully pressurized the inlet nitrogen from 100 to 380 psig (the compressor design rating)
- Performance of all heaters were verified
- The water injection system was flushed out and the operation of the injection valves and flow meters were verified



**Broken
compressor
valve (circled)**

Old



**Filter
Housing
New**

Integration with E-Gas™ Gasifier

Gasifier Type/Make	E-Gas		
Case	1	2	2* (WGS/CO ₂)
CO ₂ Capture Technology	Cold Gas Cleanup Selexol™	Warm Gas Cleanup TDA's CO ₂ Sorbent	Warm Gas Cleanup TDA's CO ₂ Sorbent
CO ₂ Capture, %	90	90	90
Gross Power Generated, kW	710,789	670,056	693,542
Gas Turbine Power	464,000	425,605	427,980
Steam Turbine Power	246,789	244,450	265,562
Syngas Expander Power	-	-	-
Auxiliary Load, kW	194,473	124,138	138,741
Net Power, kW	516,316	545,917	554,801
Net Plant Efficiency, % HHV	31.0	34.1	34.7
Coal Feed Rate, kg/h	220,549	212,265	212,265
Raw Water Usage, GPM/MW	10.9	10.3	10.0
Total Plant Cost, \$/kW	3,464	3,042	2,990
COE without CO ₂ TS&M, \$/MWh	136.8	120.5	118.8
COE with CO ₂ TS&M, \$/MWh	145.7	128.6	126.7
Cost of CO ₂ Captured, \$/tonne	53.2	37.4	35.8

- IGCC plant efficiency is estimated as 34.7% with TDA's WGS/CO₂ system
- Cost of CO₂ capture is estimated as less than \$26/tonne (including TS&M less than \$35.8/tonne)

Process Economic Analysis - CTL

Gasifier	Shell	
Coal	Bituminous	
Case	9	10A
CO ₂ Capture Technology	Cold Gas Cleanup Rectisol™	Warm Gas Cleanup TDA's CO ₂ Sorbent
CO ₂ Capture, %	90	90
Gross Power Generated, kW	462,568	458,830
Gas Turbine Power	130,283	130,519
Steam Turbine Power	332,285	328,311
Syngas Expander Power	-	-
Auxiliary Load, kW	397,803	365,956
Net Power, kW	64,764	92,875
Net Plant Efficiency, % HHV	1.08	1.55
Naphtha Production rate, ST/D	1,803	1,722
Diesel Production rate, ST/D	4,789	4,933
Coal Feed Rate, kg/h	793,864	793,864
Raw Water Usage, GPM	14,032.6	12,394.0
Total Plant Cost, \$/kg/D	949.87	864.94
NAPHTHA		
1st year Required Selling Price (RSP) w/o CO ₂ TS&M, \$/bbl	107.0	100.0
DIESEL		
1st year Required Selling Price (RSP) w/o CO ₂ TS&M, \$/bbl	153.0	143.0

- Integrated WGS with CO₂ capture reduced the required selling price for Naphtha to \$100 per bbl compared to \$107 per bbl for a CTL plant with Rectisol
- Integrated WGS with CO₂ capture reduced the required selling price for Diesel to \$143 per bbl compared to \$153 per bbl for a CTL plant with Rectisol

Future Work

- **Testing of the unit at Praxair – Field Test Campaign #2**
 - Scheduled to start on September 14, 2020
- **Complete CFD Model validation with Praxair Test Data**
- **Complete an Environmental, Health and Safety (EHS) assessment**

Acknowledgement

- **NETL, Project Manager, Diane Madden Ravey**
- **Chuck Shistla, GTI**
- **Sean Kelly, Juan Li, Praxair**
- **Frank Morton, NCCC**
- **Ashok Rao, UCI**