## Durability and Reliability of SOFCs

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## Acknowledgments

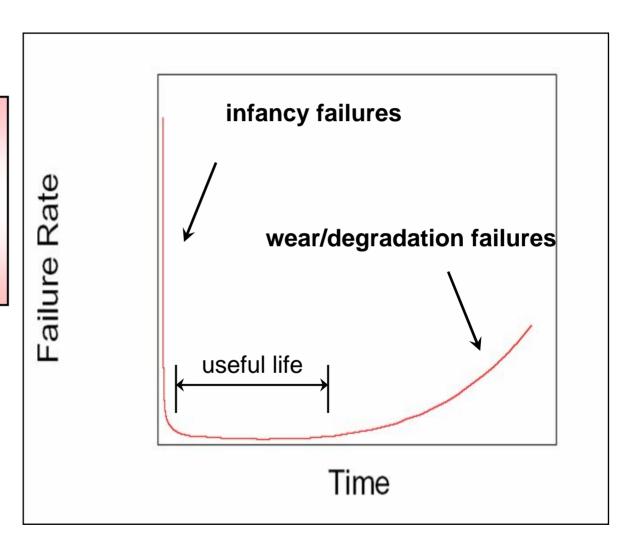
- Miladin Radovic
- Rosa M. Trejo
- Chris Cofer
- Claire Luttrell
- Tom Watkins

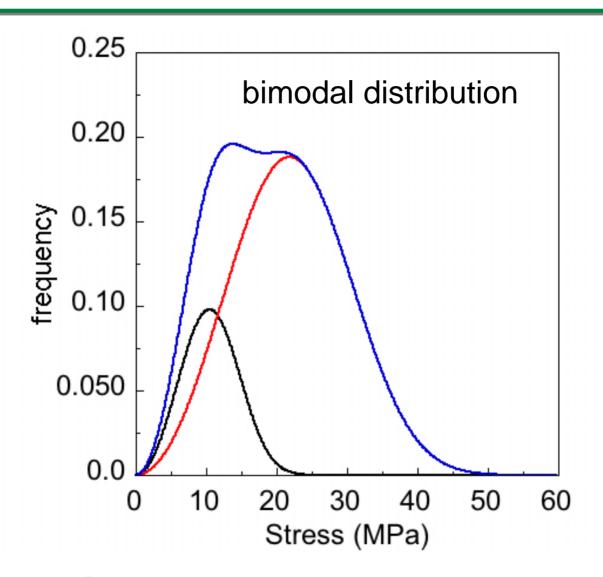
- DOE, SECA Program.
- Travis Shultz

### **Outline**

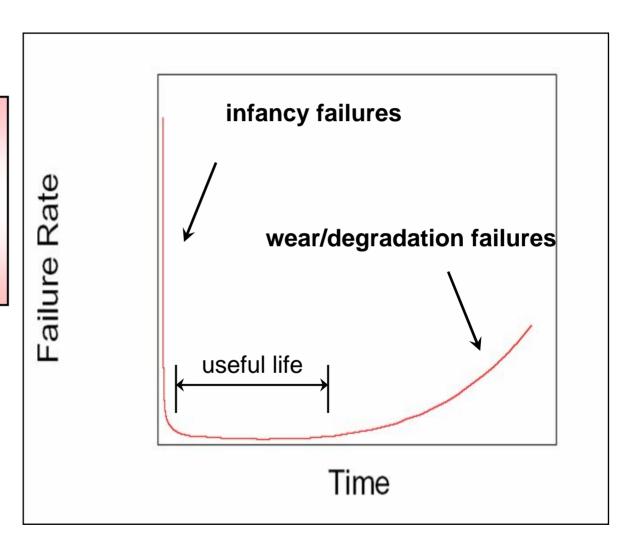
- Durability and Probabilistic Analysis of SOFCs
- Degradation and Wear
  - Creep Deformation
  - Thermal Cycling
  - Slow-crack growth
- Future work

The failure rate of complex systems can be described by the bathtub curve

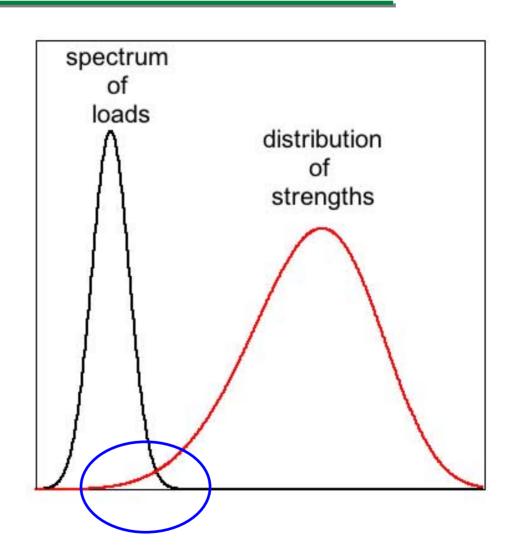




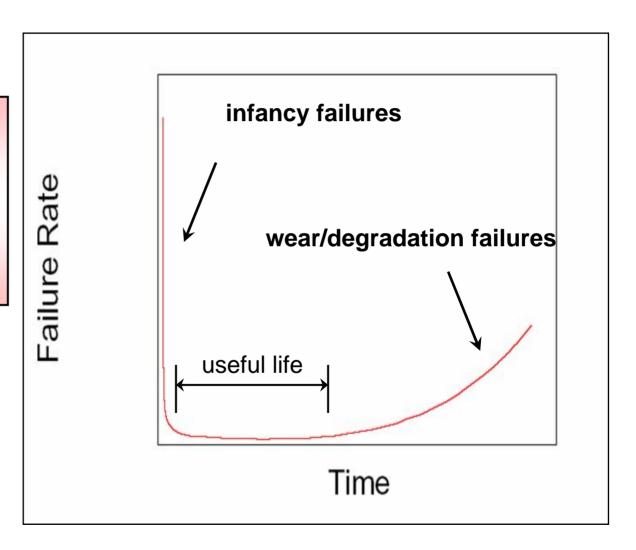
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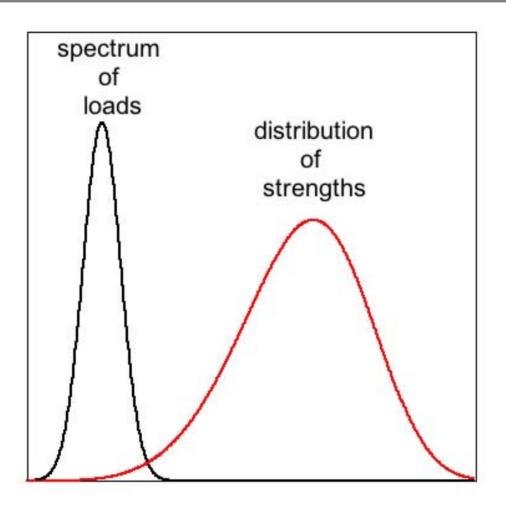


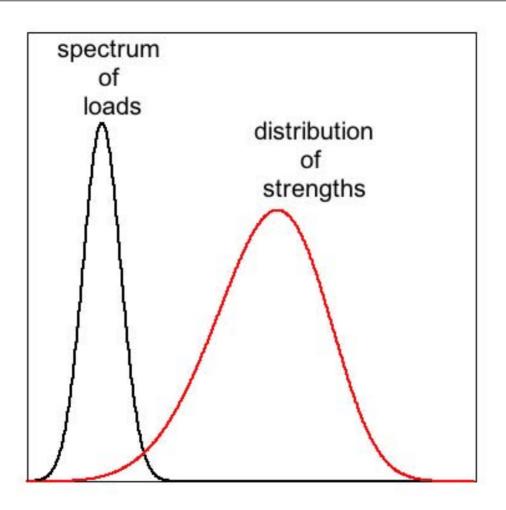
- Failure is determined by the intersection of the distributions of loads and strengths.
- Failure can be avoided by designing components so that these distributions don't intersect
- The weakest elements of the population determine the reliability of the system.

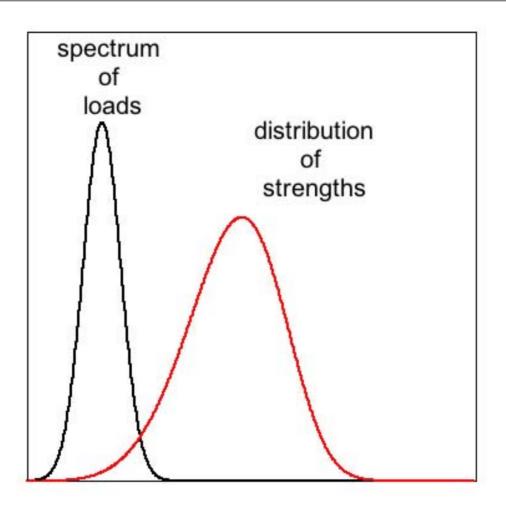


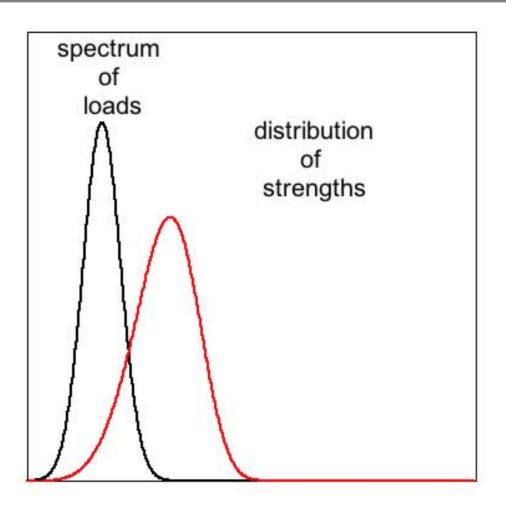
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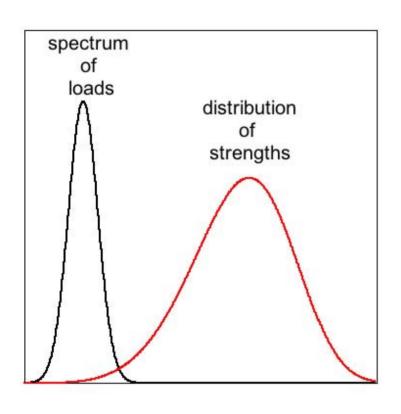


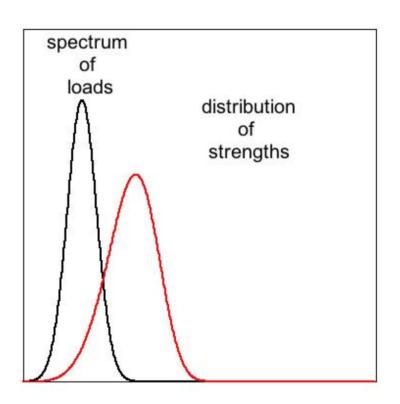












before

after

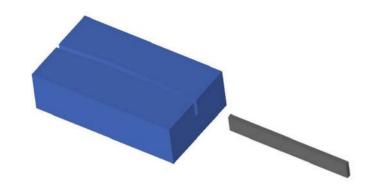
Mechanisms that contribute to wear and degradation

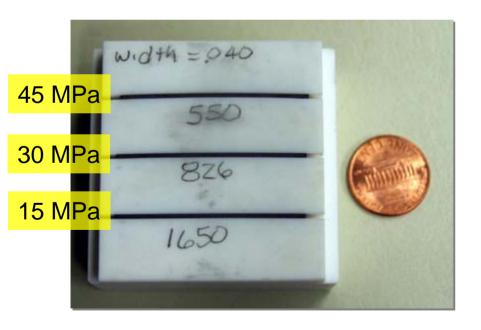
- Creep deformation
- Thermal cycling and thermal aging
- Slow-crack growth

- Is creep deformation really an issue for SOFCs?
- Stress relaxation testing provides a rapid means to answer that question.
- Beam-shaped test specimens are subjected to constant bending strain at high temperature



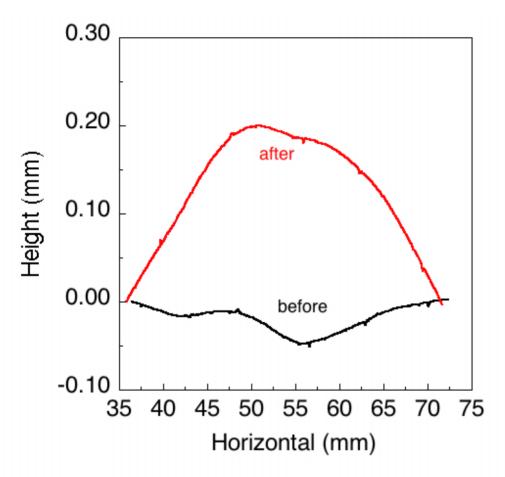
 The curvature of the beam is monitored before and after the test





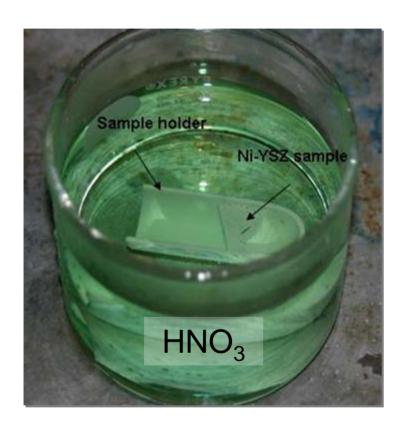
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- Ni-YSZ
- 40% final porosity
- 43% Ni (vol. solid phase)
- 1.5" x 0.15" x 0.04"
- curvature determined by laser profilometry
- Macor® fixture with channels of different radii of curvature.
- 50-hr stress relaxation test at 800°C in H<sub>2</sub> (4%)-Ar (96%)



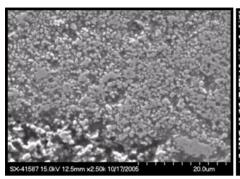
- After stress-relaxation testing test specimens retained the curvature of the fixture channels.
- Therefore, this material is prone to creep deformation.
- What is the mechanism?

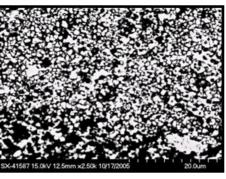
#### Nickel dissolution



- 14 hrs in 75% HNO<sub>3</sub> solution
- weight after reduction:2.279 g
- weight after Ni removal:1.0823 g
- removed Ni (from weight loss): 99.4%

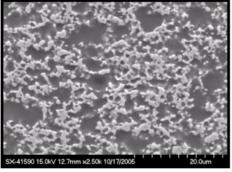
### Nickel dissolution

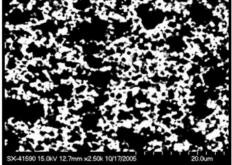




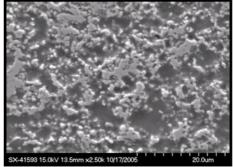
27/\*\*% porosity

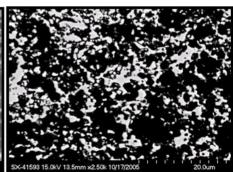
34/62% porosity



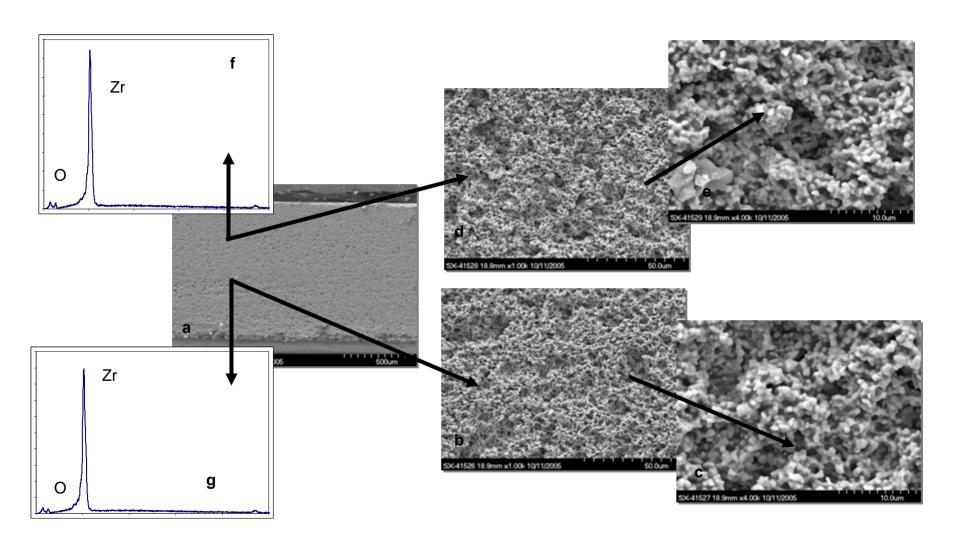


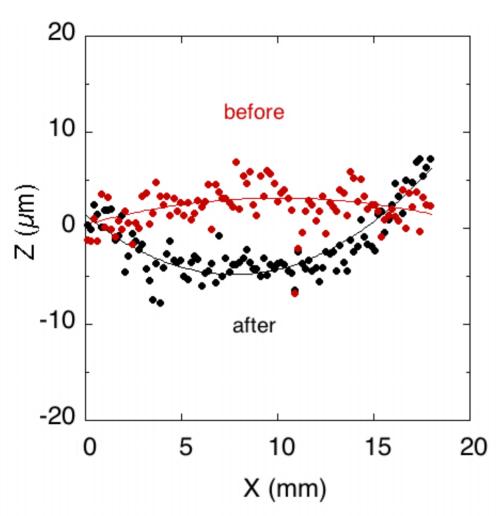
40/66% porosity



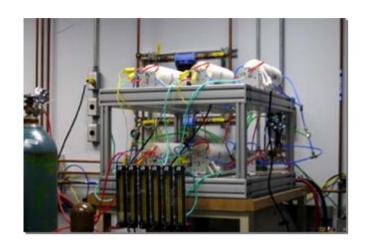


## Nickel dissolution

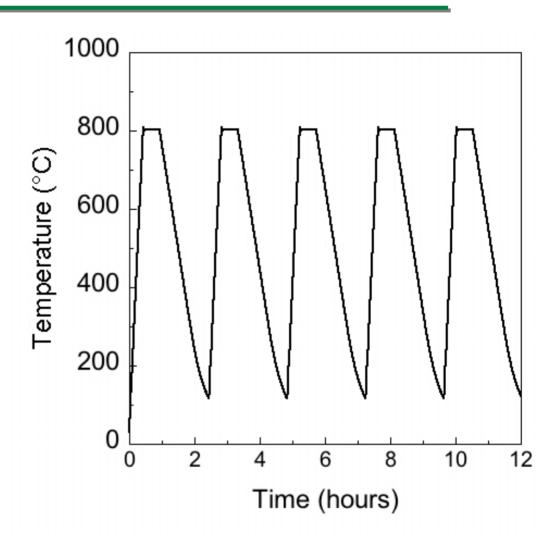


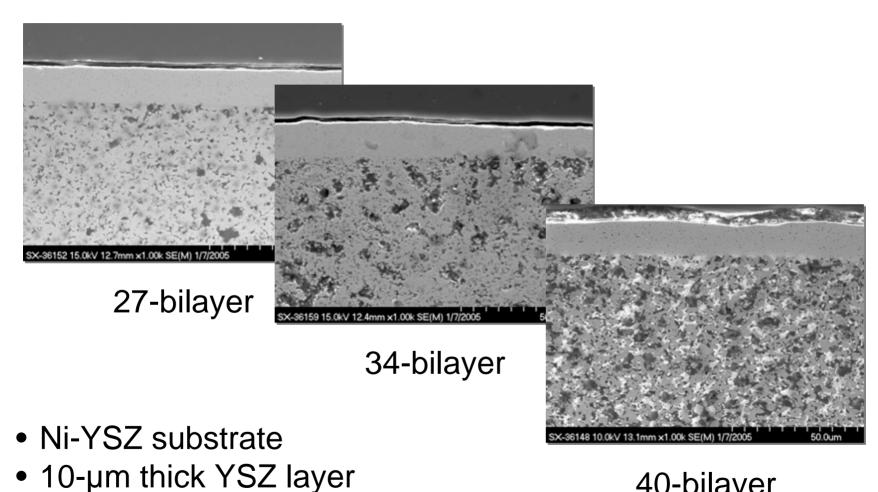


- Stress-relaxation tests of porous YSZ scaffold
- 50-hr stress relaxation test at 800°C in H<sub>2</sub> (4%)-Ar (96%)
- Material experiences minimal stress relaxation
- Nickel is mostly responsible for creep deformation experienced by Ni-YSZ at 800°C.



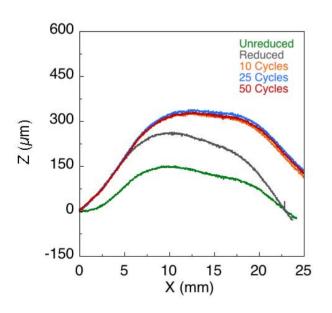
- H<sub>2</sub> (4%)-Ar (96%)
- tubular furnaces

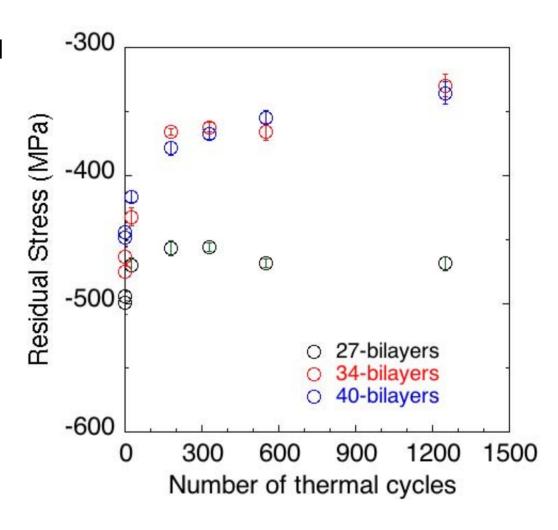




40-bilayer

- residual stresses determined in YSZ layer by X-ray diffraction
- Curvature measurements by laser profilometry





- Microstructural and physical characterization in progress
- Aging tests in progress to distinguish between thermal and cycling effects



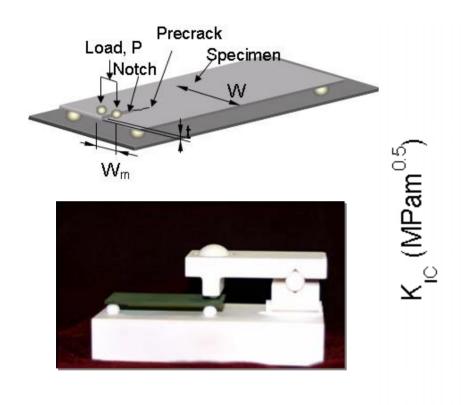
# Slow crack growth

## Slow-crack growth

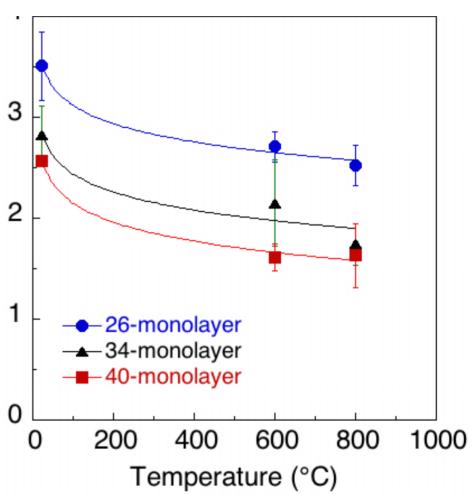
- Slow-crack growth of preexisting flaws is recognized as a primary source of static fatigue failure of ceramics.
- Knowledge of crack velocities can be used to predict the service life of ceramic components.

$$v = A[K_I/K_{IC}]^n$$

## Fracture toughness

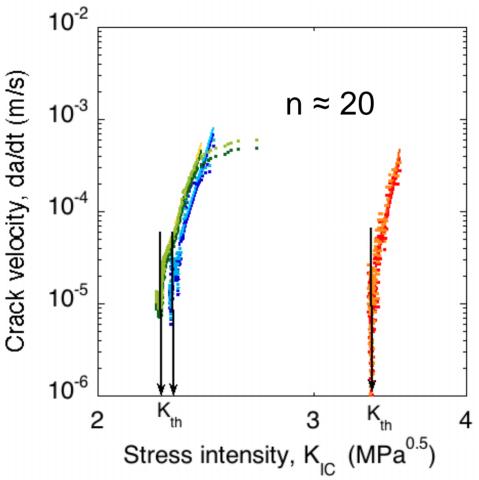


 fracture toughness and slowcrack growth determined by double-torsion testing

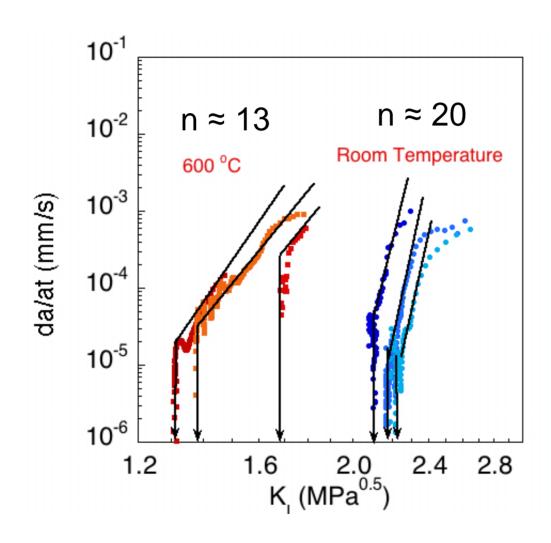




- 27-Anode-a27-anode-b
- 40-Anode-a40-Anode-b

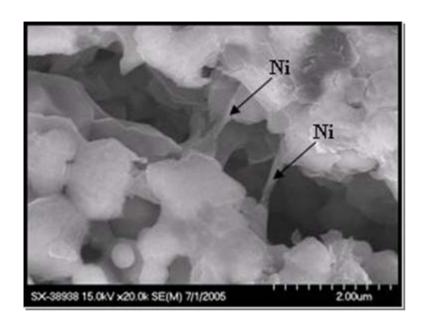


- Ni-YSZ
- 20°C



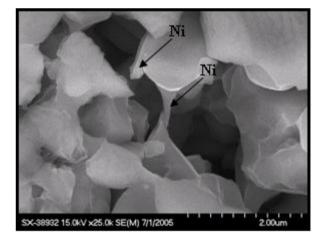
- Ni-YSZ
- H<sub>2</sub>(4%)-Ar(96%)

## Slow-crack growth

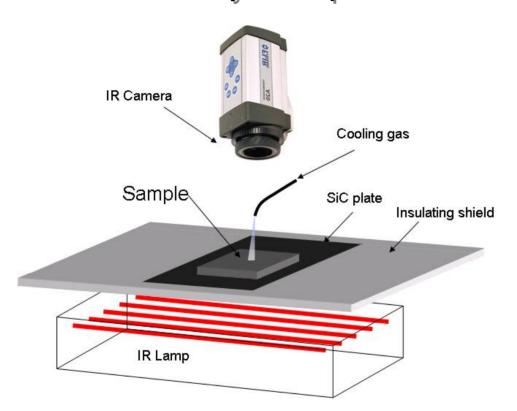


SX-38936 15.0kV x20.0k SE(M) 7/1/2006 2.00um

Role of microstructure on crack growth in Ni-YSZ at 600°C



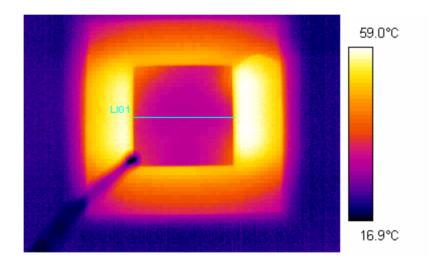
#### Probabilistic analysis to predict durability and reliability



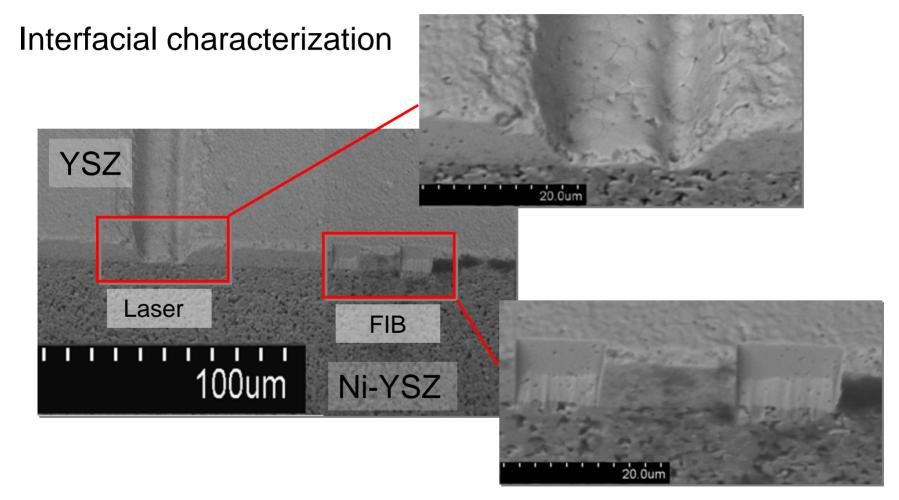


Verification of reliability predictions for bi- and tri-layers subjected to arbitrary temperature distributions

#### Probabilistic analysis to predict durability and reliability



Verification of reliability predictions for bi- and tri-layers subjected to arbitrary temperature distributions



## Summary

- Nickel is responsible for the creep deformation of Ni-YSZ at 800°C
- Residual stresses in Ni-YSZ decrease in magnitude with number of thermal cycles.
- The fracture toughness of Ni-YSZ decreases with both porosity and temperature
- Ni-YSZ exhibits slow-crack growth both at ambient and elevated temperatures. The microstructure does play a role on crack propagation
- Thermal and physical properties of materials have been determined