

# *Novel Materials for Obtaining Compliant, High-Temperature Seals for SOFCs*

*SECA Core Technology Program*

*Ceramatec, Inc.*

*Supported in part by*

**US DOE Phase I SBIR DE-FG03-02ER83385**

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*Presented at*

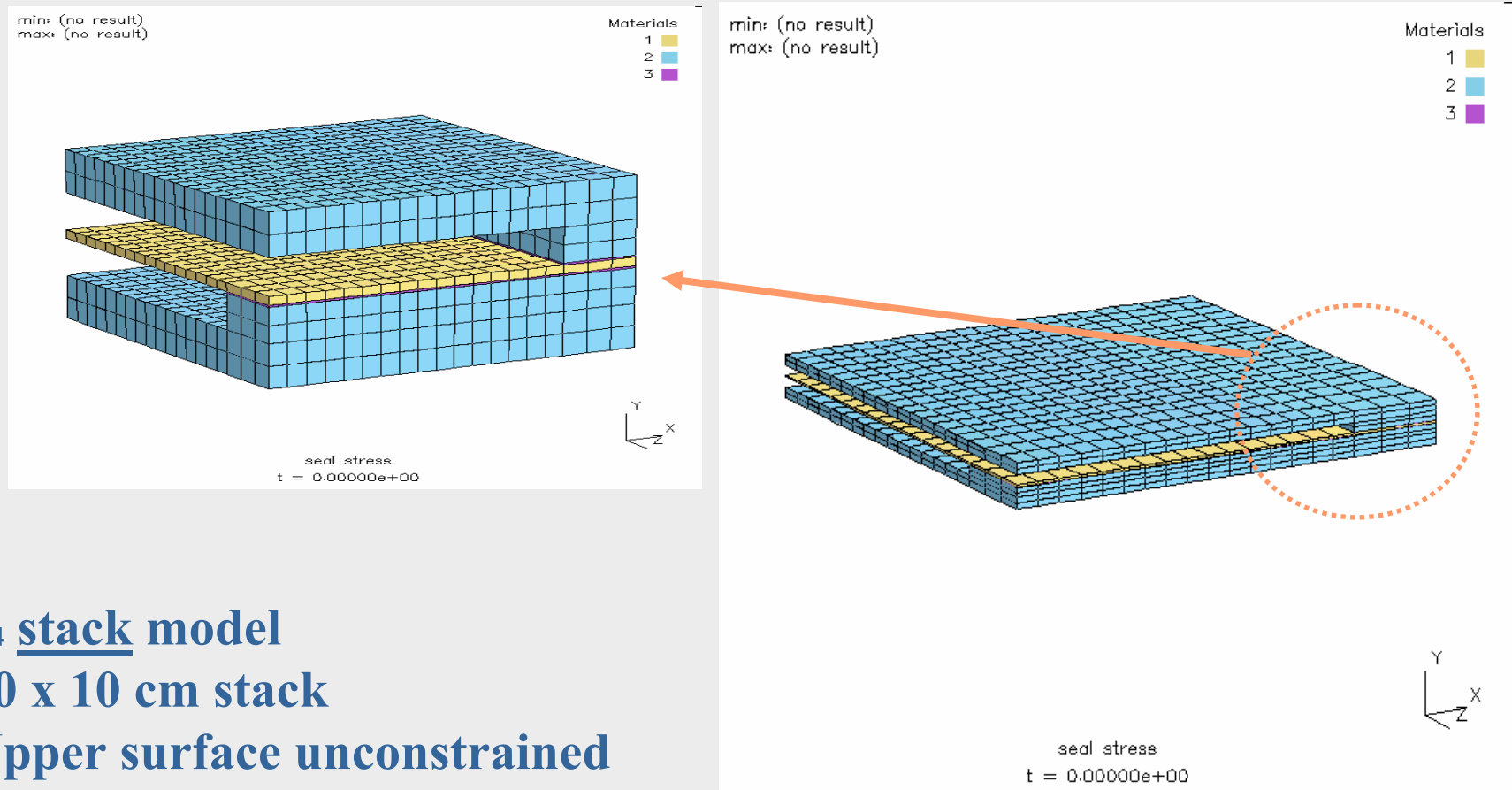
*Albany, NY*

*01 October 2003*

# Seal Requirements

- **Low leak rate: good adhesion, high density.**
- **Ability to withstand thermal cycling/CTE match with cell components.**
- **Compatible with cell materials.**
- **Environmental stability in oxidizing and reducing conditions.**
- **No negative effect on cell performance.**
- **Acceptable cost.**

# Mechanical behavior of seals – FEA analysis



- 1/4 stack model
- 10 x 10 cm stack
- Upper surface unconstrained
- Bottom surface fixed in vertical direction
- Symmetric boundary conditions on cut planes
- Stresses calculated for cooling from fabrication temperature

# FEA model

## Material Properties

Component	E (GPa)	$\nu$	CTE (ppm °C <sup>-1</sup> )
Interconnect	200	0.29	12
Electrolyte	185	0.31	11
Seal	20, 100, 200	0.20	11

- Stress free temperature: 1000°C
- Seal dimensions: 50 microns thick, 1 cm wide

# Seal Stresses – FEA analysis

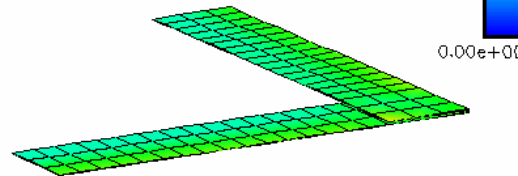
$$E_{\text{seal}} = 20 \text{ GPa}$$

min: 9.77e+06, brick 1915  
max: 3.64e+07, brick 1799

Maximum Shear Stress

3.64e+07

0.00e+00



seal stress  
t = 1.00000e+00

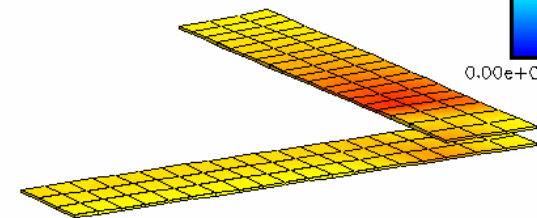
$$E_{\text{seal}} = 200 \text{ GPa}$$

min: 1.05e+08, brick 1802  
max: 1.38e+08, brick 1906

Maximum Shear Stress

1.42e+08

0.00e+00



seal stress  
t = 1.00000e+00

# Electrolyte Stresses – FEA analysis

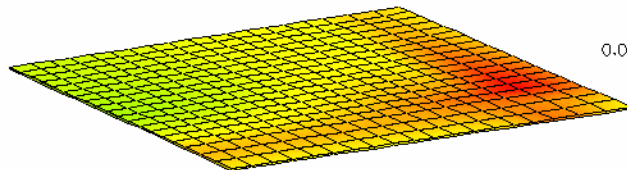
$$E_{\text{seal}} = 20 \text{ GPa}$$

min: 9.69e+07, brick 897  
max: 1.47e+08, brick 1852

Maximum Shear Stress

1.45e+08

0.00e+00



seal stress  
t = 1.00000e+00

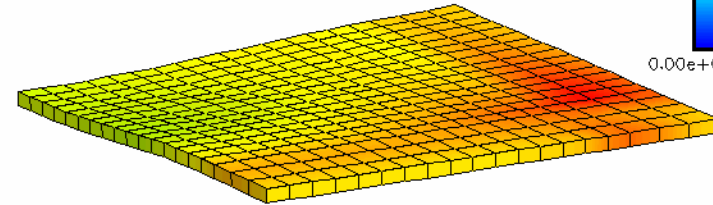
$$E_{\text{seal}} = 200 \text{ GPa}$$

min: 9.71e+07, brick 897  
max: 1.43e+08, brick 1849

Maximum Shear Stress

1.42e+08

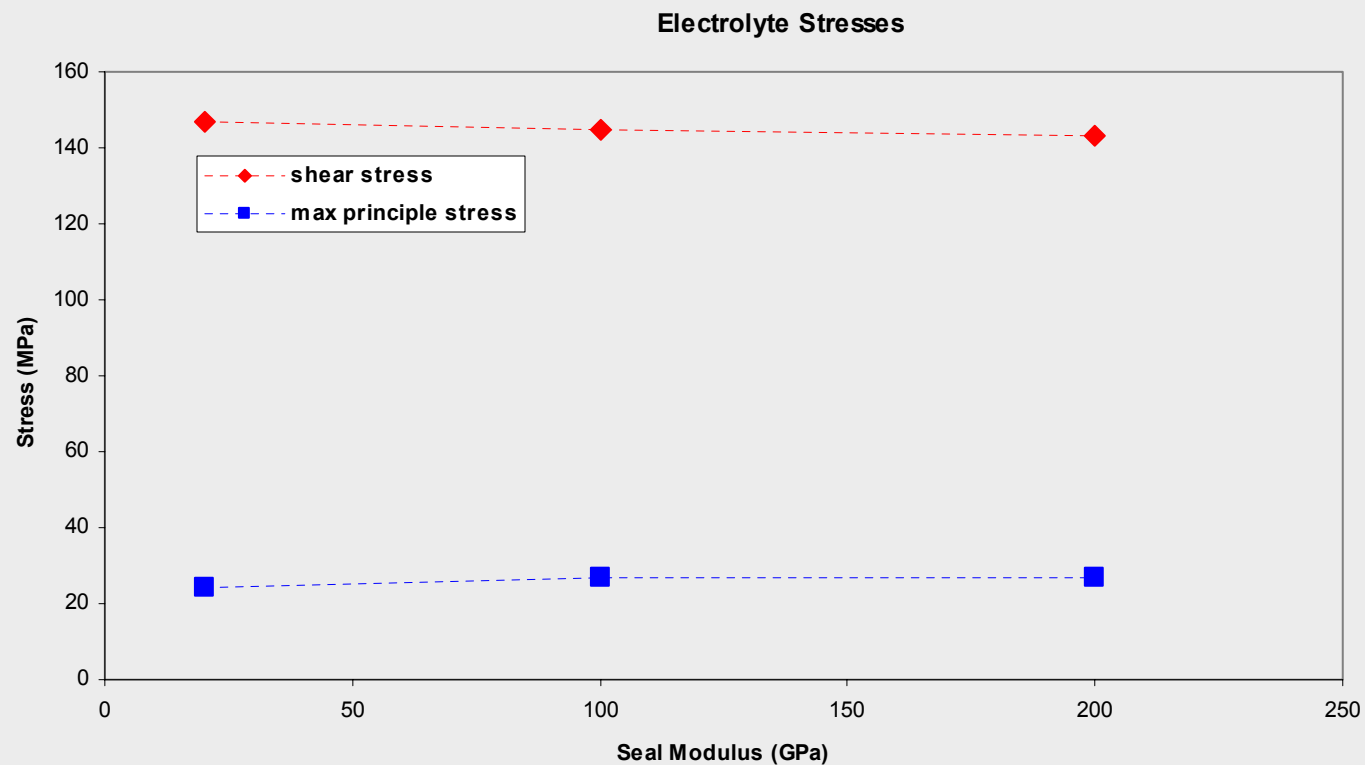
0.00e+00



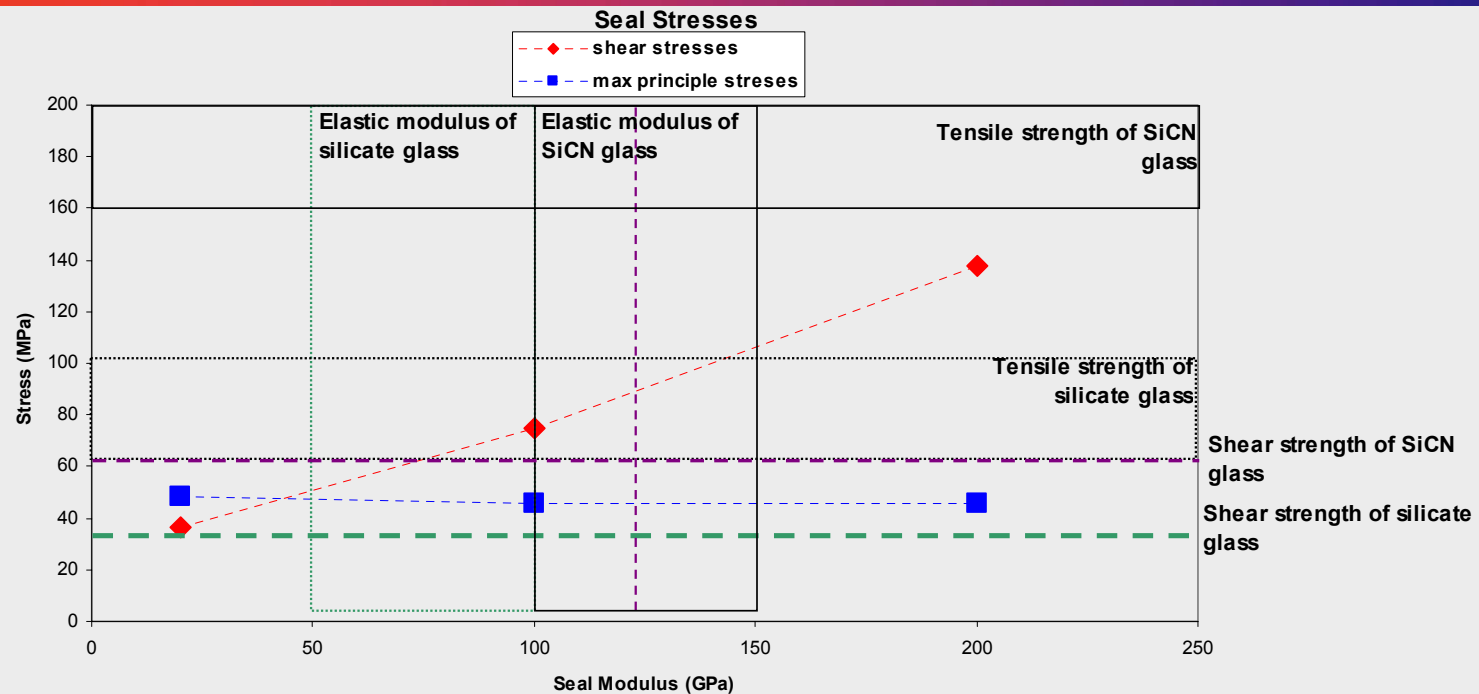
seal stress  
t = 1.00000e+00

# Electrolyte Stresses – FEA analysis

➤ Seal compliance doesn't significantly affect electrolyte stresses, since weight of stack constrains displacements.



# Seal material selection



- Compliant materials, with required properties, have low strength.
- High strength materials, with required properties, have low compliance.
- Composite seals combine benefits of high-temperature materials and compliant materials.
- Seal designs can also be used to modify stress states.



# Thermal Shock

$$R' = k\sigma_{\max}(1-\nu)/(E\alpha)$$

composition	k (W/m-K)	E (GPa)	$\alpha$ (ppm-C <sup>-1</sup> )	$\nu$	$\sigma_{\max}$ (MPa)	R'
silicate	1	75	10	0.2	60-100	85.3
SiCN	10	120	10	0.2	160-200	<b>1200</b>

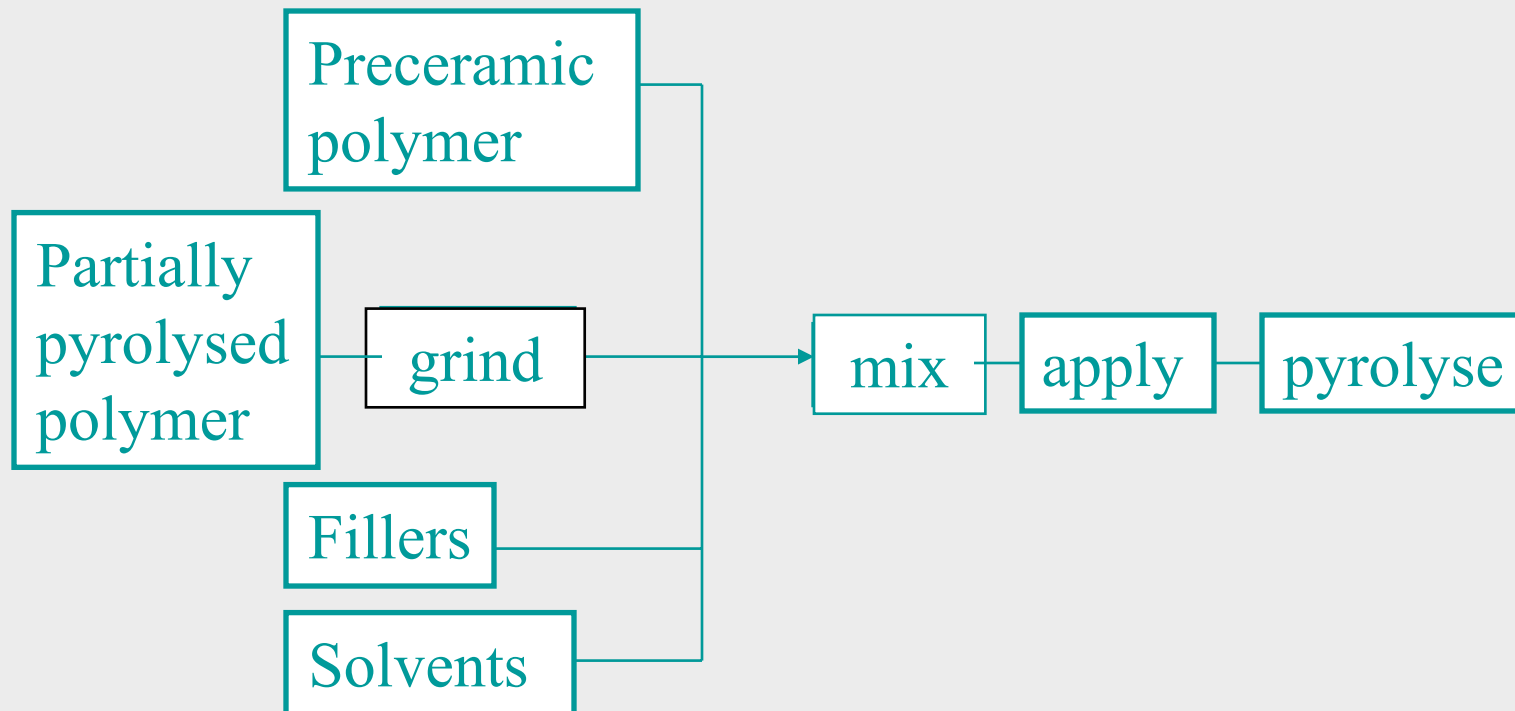
➤ Amorphous, non-oxide-based seal materials should have significantly higher resistance to thermal shock and, hence, thermal cycling.

# Preceramic polymer precursor derived seals - rationale

- Allows for introduction of a variety of fillers and additives that provide for thermophysical compatibility and mechanical compliance.
- Leads to formation of chemically inert, microstructurally stable, non-reactive (w/SOFC components) amorphous, non-oxide materials with enhanced mechanical properties compared to alternative, high temperature materials.
- Allows liquid and polymeric processing methods – dip coating, spray coating, molding, injection, etc.
- Relatively low processing temperature (900 - 1000°C).
- Suitable for intermediate and high temperature operation.

# Seal Fabrication

## Process Flowchart



# Test seals - fabrication



Application

Pyrolysed seals

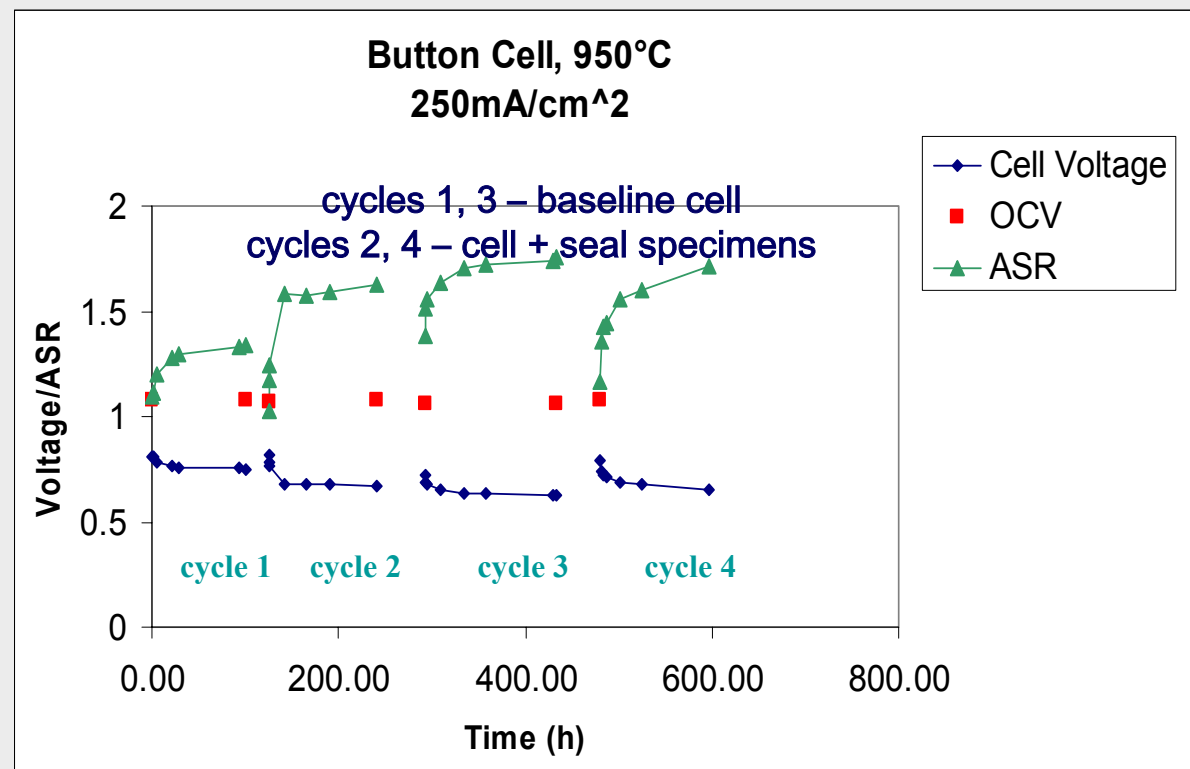
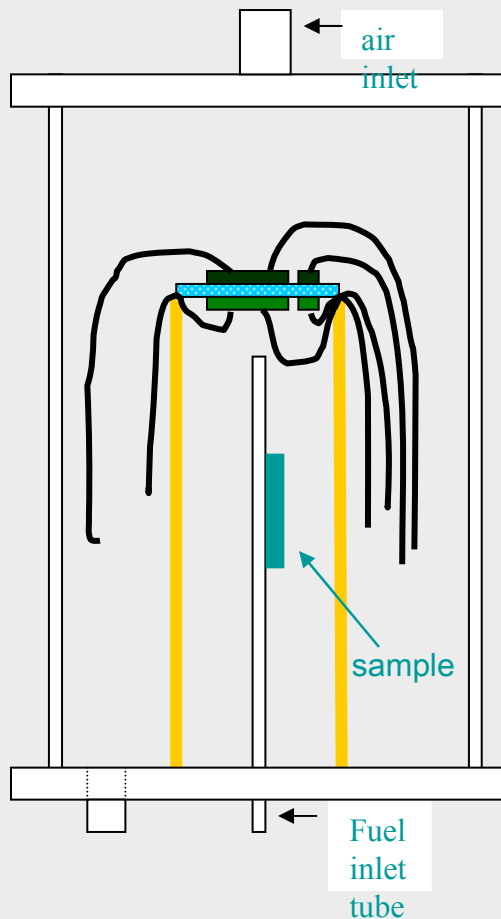


# High thermal expansion, inert fillers used to control CTE

Composition	Temperature Range (°C)	CTE (ppm °C <sup>-1</sup> )
<i>8 mol% yttria-doped zirconia</i>	<i>25-1000</i>	<i>10.6-11.1</i>
polycarbosilane/Metal 1	200-700	10.0
polycarbosilane/Metal 2	200-700	7.0
polycarbosilane/Metal 3	200-700	9.0
polycarbosilane/Ceramic 1	200-700	7.0
polycarbosilane/Glass 1*	200-600	7.0
polycarbosilazane/Metal 1	200-600	10.0
polycarbosilazane/Metal 2	200-700	5.0
polycarbosilazane/Metal 3	200-700	10
polycarbosilazane/Ceramic 1	200-700	8.0

\* Glass provided by Dr. R. Loehman, Sandia National Laboratory, Albuquerque, NM..

# Compatibility with SOFCs



➤ Preliminary results indicate cell performance is not affected by the presence of seal material in the fuel stream

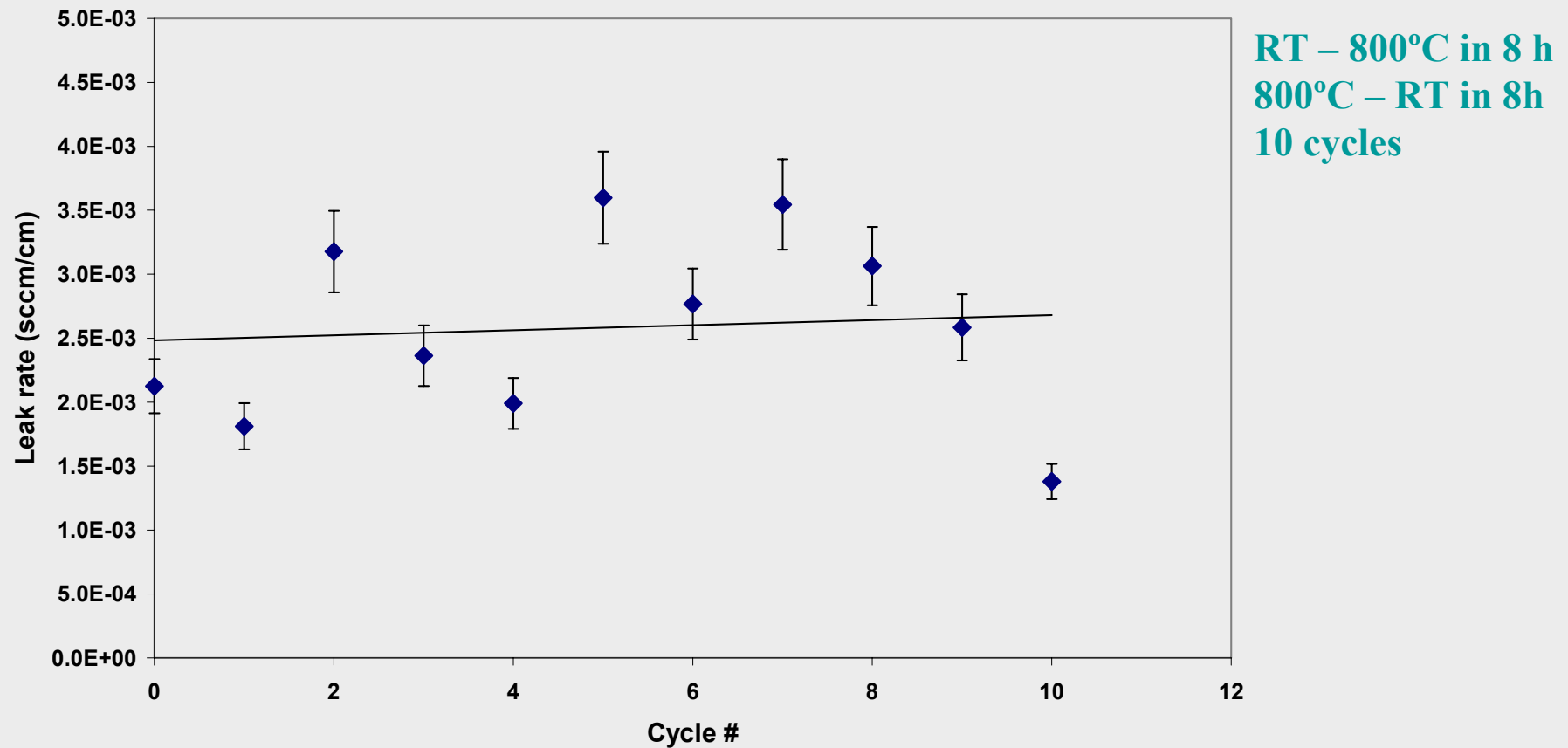
# Leak rate

Substrates	Leak rate (sccm/cm)
Zirconia electrolyte/zirconia electrolyte	$1.3 \times 10^{-3}$ *
Zirconia electrolyte/metal interconnect	$1.9 \times 10^{-3}$
Metal interconnect/metal interconnect	$2.7 \times 10^{-2}$
<i>Alumina/inconel sealed w/compressive, hybrid mica seal (PNNL data measured at 800°C)</i>	$1.6 \times 10^{-4}$

## ➤ Seals tested without applied, compressive force

\* Same as for a proprietary glass seal w/matched thermal expansion but higher reactivity with ceramic SOFC components.

# Leak rate – effect of thermal cycling

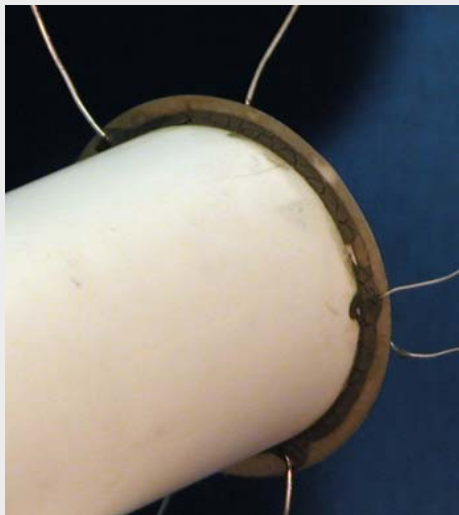
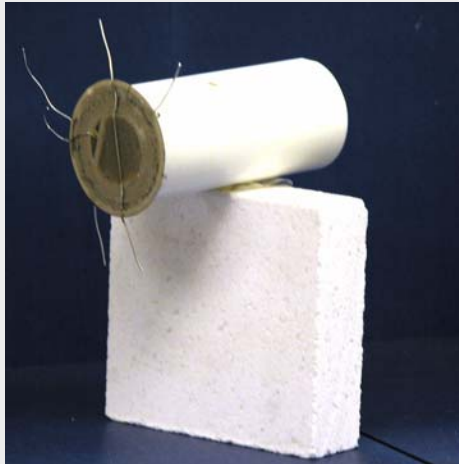


➤ Very little degradation in leak rate due to thermal cycling



# Seal performance

## 4 cm diameter SOFC tests



Temp. (°C)	polycarbosilane + metal filler	polycarbosilane + ceramic filler
800	1.038 V	1.065 V
850	1.030 V	1.052 V
900	1.008 V	1.042 V
cooled to 50°C		
800	1.031	1.073
850	0.992	1.062
900	0.949	1.050

# Summary

- **Pyrolysis of preceramic polymer precursors offers a promising method for sealing SOFCs.**
- **Fillers and partial-pyrolysis can be used to mitigate shrinkage stresses and to control thermoelastic properties.**
- **Additional studies of leak rate reduction, adhesion, CTE, and environmental stability are underway, but preliminary results are encouraging.**