

2005 SECA Core Technology Review

High Temperature Strain Gages for SOFC Application

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Tampa, FL

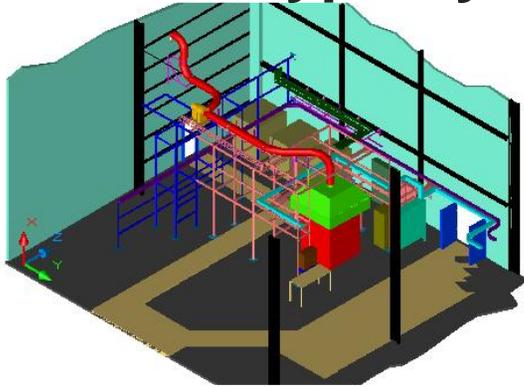


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Sponsor: SECA Program

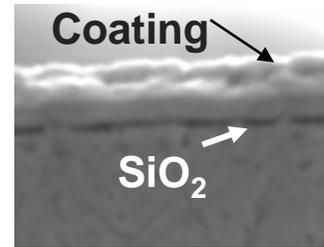


Overview of NETL SECA Support

- Independent Testing of SECA Prototype Systems

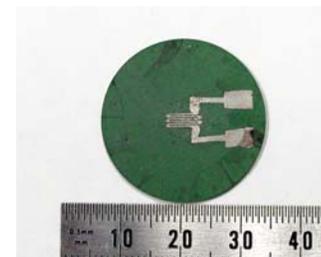
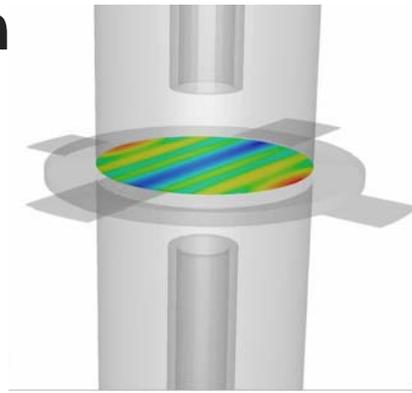
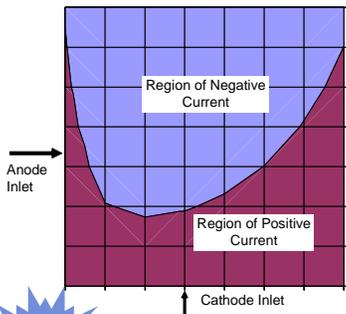


- Interconnect Development (coatings)



- Sensor Development

- Model Development and Application



Sensor Development Review

- **Technical Issues**
- **R&D Objective**
- **Approach**
- **Results**
- **Applicability to SOFC Commercialization**
- **Activities for next 12 months**



Technical Issues / Challenges

- **Cell mechanical failure occurs frequently but is little understood**
 - Sudden event upon application of a load > critical strength (thermally or mechanically induced)
 - Can occur after numerous hours at a SCCG loading
- **There are few tools available for the engineer to employ**
 - ‘Integral’ strain measurements; Luna Innovations, Inc. (optical fiber; >800 deg. C)
 - Optical profilometry; Solarius Development, Inc. (optical access)
 - Acoustic emission for catastrophic failure detection
- **What is happening ‘inside the box’?**
 - Stack compression/creep?
 - Cell strain prior to failure?
 - Are FEA models working?



R&D Objective

Investigate/extend high temperature strain gage sensors to SOFC applications

- NASA (and others) have supported the development of high temperature strain sensors for in-situ turbine mechanical study
- Apply to prototype SOFC cells and subcomponents to assess feasibility as a new tool for engineering analysis
 - test in oxidizing & reducing environments—prove capability
 - measure fuel cell strain during start-up, shut-down, load changes, and fuel and oxidant concentration gradients



Approach

High Temperature Strain Sensors

- **Standards exist for resistive and capacitive gages**
 - ASTM E1319–98 (2003) Standard Guide for High-Temperature Static Strain Measurement
 - *Prototype evaluation: gage + calibration device + hardware + instrumentation for system behavior checkout and qualifying installation procedures.*
- **Issues: good sensitivity (high gage factor), zero drift, sensitivity drift, repeatability, hysteresis, thermal response**

Gage factor:

$$K = ((R - R_{ref})/R_{ref}) / (L - L_{ref})/L_{ref}$$

$$= (\Delta R/R_{ref})/\varepsilon$$

$$K \sim 1.0 \text{ to } 20.0$$



Approach (cont.)

High Temperature Strain Sensors

- **Resistive → suited for dynamic or short term static meas.**
 - Gage Factor; $K \sim 2-6$ for most metals (Fraden, 1993)
 - PdCr; $K \sim 2$
 - oxidation effects (not used for long tests)
 - 800 deg. C max
- **Capacitive → suited for long term tests (creep)**
 - not affected by temperature, oxidation, phase change

Approach (cont.)

High Temperature Strain Sensors

- **Piezo-resistive Semiconductors → suited for dynamic measurement**
 - Gage Factor; $K \sim 10$ @ 800 deg. C
 - indium-tin oxide (ITO); n-type ceramic
 - proven good thermal stability
 - oxidation resistance
 - good electrical response
 - used to study high cycle fatigue in jet engines (URI) up to 1500 deg. C (18-million cycle lifetime)

Thin Film Strain Sensors For SOFC

- **Benefits**

- non-intrusive
- small footprints
- little thermal mass
- sensitive for detecting small fluctuations associated with transient operation

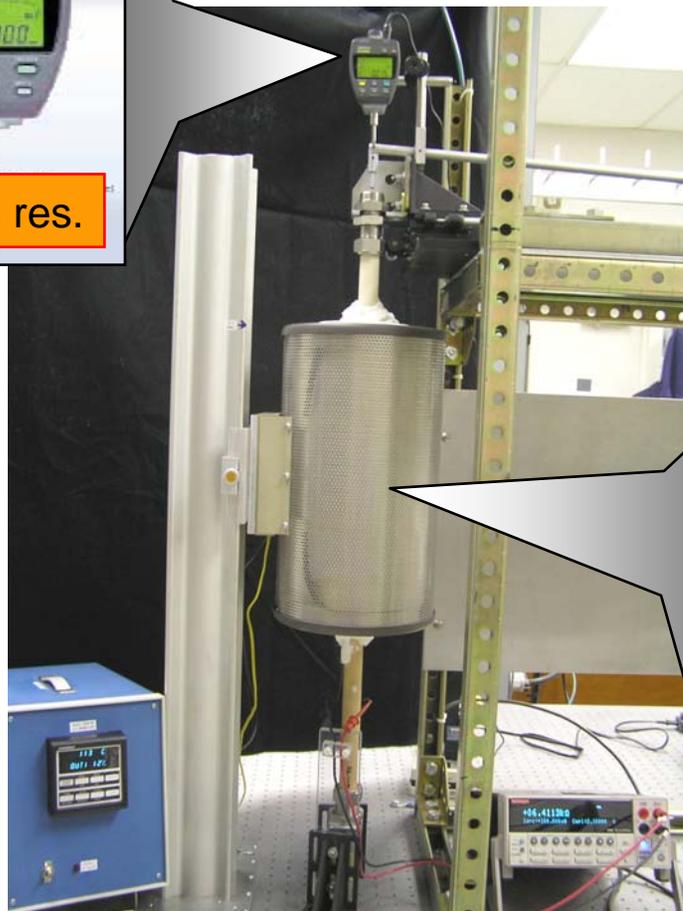
Thin Film Strain Sensors For SOFC

Pd-Cr/Indium-Tin Oxide

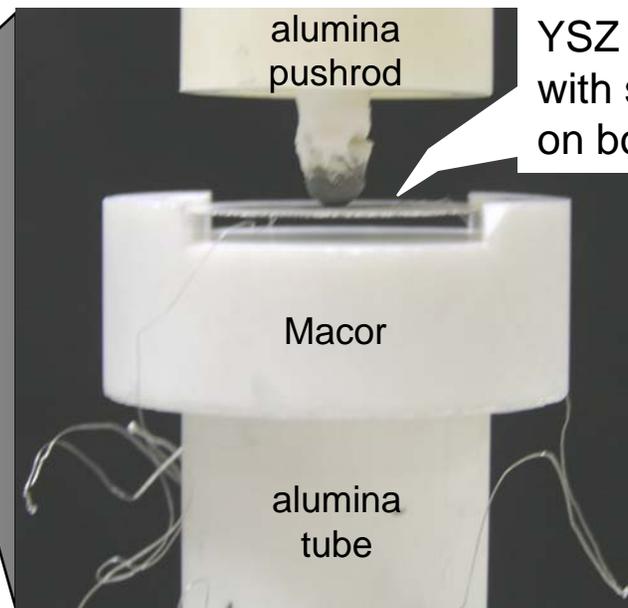
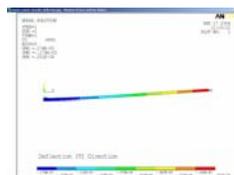
- **Fabrication:**
 - passivation / electrical isolation
 - patterning of the thin film leads using masks
 - patterning of the active strain sensor elements using photolithography
 - deposition of the thin film leads and bond pads as well as the active strain material using rf sputtering
 - lead wire attachment

Experimental & Analysis Approach

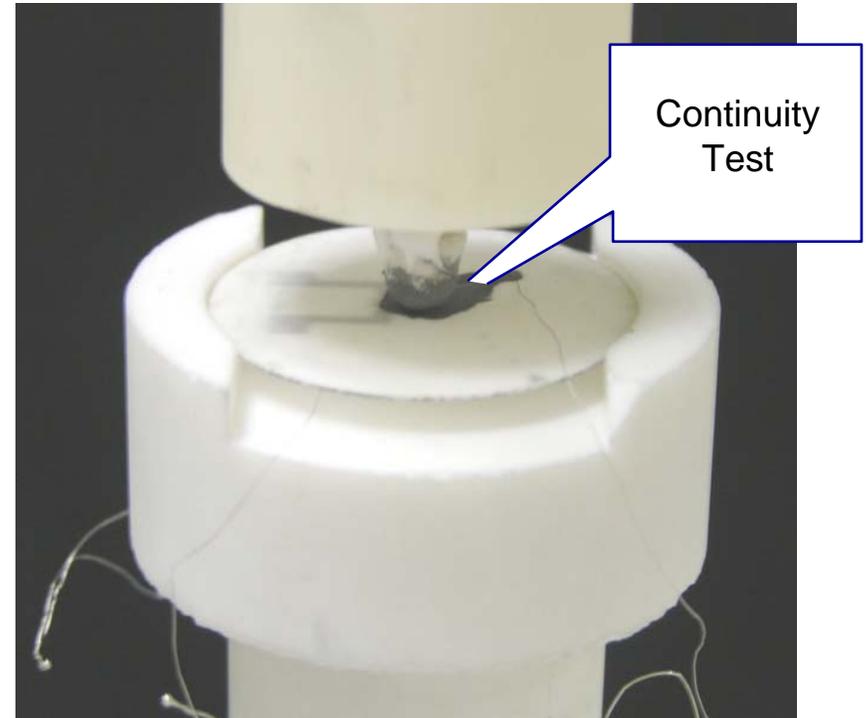
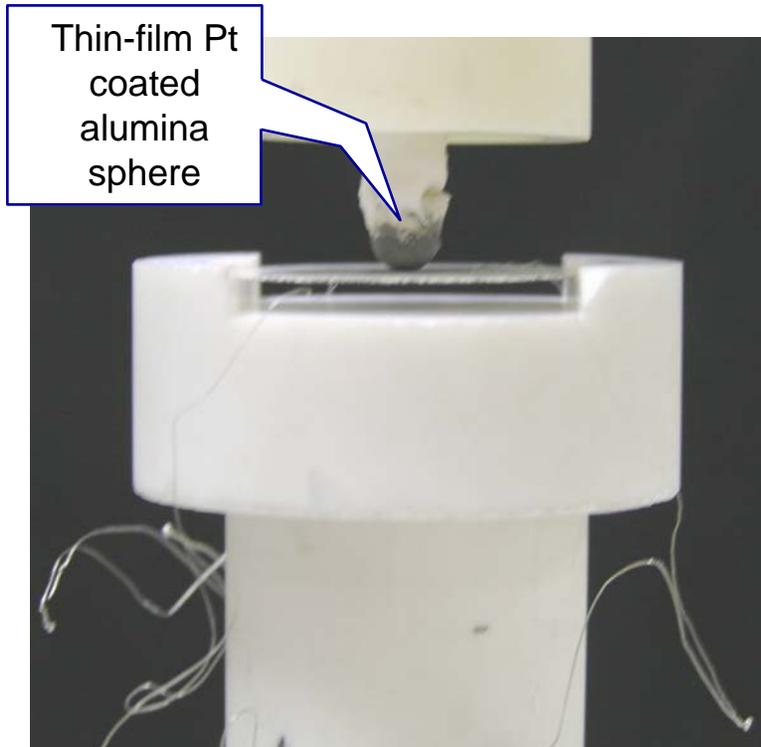
Strain Gage CTR



- Initial bi-axial tests worked
- 3-point measurements gave improved resolution
- ANSYS used to predict strain

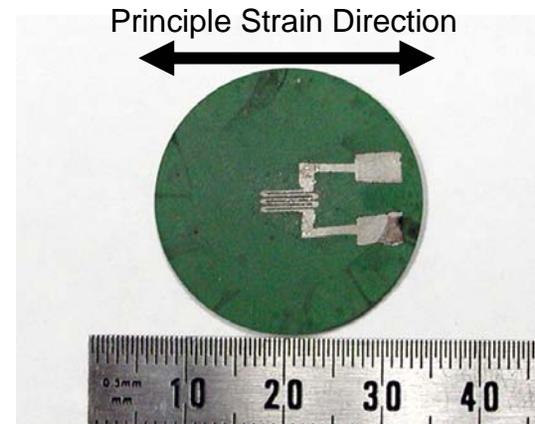


11/09/04 PdCr gage (*zero reference method for deflection*)



Specimens Studied

- **PdCr**
 - 8YSZ wafer (191 μ m thick)
 - simplicity
 - ease of characterization
 - button cell
- **Indium-Tin-Oxide**
 - 8YSZ wafer (280 μ m thick)
 - button cell
- **Monoaxial design (see photo)**
- **Non-Temperature Compensated**



PdCr strain gage applied to SOFC anode

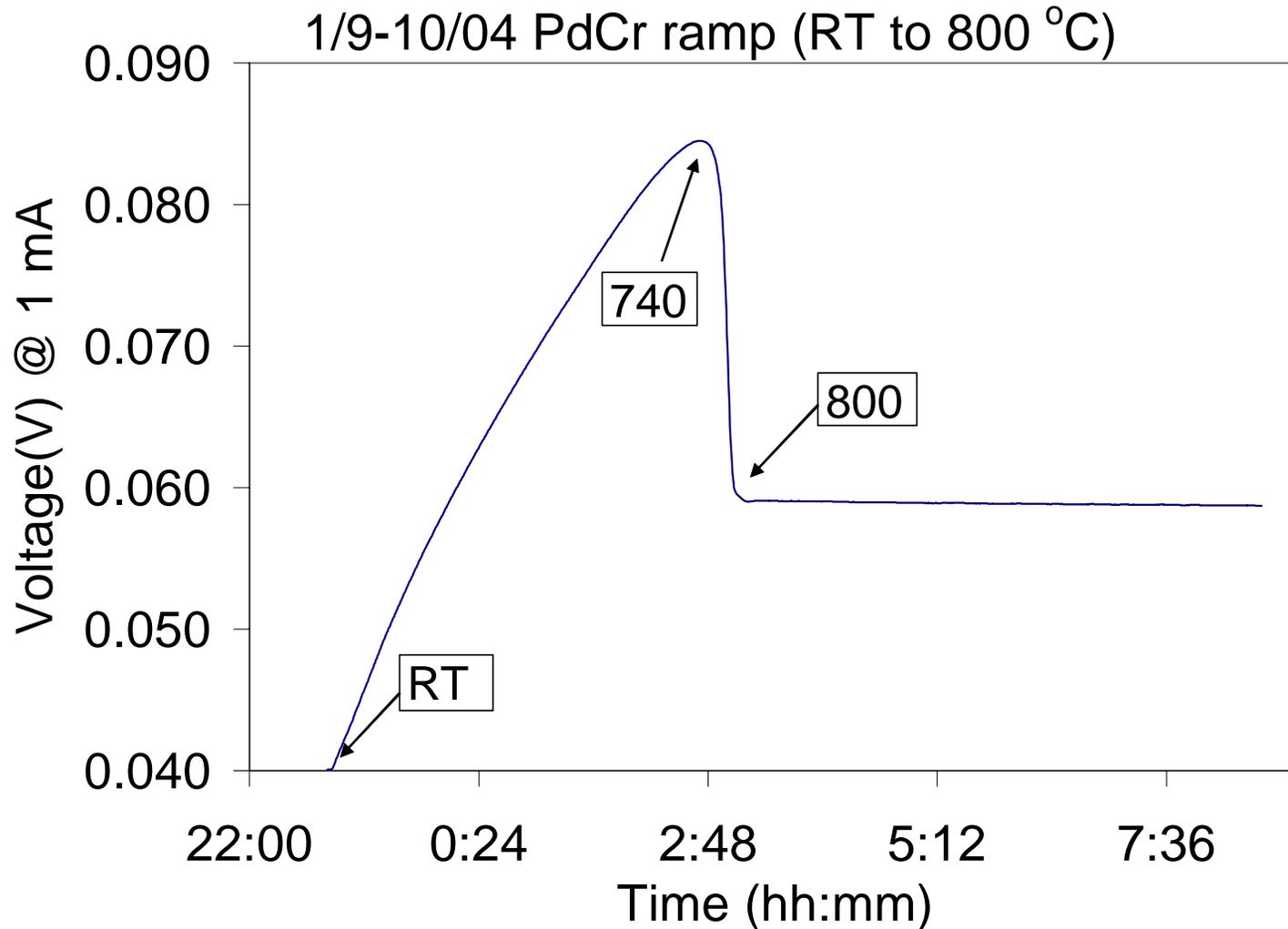
PdCr Results



Thermal Response
Gage Resistance (vs. T)
Stability (in Air)
Strain Response
Gage Factor

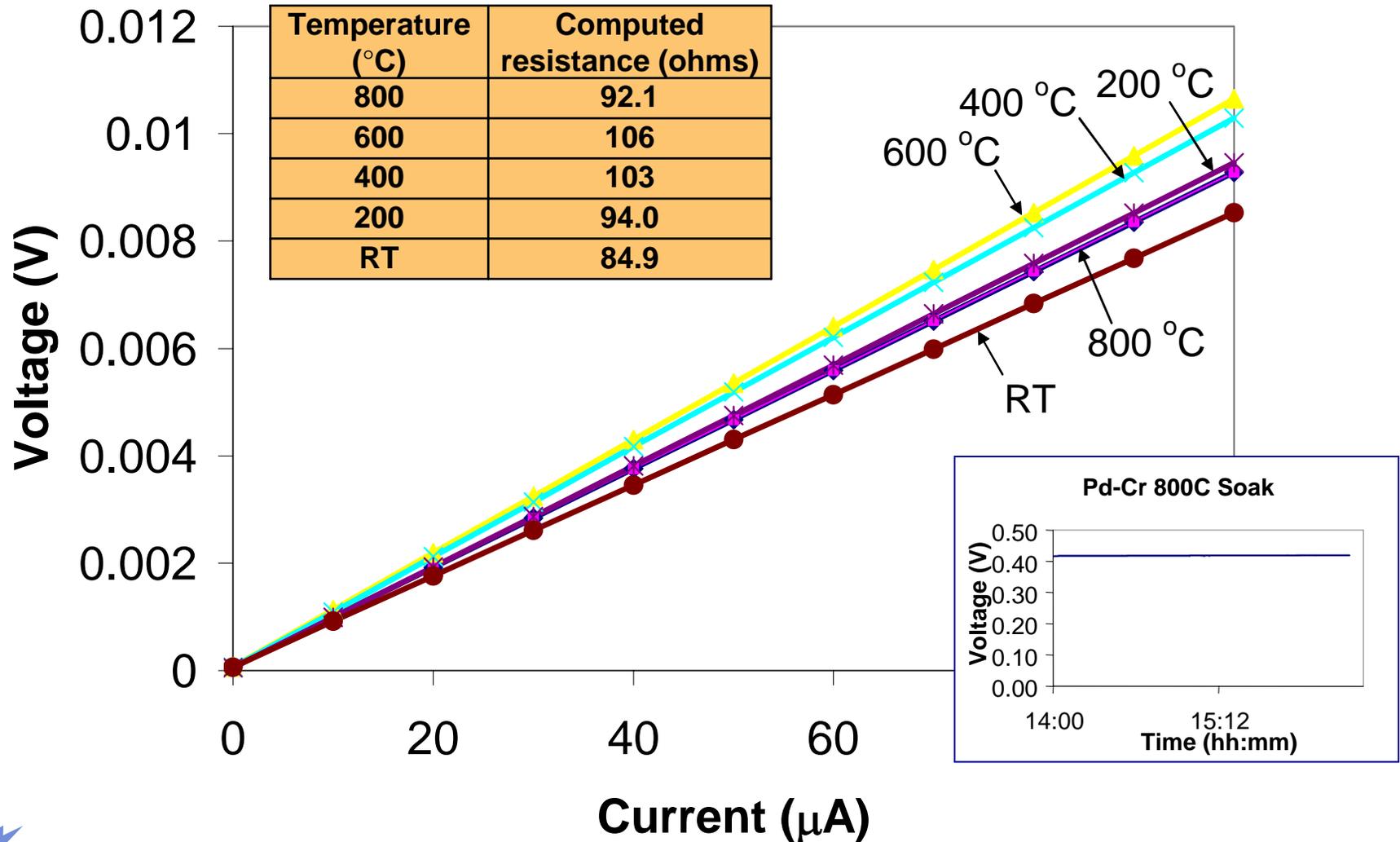
Pd-Cr Thermal Response

(8YSZ Wafer; Non-Temperature Compensated)



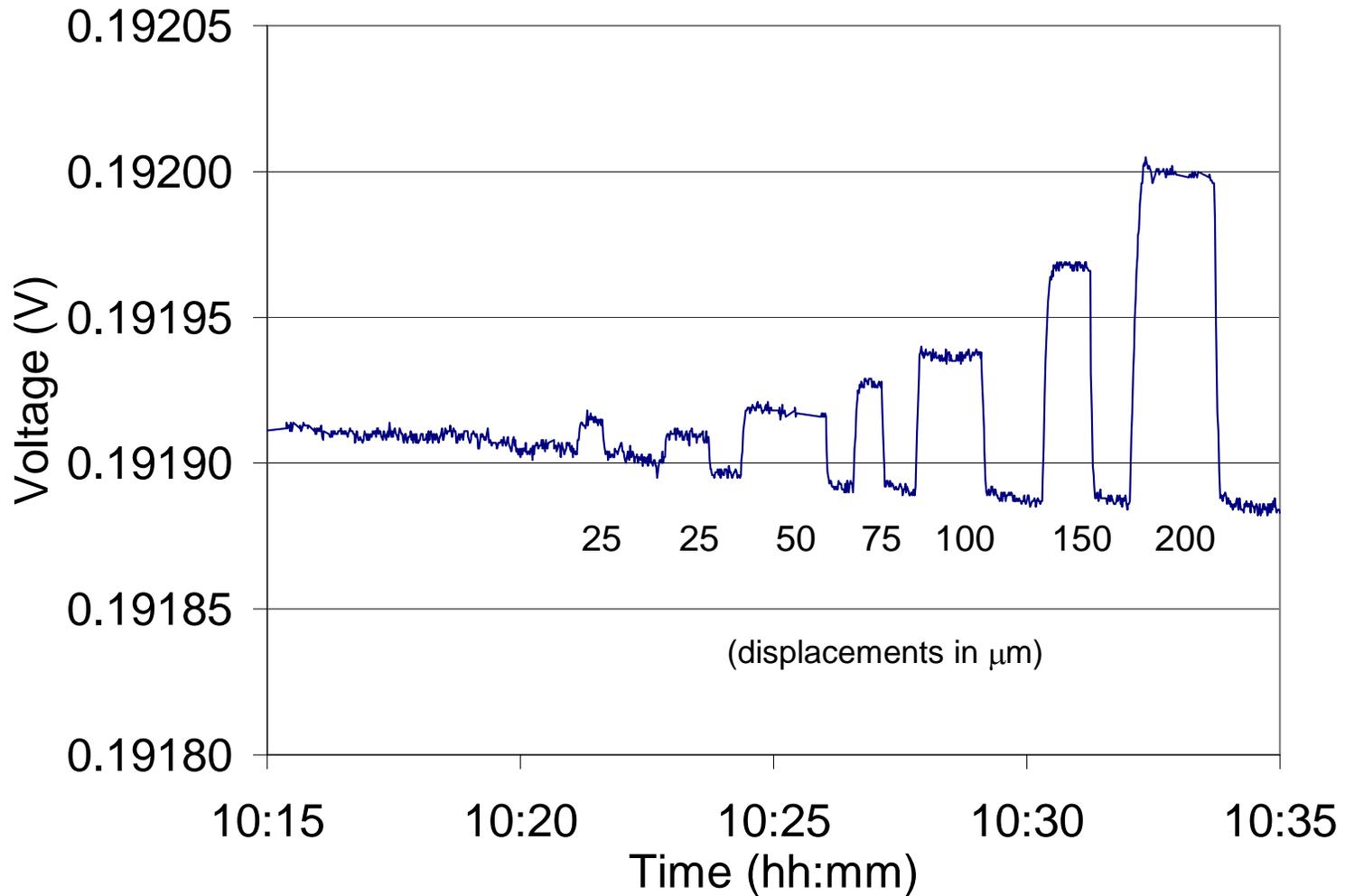
Pd-Cr Resistance

(8YSZ Wafer; Non-Temperature Compensated)



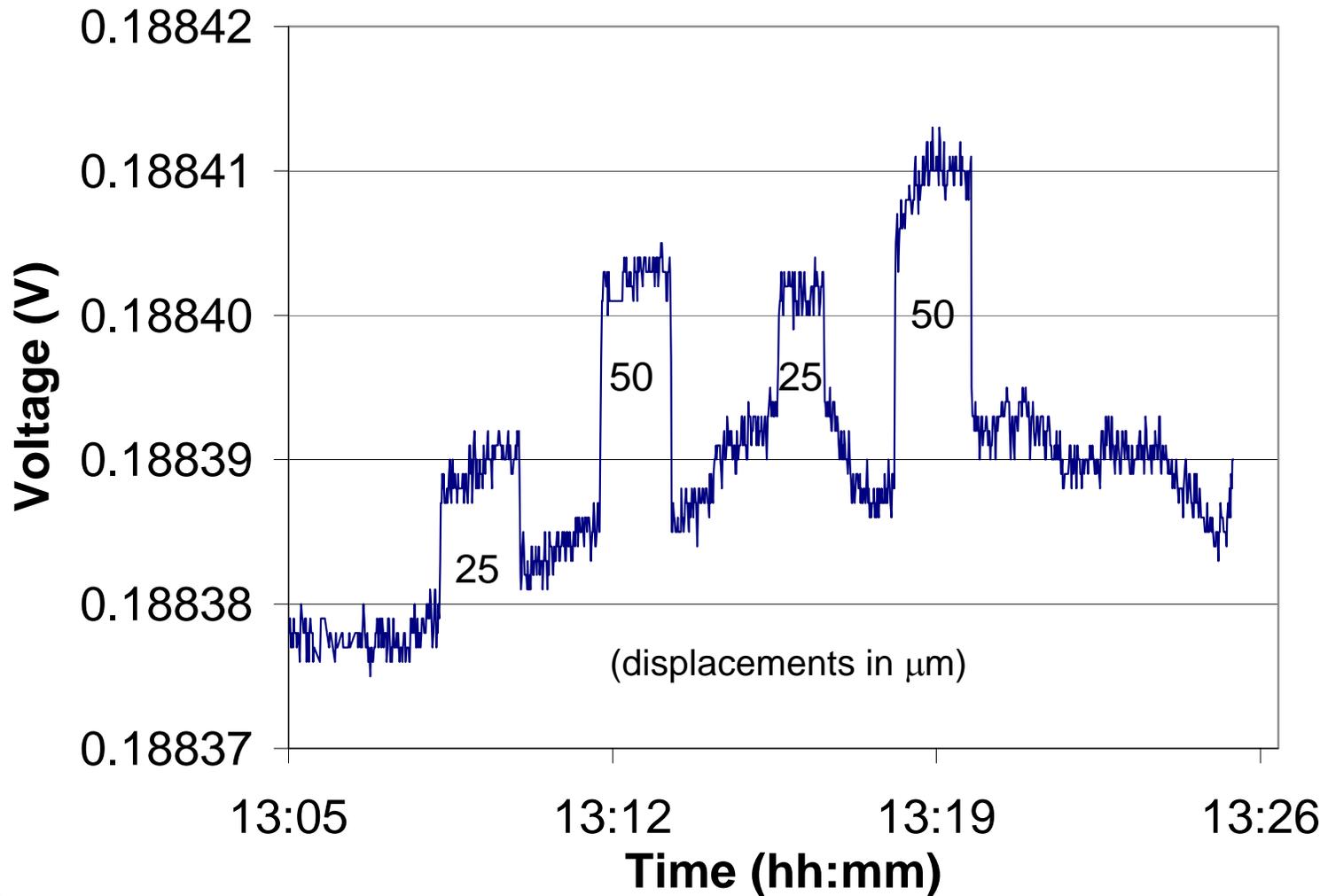
PdCr RT Strain Response

(8YSZ Wafer; Non-Temperature Compensated)



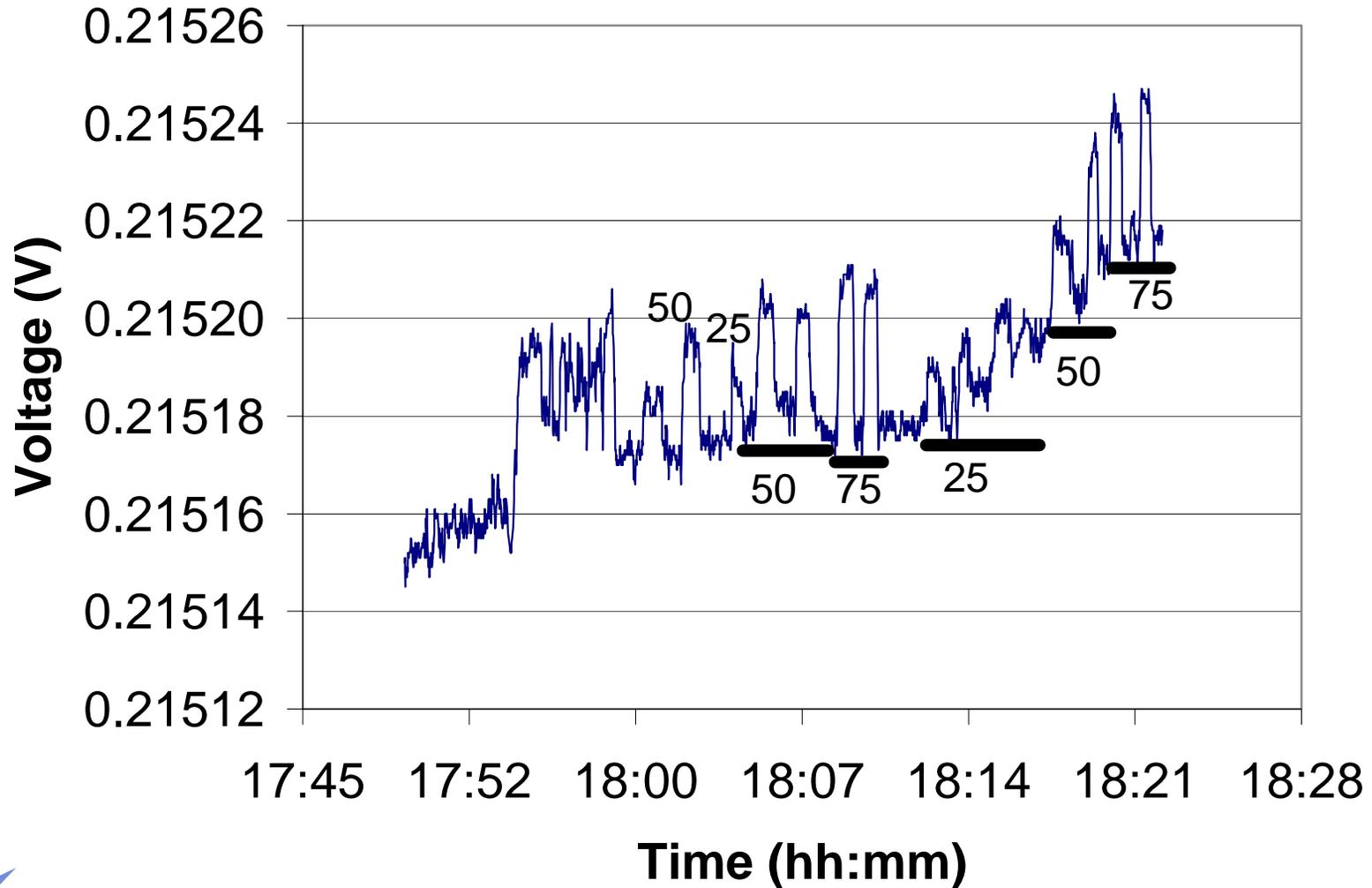
PdCr 50 °C Strain Response

(8YSZ Wafer; Non-Temperature Compensated)



PdCr 550 °C Strain Response

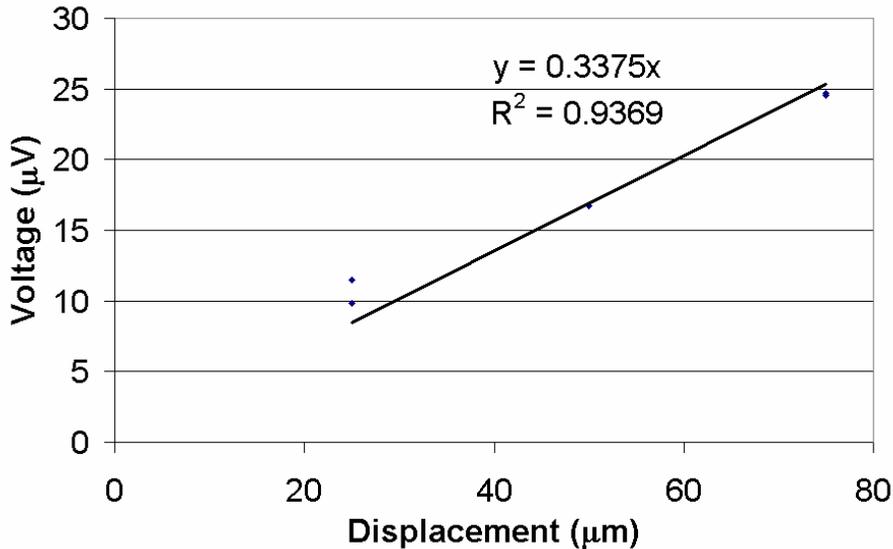
(8YSZ Wafer; Non-Temperature Compensated)



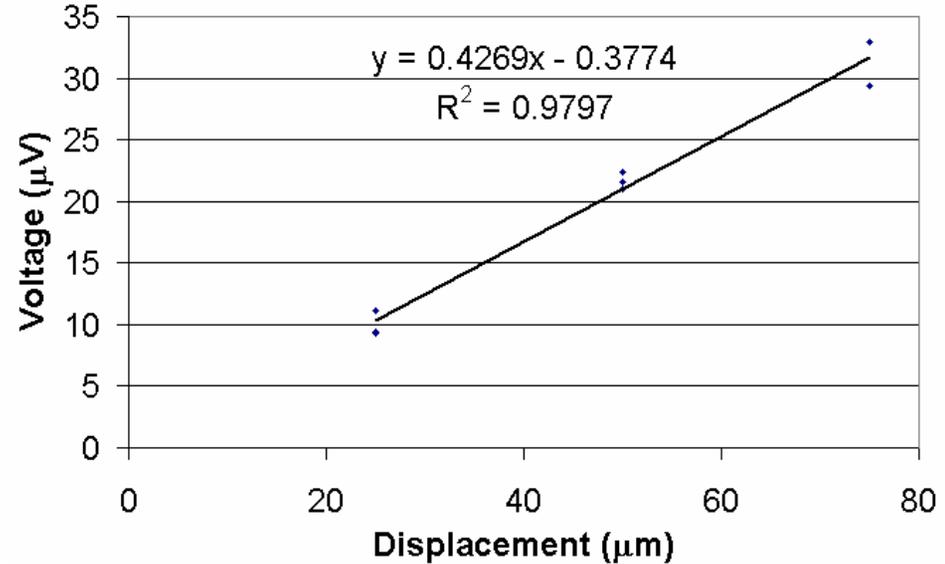
Pd-Cr Strain Response

(8YSZ Wafer; Non-Temperature Compensated)

11/12/04 Pd-Cr Strain Response @ RT



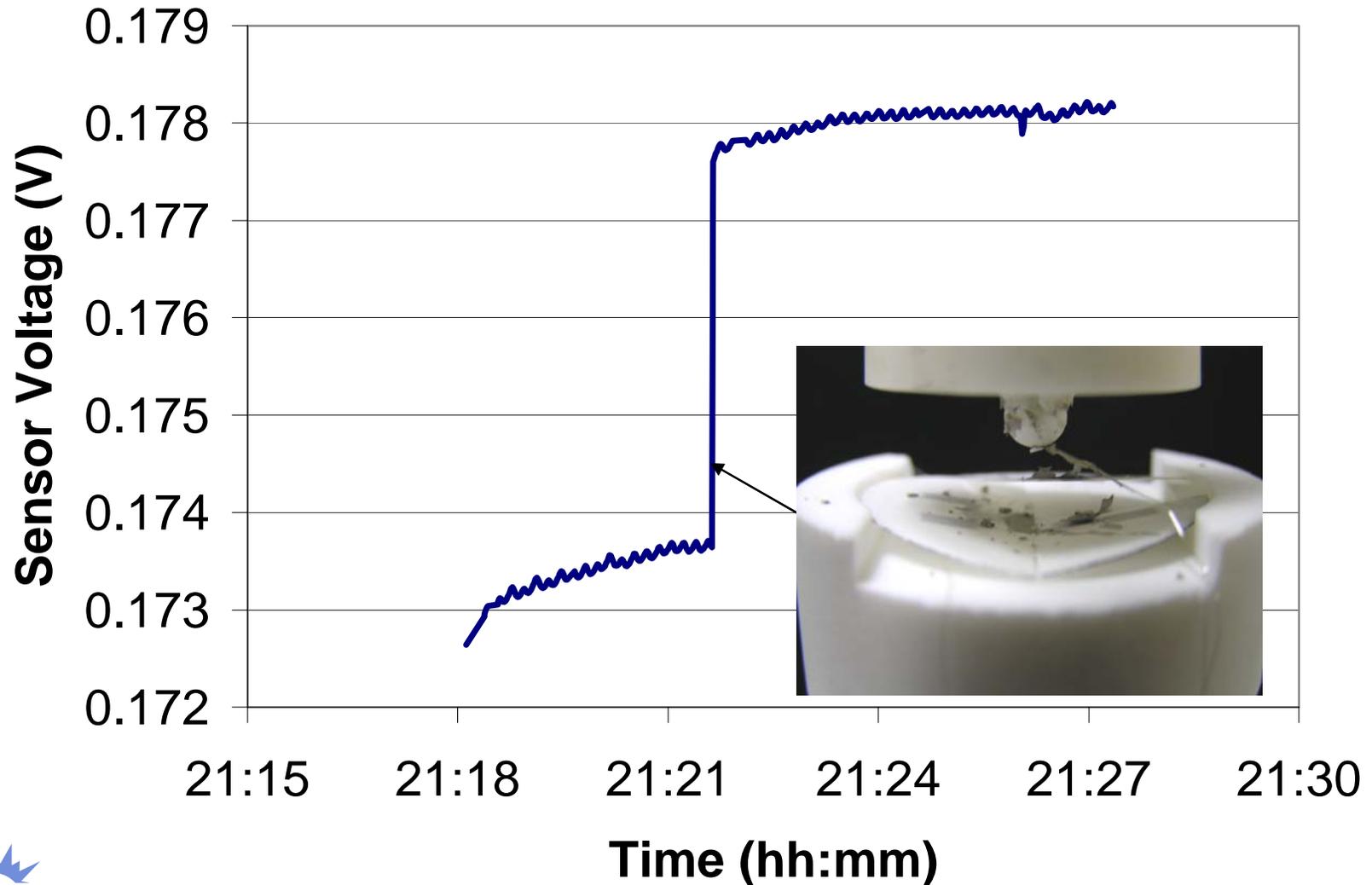
11/12/04 Pd-Cr Strain Response @ 550C



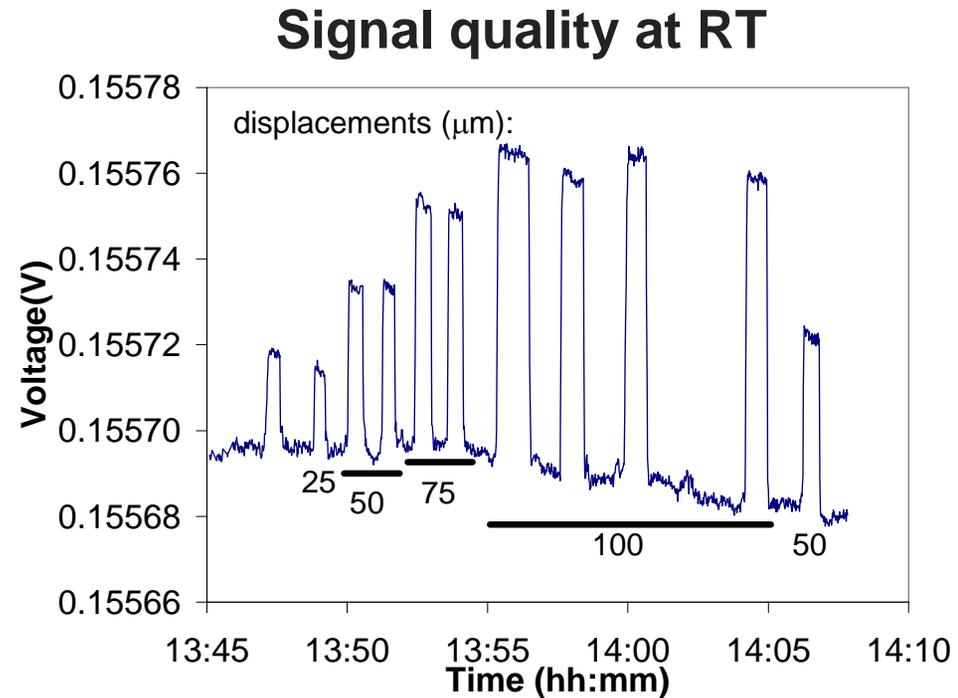
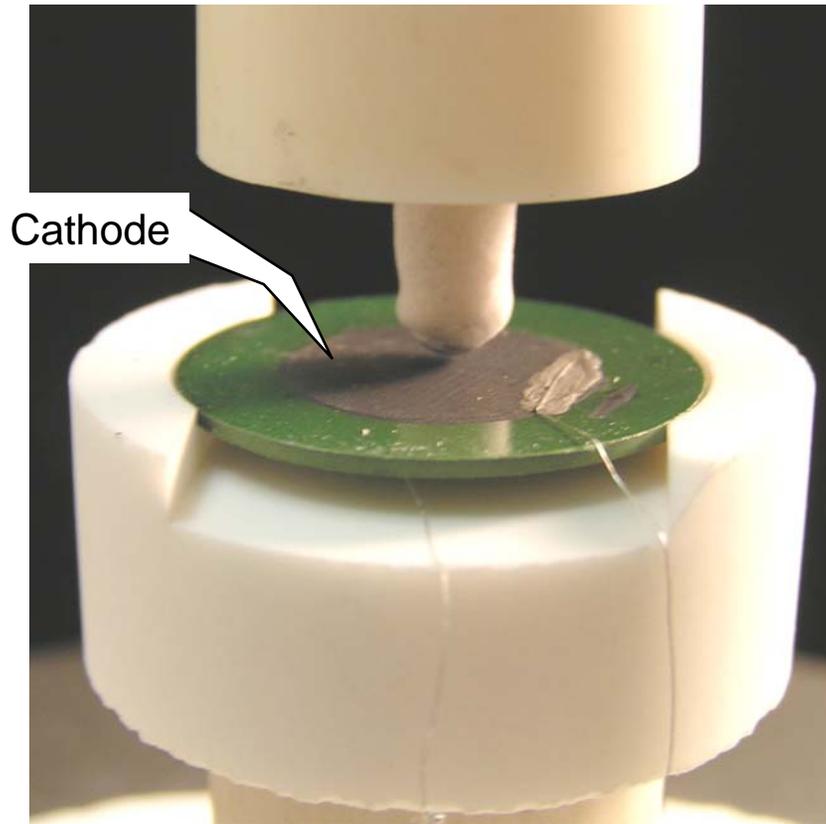
- **Good S/N Ratio at $T < 200\text{ }^\circ\text{C}$**
- **Gage factor is slightly increased at higher temperatures**

PdCr Fracture Signal (750 °C)

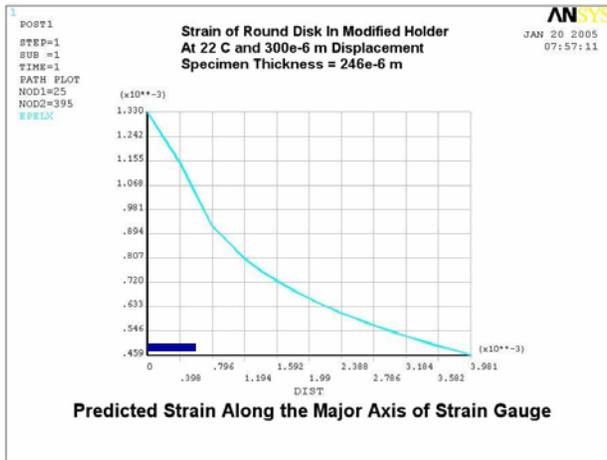
(8YSZ Wafer; Non-Temperature Compensated)



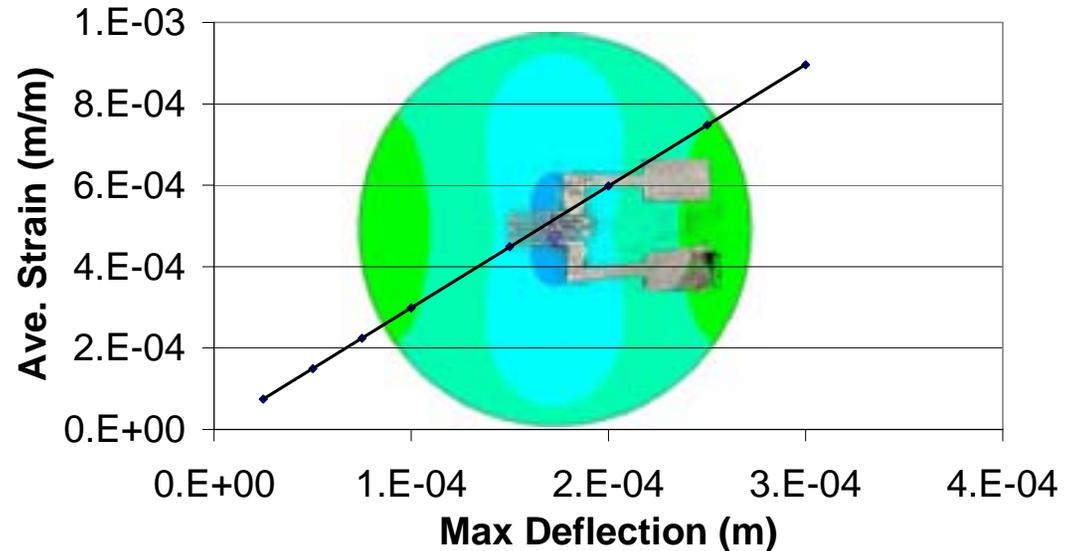
PdCr Sensor on 1-mm Anode Supported Cell



ANSYS



Ave Strain In Gauge vs Max Deflection
(246e-6 m thick disk specimen)



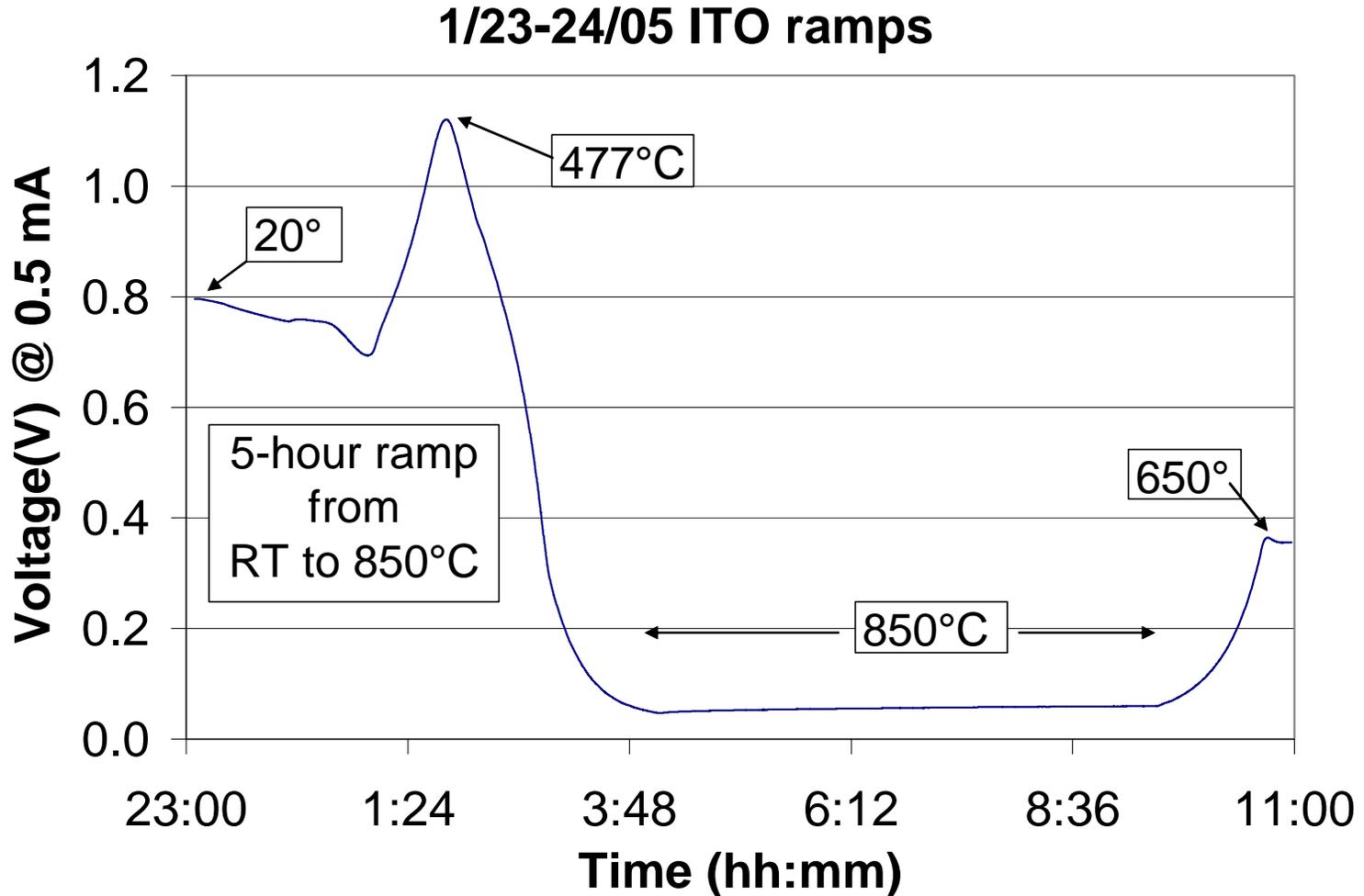
- **Calculated gage factor for PdCr sensor**
 - K=0.78 at RT
 - K=0.93 at 550 °C

ITO Results



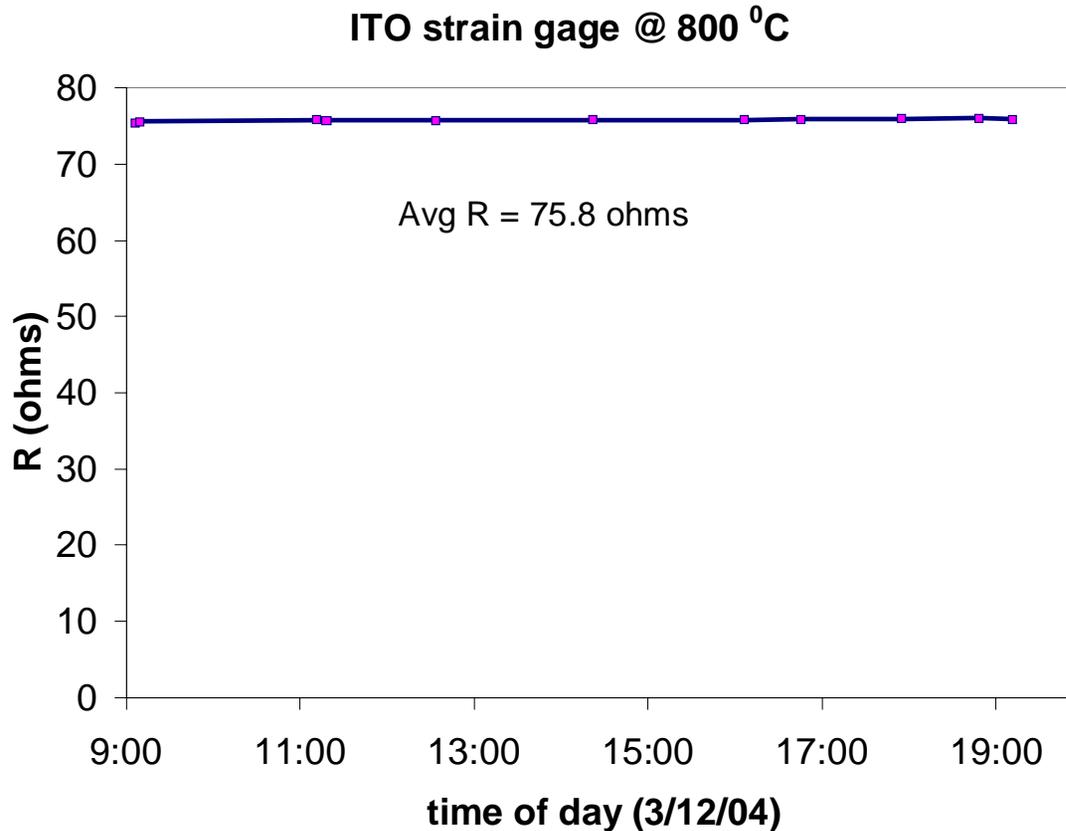
**Thermal Response
Stability in Air
Strain Response**

ITO Thermal Response



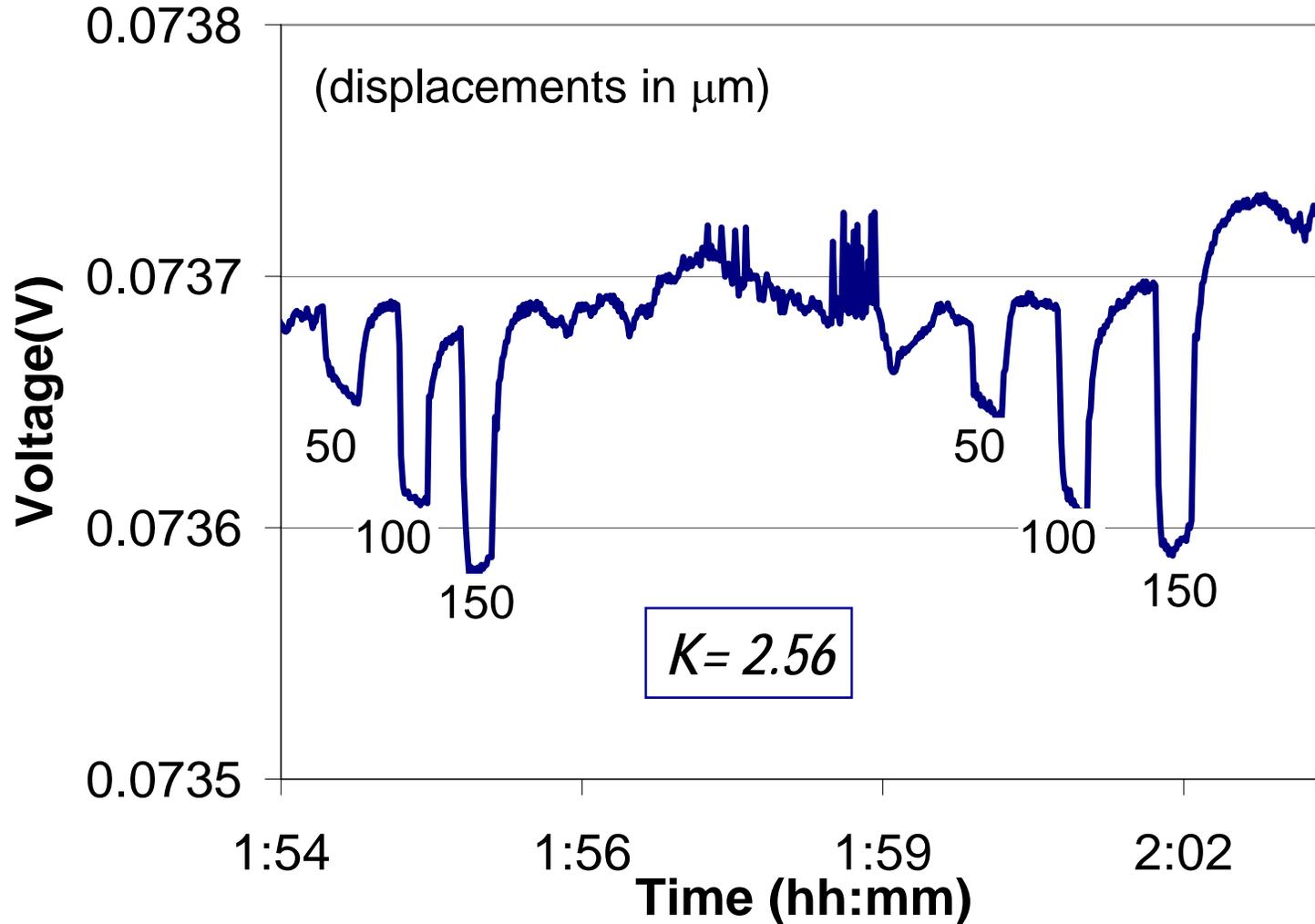
ITO Stability

- ITO at 800 °C for one week with resistance measurements taken periodically



ITO 650 °C Strain Response

(8YSZ Wafer; Non-Temperature Compensated)



Summary

- ITO strain gage has far better S/N ratio over PdCr
- Strain signal sufficient for detecting strain in SOFC materials
- Gage factors lower than typically cited
 - PdCr ~ 0.93
 - ITO ~ 2.5

Application to SECA

- **High temperature strain gages may be of use in development of SECA cell and stack technology**
 - Diagnostic during stack assembly (stack compression)
 - Diagnostic for ensuring creep effects are not relieving/removing desired compressive load for sealing
 - Diagnostic for stack state of stress
 - Diagnostic for on-cell state of stress
 - Experimentally validate models (e.g., GTech)
- ...and thereby improve our design capabilities through better modeling/prediction of mechanical performance



FY05-06 Project Tasks

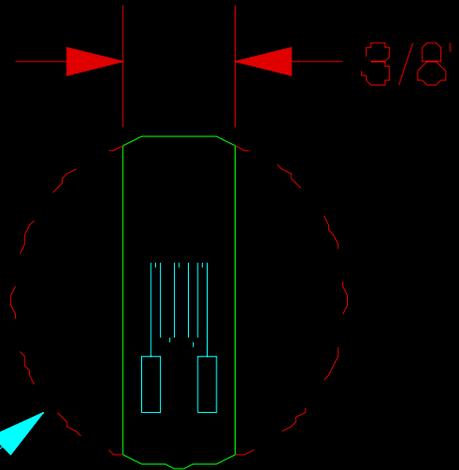
(focus on ITO)

- **Task 1 –YSZ Substrates**
 - Confirm ITO sensor response (gage factor) at 200, 400, 600 and 800 deg. C.
 - Determine stability in reducing atmosphere
 - Characterize temperature-compensated sensor
- **Task 2 – Apply Sensor to Button Cell**
 - Evaluate in-situ response during cell operation
- **Task 3 – Model Experimental Conditions**
 - Apply models to experimental cases
 - Determine ability of model to follow strain (mechanically or thermally induced)
- **Task 4 – Journal Publications and Presentations**



proposed 8YSZ strain beam

strain gage centered
on strain beam



approximately 1.1" dia 8YSZ disk
pressed, sintered & lapped;
2 sides scored & removed with
cut edges ground to width
(supplied by MSRI)

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- Fraden J., “*AIP handbook of modern sensors: physics, designs and applications*”, AIP, New York, 1993.