# **DOE FE Advanced Turbines Program**





# **Presentation Overview**

2017 University Turbine Systems Research Project Review Meeting

- Program elements / goals
- System studies
  - $H_2$  turbine at 3,100°F
  - SCO2 w/ oxy-CFB
  - SCO2 direct (coal gasification based)

## • Program project work

- Core projects
- UTSR projects
- START rig
- NETL RIC
- Next steps

### • Summary







# **Advanced Turbines Program Elements**

Research Focused in Three Key Technology Areas

- Advanced Combustion Turbines
  - CC eff. ~ 65 % (LHV, NG bench mark), TIT of 3,100 F
  - Delivers transformational performance benefits by 2025

# • SCO2 Turbomachinery

- Recompression Brayton Cycles (Indirect) for "boilers"
- Allam Cycles (Direct) for gasification and NG
- Pressure Gain Combustion
  - Alternate pathway to high efficiency







## H<sub>2</sub> Turbines - Performance and Cost Comparisons

Reference, Advanced H2 Turbine, and Transformation H2 Turbine "All-in" Cases





Parameter	"F" Turbine (reference)	AHT (2650 F)	THT (3100 F)
H <sub>2</sub> Turbine (MW)	464	680	940
Fuel Gas Expander (MW)	7	3	7
Air Expander (MW)	n/a	14	39
Steam Turbine (MW)	248	392	485
Gross Power (MW)	719	1,090	1,471
Auxiliary Power (MW)	-186	-262	-338
Net Power (MW)	533	828	1,133
Coal Feed (lb/hr)	481,783	635,089	816,118
Plant Efficiency (%)	32.4	38.1	40.6
COE (\$/MWh)*	134.5	104.1	92.7
* w/o T&S			



# **Oxy-CFB Coal-fired Rankine Cycle Power Plant**



Steam Rankine Comparison Cases

- LP Cryogenic ASU
  - 99.5% O<sub>2</sub>
  - 3.1% excess  $O_2$  to CFB
- Atmospheric oxy-CFB
  - Bituminous coal
  - 99% carbon conversion
  - In-bed sulfur capture (94%), 140% excess CaCO<sub>3</sub>
  - Infiltration air 2% of air to ASU MAC
- Operating conditions for Rankine plants
  - Supercritical (SC) Rankine cycle (Case B22F: 24.2 MPa/ 600 °C/ 600 °C)
  - Advanced ultra-supercritical (AUSC) Rankine cycle (Case B24F: 24.2 MPa/ 760 °C / 760 °C)
- No low temperature flue gas heat recovery
- 45% flue gas recycle to CFB
- CO<sub>2</sub> purification unit
  - ~100% CO<sub>2</sub> purity
  - 96% carbon recovery



Source: NETL



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## Oxy-CFB Coal-fired Indirect sCO<sub>2</sub> Power Plant

#### Baseline sCO<sub>2</sub> process

- LP Cryogenic ASU
  - 99.5% O<sub>2</sub>
  - 3.1% excess  $O_2$  to CFB
- Atmospheric oxy-CFB
  - Bituminous coal
  - 99% carbon conversion
  - In-bed sulfur capture (94%), 140% excess CaCO<sub>3</sub>
  - Infiltration air 2% of air to ASU MAC
- Recompression sCO<sub>2</sub> Brayton cycle
  - Turbine inlet temperature 620 °C and
  - Turbine inlet temperature 760 °C
- Low temperature flue gas heat recovery in sCO<sub>2</sub> power cycle
- 45% flue gas recycle to CFB
- CO<sub>2</sub> purification unit

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- ~100% CO<sub>2</sub> purity
- 96% carbon recovery





## **Oxy-CFB Coal-fired Indirect sCO<sub>2</sub> Power Plant**

Four sCO<sub>2</sub> cycle configurations analyzed

- Baseline configuration
- Reheat sCO<sub>2</sub> turbine
- Intercooled 2-stage main sCO<sub>2</sub> compressor
- Reheat sCO<sub>2</sub> turbine and Intercooled main sCO<sub>2</sub> compressor

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# **Summary of Overall Plant HHV Efficiencies**

### • Relative to the steam Rankine cycles:

- At 620 °C, sCO<sub>2</sub> cycles are 1.1 3.2 percentage points higher in efficiency
- At 760 °C, sCO<sub>2</sub> cycles are 2.6 4.3 percentage points higher
- The addition of reheat improves sCO<sub>2</sub> cycle efficiency by 1.3 – 1.5 percentage points
- The addition of main compressor intercooling improves efficiency by 0.4 – 0.6 percentage points
  - Main compressor intercooling reduces compressor power requirements for *both* the main and bypass compressors

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Power Summary (MW)	B22F	Base	IC	Reheat	Reheat+IC
Coal Thermal Input	1,635	1,586	1,557	1,519	1,494
sCO <sub>2</sub> Turbine Power	721	1,006	933	980	913
CO <sub>2</sub> Main Compressor		160	154	148	142
CO <sub>2</sub> Bypass Compressor		124	60	117	58
Net sCO <sub>2</sub> Cycle Power	721	711	708	704	702
Air Separation Unit	85	83	81	79	78
Carbon Purification Unit	60	56	55	54	53
Total Auxiliaries, MWe	171	161	158	154	152
Net Power, MWe	550	550	550	550	550



# Summary of COE

Steam Rankine vs. sCO<sub>2</sub> Cases

- Note that there is significant uncertainty in the CFB and sCO<sub>2</sub> component capital costs (-15% to +50%)
- Large capital cost uncertainties being addressed in projects funded by NETL, EPRI and OEM(s):
  - sCO<sub>2</sub> turbine (GE, Doosan, Siemens)
  - Recuperators (Thar Energy, Brayton Energy, Altex)
  - Primary heat exchanger (B&W, GE)
- sCO<sub>2</sub> cases have comparable COE to steam Rankine plant at 620 °C, and lower COE for 760 °C cases
- Main compressor intercooling improves COE 2.2 3.5 \$/MWh
  - Low cost means of reducing  $sCO_2$  cycle mass flow
- Reheat reduces the COE for the 620 °C cases, but increases COE for turbine inlet temperatures of 760 °C
  - Due to the high cost of materials for the reheat portions of the cycle in 760 °C cases







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# Comparison of sCO<sub>2</sub> versus Rankine Cases

COE vs. Process Efficiency Analysis, with CCS

- Reference: Supercritical Oxycombustion CFB with Autorefrigerated CPU (Case B22F)
  - \$0/tonne CO<sub>2</sub> Revenue
  - 550 MWe
- COE reductions are relative to an air fired, supercritical PC coal plant with CCS (B12B)
- Higher efficiency and lower COE for sCO<sub>2</sub> cycles relative to steam
  - Large uncertainty in commercial scale sCO<sub>2</sub> component costs
- Further improvements to the sCO<sub>2</sub> cycle are currently under investigation





# Analysis of Integrated Gasification Direct-Fired sCO<sub>2</sub> Power Cycle



- <u>NETL Study Objective</u>: Develop a performance and cost baseline for a syngas-fired direct sCO<sub>2</sub> cycle
- Gasification-direct sCO<sub>2</sub> plant design:
  - Low pressure cryogenic Air Separation Unit (ASU) with 99.5% oxygen purity [3]
  - Down-selected to commercial Shell gasifier with standard AGR technology
    - Dry-fed gasifier with high cold gas efficiency
  - CO<sub>2</sub> purification unit (CPU) used to meet CO<sub>2</sub> pipeline purity specifications
  - sCO<sub>2</sub> turbine cooling flows included [4]
  - Condensing sCO<sub>2</sub> cycle operation (CIT = 27 °C)
  - Thermal integration between sCO<sub>2</sub> cycle, gasifier, and Balance of Plant (BOP)
    - Preheats syngas and sCO<sub>2</sub> prior to combustion
    - Includes process steam plant for BOP thermal duties



Source: NETL



# sCO<sub>2</sub> and IGCC Economic Comparison



- sCO<sub>2</sub> Total Plant Costs are similar relative to reference IGCC plant:
  - Higher syngas cooler and ASU costs
  - Lower gas cleanup and CO<sub>2</sub> storage compression costs
  - Comparable Power cycle + HRSG + Steam Plant costs
- Case 2 TPC is 5% lower than the Baseline sCO<sub>2</sub> Case
  - Syngas cooler cost reduced by eliminating HT sCO<sub>2</sub> preheating
  - sCO<sub>2</sub> cycle cost increases with CO<sub>2</sub> flow rate, recuperator duty, and increased power output
- sCO<sub>2</sub> plants have lower COE than IGCC plant
  - TPC better on a \$/MW basis
  - sCO<sub>2</sub> Baseline COE is 10% lower than IGCC plant, Case 2 is 20% lower
  - Case 2 has 11% lower COE compared to Baseline sCO<sub>2</sub> plant, due to lower TPC and increased efficiency

Parameter	IGCC [5]	sCO <sub>2</sub> Baseline	sCO <sub>2</sub> Case 2		
Capital Costs (TPC, \$1,000)					
Coal Handling System	43,156	41,775	41,775		
Coal Prep and Feed	218,724	199,571	199,571		
Feedwater & Miscellaneous BOP	65,849	21,252	21,363		
Gasifier and Accessories	429,678	667,292	540,793		
Cryogenic ASU	251,490	346,824	348,623		
Gas Cleanup & Piping	323,580	160,519	160,528		
CO <sub>2</sub> Compression & Storage	81,688	60,601	61,460		
sCO <sub>2</sub> Cycle/Comb. Turbine & Acc.	160,049	261,793	290,387		
HRSG Ductwork & Stack	56,527	0	0		
Steam Plant	85,322	34,428	29,214		
Cooling Water System	39,217	39,523	39,332		
Balance of Plant	222,322	226,634	230,227		
Total Plant Cost (TPC)	1,977,603	2,060,211	1,963,273		
Operating & Maintenance Costs (\$1,000/yr)					
Fixed O&M	71,389	76,877	73,508		
Variable O&M	45,146	45,479	43,573		
Fuel	111,740	104,867	104,867		
COE (w/o T&S) (2011\$/MWh)	152.6	137.3	122.7		



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## **Comparison with Other Gasification Studies**

Plant Design and Performance Comparison

- Thermal integration in Case 2 improves thermal efficiency by 2.9 percentage points relative to Baseline sCO<sub>2</sub> case
- Both cases compare favorably to the EPRI sCO<sub>2</sub> study, which does not include turbine blade cooling or combustor pressure drops [3]
- sCO<sub>2</sub> cases deliver higher efficiency than IGCC cases with a gas turbine + steam combined cycle power island
  - Change to GE gasifier may improve efficiency [5]
  - Optimized sCO<sub>2</sub> outperforms advanced (AHT) and transformational hydrogen turbine (THT) cases from the IGCC Pathway Study [8]
    - Turbine only comparison, with GE gasifier





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## **Comparison with Other Gasification Studies**

Economic Analysis Results - COE

- The COE for the sCO<sub>2</sub> plant is 11-20% lower than the COE for the reference IGCC plant
- Decrease in COE is primarily due to the higher efficiency of the sCO<sub>2</sub> plant
- Comparable COE to EPRI study, though this uses lower cost PRB coal [3]
- IGCC AHT and THT cases based on a GE gasifier with a radiant syngas cooler [8]
  - TPC 15% lower than Shell gasifier [5]
  - COE \$17.2/MWh lower (-11.3%)





# Core projects of the AT program

Component development for combustion turbines and SCO2 turbomachinery

- Phase II 2016 awards 6 projects supporting 3100 F TIT and SCO2 turbomachinery
  - GE Low-Leakage Shaft End Seals for Utility-Scale sCO<sub>2</sub> Turbo Expanders
  - SwRI High Inlet Temperature Comb. for Direct Fired Supercritical Oxy-Combustion
  - Aerojet Rocketdyne RDC for GT and System Synthesis to Exceed 65% Eff.
  - GE High Temperature Ceramic Matrix Composite (CMC) Nozzles for 65% Efficiency
  - Siemens Ceramic Matrix Composite Advanced Transition for 65% Combined Cycle
  - GE Advanced Multi-Tube Mixer Combustion for 65% Efficiency



## UTSR Project Portfolio Existing / Active Projects

Microstructure Sensitive Crystal Viscoplasticity for Ni-Base Superalloys	Georgia Tech
Evaluation of Flow and Heat Transfer Inside Lean Pre-Mixed Combustor Systems Under Reacting Flow Conditions	Virginia Tech
High-Pressure Turbulent Flame Speeds and Chemical Kinetics of Syngas Blends with and without Impurities	Texas A&M
New Mechanistic Models of Creep-Fatigue Interactions for Gas Turbine Components	Purdue University
Effects of Exhaust Gas Recirculation (EGR) on Turbulent Combustion and Emissions in Advanced Gas Turbine Combustors with High-Hydrogen-Content (HHC) Fuels	Purdue University
Thermally Effective and Efficient Cooling Technologies for Advanced Gas Turbines	U. North Dakota
Abradable Sealing Materials for Emerging IGCC-Based Turbine System	U. California, Irvine
An Experimental and Modeling Study of NOX-CO Formation in High Hydrogen Content Fuels Combustion in Gas Turbine Applications	U. South Carolina
Predictive Large Eddy Simulation Modeling and Validation of Turbulent Flames and Flashback in Hydrogen Enriched Gas Turbines	U. Texas at Austin
Investigation of Autoignition and Combustion Stability of High Pressure Supercritical Carbon Dioxide Oxycombustion	Georgia Tech
Chemical Kinetic Modeling Development and Validation Experiments for Direct Fired Supercritical Carbon Dioxide Combustor	U. Central Florida
A Joint Experimental/Computational Study of Non-Idealities in Practical Rotating Detonation Engines	U. Michigan
Revolutionizing Turbine Cooling with Micro-Architectures Enabled by Direct Metal Laser Sintering	Ohio State
Advancing Pressure Gain Combustion in Terrestrial Turbine Systems	Purdue University
High Temperature, Low NOX Combustor Concept Development	Georgia Tech
Understanding Transient Combustion Phenomena in Low-NOx Gas Turbines	Penn State
Effect of Mixture Concentration Inhomogeneity on Detonation Properties in Pressure Gain Combustion	Penn State
Design, Fabrication and Performance Characterization of Near-Surface Embedded Cooling Channels (NSECC) with an Oxide Dispersion Strengthened (ODS) Coating Layer	U. Pittsburgh



exhaust

C9H20 Mass Fraction

well-mixed

poorly-mixed \*









# **UTSR Project Portfolio**

New 2017 UTSR Awards



Discrete Element Roughness Modeling For Design Optimization Of Additively And PSU Conventionally Manufactured Internal Turbine Cooling Passages GA Tech High-Frequency Transverse Combustion Instabilities In Low-Nox Gas Turbines Real-Time Health Monitoring For GT Components Using Online Learning And High GA Tech **Dimensional Data** Embry-Improving NOx Entitlement with Axial Staging Riddle Integrated Transpiration and Lattice Cooling Systems Developed by Additive U of Pitt Manufacturing with Oxide-Dispersion-Strengthened Alloys Integrated TBC/EBC for SiC Fiber Reinforced SiC Matrix Composites for Next-Clemson Generation Gas Turbines Development of High Performance Ni-Base Alloys for Gas Turbine Wheels using a OSU **Coprecipitation Approach** Optical Monitoring of Operating GT Blade Coatings Under Extreme Environments UCF Fuel Injection Dynamics and Composition Effects on RDE Performance Michigan



## Steady Thermal Aero Research Turbine (START) Facility

eady Thermal Aero Research Turb



Government, Industry, and Academia Collaboration





- Collaboration between DOE/NETL, Penn State, and Pratt & Whitney
- Working with NASA, DOD, OEMs
- One of the world's leading gas turbine test facilities for aerodynamics and heat transfer









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# NETL RIC Advanced Turbines Research

*Goal* – Develop technology toward achieving the program goal of 3-5% points increase in efficiency. *Approach* – Perform R&D in three important areas: Combustion, Heat Transfer and Advanced Cycles. Perform systems analyses to support research focus and verify performance targets.

**Pressure Gain Combustion\*** Improving efficiency through pressure increase across combustor.



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### Aerothermal and Heat

<u>Transfer</u> Improving efficiency by increasing firing temperature and reducing cooling load. **Supercritical CO<sub>2</sub> Cycles** Improving efficiency through unique properties of supercritical CO<sub>2</sub> as a working fluid.

#### <u>Systems Analysis</u> Support research focus and verify performance targets. Efficiency (% HHV)





### Supercritical Carbon Dioxide 10 MWe Pilot Plant Test Facility



Gas Technology Institute

### Objectives

- Plan, design, build, and operate
   a 10 MWe sCO<sub>2</sub> Pilot Plant Test Facility
- Demonstrate the operability of the sCO<sub>2</sub> power cycle
- Verify performance of components (turbomachinery, recuperators, compressors, etc.)
- Evaluate system and component performance capabilities
  - Steady state, transient, load following, limited endurance operation
- Demonstrate potential for producing a lower COE and thermodynamic efficiency greater than 50%

### GAS TECHNOLOGY INSTITUTE

FE0028979 Partners: SwRI, GE Global Research 10/1/2016 – 9/30/2022				
BUDGET				
DOE	Participant	Total		
\$79,999,226	\$33,279,408	\$113,278,634		



# **Technology Maturation**

Turbine technology market provides a special case for TRL acceleration

- Competitive market place
  - US, International, and secondary markets
- Synergies with DOE and DOD
- US universities fully engaged
- Significant deployment of NGCC
- Significant small business opportunities
- FE invests in basic R&D at the component scale leading to early applied solutions
- OEMs eager to deploy components in the existing fleet leading to TRL acceleration
- New products by OEMs can then incorporate FE sponsored advanced technology at lower risk

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- Status of the current CC goal 65 %
  - Are higher efficiencies on our current path
- Advanced manufacturing to realize GT performance goals
  - Additive, coatings, castings, MRO, ceramics, materials, digital solutions, instrumentation, etc.
- Raising the digital twin
- The existing fleet
- Advanced power systems
- Technology maturation







- Advanced Turbines Program focused on three areas
  - Combined cycle combustion turbine
  - Turbomachinery for SCO2 power cycles
  - Pressure gain combustion
- System to realize these benefits
- Technology / market synergies in manufacturing, across agencies, applications etc. will facilitate program success

