Pulse Detonation Engine for Power Extraction from Oxy-Combustion of Coal-Based Fuels



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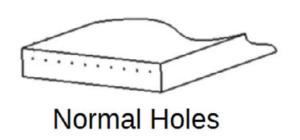
Air Force Research Laboratory: Drs. Fred Schauer and John Hoke at team

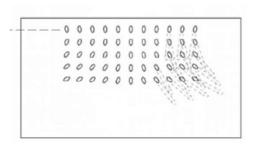
Daiki Ichinokiyama (University of Tsukuba)



Motivation

- Improvements in thermodynamic efficiency of power plants needed
- Pressure gain combustion using detonations can significantly improve efficiency
- Yet ...

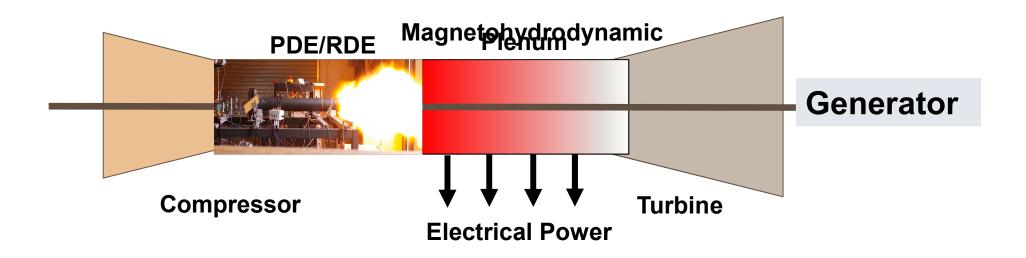




Shaped Array

Richardson, Blunck et al., Combustion and Flame 2016

Motivation



Advantages of detonation-fed MHD: $P \propto \sigma \times V^2 \times B^2$

- High velocities (Ma > 2)
- High temperatures (T > 3000 K) increase electrical conductivity



Prior Research

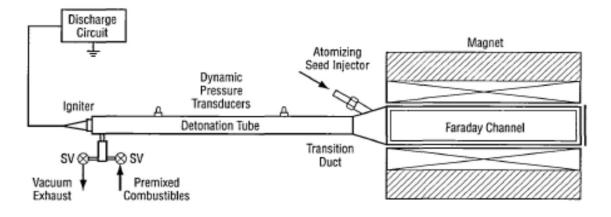


Illustration of detonation and MHD system [Litchford, NASA TP 2001]

Prior research

- Litchford et al. (NASA) & Cambier et al. (Air Force): MHD power extraction possible from propulsive PDE system [3,10,11]
- Matsumoto et al. [12]: hydrogen-air PDE-powered MHD system

Major limitations:

- Primarily propulsive systems; significant insight still needed into interactions between detonation and MHD field
- Coal and CH₄ significantly different than hydrogen

Use of Coal for Detonations

- Coal abundant resource in United States (and has funding)
- Prior (limited) research has considered detonations coupled with MHD, primarily for gaseous fuels
- Most research investigating coal detonations has focused on safety
- Physical and thermal properties of coal detonations need to be measured to understand coupling with MHD



Technical Objectives

Overall Goal

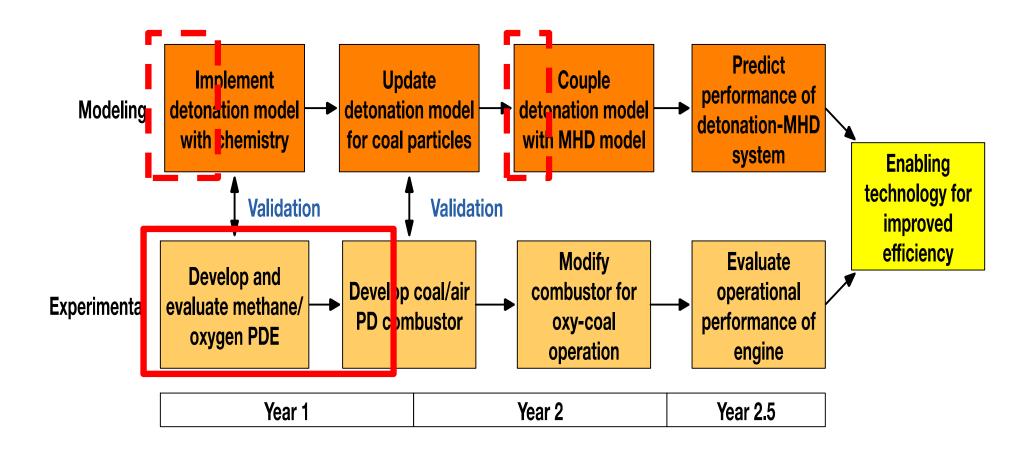
Develop and evaluate a pulse detonation engine system which can be coupled with a MHD system, and analyze MHD and detonation performance.

Specific Objectives:

- 1) Design, build, and operate a pulse detonation engine that operates on gaseous or solid fuels with oxygen as the oxidizer.
- 2) Evaluate the operational envelope and performance of the pulse detonation device with both seeded and unseeded flows.
- 3) Develop and use a numerical design tool to calculate the performance of pulse detonation and coupled detonation-MHD systems.



Overview of Tasks



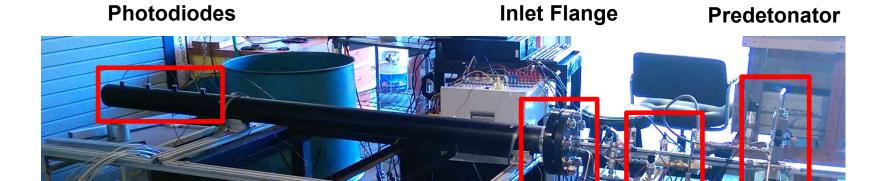


Remainder of Talk

- 1) Development of Pulse Detonation Engine (Task 2)
- 2) Knowledge Gained (Task 2)
- 3) Development of Coal Seeder (Task 3)
- 4) Preliminary Calculations (Task 4)
- 5) Future Work



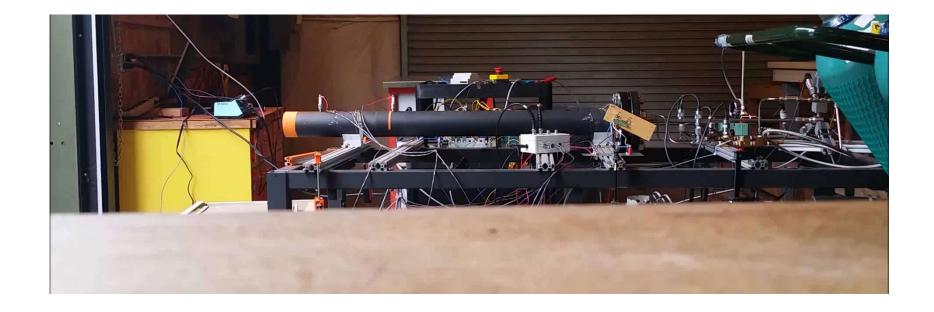
Pulse Detonation System



Valving to Cycle Engine



Operation of the PDE



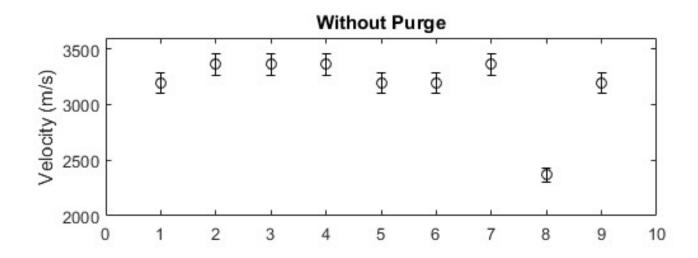


Continuous Firing

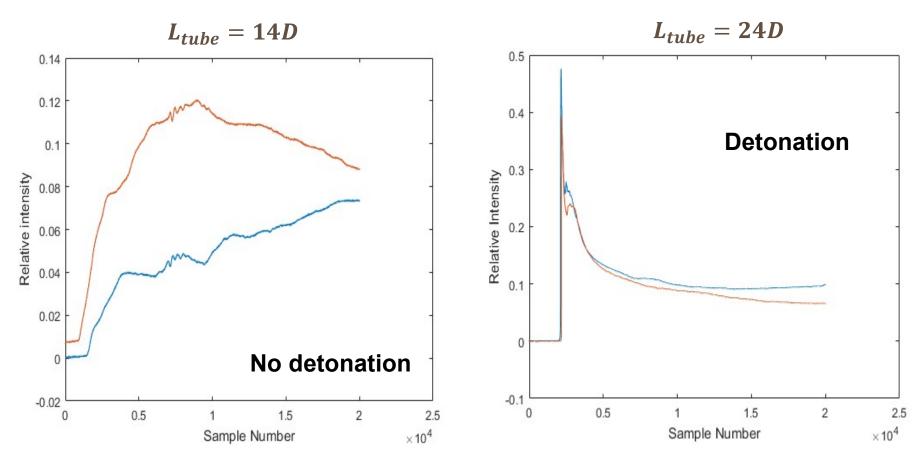




Achieving Consistent Velocities: Purging



Achieving Consistent Velocities: Consistent DDT

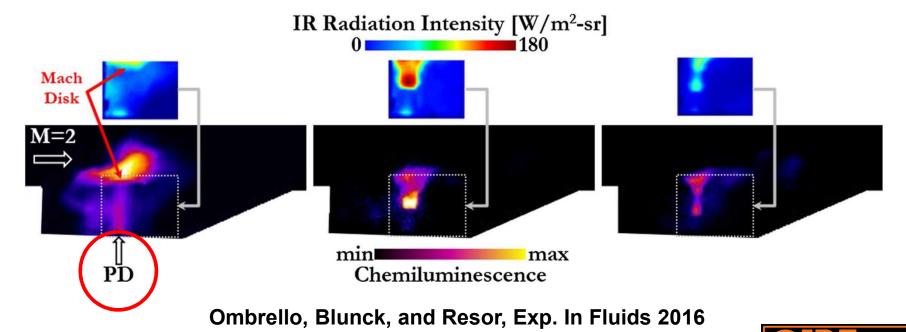


Shchelkin spiral helpful in achieving consistent DDT

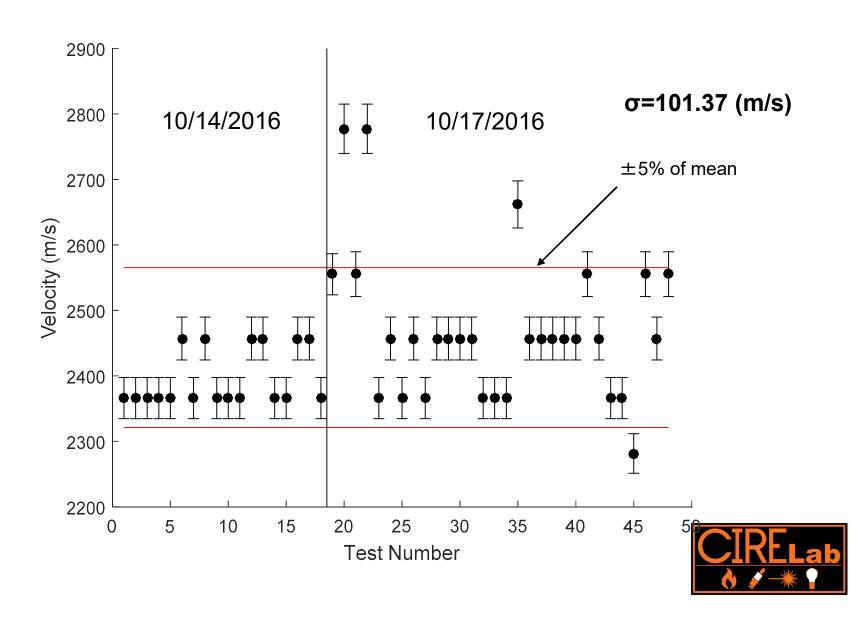


Achieving Consistent Velocities: Temperature Effects

- Little sensitivity of detonation velocities to initial temperatures
- Notable sensitivity of pulse detonator to initial temperature



Achieving Consistent Results

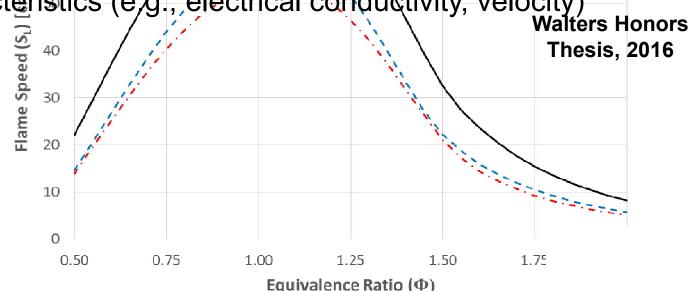


Knowledge to be Gained using Detonation Tube

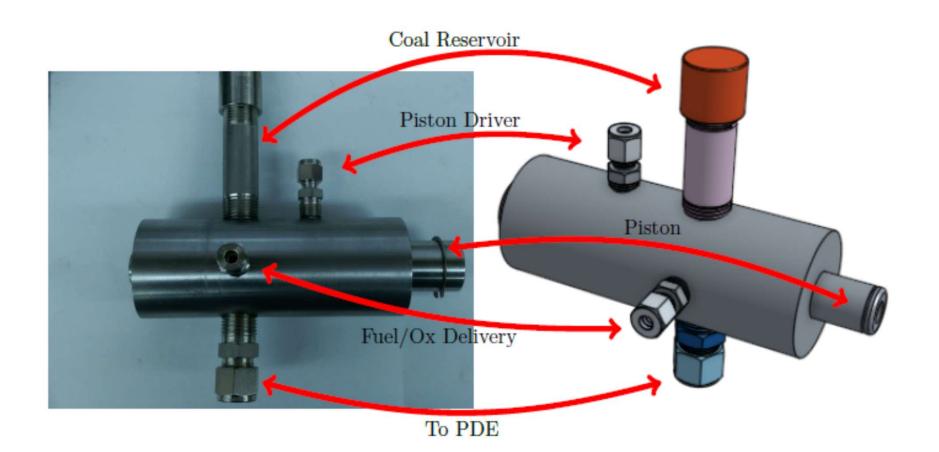
1) Quantify sensitivity of detonation velocities to combustion products

2) Provide boundary conditions for parametric study of MHD-detonation system

3) Identify the influence of coal or gaseous fuels on the detonation characteristics (e.g., electrical conductivity, velocity)



Development of Coal Seeder





Governing Eq. for MHD/Detonation

Mass conservation equation:

$$\frac{\partial}{\partial t} \iint_{S} \rho dS = -\int_{l} \rho \boldsymbol{u} \cdot \boldsymbol{n} dl$$

u: Gas Velocity ρ : Density p: Pressure

B: Magnetic Flux Density **J**: Electric Current Density

Momentum conservation equation: E: Total Energy σ : Electrical Conductivity

$$\frac{\partial}{\partial t} \iint_{S} \rho \mathbf{u} dS = -\int_{l} \{\rho \mathbf{u}(\mathbf{u} \cdot \mathbf{n}) + p\mathbf{n}\} dl + \int_{l} \bar{\bar{\tau}} \cdot \mathbf{n} dl + \iint_{S} \mathbf{J} \times \mathbf{B} dS$$

Total energy conservation equation:

$$\frac{\partial}{\partial t} \iint_{S} \rho E dS = -\int_{l} (\rho E \boldsymbol{u} \cdot \boldsymbol{n} + p \boldsymbol{u} \cdot \boldsymbol{n}) dl + \int_{l} (\bar{\bar{\tau}} \cdot \boldsymbol{u}) \cdot \boldsymbol{n} dl + \iint_{S} \left\{ \frac{\boldsymbol{J}^{2}}{\sigma} + \boldsymbol{u} \cdot (\boldsymbol{J} \times \boldsymbol{B}) \right\} dS$$

Here,

$$E = \sum_{s=1}^{N_{sp}} Y_s (h_{298}^0 + \int_{T'=298 \text{ K}}^T c_p^0 dT') - p/\rho + \frac{1}{2} |\boldsymbol{u}|^2$$

Mass conservation equation of Chemical Species:

$$\frac{\partial}{\partial t} \iint_{S} \rho Y_{S} dS = -\int_{I} \rho Y_{S} \boldsymbol{u} \cdot \boldsymbol{n} dl + \iint_{S} \rho \dot{Y}_{S} dS$$

Charge Neutrality Equation $\frac{Y_e}{m_e} = \sum_{i} \frac{Y_{io}}{m_{ion}}$

h: Specific Enthalpy

Y_s: Mass Concentration

 \dot{Y}_s : Mass Production Rate

 c_p : Specific Heat at

Constant Pressure



Governing Equations in Electrodynamics

Generalized Ohm's Law

$$\mathbf{j} = \sigma(\mathbf{E} + \mathbf{u} \times \mathbf{B}) - \frac{\beta}{|\mathbf{B}|} \mathbf{j} \times \mathbf{B}$$

j: Electric Current Density E: Electric Field u: Gas Velocity B: Magnetic Flux Density

Electrical Conductivity
$$\sigma = \frac{e^2 n_e}{m_e \sum_{i=1}^{N_{Sp}} v_{ei}}$$

$$\beta = \frac{e|\mathbf{B}|}{m_e \sum_{i=1}^{N_{Sp}} \nu_{ei}}$$

Collision Frequency of $v_{ei} = n_i Q_{ei} c_e$ **Electron with Species**

$$v_{ei} = n_i Q_{ei} c_e$$

Steady Maxwell Equations

$$\nabla \times \mathbf{E} = \mathbf{0} \\
\nabla \cdot \mathbf{j} = 0$$

e: Elementary Charge

 n_e : Electron Number Density

 m_e : Electron Mass

 n_i : Species Number Density

 Q_{ei} : Electron Collision

Cross Section with

Species

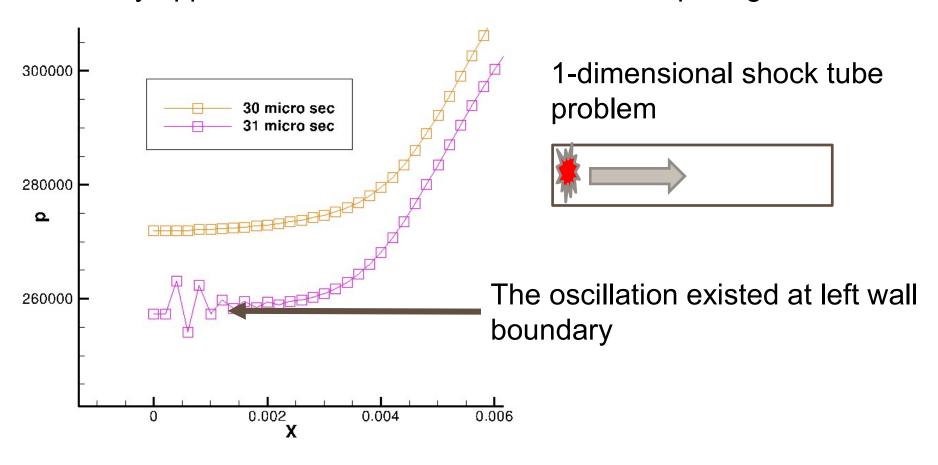
c_e: Electron Mean Thermal

Sped



Solving Compressible Flow Equations

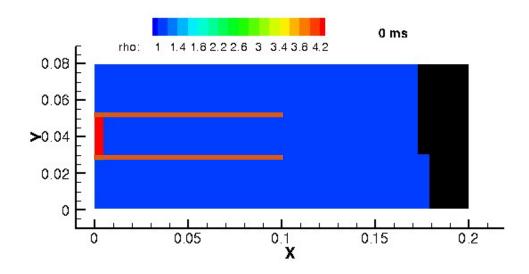
Initially applied 2nd-order Van Leer vector flux splitting scheme



3rd-order WENO-LF scheme then applied



Density Distribution using WENO-LF Scheme





Solving for Electric Field

Generalized Ohm's Law

$$j = \sigma(E + u \times B) - \frac{\beta}{|B|} j \times B$$

$$j = f(E)$$

$$E = -\nabla \phi$$

$$j = f(\phi)$$

Steady Maxwell Equations

$$\nabla \times \mathbf{E} = \mathbf{0} \longrightarrow \mathbf{E} = -\nabla \Phi$$

$$\nabla \cdot \boldsymbol{j} = 0$$

Known: σ , \boldsymbol{u} , \boldsymbol{B} , β

Unknown: ϕ

 2^{nd} -order partial differential equation for ϕ



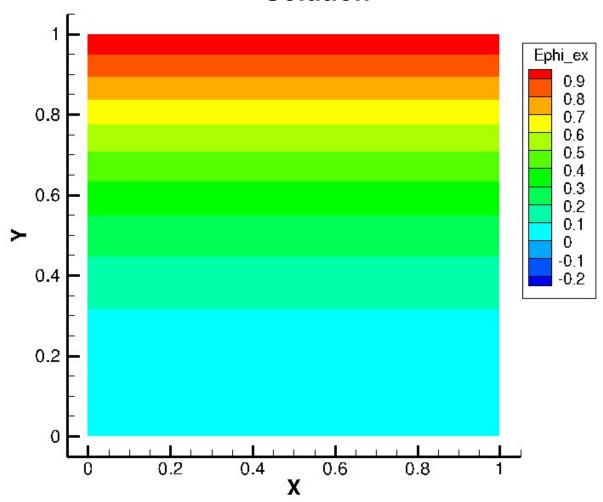
Simultaneous Linear Equations

Solved by GMRES Method



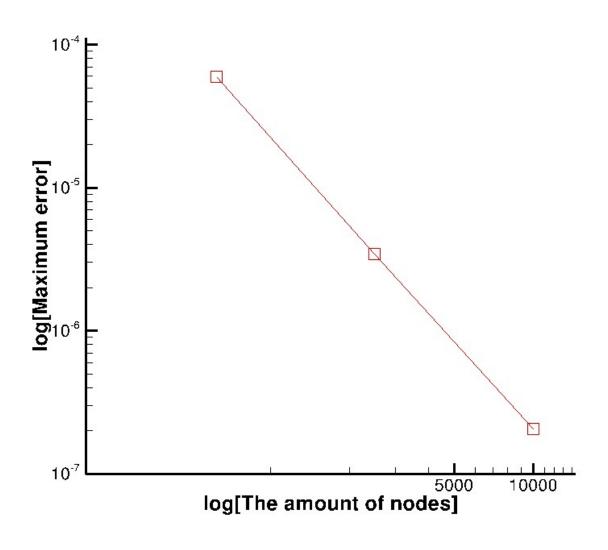
Test Case for Electric Field

Distribution of Electric Potential using Manufactured Solution



Test Case for Electric Field

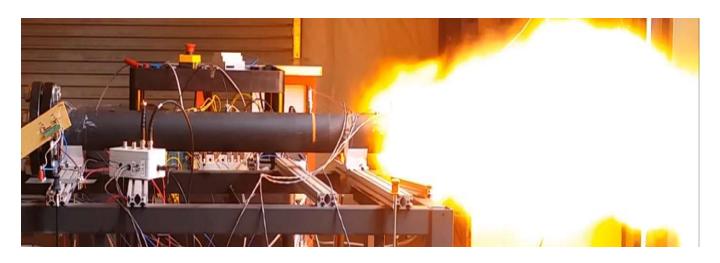
Error in Solution for different nodes





Summary

- 1) Pulse detonation engine has been developed
- 2) Significant evaluation to improve repeatability
- 3) Prototype seeder developed
- MHD solver developed for non-reacting compressible flows



Future Work

Experimental

- 1) Transition PDE to operate using oxy-coal
- Measure boundary conditions and velocities for calculations
- 3) Quantify changes in detonation characteristics between solid and gaseous fuels

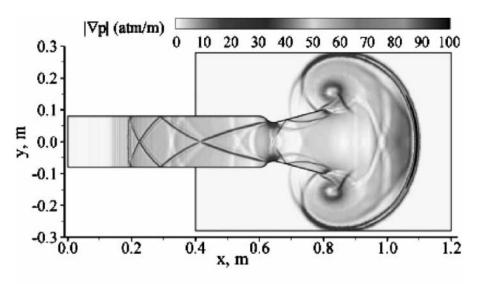
Computational

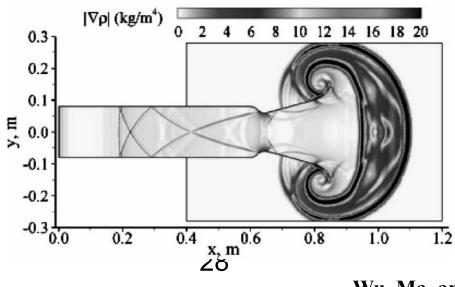
- 1) Couple MHD solver with detonation code
- 2) Develop detonation code
- 3) Parametric study of MHD performance for detonations (long-term)

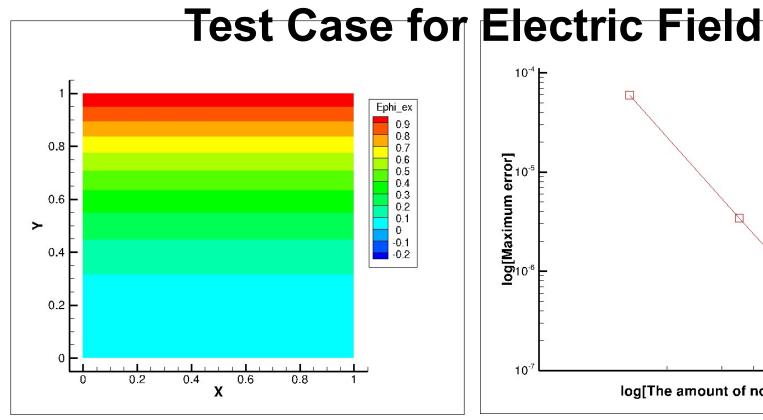




CE/SE Method: 2D Detonation Example







log[Maximum error] 10000 log[The amount of nodes]

Distribution of electric potential

Maximum error for an amount of nodes

Condition

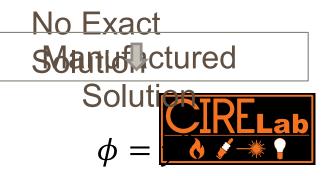
$$\delta = 1 \text{ S/m}$$

 $\beta = 2$

$$|B| = 3 \text{ T}$$

$$u_x = -\cos 2\pi x \sin 2\pi y$$

$$u_y = \cos 2\pi y \sin 2\pi x$$



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