Development of Low-Cost, Highly-Sinterable (Ni,Fe)<sub>3</sub>O<sub>4</sub>-Based Materials for SOFC Cathode-Side Contact Application

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# Outline

- Introduction and Project Objectives
- Major Progress/Conclusions
- Effect of Starting Powders on the Spinel Layer Formation
- Performance Evaluation of the Spinel Contact Layer
  Area Specific Resistance (ASR), Chemical Compatibility, etc.
- Ongoing Research Efforts
- Concluding Remarks
- Acknowledgments

# **Contact Layers in SOFC Stack**

- To minimize the ohmic resistance at the interconnectelectrode interfaces.
- To improve mechanical bonding
- To provide for additional gas channels to the electrodes



Schematic of a Planar SOFC Stack

Schematic of the Cathode-Interconnect Interface

Finding a suitable material for electrical contact between the cathode and interconnect is more challenging.

# Why NiFe<sub>2</sub>O<sub>4</sub>-Based Spinel as Contact Material?

80

70

60

50

40

30

20 10

ASR (mΩ·cm<sup>2</sup>)

**Initial Sintering:** 

850°Cx10 h in air

100

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(Zhu et al., Unpublished Results)

200

Comparison in cell ASR with the MnCo<sub>2</sub>O<sub>4</sub> and the LSCF contact layers at 800°C

300

**Cumulative Exposure Time (h)** 

LSCF - Cracking

400

500

MnCo<sub>2</sub>O<sub>4</sub> (No Cracking)

- Most of cathode contact developments have focused on (<u>La,Sr</u>)(<u>Mn,Co,Fe,Ni</u>)O<sub>3</sub> perovskites; however, it is difficult to balance the electrical conductivity, CTE, and sinterability.
- Several spinels such as  $(Co,Mn)_3O_4$ ,  $CoFe_2O_4$ , NiCo<sub>2</sub>O<sub>4</sub> and NiFe<sub>2</sub>O<sub>4</sub> are also promising candidates as cathode-side contact.



# Why NiFe<sub>2</sub>O<sub>4</sub>-Based Spinel as Contact Material?

- NiFe<sub>2</sub>O<sub>4</sub>-based spinels have reasonable CTE (12x10<sup>-6</sup>/°C) and electrical conductivity.
- With the absence of Co and a low Ni content, this spinel system is a low cost alternative.

Metal	Cost (\$/lb)	
Cobalt	13.5	
Nickel	4.5	
Iron	0.2	

- The sinterability of NiFe<sub>2</sub>O<sub>4</sub> is poor (≥1200°C).
  - How to lower the sintering temperature?



Electrical Conductivity of the (NI,Fe)<sub>3</sub>O<sub>4</sub> Spinel, as Compared with Several Other Oxides.

# Utilization of EARS for Reduced-Temperature Sintering of Co-free (Ni,Fe)<sub>3</sub>O<sub>4</sub> spinel Contact

- Employment of metallic powders instead of oxide powders as the starting precursor to lower the sintering temperature
  - <u>Environmentally-Assisted</u> <u>Reactive Sintering (EARS)</u> with the participation of oxygen from environment in the spinel forming reaction:

Ni + 2Fe + 
$$2O_2(g) = NiFe_2O_4$$
  
VS.  
NiO + 2Fe<sub>2</sub>O<sub>3</sub> = NiFe<sub>2</sub>O<sub>4</sub>



EARS process for synthesis of  $(Ni,Fe)_3O_4$  ("S") using different precursors: (a) a mixture of Fe and Ni powders; (b) a Ni-Fe alloy powder.

- Enhanced sintering via EARS due to the following facts:
  - Heat released during the reaction;
  - Volume expansion upon conversion of metal to metal oxide;
  - Formation of highly active, nanoscale surface oxides

# **Project Objectives**

 Optimization of the (Ni,Fe)<sub>3</sub>O<sub>4</sub> spinel layer formation via controlling the parameters involved in EARS (especially the metallic precursors).

- Critical assessment of the performance of the EARS (Ni,Fe)<sub>3</sub>O<sub>4</sub> layer
- Exploration of further performance improvement of the spinel-based contacts



Flow Chart of the Research Tasks Involved in this Project

#### **Major Progress/Conclusions**

- Both a mixture of Ni and Fe powders and an Ni-Fe alloy powder can be used as the precursor to form a spinel contact layer.
- The alloy powder is preferred, due to more uniform spinel conversion, better microstructure and lower ASR.
- Approaches to further improve the performance of the spinel contact are being pursued.



Crofer NiFe<sub>2</sub>O<sub>4</sub> Contact Layer LSM

Cross-Sectional View of a Crofer//NiFe<sub>2</sub>O<sub>4</sub>//LSM Cell with a Ni-Fe Alloy Precursor Layer after ASR Testing in Air at 800°C for 1000 h



# With mixed Ni and Fe powders, the converted layer had a significant amount of Fe<sub>2</sub>O<sub>3</sub> near the surface



- With the starting powder mixture of 2  $\mu$ m Ni and 3  $\mu$ m Fe, the metallic layer was fully converted after 900°Cx2h in air;

- A surface  $Fe_2O_3$  layer and some areas of internal NiO and  $Fe_2O_3$  were observed, indicating a non-uniform microstructure.



Cross-section of an Fe microparticle after oxidation at 700°C for 30 min



Surface morphology of an Fe microparticle after oxidation

> Qin et al., J. Mater. Chem. A, 2 (2014)

# With a large-sized Ni-Fe alloy powder, a fully-converted contact layer could not be achieved after 900°C exposure



Cross-section and area mapping of an Ni-Fe microparticle after oxidation at 700°C for 30 min

- The Ni-Fe powder was sieved through a 625-mesh screen, and the collected powder was  $\leq$  20  $\mu$ m in size.

Qin et al., J. Mater. Chem. A, 2 (2014)

 After 900°C x 2 h conversion, the metallic particles were not fully oxidized, and a graded composition/structure was obtained.

#### Further Reduction of the Ni-Fe Powder Size via Sonication + Skimming



Morphological Features of the Skimmed Particles



– The size of the skimmed particles was reduced to < 7  $\mu$ m.

 The converted spinel layer with the skimmed powder was relatively uniform microstructurally and compositionally.

#### Effect of Sintering Temperature on the Phase Formation in the Contact Layer



800°C x 2h

850°C x 2 h

900°C x 2h

950°C x 2 h

- For the skimmed alloy powder, regardless of the conversion temperature used the Ni-Fe alloy layer was fully converted to an oxide layer.
- As the sintering temperature increased, the microstructure became more uniform and a higher amount of the spinel was detected in the contact layer.

#### XRD Results of the Phases Present in the Contact Layer Thermally Converted at Different Temperatures



- As the conversion temperature increased, the amount of  $NiFe_2O_4$ increased while the amounts of  $Fe_2O_3$  and NiO dropped significantly.

For a new alloy powder with a modified composition, a single-phase spinel layer was achieved after 900°Cx2h conversion.

## Area-Specific Resistance (ASR) Measurement

- A number of test cells were constructed, and significant improvement of the contact layer uniformity with regard to its thickness and microstructure has been made.
- The test cells are spring-loaded and the ASR change during either isothermal or cyclic exposure at 800°C in air is monitored using a special 6-cell test rig.



Schematic of the ASR test cell and test configuration

## ASR Change as a Function of Time for Test Cells with Different Contact Pastes

- The ASR for the test cell with NiO and Fe<sub>2</sub>O<sub>3</sub> precursors were the highest, due to poor contact layer sintering.
- Low and stable ASR was observed for the cells with metallic precursors in the contact layer.
- The lowest ASR was observed in the cell with the alloy precursor.



Comparison cell ASR with in several contact layers with either oxide or metal 800°C in air during precursors at (initial isothermal exposure sintering: 900°Cx2 h in air)

The cell ASR was either stable or dropping for the cells with the metallic precursors, indicative of their exceptional performance.

### Cross-Sectional View of Tested Cells with the Ni-Fe Alloy Contact Paste



- On the Crofer 22 APU side, a thin Cr<sub>2</sub>O<sub>3</sub> scale was formed after 1000-h testing and both Cr and Mn were detected in the contact layer near the interface.
- On the cathode side, negligible interdiffusion between the contact layer and LSM was observed. No Cr was detected in LSM.

## Cross-Sections of Tested Cells with the Contact Paste of a Mixture of Ni+Fe Powders



 The Ni+Fe contact layer was less uniform compositionally and structurally compared to the Ni-Fe alloy contact.

• Mn and Cr diffusion into the contact layer was observed. 17

# Cross-Sections of Tested Cells with the Contact Paste of a Mixture of NiO+Fe<sub>2</sub>O<sub>3</sub> Powders

 The NiO+Fe<sub>2</sub>O<sub>3</sub> contact layer cracked and detached from the cathode after cooling down to room temperature, due to the poor sintering of the contact layer, consistent with its higher ASR.

 More significant diffusion of Mn and Cr into the contact layer.





#### Further Improvement of NiFe<sub>2</sub>O<sub>4</sub>-Based Spinel Contact: Effect of Stoichiometry and Doping

- CTE of (Ni,Fe)<sub>3</sub>O<sub>4</sub> with different Ni/Fe ratios was measured, which ranged from 11.6 to 12.1 x 10<sup>-6</sup> /°C.
- As the Fe content in the spinel increases, the electrical conductivity increases accordingly.
- Doping with transition metal cations such as Mn, Co, Cu, etc. might further improve the performance of this spinel.





Formation of a Doped Spinel Layer via Mixing a Metal Elemental Powder (5wt.%) with the Ni-Fe Alloy Powder after 900°Cx2h Conversion

#### Further Improvement of NiFe<sub>2</sub>O<sub>4</sub>-Based Spinel Contact: Formation of a Composite Contact by Second-Phase Addition

- The second phase should be highly electrically conductive, CTE-matched, and chemically compatible with the cathode, interconnect, and the NiFe<sub>2</sub>O<sub>4</sub> spinel, and preferably Crabsorbing.
- Potential candidates includes LSM, LSCF, LNF, LCN, LSCM, etc.
- Initial study
  indicates minimal
  interdiffusion
  between LSM and
  NiFe<sub>2</sub>O<sub>4</sub>.



XRD Patterns of a 50wt% LSM + 50 wt.% NiFe<sub>2</sub>O<sub>4</sub> Composite After Firing at 1200°C in Air 20

# **Concluding Remarks**

- Low-cost, EARS-processed (Ni,Fe)<sub>3</sub>O<sub>4</sub>-based layers with promising performance have been successfully synthesized.
- While both a mixture of Ni & Fe powders and an Ni-Fe alloy powder can be used as the precursor for the spinel-layer synthesis, the alloy powder approach is preferred:
  - Better spinel phase purity
  - Lower ASR
  - Cost advantages
    - Only one powder is needed (lower powder process cost)
    - No need of powder mixing
    - Doped spinel formation via alloy composition adjustment (multi-component alloys)



(J.H. Zhu et al., "Reduced-temperature sintering of coatings and layers with metallic alloy powder precursors", US Patent Application #62/349,997, 2016.)

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