

Alstom's Limestone-based Chemical Looping Development For Advanced Gasification DOE/NETL Agreement DE-FE0023497

Armand Levasseur ALSTOM Power Inc.

DOE Workshop: Gasification Systems and Coal & Biomass to Liquids

Morgantown, WV August 10, 2015



Alstom Limestone Chemical Looping Process Key Attributes



- Avoids large investment costs and parasitic power associated with cryogenic air separation units (ASU's),
- Flexibility for coal-based power generation with CO₂ capture from coal via combustion/steam generation or hydrogen production/ GTCC as well as syngas for chemical feedstock,
- Uses abundant, low cost limestone to provide oxygen carrier,
- Builds upon Alstom's proven CFB technology and uses conventional materials and fabrication techniques,
- Techno-economic assessments consistently show Chemical Looping-based power generation systems have the potential for the lowest costs of electricity with $\rm CO_2$ capture.

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Limestone Chemical Looping Process: **Options and Applications**



Option 1 – Combustion with CO2 Capture – LCL-C[™]







Option 3 – Hydrogen with CO2 Capture – LCL-H2™

Main

Combustion

- CO₂ Capture PC/CFB Retrofit
- CO₂ Capture-Ready Power Plant
- Advanced Steam Cycles with CO₂ Capture

Syngas

- IGCC with or without Down-Stream CO₂ Capture
- IGCC with Water-Gas Shift for H2 (CO₂ Capture)
- Industrial Syngas production
- Coal-to-Liquid Fuels

Hydrogen

- Fuel Cell Cycles with CO₂ Capture
- Hydrogen for IGCC with CO₂
- Industrial Hydrogen with CO₂



Reducer (Fuel Reactor) $C_{fuel} + CO_2 + Heat \rightarrow 2CO$ $2CO + CaSO_{4} \rightarrow CaS + 2CO_{2}$

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Alstom LCL-G[™] System Concept Near-Term Syngas



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Techno-Economic Study: LCL-Gasification

Study Cases:

Two cases compared against DOE's Baseline Cases:

- LCL-G[™] based power plant with >90% carbon capture (IGCC using H₂ product gas)
- LCL-G[™] based coal-to-liquid plant (syngas product H₂/CO >2.0) with Fischer-Tropsch / refinery for making diesel fuel

DOE Baseline Cases:

- GE IGCC with CO₂ capture (Case 2 Vol 1)
- Shell CTL plant for making diesel fuel (Case 4 Vol 4)

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IGCC Base Case (IGCC w CO₂ Capture) DOE Baseline Report Case 2 – Volume 1



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Limestone Chemical Looping Preliminary Economics for Power Generation

IGCC Base PC Base LCL-C™ H2 for Power Time Frame Today Today After DOE 9498 After DOE 9498 After ODE 9498 <td< th=""><th></th><th></th><th></th><th></th><th></th><th>\frown</th><th></th></td<>						$ \frown $	
IGCC Base PC Base LCL-C™ /H2 for Power Time Frame Today Today After DOE 9498 After DOE 9498 After DOE 9498 After 2020 Gasifier/Combustor GE IGCC SCC LCL-C™ LCL-G™ LCL-G™ LCL-G™ DOE DOE DOE DOE DOE Alstom Alstom CO2 Capture Method WGS/Selexol None LCL-C™ WGS/Selexol Power Purpose Steam Cycle Subcritical SC SC Sub Critical SC Combustion Turbine 7 FA - - 7FA 7HA Total SC Carbon Capture (% of Coal) 90 0 97 90 98 98 Performance Fuel Fired (Ib/Ir) 487,011 409,528 449,595 450,000 450,000 Fuel Fired, HHV (MMBtu/hr) 5,681 4,778 5,245 5,250 5,250 Reducer,Gasifier,Boiler Stoichiometry 39 120 43					POWER CA	SES	
Time Frame Today Today After DOE 9498 After DOE 23497 After 2020 Gasifier/Combustor GE IGCC SCPC LCL-C™ LCL-G™ None LCL-G™ MGS/Selexol LCL-G™ Power Power Power Power Power Power Selexol Selexol Selexol Selexol Selexol Selexol Selexol Selexol Selexol			IGCC Base	PC Base	LCL-C™	H2 for Pov	wer
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CO2 Capture Method WGS/Selexol None LCL-C™ WGS/Selexol Power Purpose Power Power <t< th=""><th></th><th></th><th>DOE</th><th>DOE</th><th>Alstom</th><th>Alstom</th><th>Alstom</th></t<>			DOE	DOE	Alstom	Alstom	Alstom
Purpose Power Subcritical SC Steam Cycle Subcritical SC SC Sub Critical SC Sub Critical SC Combustion Turbine 7 FA - - 7FA 7HA Reducer/Boiler/Gasifier Press (ata) 55 1 1 1 7 Carbon Capture (% of Coal) 90 97 90 98 Performance Fuel Fired (lb/hr) 487,011 409,528 449,595 450,000 450,000 Fuel Fired, HHV (MMBtu/hr) 5,681 4,778 5,245 5,250 5,250 Reducer,Gasifier,Boiler Stoichiometry 39 120 120 43 58 SynGas Energy, HHV (% of Input) 68 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 8		CO2 Capture Method	WGS/Selexol	None	LCL-C™	WGS/Selexol	LCL-G™
Steam Cycle Subcritical SC SC Sub Critical SC Combustion Turbine 7 FA - - 7FA 7HA Reducer/Boiler/Gasifier Press (ata) 55 1 1 1 7 Carbon Capture (% of Coal) 90 0 97 90 98 Performance Fuel Fired (lb/hr) 487,011 409,528 449,595 450,000 450,000 Fuel Fired, HHV (MMBtu/hr) 5,681 4,778 5,245 5,250 5,250 Reducer, Gasifier, Boiler Stoichiometry 39 120 120 43 58 SynGas Energy, HHV (% of Input) 15 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost Capacity Factor 80 85 85 80 85		Purpose	Power	Power	Power	Power	Power
Combustion Turbine 7 FA - - 7FA 7HA Reducer/Boiler/Gasifier Press (ata) 55 1 1 1 7 Carbon Capture (% of Coal) 90 0 97 90 98 Performance Fuel Fired (lb/hr) 487,011 409,528 449,595 450,000 450,000 Fuel Fired, HHV (MMBtu/hr) 5,681 4,778 5,245 5,250 5,250 Reducer,Gasifier,Boiler Stoichiometry 39 120 120 43 58 SynGas Energy, HHV (% of Input) 68 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost Coapacity Factor 80 85 85 80 85		Steam Cycle	Subcritical	SC	SC	Sub Critical	SC
Reducer/Boiler/Gasifier Press (ata) 55 1 1 1 1 7 Carbon Capture (% of Coal) 90 0 97 90 98 Performance Fuel Fired (lb/hr) 487,011 409,528 449,595 450,000 450,000 Fuel Fired, HHV (MMBtu/hr) 5,681 4,778 5,245 5,250 5,250 Reducer, Gasifier, Boiler Stoichiometry 39 120 120 43 58 SynGas Energy, HHV (% of Input) 68 - - 75 50 Power Steam Energy, HHV (% of Input) 15 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.6		Combustion Turbine	7 FA	-	-	7FA	7HA
Carbon Capture (% of Coal) 90 0 97 90 98 Performance Fuel Fired (lb/hr) 487,011 409,528 449,595 450,000 450,000 Fuel Fired, HHV (MMBtu/hr) 5,681 4,778 5,245 5,250 5,250 Reducer, Gasifier, Boiler Stoichiometry 39 120 120 43 58 SynGas Energy, HHV (% of Input) 68 - - 75 50 Power Steam Energy, HHV (% of Input) 15 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Capacity Factor 80 85 85 80 85 Capacity Factor 80 85 85 80 0.51 <td< th=""><th>Reducer/Boil</th><th>er/Gasifier Press (ata)</th><th>55</th><th>1</th><th>1</th><th>1</th><th>7</th></td<>	Reducer/Boil	er/Gasifier Press (ata)	55	1	1	1	7
Performance Fuel Fired (lb/hr) 487,011 409,528 449,595 450,000 450,000 Fuel Fired, HHV (MMBtu/hr) 5,681 4,778 5,245 5,250 5,250 Reducer,Gasifier,Boiler Stoichiometry 39 120 120 43 58 SynGas Energy, HHV (% of Input) 68 - - 75 50 Power Steam Energy, HHV (% of Input) 15 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Capacity Factor 80 85 85 80 85 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 1.76 1.00 1.15 1.05 0.90 0.55 0.63<	Carbon C	apture (% of Coal)	90	0	97	90	98
Fuel Fired, HHV (MMBtu/hr) 5,681 4,778 5,245 5,250 5,250 Reducer,Gasifier,Boiler Stoichiometry 39 120 120 43 58 SynGas Energy, HHV (% of Input) 68 - - 75 50 Power Steam Energy, HHV (% of Input) 15 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Capacity Factor 80 85 85 80 85 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 1.76 1.00 1.15 1.05 0.90 0.55 0.63 0.55	Performance Fuel Fir	ed (lb/hr)	487,011	409,528	449,595	450,000	450,000
Reducer,Gasifier,Boiler Stoichiometry 39 120 120 43 58 SynGas Energy, HHV (% of Input) 68 - - 75 50 Power Steam Energy, HHV (% of Input) 15 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 1.76 1.00 1.15 1.05 0.90 0.55 0.63 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 0.63 1.15 1.00 0.91 0.70 0.63	Fuel Fired, H	IV (MMBtu/hr)	5,681	4,778	5,245	5,250	5,250
SynGas Energy, HHV (% of Input) 68 - - 75 50 Power Steam Energy, HHV (% of Input) 15 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 1.76 1.00 1.15 1.05 0.90 0.55 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 1.15 1.00 0.91 0.70 0.63 0.75 0.68 0.75	Reducer, Gasifier, Boil	er Stoichiometry	39	120	120	43	58
Power Steam Energy, HHV (% of Input) 15 - - 20 45 Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 Relative Cost of Elect w/ CO2 T&S 1.00 0.58 0.75 0.68 0.59	SynGas Energy, H	IV (% of Input)	68	-	-	75	50
Gross Power " 734,000 580,400 649,700 765,298 825,040 Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 Relative Cost of Elect w/ CO2 T&S 1.00 0.58 0.75 0.68 0.75	Power Steam Energy, H	IV (% of Input)	15	-	-	20	45
Net Power " 543,250 549,990 550,003 650,420 713,553 Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 Relative Gasification Cost / Coal Flow 1.00 0.877 0.79 0.61 0.55 Relative Cost of Elect w/ CO2 T&S 1.00 0.58 0.75 0.68 0.75	Gross Power	"	734,000	580,400	649,700	765,298	825,040
Net Plant eff., HHV (%) 32.6 39.3 35.8 42.3 46.4 Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Capacity Factor 80 85 85 80 85 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 1.76 1.00 1.15 1.05 0.90 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 1.15 1.00 0.91 0.70 0.63 0.59 0.63	Net Power	u	543,250	549,990	550,003	650,420	713,553
Total Plant Cost 1,783,649 1,097,067 1,246,480 1,283,798 1,277,370 Capacity Factor 80 85 85 80 85 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 1.76 1.00 0.87 0.79 0.61 0.55 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 1.15 1.00 0.91 0.70 0.63 0.59	Net Plant eff., HH	V (%)	32.6	39.3	35.8	42.3	46.4
Capacity Factor 80 85 85 80 85 Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 Image: Capacity Factor 1.76 1.00 1.15 1.05 0.90 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 Image: Cost of Elect w/ CO2 T&S 1.00 0.58 0.75 0.68 0.59	Total Plant Co	st	1,783,649	1,097,067	1,246,480	1,283,798	1,277,370
Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 1.76 1.00 1.15 1.05 0.90 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 1.15 1.00 0.91 0.70 0.63		Capacity Factor	80	85	85	80	85
Relative Capital Cost / Coal Flow 1.00 0.57 0.65 0.60 0.51 1.76 1.00 1.15 1.05 0.90 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 1.15 1.00 0.91 0.70 0.63							
1.76 1.00 1.15 1.05 0.90 Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 1.15 1.00 0.91 0.70 0.63 Relative Cost of Elect w/ CO2 T&S 1.00 0.58 0.75 0.68 0.59	Relative Ca	pital Cost / Coal Flow	1.00	0.57	0.65	0.60	0.51
Relative Gasification Cost / Coal Flow 1.00 0.87 0.79 0.61 0.55 1.15 1.00 0.91 0.70 0.63			1.76	1.00	1.15	1.05	0.90
1.15 1.00 0.91 0.70 0.63 Relative Cost of Elect w/ CO2 T&S 1.00 0.58 0.75 0.68 0.59	Relative Gasific	tion Cost / Coal Flow	1.00	0.87	0.79	0.61	0.55
			1.15	1.00	0.91	0.70	0.63
	Relative Cost of	Elect w/ CO2 T&S	1.00	0.58	0.75	0.68	0.59
1.71 1.00 1.29 1.17 1.00			1.71	1.00	1.29	1.17	1.00

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Limestone Chemical Looping Preliminary Economics for Coal-to-Liquids

	1											
		DIESEL CASES										
		Petro Diesel	DOE-base	SynC	Bas for CTL D	iesel)						
	Time Frame		Today	After DOE 23497	Ater DOE 23497	After 2020						
	Gasifier/Combustor		Shell Gasifier	LCL-G™	LCL-G™	LCL-G™						
		DOE	DOE	Alstom	Alstom	Alstom						
	CO2 Capture Method	-	WGS/Selexol	WGS/Selexol	WGS/Selexol	LCL-G™						
	Purpose	Petroleum	SynGas	SynGas	SynGas	SynGas						
	Steam Cycle	-	Sub Critical	Sub Critical	Sub Critical	SC						
	Combustion Turbine	-	7FA	7FA	7FA	7HA						
Reducer/Boile	/Gasifier Press (ata)	-	1	1	1	7						
Carbon Ca	oture (% of Coal)	0	90	60	90	90						
Carbon Capture	(% of Total Carbon)	-	60	60	60	60						
H2/CO to Fisc	her-Tropsch (molar)	-	2	2	2	3						
Biom	nass (% of Fuel HHV)	-	30	0	30	30						
Performance Fuel Fired	l (lb/hr)	59928 (bpd)	487,011	450,000	450,000	450,000						
Fuel Fired, HHV	(MMBtu/hr)	13,379	5,681	5,250	5,250	5,250						
Reducer, Gasifier, Boiler Air/Coa	(molar)	-	39	43	43	40						
SynGas Energy, HHV	(% of Input)	-	68	75	75	70						
Power Steam Energy, HHV	(% of Input)	-	15	20	20	25						
Gross Power	"	34,000	180,363	105,174	105,174	185,438						
Net Power	"	-	-	-	-	124,271						
Net Plant eff., HHV	(%)	85.5	51.6	57.3	57.3	53.5						
CBTL Production	I (MMBtu/hr)		2,932	3,008	3,008	2,810						
CBTL Production	(bbl/day)	53,753	14,211	14,584	14,584	13,624						
Total Plant Cos		1,917,000	1,576,566	1,016,880	1,016,880	928,688						
	Capacity Factor	90	80	80	80	85						
Die	sel production (gal/yr)	706,314,420	165,989,604	170,344,435	170,344,435	169,073,648						
Diese	l production (Bbl/day)	46,074	10,828	11,112	11,112	11,029						
			1.00									
Relative Cap	tal Cost / Coal Flow	-	1.00	0.63	0.63	0.58						
		-	1.00	0.04	0.01	0.50						
Relative Gasificat	on Cost / Coal Flow	-	1.00	0.64	0.64	0.59						
Rolativ	e Cost of Diesel	0.58	1.00	0.56	0.73	<u> </u>						
Kelativ		1.00	4 74	0.07	1.00	4.45						
L		1.00	1./4	0.97	1.20	1.15						

Limestone Chemical Looping Technology **Commercialization Plan**



Limestone Chemical Looping Scale-up to 3-MW_{th}

Alstom 3 MW_{th} LCL Prototype – Major Milestones Completed (LCL-Combustion):

- Engineering (Oct 2008 Apr 2010)
- EPC and Shakedown (Apr 2010 Dec 2010)
- First auto thermal operation achieved in July 2012; **May 2013**
- Identification of 7 Main Technical Gaps
- Oct 2013 Autothermal operation and testing to address gaps
- June 2015 Relocated to New Alstom Lab in Bloomfield, CT
- July 2015 Prototype re-commissioned and resumed testing (Test 2 completed)

Largest chemical looping facility in the world

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Prototype (3 MWt)



Alstom Test Facility Relocation



Windsor Test Facilities Fully Operational







Move to Tobey Road - Bloomfield, CT R&D Test Facilities - Feb 2014

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Chemical Looping Facility –Construction/Relocation Now Ready to Continue Testing



Cut Opening -April 2014



Tower Steel - June 2014





Tower Complete - March 2015



Outside Equipment Complete March 2015

Aerial View of Alstom R&D Test Facilities May 2015

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Limestone Chemical Looping (LCL[™]) Development Advanced Oxy Combustion – Project Objectives and Status

DOE/NETL Cooperative Agreement No. DE-FE0009484 Phase 1 and 2 - October 2012 to Sept. 2016

- Techno-economic studies on 4 LCL-C[™] cases
 Completed June 2013
- Address 7 main technology gaps
 - <u>Seven 3 MW_{th} prototype tests</u> incorporating system modifications Test 1 Completed Oct 2013 Test 2 Completed July 2015
 - Various supporting bench, small pilot, physical flow and CFD modeling studies On-going





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Limestone Chemical Looping (LCL[™]) Development Advanced Gasification – Project Objectives and Scope

DOE/NETL Cooperative Agreement No. DE-FE0023497 – October 2014 to March 2017

Objective:

To further develop LCL-GTM technology for generation of high-H₂ syngas from coal for liquid fuel production and/or power generation with CO_2 capture.

Scope:

- Small-scale developmental testing (including 100mm diameter 50ft LCL-G pilot tests)
- Cold flow model testing
- Computational modeling simulations
- 3.0 MWth prototype testing
- Techno-economic assessments



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Technology Development Areas

	LCL-G [™] Technology Development											
	Development Item/Gap	Success Criteria	Testing									
1	solids/gas transport	stable & controllable	CFM, PSTF, Prototype (w/ Contract 9484)									
2	carbon conversion	> 90% of carbon in coal	Bench, PSTF, Prototype (w/ Contract 9484)									
3	sulfur capture/retention	90% of sulfur retained	Bench, PSTF, Prototype (w/ Contract 9484)									
4	sorbent activation	Minimal/acceptable degradation	Bench, PSTF, Prototype (w/ Contract 9484)									
5	simultaneous WG shift & carbon capture	>90% within 1 second	Bench testing, TEA									
6	calcination	calcine < 1 second	Bench testing, TEA									
7	product gas stability during load change	10% per minute	PSTF, Prototype testing									
8	- Biomass co-firing	10 to 50%, HHV	Bench, PSTF									
9	Integration w/ F-T Liquefaction	acceptable TEA/TGA	Future Development									



Limestone Chemical Looping (LCL[™]) Development DOE Award 9484– Prototype Testing - Addressing Gaps

Modifications & Planned Work



Prototype (3 MWt)

ID	TECHNICAL GAP	AFFECTS
1	High Solids Loss Rate	operability
2	Main DipLeg Flushing	operability
3	Solids stability	operability
4	Sorbent Activation	operability
5	Sulfur Capture / Loss	operability
6	Low temperatures during some tests	operability
7	Carbon Carryover to Oxidizer	performance

(Additional Gap: Reducer Gas Oxygen Demand – To Be Addressed in Future)

Define Gap / check solution:

Prototype Performance Shortfall Analyze Prototype Data Define Bench Test

find solution:

40-Ft CFM for Solids Transport

50-Ft & Bench Test Rig(s) for Chemistry, Conversions, Transport

Three Main Areas To Further Address: Solids Management, Carbon Capture and Sulfur Retention

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Award 9494 - LCL-C[™] Prototype Testing Solids Transport Management

Key Issues:

DipLeg Inventory Control - Affects:

- Solids loss thru cyclone
- Carbon conversion

DipLeg Gas Generation - Affects:

- DipLeg solids inventory control
- Solids recycle rate control and stability.
 - Sulfur retention via solid/gas stoichiometry
 - Recycle rate controls Reducer temperature



Solids Management Critical to Operability and Performance

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Limestone Chemical Looping Test 2 Modifications – Gas Drain System



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Award 23497 Gasification 3 MWth Prototype Testing

Prototype LCL-G[™] test program to maximize syngas H_2 , minimize CH_4 and minimize N_2

- Three (3) piggyback LCL-G test campaigns combined with Project 9484 LCL-C test campaigns;
 Final dedicated test after LCL-G modifications
- Assess effects and optimize key parameters such as reduce and oxidizer stoichiometry and temperatures, reducer steam flow
- Reducer carbon conversion, volatile cracking and gasification
- Oxidizer CaS oxidization behavior, Oxidizer/ Reducer ۲ sulfur capture and release mechanisms
- Solids transport behavior
- Behavior of different fuel types, fuel and limestone size
- Evaluate carrier behavior and performance, different • limestone types, carrier mixtures and additives

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Small-Scale Testing and Process Development 100mm Pilot-Scale Test Facility (PSTF)

Map conditions to better understand behavior – single and double loop tests, vary reactor sizes

- Assess effects and optimize key parameters such as reducer and oxidizer stoichiometry and temperatures, reducer steam flow
- Reducer carbon conversion and residence time requirements
- Coal volatile cracking and conversion
- Oxidizer CaS oxidization behavior
- Oxidizer/Reducer sulfur capture and release mechanisms
- Solids flow and circulation behavior
- Behavior of different fuel types
- Evaluate carrier behavior and performance, different limestone types, carrier mixtures and additives

100 mm Dia. 50ft. Riser (Oxidizer or Reducer)

Under Construction – To Be Completed September 2015

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100 mm Pilot Scale Test Facility – Under Construction



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Oxidizer



. .

Reducer



Electric and I&C Supply





Limestone Chemical Looping Development Planned Workscope & Schedule

Calender Year					201	۱5								·	20	16										201	017											
	Α	N	1 J	J	Α	S	0	Ν	D	J	F	Μ	Α	М	J	J	Α	S	0	Ν	D	J	F	Μ	Α	Μ	J	J	Α	S								
Alstom Lab Relocation																																						
LCL-Combustion (Award 9484)																																						
Techno-economic Update																			Ì																			
Support Testing (PSTF -						4		4	1		▲		1																									
3 MW Prototype Mods & Testing					4							۸			44			[
LCL-Gasification (Award 23497)																																						
Techno-economic Assessment																																						
Support Testing (PSTF -								Δ		4				4					Δ]															
3 MW Prototype Mods & Testing									4				Δ		1	4		<u> </u>			1																	
Reducer O2 Demand (Planned)		-																																				
Support Testing (PSTF -		-																		Δ				Á			Δ											
3MW Prototype Testing																													Δ									
Demo Pre-FEED & FEED (Planned)																																						

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Alstom Limestone Chemical Looping Summary

- Techno-economic studies continue to indicate that Limestone Chemical Looping technology has the potential for lowest cost coal-based power generation with CO₂ capture.
- Alstom been developing chemical looping technologies for more than a decade:

Significant knowledge and understanding has been developed through comprehensive testing, modeling and engineering studies.

- Autothermal operation has been achieved at the 3 $\rm MW_{th}$ scale confirming chemical looping reactions and performance potential.
- Development gaps have been identified and comprehensive programs are in-progress to address them.
- Alstom is continuing development efforts and on track
 with its commercialization roadmap



Acknowledgements and Disclaimer

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Techno-Economic Study: LCL-Combustion

Study Cases: 550 MW_e Power Plant with CO₂ Capture

(Applying DOE Economic Methodologies and Guidelines)

- Case 1 LCL-C[™] system using transport reactors
- Case 2 LCL-C[™] system with the Reducer reactor in the CFB mode
- Case 3 LCL-C[™] system of Case 1 with an advanced ultra-supercritical (AUSC, 350bar/730°C/760°C) steam cycle
- Case 4 LCL-C[™] system with pressurized Reducer reactor with an AUSC steam cycle

Comparison Basis:

- State-of-the-art SCPC case Case 11 from Cost and Performance Baseline for Fossil Energy Plants Volume 1, DOE/NETL-2010/1397
- 1st generation Oxy-combustion PC case Case 5 from Pulverized Coal Oxy-combustion Power Plants, DOE/NETL-2007/1291 (COE increased 53.5% from Case 11)





LCL-C[™] Power Island Process



Fully integrated with AQCS and CO₂ capture system

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Chemical Looping Development Phase 1 - LCL-C[™] Techno-economic Analysis

	Baseline: US DOE SCPC plant, no capture	US DOE Oxy-SCPC plant	Alstom SC Chem Loop Plant, Case 1
Nominal output (net, MW)	550	550	550
Capacity factor (%)	85	85	85
HHV efficiency (% HHV)	39.3	29.3	35.8
CO ₂ capture (%)	0	93	97
CO ₂ emitted rate (lb/MWh)	1210	113	40
EPC overnight cost (\$/kW)	2452	3977	DOE gool 2795
Cost of Electricity Breakdown			
Fuel (\$/MWh)	25.53	34.25	>90% 28.04
Capital (\$/MWh)	38.19	66.23	46.55
O&M fixed (\$/MWh)	9.48	14.24	10.58
O&M variable (\$/MWh)	7.74	9.54	11.53
T&S adder to COE (\$/MWh)	0	8.29	DOE goal: 7.08
1 st yr COE (w/o T&S, \$/MWh)	80.95	124.25	<35% 96.7
LCOE (w/o T&S, \$/MWh)	102.64	157.55	122.62
Fuel cost (\$/MMBtu)	2.94	2.94	2.94
Construction period (yrs)	**************************************	5	10000000000000000000000000000000000000
Operational period (yrs)	30	30	30
% Increase – Levelized COE		53.5	19.5

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Support Testing - Physical Flow Model and **CFD Modeling**



40ft Cold Flow Model



- ~ 1 million computational particles
- 78,000 cells (discounting null cells) 40 sec real time/day



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