**Area of Interest 1: Geomechanical Research** 

#### Development of Geomechanical Screening Tools to Identify Risk: An Experimental and Modeling Approach for Secure CO<sub>2</sub> Storage

DE-FE0023314

#### **Dr. Mary F. Wheeler**

#### The University of Texas at Austin



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#### Outline



#### **Benefit to the Program**



#### **Goals and Objectives**



#### Technical Status from Tasks 2 to 6



#### Accomplishments to Date



#### **Synergy Opportunities**





#### Benefit to the Program

Develop a Geomechanical Screening Tool to Identify Risk

Experimental & Modeling Approach for Secure CO<sub>2</sub> Storage





### Project Overview: Goals and Objectives

Develop a screening tool for improved understanding of geomechanical effects associated with CO<sub>2</sub> injection

□ Derive a workflow from experimental and computational studies conducted for specific CO<sub>2</sub> sites, e.g. Frio, Cranfield

Task 1 Project management (M.F. Wheeler-lead)

Task 2 Conduct laboratory experiments for hydro-mechanical rock properties (N. Espinoza–lead)

Task 3 Upscale to bridge from laboratory to field scales (M.F.W.–lead)

Task 4 Extend simulator capability to model CO<sub>2</sub> storage field scale studies (M. Delshad–lead)

Task 5 Perform parameter estimation & uncertainty quantification (M.F.W.-lead, S. Srinivasan-consultant)

Task 6 Integrate results to generate geomechanical screening tool / workflow (M.F.W.-lead, S.S.-consultant)



#### Model Field Sites









Large Axisymmetric Triaxial Frame

ø 4 in





- 140 MPa (20 ksi) confining/pore pressure
- Ultrasonic monitoring
- Local strain measurement
- Strain/pressure control
- Temperature up to 150°C (300°F)
- Connected to CO<sub>2</sub> ISCO pumps



Rock Samples



Fluvial Oligocene, poorly consolidated Courtesy S. Hovorka (DE-AC26-98FT40417) Cretaceous, chlorite/quartz cemented BEG-UT Austin Core Research Center

#### **Outcrop : Castlegate Sandstone**

 Cretaceous Mesaverde group, cemented by calcite. This sandstone is attractive for testing because it can serve as an end-member due to weak cementing bonds presumably susceptible to CO<sub>2</sub> alteration. Available in several sizes from commercial vendors.



Planned Tests

Basic Rock Properties						
Dry conditions	Saturated with water					
<ul> <li>Mineralogy (XRF)</li> <li>Drained mechanical moduli</li> <li>Elastic nonlinearity</li> <li>Mechanical anisotropy</li> <li>Shear and tensile strength</li> <li>Fracture toughness</li> <li>Creep</li> </ul>	<ul> <li>Porosity</li> <li>Absolute permeability</li> <li>Biot's coefficient</li> <li>Thermal expansion coefficient</li> <li>Thermal conductivity</li> <li>Specific heat</li> </ul>					

Advanced Rock Properties							
Fluid flow properties with a CO <sub>2</sub> phase	Mechanical						
Capillary pressure	Transition brittle to ductile						
Relative permeability	Strain localization						
Chemo-mechanical coupling	Scale effects						
Porosity change with chemical dissolution	Thermo-mechanical coupling						
Permeability change with chemical dissolution	Thermal induced stress						
Chemically enhanced creep	Poro-mechanical coupling						
Stress relaxation with chemical dissolution	Stress sensitivity of permeability						



Obj	ectives	Upscale measured rock properties ( relevant to field processes (M.F. Wh	fluid flow & geomechanics) to scale neeler–lead)
+	combinin	ment of <b>homogenization</b> schemes g numerical and analytical nes, e.g. multiscale mortar method	$\int_{z_{2}}^{\sigma_{33}} p_{c} p_{c}$ $\int_{z_{2}}^{\sigma_{22}} \left[ \underbrace{\sigma}_{z} = \underbrace{c}_{z} - \alpha p_{c} I \right]$
•	natural f	r emphasis will be put on including <b>ractures</b> in effective properties and on effects	$\sigma_{11} \begin{cases} \underline{\sigma} = C \\ \underline{\varepsilon} = -\alpha p_c I \\ \varphi = p_c / N + \alpha \varepsilon_v \end{cases}$
Ļ	perform	eld scale constitutive parameters to coupled fluid flow and hanical numerical simulation	



• Task 3.0: Upscale to Bridge Laboratory to Field Scales

Homogenization	Simulator Development
<text><list-item></list-item></text>	<text><list-item><list-item><ul> <li>MFDFrac: developed using mimetic finite differences</li> <li>Sample fracture realizations from parameterized space</li> <li>Generate unstructured polyhedral meshes based on fracture geometries</li> </ul></list-item></list-item></text>

Homogenization for Upscaling: Methodology

#### **Choice of Unit Cell Model**

- Darcy's law for unit cell (mesoscale) and field (macroscale) problems
- Characteristic length scales:  $L_{unit}/L_{reservoir} = \epsilon \ll 1$
- Solve an auxiliary unit cell problem to obtain effective permeability
- Use different unit cell models in different domains (sands A, B, C, etc.) for characterizing reservoir heterogeneity





• Homogenization for Upscaling: Methodology

#### **Choice of Unit Cell Model**

- Auxiliary Unit Cell Problem  $-\nabla \cdot \left[ K(y) \left( \nabla w_j + \overrightarrow{\mathbf{e}_j} \right) \right] = 0$  in Y $w_i = 0$  on  $\partial Y$
- Effective Permeability

$$K_{eff} = \frac{1}{|Y|} \int_{Y} K(y) \left[ \nabla w_{i} + \overrightarrow{\mathbf{e}_{i}} \right] \cdot \left[ \nabla w_{j} + \overrightarrow{\mathbf{e}_{j}} \right] dy$$





• Homogenization for Upscaling: Application to Frio Field, TX





• Homogenization for Upscaling: Application to Frio Field, TX

Reservoir Characteristics	Permeability in C Sandstone
<ul> <li>Reservoir Characteristics</li> <li>Sandstone reservoirs         <ul> <li>Periodic deposition due to flooding of river beds</li> <li>Shale layer marks the end of one deposition cycle</li> <li>Idealize as a periodic porous medium</li> </ul> </li> </ul>	5040 5060 5060 1545
<ul> <li>Identify meso-scale periodicity from well log data</li> <li>Characterize period <ul> <li>✓ High permeability &amp; Low permeability</li> </ul> </li> <li>Solve local period problem to estimate up-scaled field scale permeability</li> </ul>	(t) t) t) t) t) t) t) t) t) t)

#### Task 4: Simulator Development





#### Task 4: Simulator Development

• Geomechanical Effects of CO<sub>2</sub> Injection with a Poro-plasticity Model

Fluid Flow	$\frac{\partial(\rho(\phi_0 + \alpha\varepsilon_v + \frac{1}{M}(p - p_0)))}{\partial t} + \nabla \cdot \left(\rho \frac{K}{\mu}(\nabla p - \rho g \nabla h)\right) - q = 0$						
Stress Equilibrium	$\nabla \cdot (\sigma'' + \sigma_o - \alpha(p - p_0)I) + f = 0$						
Hooke's law	$\sigma'' = D^e : (\varepsilon - \varepsilon^p)$	Druker-Prager Yield Surface					
Strain-Displacement Relation	$\varepsilon \;=\; \frac{1}{2} (\nabla u + \nabla^T u)$	$\sigma_2$					
Plastic Strain Evolution	$\begin{split} \dot{\varepsilon}^p &= \lambda \frac{\partial F(\sigma'')}{\partial \sigma''},  \text{at } Y(\sigma'') = 0\\ \dot{\varepsilon}^p &= 0,  \text{at } Y(\sigma'') < 0 \end{split}$						
Yield and Flow Functions	$Y = q + \theta \sigma_m - \tau_0$ $F = q + \gamma \sigma_m - \tau_0$	$\sigma_3$ $\sigma_1$					



#### Task 4: Simulator Development

• Preliminary Poro-plasticity Results with Application to Cranfield, MS

Pore Pi	ressure	Vertical Displacement	Volumetric Plastic Strain				
PCL		DISPX 4220-02 0.04 0.03 0.02 0.01 0.0000+03	VPSTRAIN           5581e04         0.0012         0.0004         2.0024         2.686e-03				
Mechanica	l Properties	Next Steps: Geometr	y and Heterogeneity				
<i>E</i> 375,581 psi		Our findings show that					
v	0.25	at normal CO <sub>2</sub> pressure					
a	1.0	injection range rock	PORO 0.38 0.38 0.34				
1/ <i>M</i>	1e-6 / psi	formation may yield.					
$ au_0$	1,600 psi		02 02 01 01 01 01 01 01 012				
θ	0.6						



	True Log(ky), Layer 1
Complex relationship betw physics attributes is honor	een the multi-
Residual uncertainty in pre migration of the CO2 is fai	40 Day a Obs-2 lite-1 pay 4



• Process of History Matching: Combination of Tasks 2 to 5





History Matching Coupled w/ Level-Set, MFDFrac, and EnKF



• Matching Results: Water Saturation for Initial & Final Realizations



Matching Results: Observed and Predicted Production Profiles



- Observed data from the reference field
- 100 realizations before updating
- 100 realizations after updating
- Average of 100 realizations





• Quarter Wellbore Model: Flow & Geomechanics Equation

#### Assumption

- Assume a linear, elastic, homogenous, and isotropic porous medium
- The reservoir is saturated with a slightly compressible viscous fluid
- Quasi-static Biot model to obtain mechanical displacements

#### **Geomechanics Equations**

Balance of Linear Momentum:  $-\operatorname{div} \boldsymbol{\sigma}^{\operatorname{por}}(\boldsymbol{u}, p) = \boldsymbol{f} \quad \operatorname{in} \Omega \setminus C$ Cauchy Stress Tensor:  $\boldsymbol{\sigma}^{\operatorname{por}}(\boldsymbol{u}, p) = \boldsymbol{\sigma}(\boldsymbol{u}) - \alpha p \boldsymbol{I}$ Effective Linear Elastic Stress Tensor:  $\boldsymbol{\sigma}(\boldsymbol{u}) = \lambda(\nabla \cdot \boldsymbol{u})\boldsymbol{I} + 2 G \boldsymbol{\varepsilon}(\boldsymbol{u})$ 

- ullet I is the identity tensor ,  $oldsymbol{u}$  is the solid's displacement , p is the fluid pressure
- lpha>0 is the Biot coefficient ,  $\lambda>0$  and G>0 are the Lamé constants
- *f* is a body force (gravity loading term)



• Quarter Wellbore Model: Flow & Geomechanics Equation

#### Assumption

- Assume a linear, elastic, homogenous, and isotropic porous medium
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#### **Geomechanics Equations**

$$\frac{\partial}{\partial t} \Big( \Big( \frac{1}{M} + c_f \varphi_0 \Big) p + \alpha \nabla \cdot \boldsymbol{u} \Big) + \nabla \cdot \boldsymbol{z} = \tilde{q} \text{ in } \Omega \setminus \mathbf{C},$$
$$\boldsymbol{z} = -\frac{1}{\mu_f} \boldsymbol{K} \Big( \nabla p - \rho_{f,r} g \nabla \eta \Big) \text{ in } \Omega \setminus \mathbf{C},$$

- ullet p and  $oldsymbol{z}$  represents the pressure and flux unknowns
- $\mu_f > 0$  represents the constant fluid viscosity
- $\rho_{f,r} > 0$  is a constant reference density (relative to the reference pressure  $p_r$ )
- $\varphi_0$  is the initial porosity ,  $\alpha \Rightarrow$  (coupling term)
- M is the Biot constant ,  $ilde{q}=rac{q}{
  ho_{f,r}}$  where q is a mass source or sink term

• Quarter Wellbore Model: Iterative Algorithm using Multi-rate Time Step





• Quarter Wellbore Model: Accumulated Number of Mechanics

#### **Simulation Time vs. Iterations**



Figure: Multirate coupling with two flow finer time steps (q = 2), within one coarser mechanics time step results in 44.2% reduction  $\downarrow$  in total number of **mechanics** linear iterations. Multirate couplings (q = 4), (q = 8) results in 69.2%, 83.5% reduction  $\downarrow$  in total number of **mechanics** linear iterations respectively.



#### Accomplishments to Date

- Set up of experimental studies on homogenization in Tasks 2 and 3
- Site characterization initiated in Tasks 2, 3, and 4
- Preliminary results from the advanced flow and geomechanics model in Tasks 3, 4, 5, and 6





## Synergy Opportunities

#### Assistance in Decision Making

 Assist in selection of suitable sites for safe CO<sub>2</sub> storage using generalized S/Ws based on a posteriori knowledge



#### Interdisciplinary Collaboration

 Enhance understanding of the effects of CO<sub>2</sub> migration on open and closed faults and fractures



### Training & Education

Support training and education of students who will take part in an interdisciplinary work, e.g. IPARS tutorial



Contribution to Identifying Geological Risk for Secure CO<sub>2</sub> Storage!



### Summary

Developing a generalized geomechanical screening tool Preliminary outcomes from interdisciplinary collaboration Homogenization / Poro-plasticity / Level-set / MFDFrac / Ensemble-based calibration / Multi-rate fixed stress split Achievement ahead of milestone



#### Acknowledgements



# Thank you for your attention

Contact: mfw@ices.utexas.edu



#### **Organization Chart**

Project Director										
M.F. Wheeler										
Task 1Task 2Task 3Task 4Task 5Task 6										
Management	agement Laboratory Bridging Modeling an		Modeling and	Uncertainty	Integrate					
	Program	between	Field Studies	Quantification	Results to					
		Laboratory and		and Parameter	Generate					
		Field Scales		Estimation	Geomechanical					
					Screening Tool					
					/ Workflow					
Task Leader	<u>Task Leader</u>	<u>Task Leader</u>	<u>Task Leader</u>	<u>Task Leader</u>	<u>Task Leader</u>					
M.F. Wheeler	N. Espinoza	M.F. Wheeler	M. Delshad	M.F. Wheeler	M.F. Wheeler					
Key Personnel	<u>Key Personnel</u>	<u>Key Personnel</u>	<u>Key Personnel</u>	<u>Key Personnel</u>	<u>Key Personnel</u>					
M. Delshad	M.F. Wheeler	S. Srinivasan	M.F. Wheeler	M. Delshad	M. Delshad					
S. Srinivasan	M. Delshad	N. Espinoza	N. Espinoza	M.F. Wheeler	S. Srinivasan					
N. Espinoza	<sup>1</sup> / <sub>2</sub> Postdoc	<sup>1</sup> / <sub>2</sub> Postdoc	<sup>1</sup> / <sub>2</sub> Postdoc	1 Student	N. Espinoza					
	1 Student	1 Student	1 Student (Y 3)	S. Srinivasan	Postdoc					
	(Y 1&2)			(Consultant)	Student					



#### **Gantt Chart**

Task		Sep. 2014 - Aug. 2015			Sep. 2015 - Aug. 2016			Sep. 2016 - Aug. 2017					
		Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4
T1	Management		А, В										
T2	Laboratory Experiment			С	D		E		F	G			
Т3	Upscale from Lab. to Field								н		I		
T4	Simulator Development				J				к	L		М	
Т5	Uncertainty Quantification								N				ο
Т6	Integrated Geo- Screening Tool												Ρ
	A to P : Milestones					Sche	dule			Acco	mplish	nment	



### IPARS

#### Integrated Parallel Accurate Reservoir Simulator (IPARS)

- > Workhorse for multiphysics, parallel, field scale simulations
- Coupled geomechanics, flow, reactive transport and thermal models
- Fractured reservoirs: hydraulic and natural fracture treatment
- Advanced well models: horizontal and deviated wells

