Project Update and Results of Analyses of Fine Particulates in Cleaned Coal Syngas and Its Combustion Products

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- The University of North Dakota (UND) Energy & Environmental Research Center (EERC) and Department of Mechanical Engineering are working with Siemens Power Generation to test a new method for joining high-temperature alloys for use in advanced high-hydrogen-gas-burning turbines.
- Thin plates of oxidation- and spallation-resistant Kanthal APMT[™] will be bonded to high-strength CM247LC and Rene[®] 80 using evaporative metal (EM) bonding.
- Bonded parts, with and without thermal barrier coatings (TBCs), will be tested for oxidation, corrosion, and spallation resistance.
- Gasifier sampling to determine appropriate corrosion conditions.



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Composition of Kanthal APMT, wt% – Dispersion-Strengthened										
	Cr	AI	Мо	Mn	Si	Fe				
APMT	22	5	3	0.4	0.7	Balance				

Composition of CM247LC, wt% – Gamma Prime-Strengthened													
	Fe	Ni	Cr	AI	Ti	Со	Мо	Та	W	Nb	Hf	Mn	Si
CM247LC	_	Balance	8.1	5.6	0.7	9.5	0.5	3.2	9.5	0.1	1.4	_	_

Composition of Rene 80, wt% – Gamma Prime-Strengthened												
	Cr	С	Мо	W	Ti	Nb	Со	AI	В	Fe	Zr	Ni
Rene 80	14.2	0.16	4.0	4.1	5.1	0.03	9.4	3.0	0.02	0.10	0.04	Balance



WORLD Microstructure of EM Joints Centers of Excelled

- Scanning electron microscopy (SEM) photo (top) and x-ray map (bottom).
- Needle growth and interdiffusion to create a joint stronger than the APMT.
- Nickel diffuses up to 700 µm into APMT.
- Iron diffuses 200 µm into CM247LC.





WorldArticulated Clamping System

- Specimens are electrodischargemachined to shape.
- Bonding surface is blasted with silica beads.
- Clamp is made from low-CTE metal (TZM molybdenum).
- Steel hemispheres (E52100) are used to articulate the pieces, which is necessary because of the thinness of the foils. Steel is used to facilitate modeling.
- Joints of APMT to CM247 and APMT to Rene 80.





Stress modeling within the clamps CENTERS OF EXCEL



Comparison of strains in the bonding assembly when loads are applied at a) joint center or b) joint ends.



Stress Distribution at Bond Surface





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$$\frac{\partial C}{\partial t} = D \left[\frac{\partial^2 C}{\partial x^2} + \frac{\partial^2 C}{\partial y^2} + \frac{\partial^2 C}{\partial z^2} \right]$$

3-D Diffusion with Constant Diffusivity

No analytical solution exists for the combination of initial and boundary conditions present in the experimental setup (midline symmetry assumed):





Research and Diffusion World-Clas Diffusion Centers of Excellence

- A finite difference algorithm was implemented within MATLAB to solve the diffusion equation.
- The 'hopscotch' iterative solver was implemented to improve accuracy and computational efficiency.
- Algorithm assumes initial midline concentration of Zn, assumes constant diffusivity, uses a rectangular geometry and allows for different mesh size in each direction (x, y, z).



WORLD-CLAS Diffusion Centers of Excelled Conters of Excelled Conte



- ~15 wt% initial centerline composition for model
- D for Zn in APMT ~2.7 E-12 m²/s
- D for Zn in Rene 80/CM 247 ~4 E-14 m²/s

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World-CLAJOINT Stresses (N/m²) Centers of Excellent



Rene 80/APMT







CM247LC/APMT



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Joint Stresses (N/m²)





1.0398e8 Max

7.0904e7

3.7827e7

4.7511e6

-2.8325e7

-6.1401e7

-9.4478e7

-1.2755e8

-1.6063e8

-1.9371e8 Min

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- Regions of tensile stresses are likely artifacts of model boundary conditions (materials fixed across interface).
- Model convergence issues occurred when alternate interface conditions used (e.g., frictional boundary, springs, etc.).
- The steel hemispheres allow for joint articulation and have a larger area to reduce stresses in the bolt due to the lower yield stress of the steel compared to the TZM molybdenum.



Characterization of Combusted Syngas Contaminants

- Information to be used in designing later corrosion testing – contaminants will not be similar to gasifier fly ash.
- Collection of microcontaminants in combusted syngas created in two pilot-scale gasifiers.
- Analysis of captured microcontaminants by SEM.





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Entrained-Flow Gasifier (EFG) 1800°C, 300 psi



Fluid-Bed Gasifier (FBG) 800°C, 600 psi



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- Included minerals are contained within the carbon matrix of the coal.
- Excluded minerals are independent of the carbon matrix of the coal.



Inorganic Forms in Coal – Organically Associated



- Bound as salts of carboxylic acids.
- Organically associated sulfur.
- Coordination complexes Al³⁺ and Fe³⁺.



Inorganic Forms in Coal – Fluid Matter



- Present in minor amounts.
- Na₂SO₄ and other soluble salts are the most common types.



Eagle Butte Coal Ash Composition





Eagle Butte Coal Mineral Compositions





Advanced Technique Analysis for Eagle Butte Fly Ash





Thermal Oxidizer Inlet FBG Firing Eagle Butte Coal (3/13/13)





Thermal Oxidizer Inlet FBG Firing Eagle Butte Coal (3/13/13)

Some larger flakes present

Flake composition is Fe oxide with some Na and S



1um





Thermal Oxidizer Outlet FBG Firing Eagle Butte Coal (3/13/13)



10µm



Thermal Oxidizer Outlet Natural Gas Firing (3/15/13)



10µm



FBG Syngas Filter Analyses by X-Ray Photoelectron Spectroscopy (XPS)





XPS Comparison of Syngas and Combusted Syngas Filters



Effects of Ion Etching on Composition of the Combusted FBG Syngas Filter



Results of FBG Particulate Analyses

- In the quenched syngas, the particulates are predominantly 0.1–0.5 µm in diameter.
- We were not able to get good energy-dispersive x-ray analyses of the small predominant particles.
- XPS shows that the average composition of the syngas particles is very close to that of the polycarbonate filter and is most likely carbonaceous soot.
- In the combusted syngas, the carbonaceous particles are more spherical than in the syngas and slightly larger, typically 0.2–2 µm.
- The combusted particles show more O, N, and S than the noncombusted particles.
- Ion etching shows that the increased O, N, and S were confined to the surface of the particles.



Thermal Oxidizer Inlet Pressurized EFG Firing Antelope Coal (10/30/13)

- Particulate loading of 6.906 mg/m³.
- Filter was heat damaged.
- Very little soot possibly because EFG produces much less tar.
- Particulate loading weight due to large flakes that had detached from the system walls.





Thermal Oxidizer Inlet Pressurized EFG Firing Antelope Coal (10/30/13)

Large flakes come from system surfaces.

Fe oxide with some C, Na, CI, S, and Zn.







Thermal Oxidizer Outlet EFG Firing Antelope Coal (10/29/13)

- Particulate loading of 0.808 mg/m³.
- Particles are 0.1 to 0.3 microns in diameter.
- They are composed primarily of carbon with some oxygen and sulfur.





Thermal Oxidizer Outlet Firing Natural Gas (11/4/13)

- Particulate loading of 0.698 mg/m³.
- Particles are smaller than when burning syngas but are still carbonaceous.





Results of EFG Particulate Analyses

- No submicron particulates were seen on the syngas filter either because the filter had softened or there is just less soot in an EFG.
- Flakes of iron oxide were collected from the syngas that came from system surfaces. They contained some C, Na, CI, S, and Zn.
- Combusted syngas contained 0.1 to 0.3 micron soot particles.
- Some soot is collected even when burning only natural gas, but particles are smaller and fewer than when burning syngas.



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- Task 5 Preparation of APMT-plated superalloy turbine parts
 - Use data from Tasks 2 and 3 to design clamping system and time—temperature heat treatment.
- Task 6 Environmental testing of plated turbine parts
 - TBC coating and oxidation and spallation testing at Siemens Energy.
 - Corrosion testing at the EERC.



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