Accelerating Technology Development: Post Combustion Capture Sorbents

David C. Miller and James C. Fisher II

National Energy Technology Laboratory

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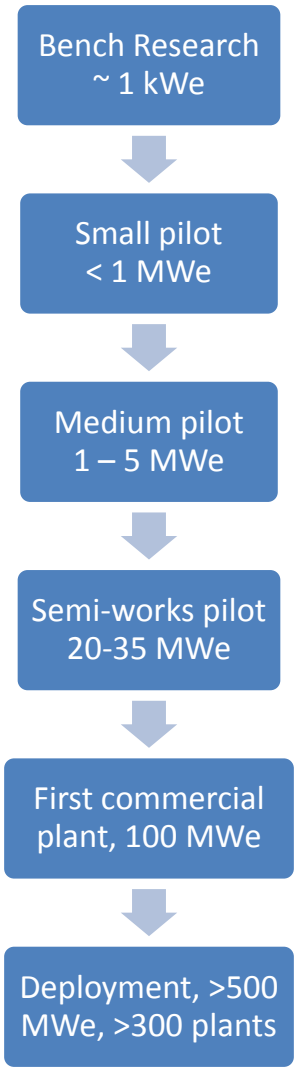
Outline

- Carbon Capture Challenge
- Computational Tools to Accelerate Technology Development
- Experimental Carbon Capture Research @ NETL
- Multiscale Model Development, Simulation & Optimization
- Experimental Validation
- Conclusions

Carbon Capture Challenge

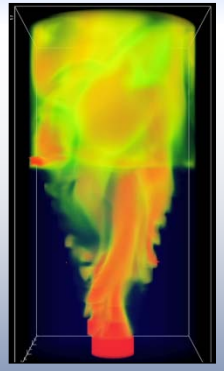
- The traditional pathway from discovery to commercialization of energy technologies can be quite long, i.e., 20-30 years
- New approaches are needed for taking carbon capture concepts from lab to power plant, quickly, and at low cost and risk
- Science-based simulations will accelerate the development of carbon capture technology, from discovery through deployment



CCSI For Accelerating Technology Development

Carbon Capture Simulation Initiative






Identify promising concepts → **Reduce the time for design & troubleshooting** → **Quantify the technical risk, to enable reaching larger scales, earlier** → **Stabilize the cost during commercial deployment**

National Labs

- Berkeley Lab
- Pacific Northwest National Laboratory
- NETL
- Los Alamos National Laboratory
- Lawrence Livermore National Laboratory

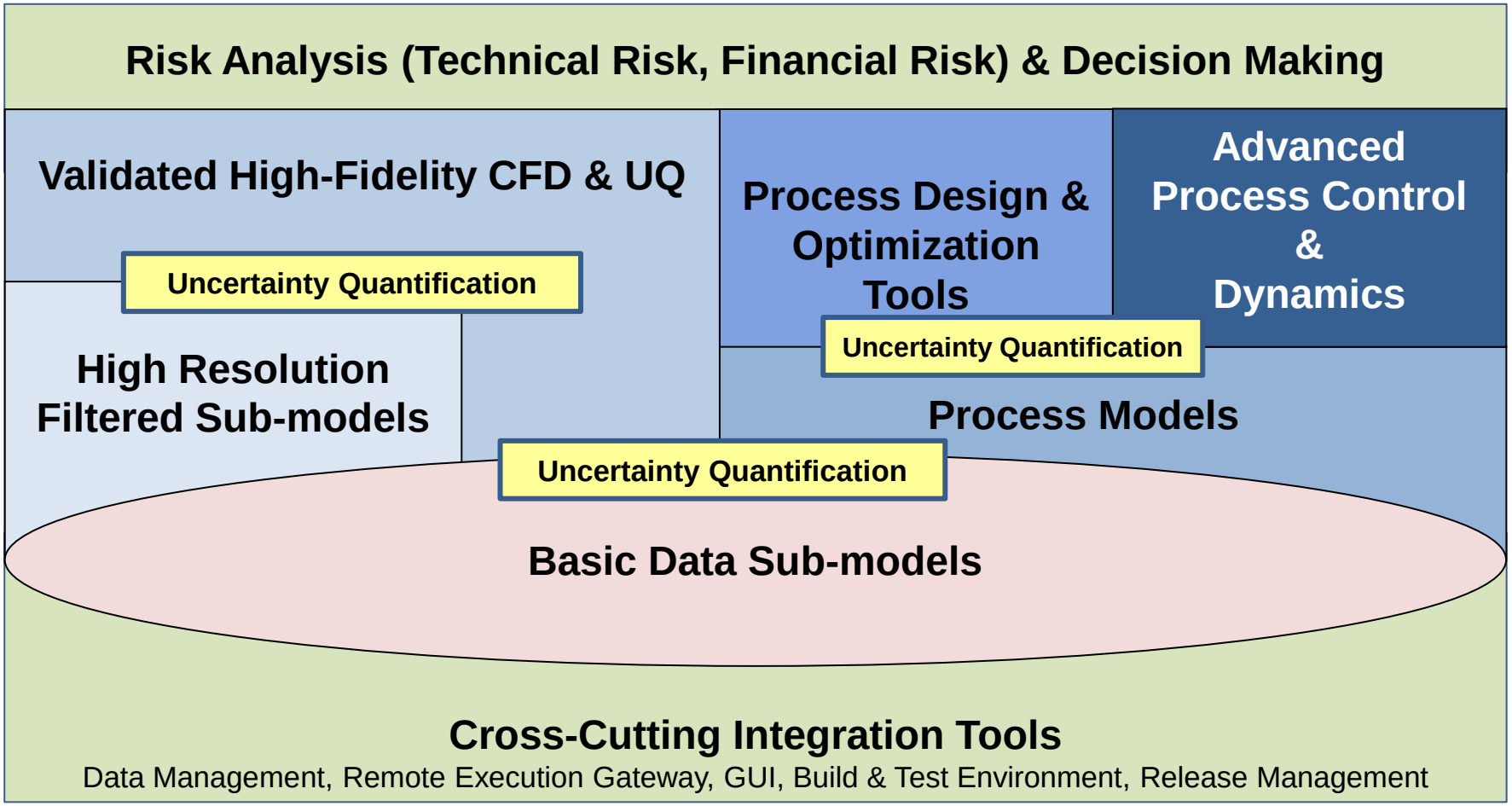
Academia

- Carnegie Mellon
- Princeton University
- West Virginia University
- Boston University
- The University of Texas at Austin
- Institute for Clean and Secure Energy, The University of Utah

Industry

- ADA Environmental Solutions
- Alstom
- B&W
- GE
- EPRI Electric Power Research Institute
- Fluor
- Southern California Edison, An Edison International Company, San Onofre Nuclear Generating Station
- Southern Company
- Phillips 66
- AEP American Electric Power
- Chevron
- URS
- ExxonMobil
- Air Products
- Eastman
- ANSYS
- aspentech
- invensys
- PSE

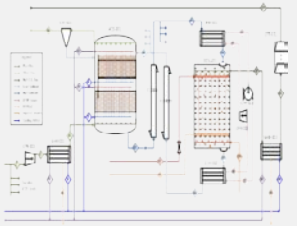
Advanced Computational Tools to Accelerate Next Generation Technology Development



Simulation & Experiments to reduce time for design/troubleshooting

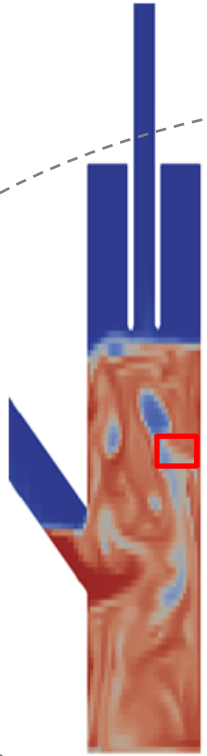
Experimental Validation

Process Models & Optimized Process

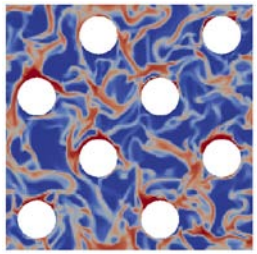


ANSYS FLUENT

Heat-transfer-tube-scale hydrodynamics

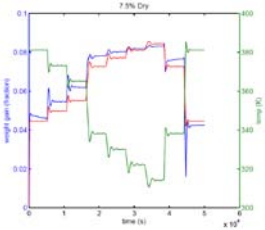


$$f^*_{drag} = \beta^*\left(-v^*_s\left|v^*_s\right|\right) + \gamma^*$$

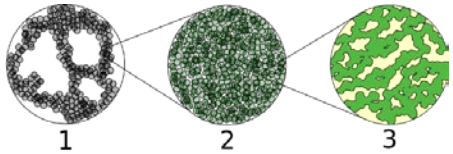


MFiX

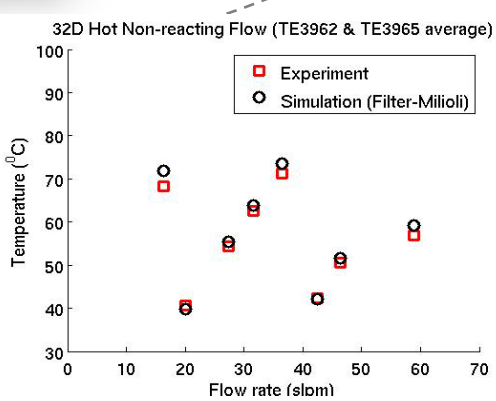
Void Fraction along vertical center plane



SORBENTFIT



Experimental Kinetic/Mass Transfer Data



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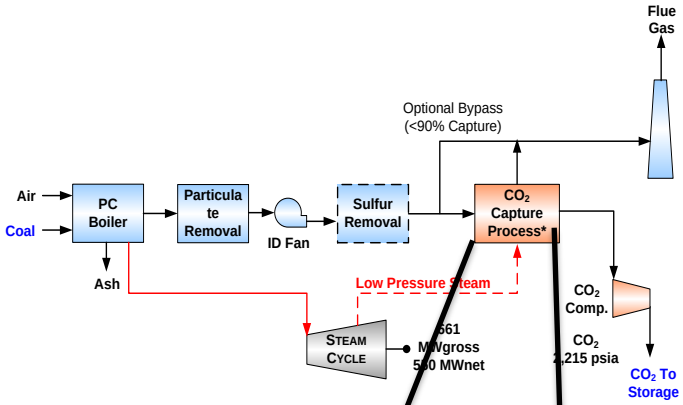
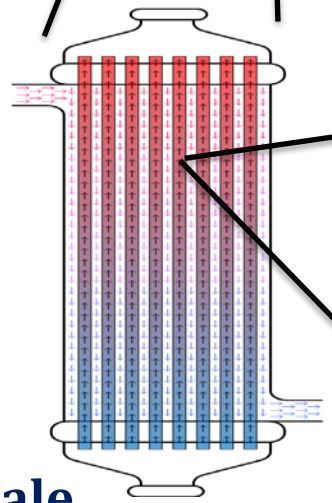
Carbon Capture

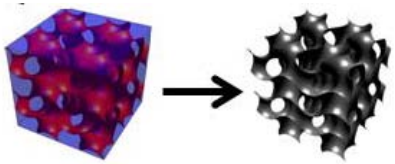


Plant Scale

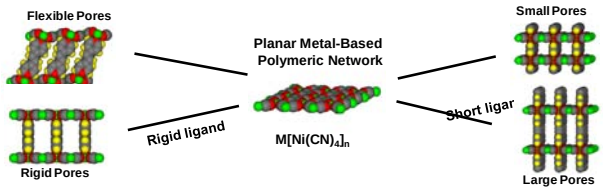


Device Scale

Development of efficient and economic carbon capture strategies applicable for post-, pre- and oxy-combustion schemes



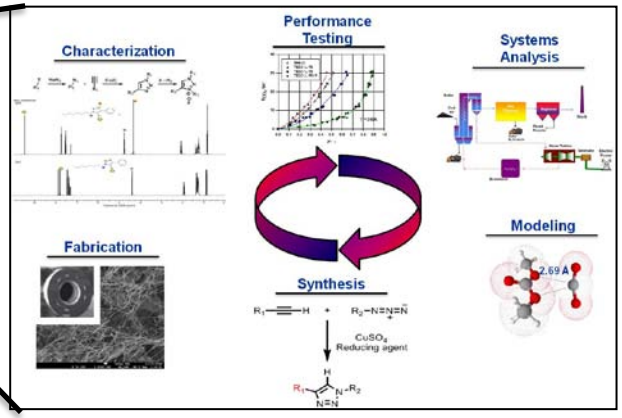
Polymers and Derivatives



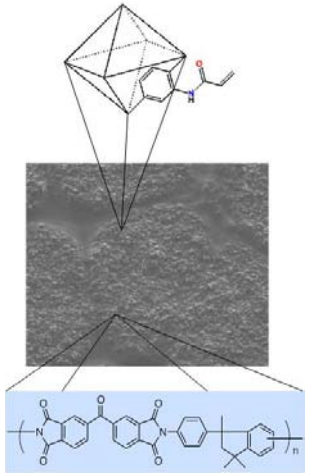
Metal-Organic Frameworks

Ionic Liquids

Integrated Materials Development



Materials Scale

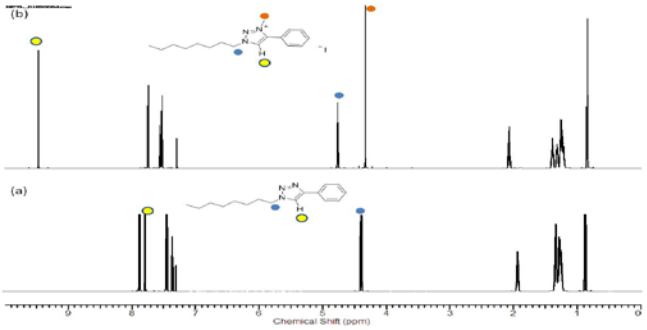


Composites

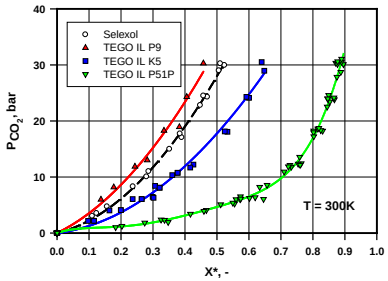
SOUTHERN COMPANY · PPG · CMS · Innovation Works · Berkeley Lab · GT · WVU · Carnegie Mellon · University of Pittsburgh

Integrated Materials Development

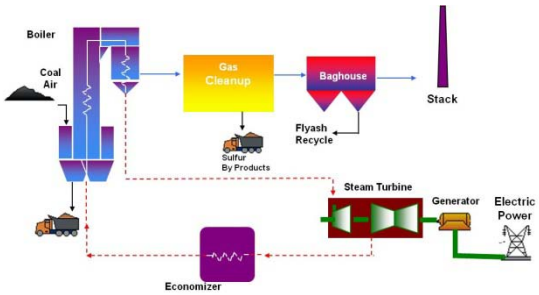
Characterization



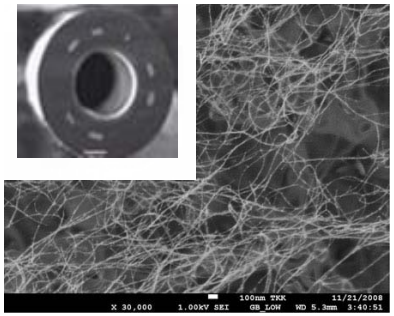
Performance Testing



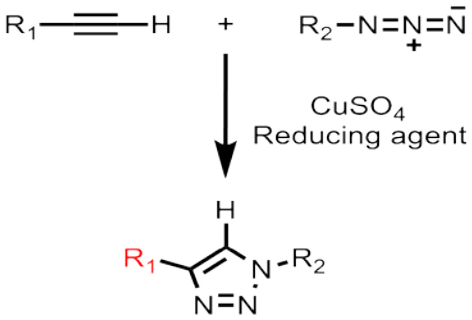
CCSI Simulation & Analysis



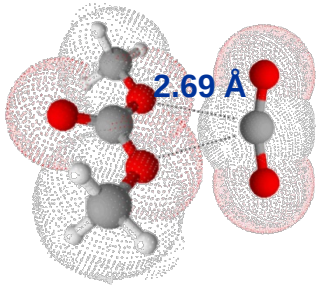
Fabrication



Synthesis

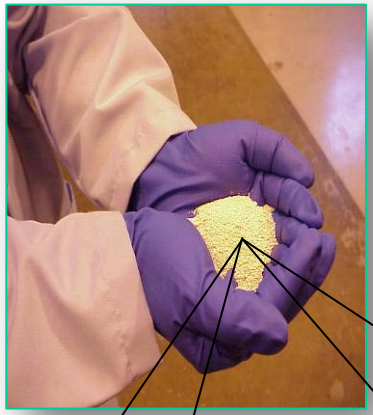


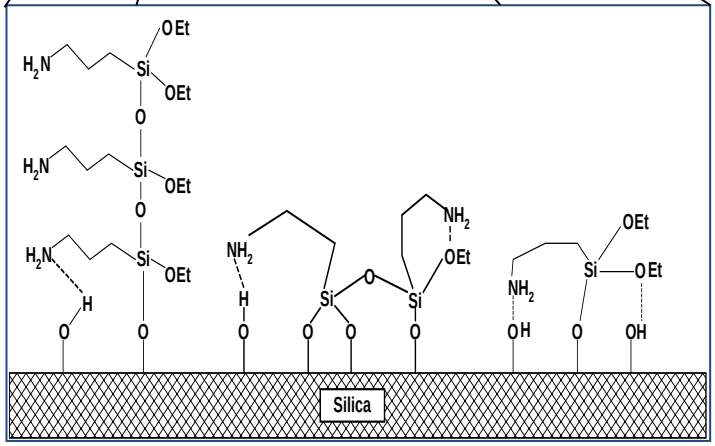
Molecular Modeling



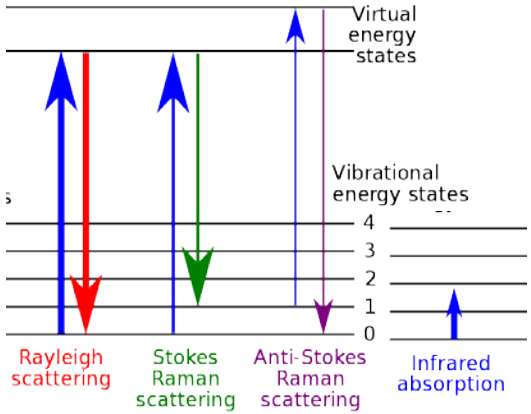
Carbon Capture

Supported Amine Sorbents

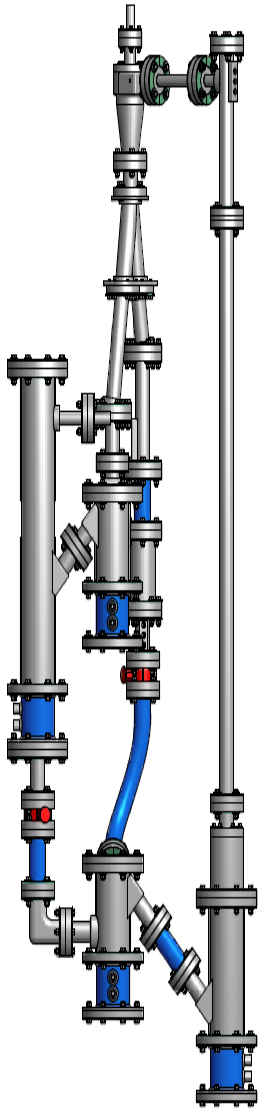




Characterization



Scale-up

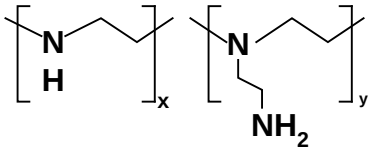


2012 R&D 100

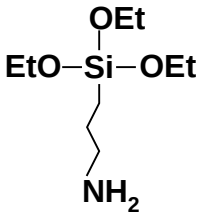
NETL-RUA Regional University Alliance

Components of Basic Immobilized Amine Sorbents (BIAS)

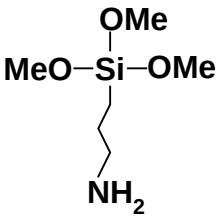
PQ 2129



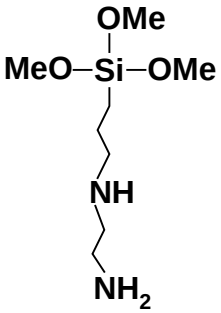
Polyethyleneimine
PEI
Mn 423-2000



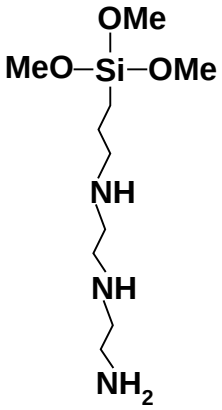
(3-Aminopropyl) triethoxysilane
APTES



(3-Aminopropyl)trimethoxysilane
APTMS



N1-(3-Trimethoxysilypropyl)
diethylenediaimine
DEDA

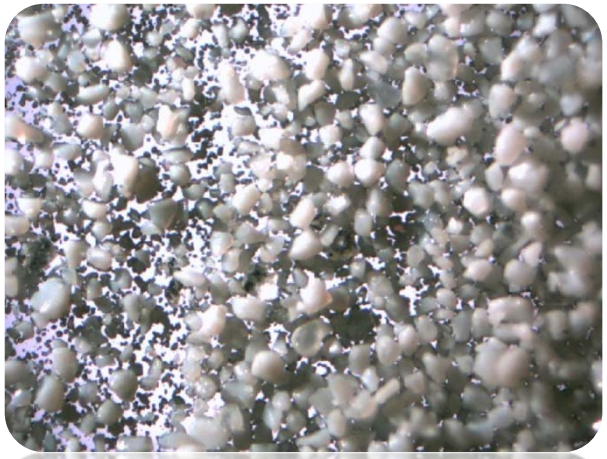


N1-(3-Trimethoxysilypropyl)
diethylenetraimine
DETA

Modification of US 7,288,136 High Capacity Immobilized Amine Sorbents
US Patent Application 13212284 filed 8/11

Sorbent AX

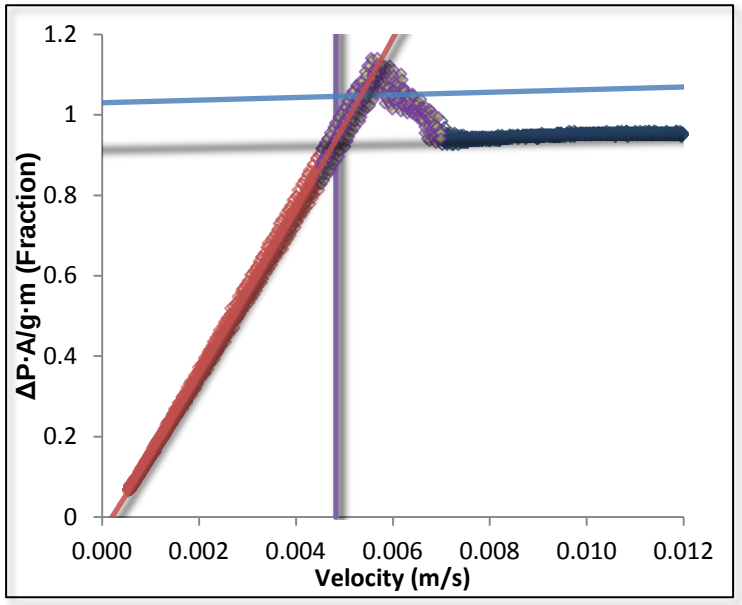
Two BIAS sorbents are being tested: AX and 32D



Sorbent AX

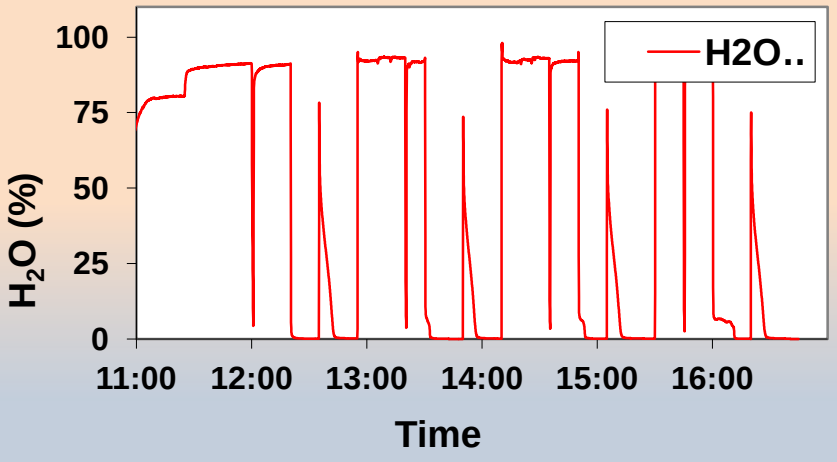
- 40% PEI - BASF M_n 2000
- Mesoporous Silica support- PQ Inc 2129
- 8 - 15 gal. drums from ADA
- Capacity (avg.) = 2.82 mmole CO_2/g adsorbent ranging from 2.60-2.87 for n=7
- ADA packed bed, 13-14% CO_2, ~55°C Capacity (avg.) =1.25 avg. mmole CO_2/g adsorbent
- u_{mf}=0.48 cm/s
- Particles behavior is Geldart Group A

Sauter mean particle diameter	(µm)	114
Spericity	(UNITLESS)	0.86
Particle porosity	(UNITLESS)	0.39
Particle skeletal density	(g/cc)	1.50
Particle density	(g/cc)	0.91

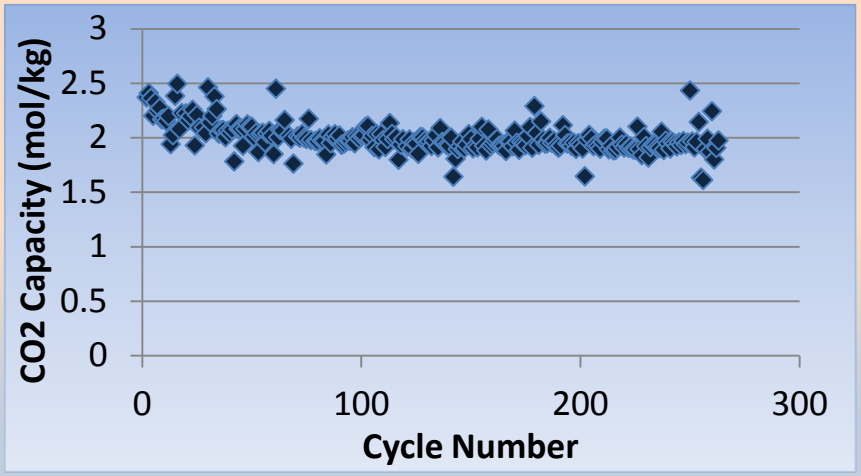


BIAS Sorbent Testing

Regeneration at 105 °C with 90% steam

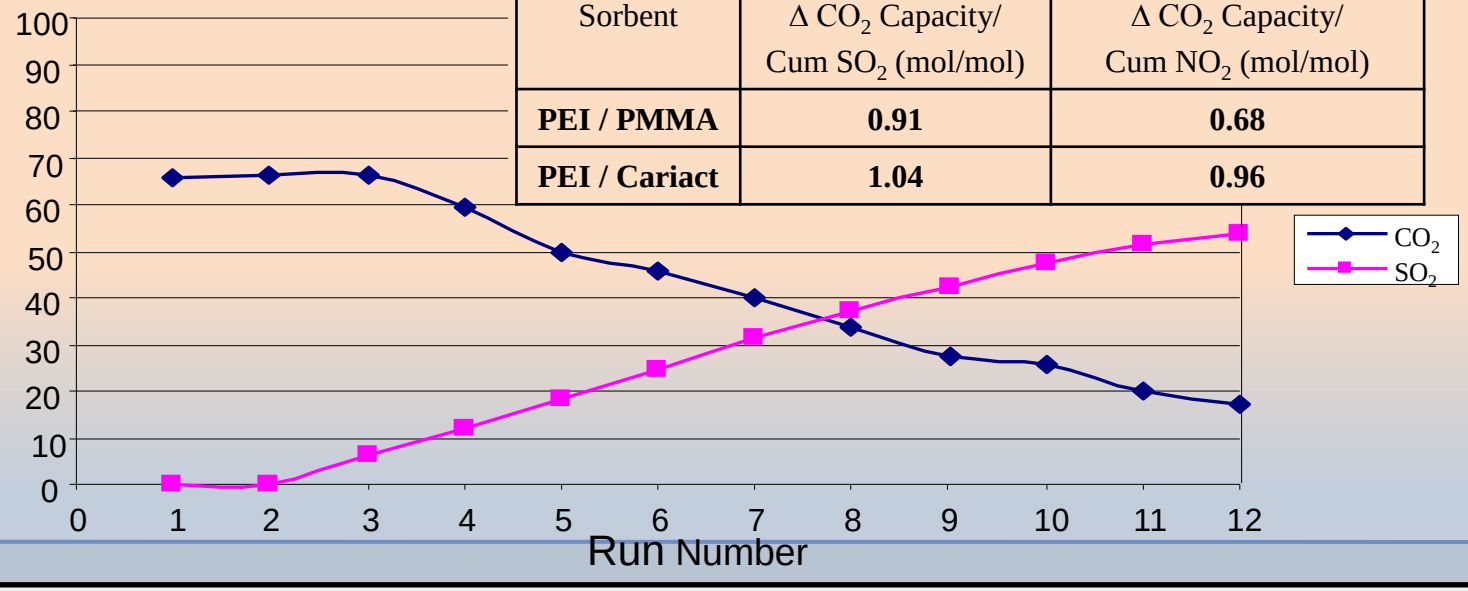


250 cycle stability under humidified conditions



Accelerated SO_x testing

Sorbent	Δ CO_2 Capacity/ Cum SO_2 (mol/mol)	Δ CO_2 Capacity/ Cum NO_2 (mol/mol)
PEI / PMMA	**0.91**	**0.68**
PEI / Cariact	**1.04**	**0.96**



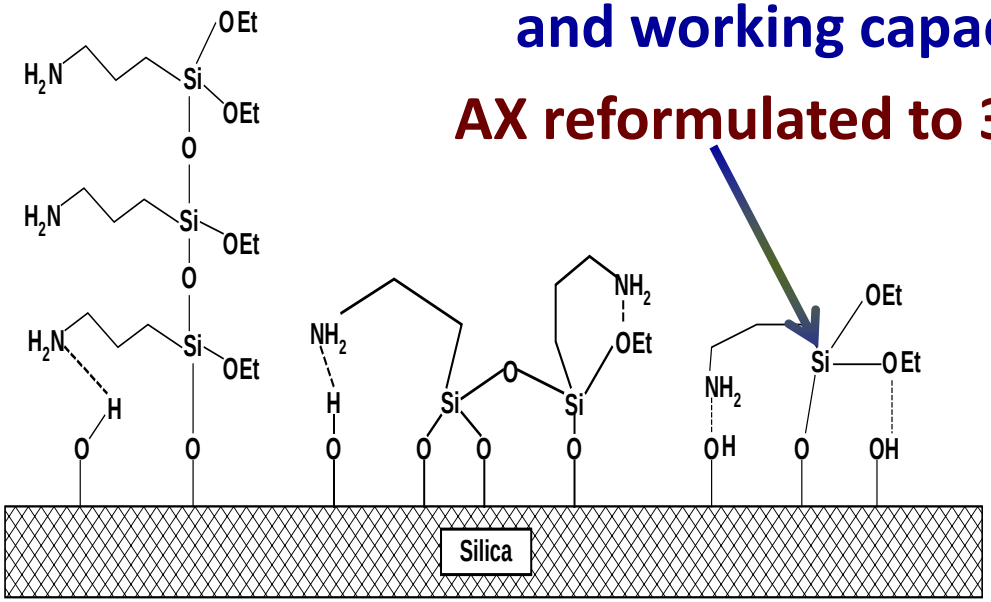
CCSI communication

Provided AX sorbent properties to CCSI

Feedback on working capacity and moisture requirements

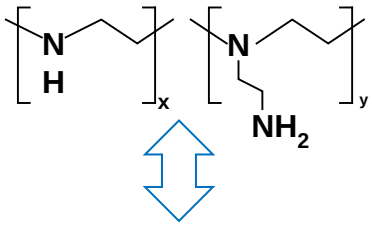
Reformulates sorbent based moisture and working capacity requirements

AX reformulated to 32D sorbent



Polyethyleneimine Silane Coupling

Polyethyleneimine Mn 423-2000



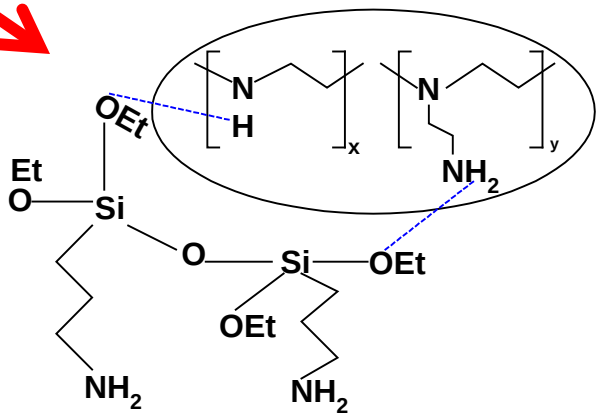
Aminosilanes

Methanol 80 C

Vacuum atm- 10 mm Hg

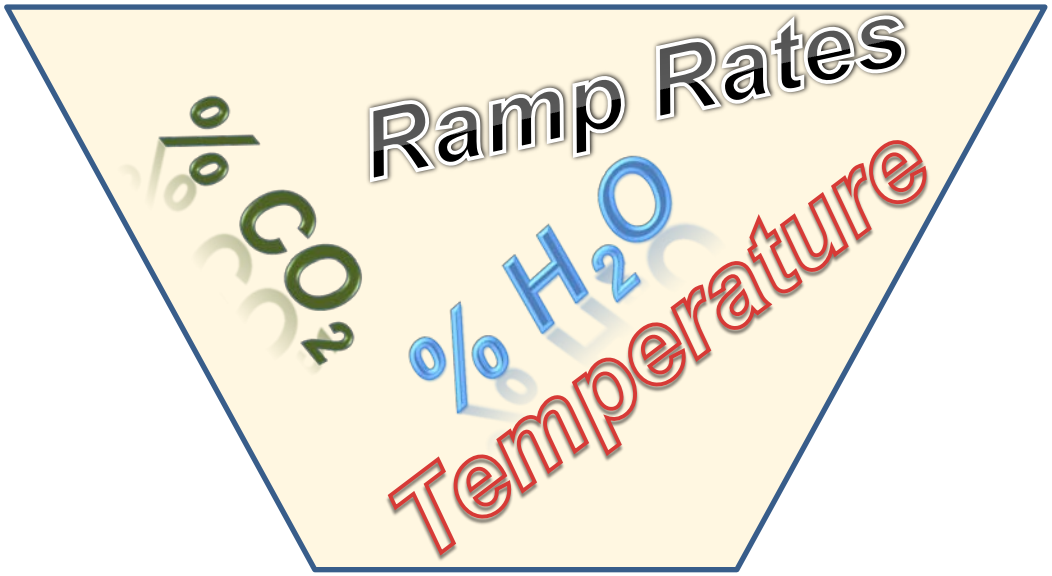
- Simple
- Scalable
- Acceptable Capacity
- Moisture Resistance
- Stability
- Saleable

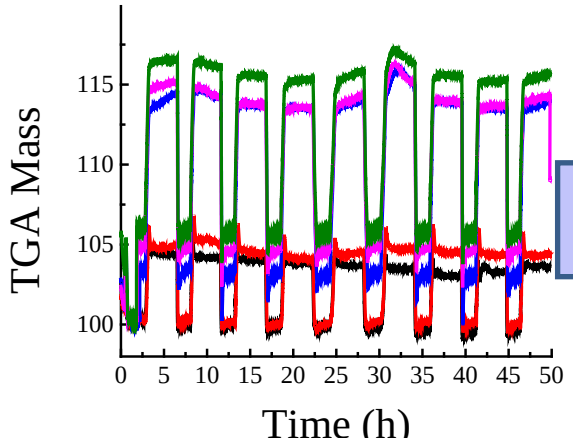
Pressure Chemical – Pan Dyer



Synthesis was scaled to 1,000 lb range

TGA Data Collection





CCSI

Sorption Kinetics

Summary for Basic Immobilized Amine Sorbent

- High delta loadings in the 3-4mol/kg range
- CO_2 regeneration improbable
- Stable at elevated temperatures
- Silica substrate candidate of choice
- Loading results confirmed by TVA and ADA-ES
- Moisture adsorption may impact energetics
- Susceptible to poisoning with SO_2 and NO_2; upstream cleaning required in process
- Kinetic study conducted

PEI on CARiACT Q10
(100 to 350 µm dia.)

Schematic and actual pilot unit

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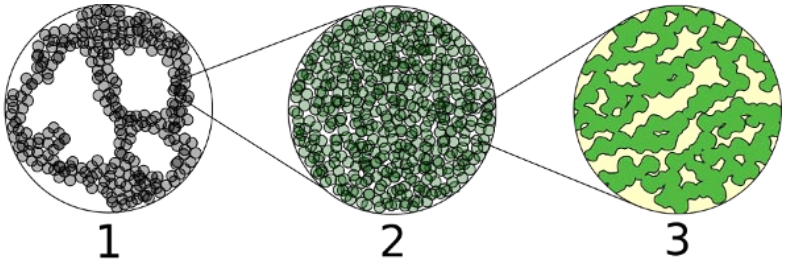
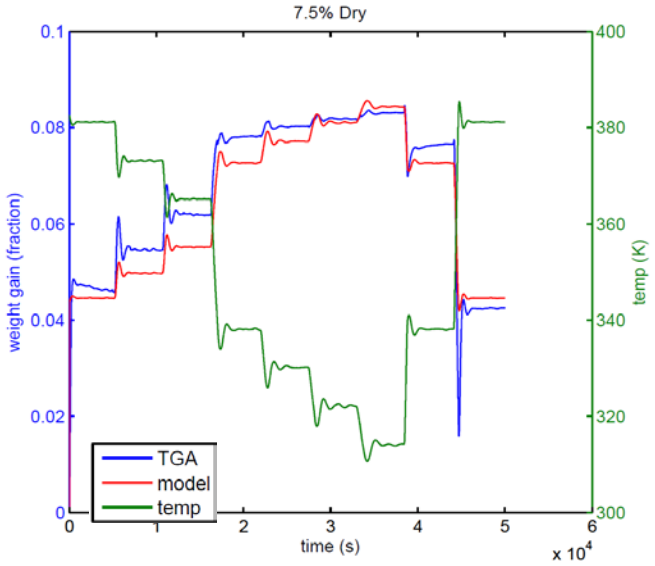
PEI-Impregnated Silica Sorbent Reaction Model

- **A general lumped kinetic model, quantitatively fit to TDA data, needed for initial CFD and process simulations**
- **High-fidelity model:**
  - Sorbent microstructure broken down into three length scales
  - Rate of reaction controlled by the diffusion of CO_2 through the amine polymer
  - Ab initio calculations indicate dependence of the diffusion process on water

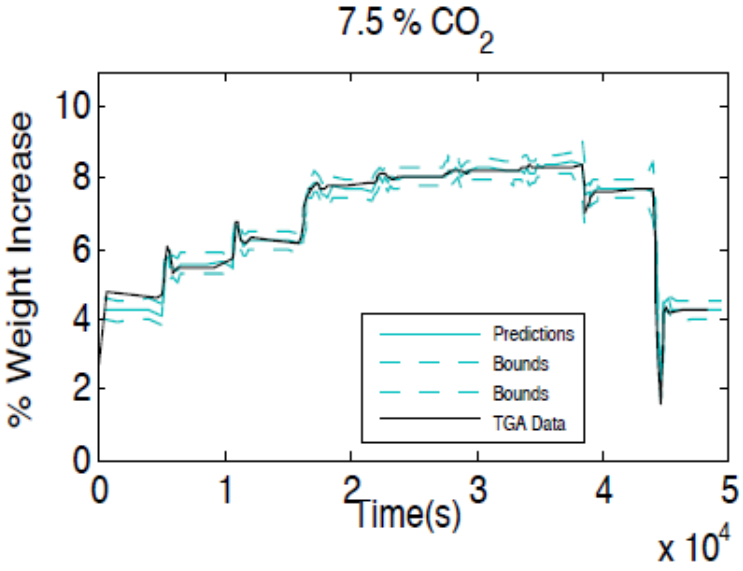
$$2R_2NH + CO_2(gas) \rightleftharpoons R_2NCO_2^- + R_2NH_2^+$$
$$R_2NH + H_2O(phys) + CO_2(gas) \rightleftharpoons HCO_3^- + R_2NH_2^+$$
$$H_2O(gas) \rightleftharpoons H_2O(phys)$$





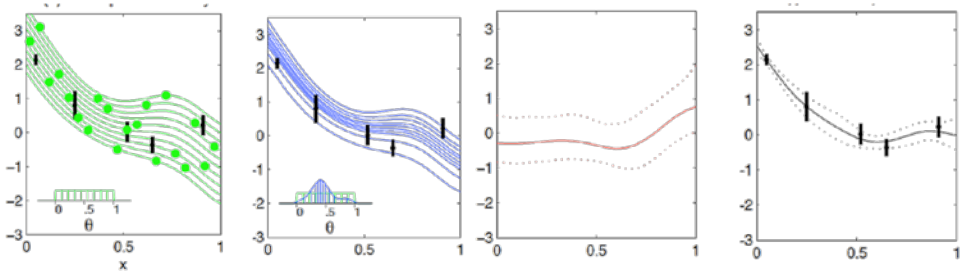
(left) lumped kinetic fit to experimental TGA for NETL-32D sorbent

(right) calibrated model with discrepancy and error bounds

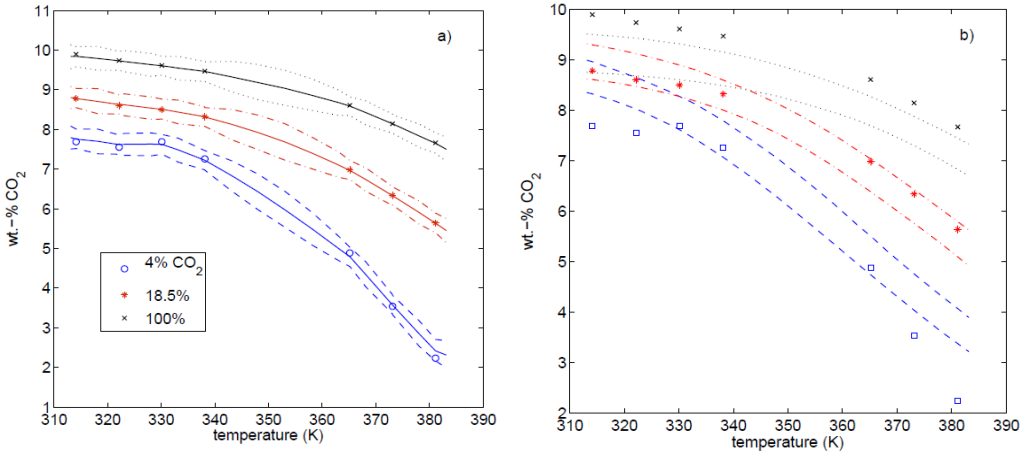


Bayesian Methods in Parameter Estimation

- *Experimental data tends to constrict the prior distribution, resulting in a experiment-based estimate influenced by theoretical calculations.*
- *A stochastic function representing the model error can also be estimated in this way.*



Above: schematic of the calibration process. Left to right: draws from the prior, draws from the posterior, discrepancy, and predictions.

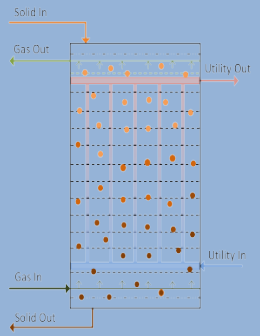


Right: model-plus-discrepancy (a) and model-only predictions (b), with confidence bounds.

Mebane DS, Bhat KS, Kress JD, Fauth DJ, Gray ML, Lee A, Miller DC., Bayesian calibration of thermodynamic models for the uptake of CO2 in supported amine sorbents using ab initio priors. Phys Chem Chem Phys. 15 (2013) 4355-66. doi: 10.1039/c3cp42963f.

CCSI Tools to develop an optimized process using rigorous models

Process Models

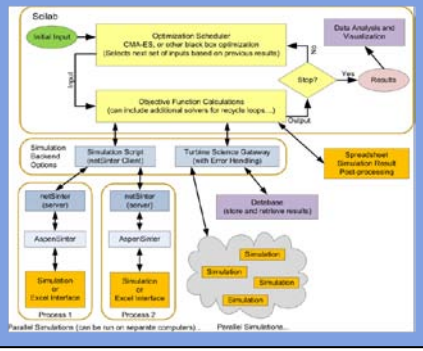


Basic Data Submodels

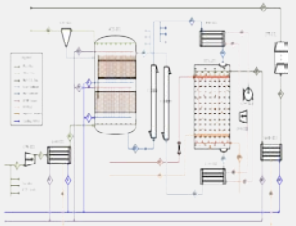
Algebraic Surrogate Models

ALAMO

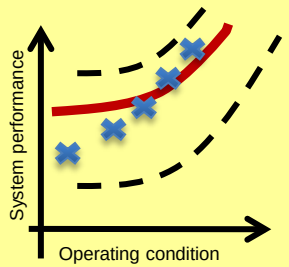
Simulation-Based Optimization



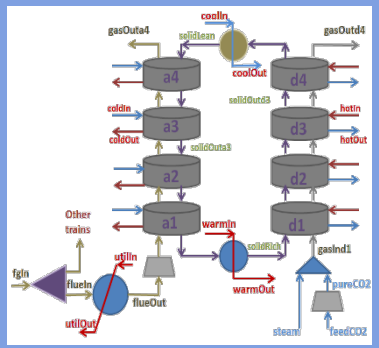
Optimized Process



Uncertainty Quantification



Superstructure Optimization (Determine Configuration)

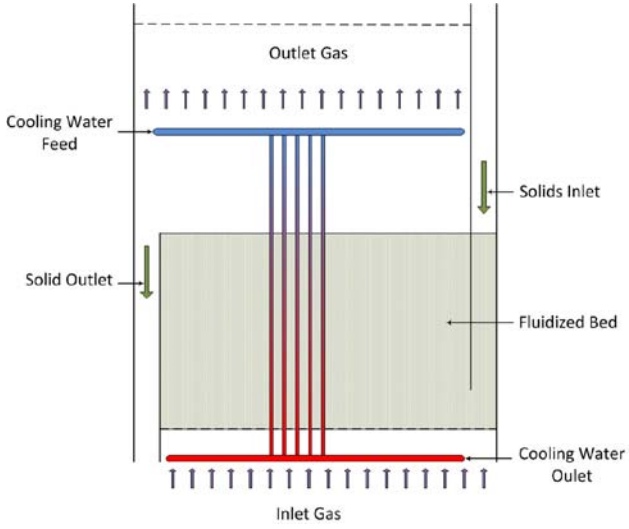


Miller, D.C.; Sahinidis, N.V.; Cozad, A.; Lee, A.; Kim, H.; Morinelly, J.; Eslick, J.; Yuan, Z. "Computational Tools for Accelerating Carbon Capture Process Development". In Proceedings of The 38th International Technical Conference on Clean Coal & Fuel Systems, Clearwater, FL, USA. June 2 to 6, 2013.

Solid Sorbent System Models

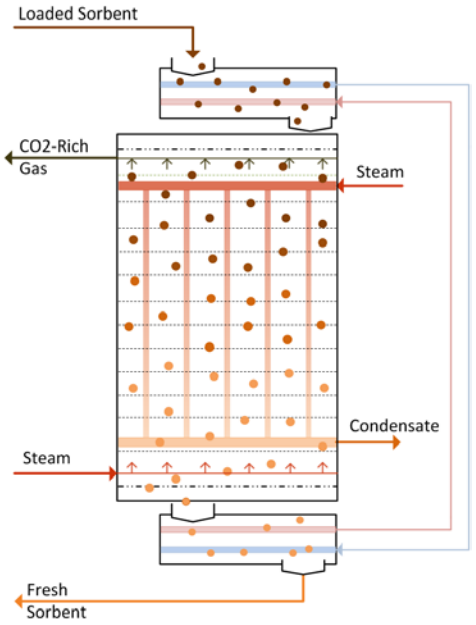
Bubbling Fluidized Bed (BFB) Models

- Flexible BFB models with immersed heat exchangers have been developed to be used as adsorber or regenerator, as needed, with varying locations for solids inlet and outlet streams
- Any number of BFB adsorbers and/or regenerators can be connected in series and/or in parallel depending on the user requirements
- A 2-stage adsorption model with customized variables suitable for incorporating UQ has been developed

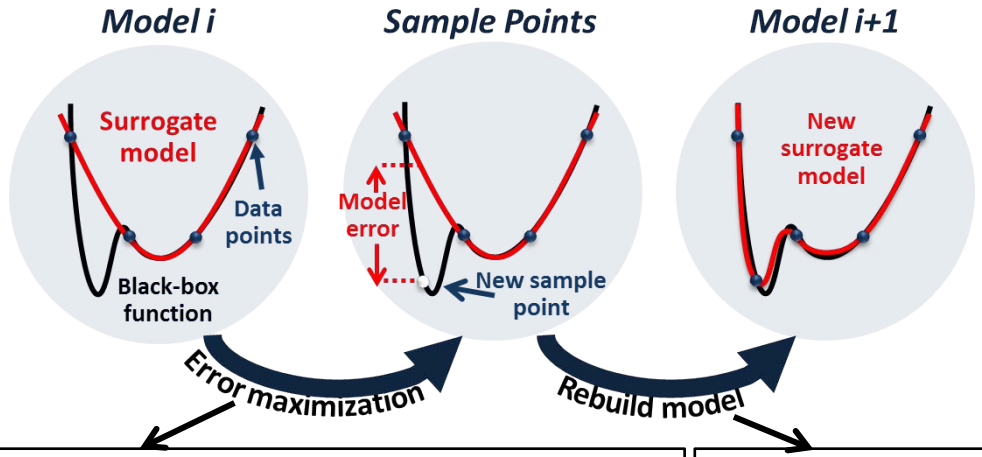


Moving Bed (MB) Models

- External resistance to mass transfer has been modeled. This is particularly important in the regenerator model due to the high operating temperature.
- Heat exchanger model, mass and heat transfer coefficients, boundary conditions, temperature specifications, and properties models are revisited for better model accuracy.



Automated Learning of Algebraic Models for Optimization



For building accurate, simple algebraic surrogate models of simulated processes

$$\max_x \left(\frac{z(x) - \hat{z}(x)}{z(x)} \right)^2$$

Surrogate model

Simulation/black-box

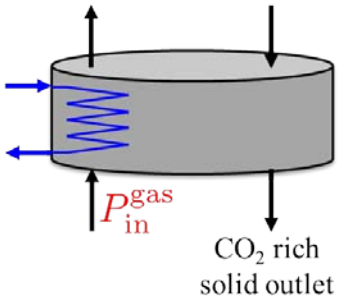
Step 1: Define a large set of potential basis functions

$$\hat{z}(x) = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_1 x_2 + \beta_4 \frac{x_1}{x_2} + \beta_5 \frac{x_2}{x_1} + \beta_6 e^{x_1} + \beta_7 e^{x_2} + \ldots$$

Step 2: Model reduction

$$\hat{z}(x) = \beta_0 + \beta_2 x_2 + \beta_5 \frac{x_2}{x_1} + \beta_7 e^{x_2}$$

Example Model: BFB Adsorber Inlet Gas Pressure



- ACM Simulation
- >900 terms possible
- 14 input variables
- 0.13% error

Pressure drop across length of bed

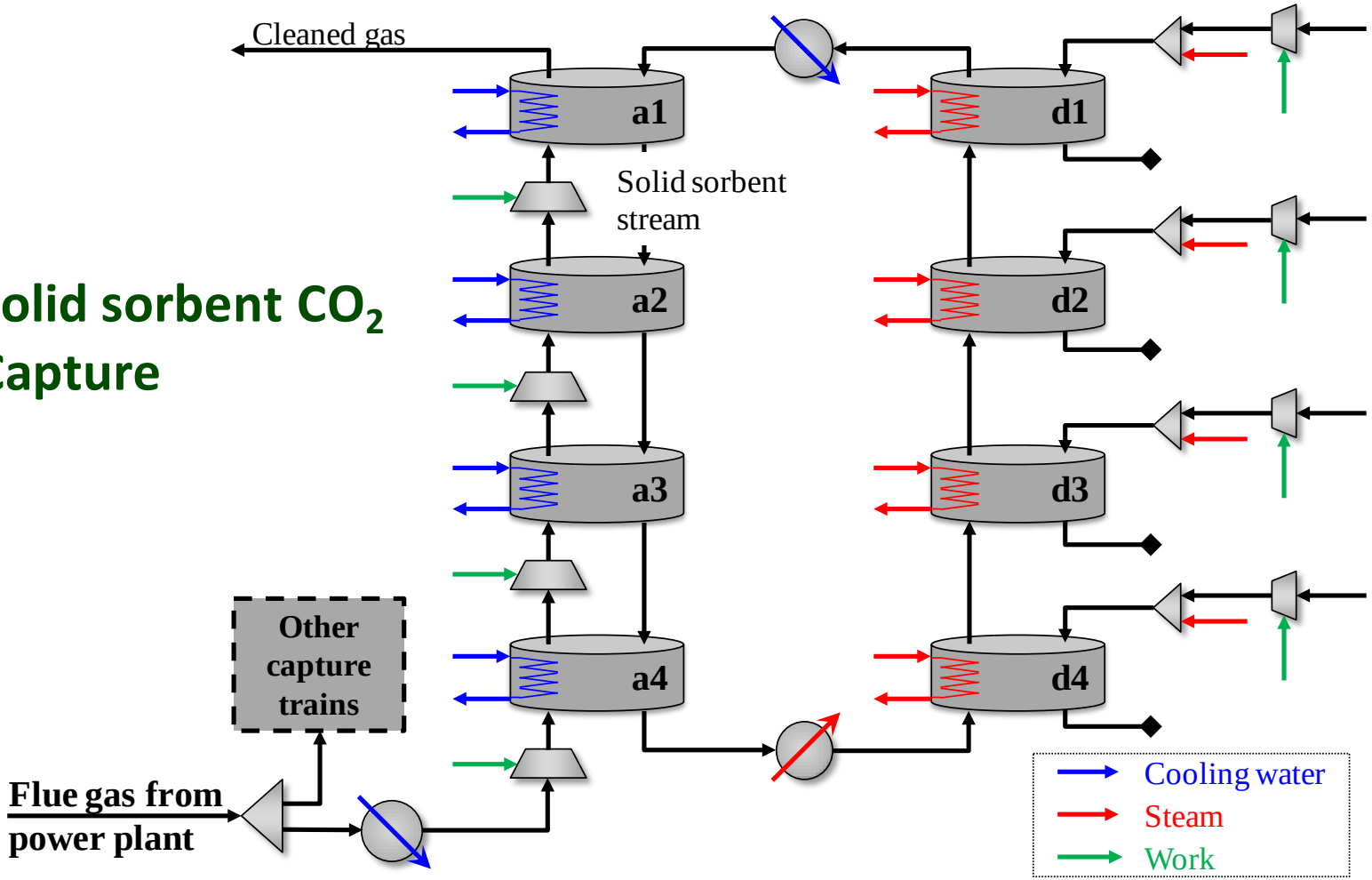
$$\hat{P}_{\text{in}}^{\text{gas}} = P_{\text{out}}^{\text{gas}} + 0.019\, L_b + 0.0055 \sqrt{D_T}$$

Proportional to outlet pressure

Pressure drop due to bed diameter

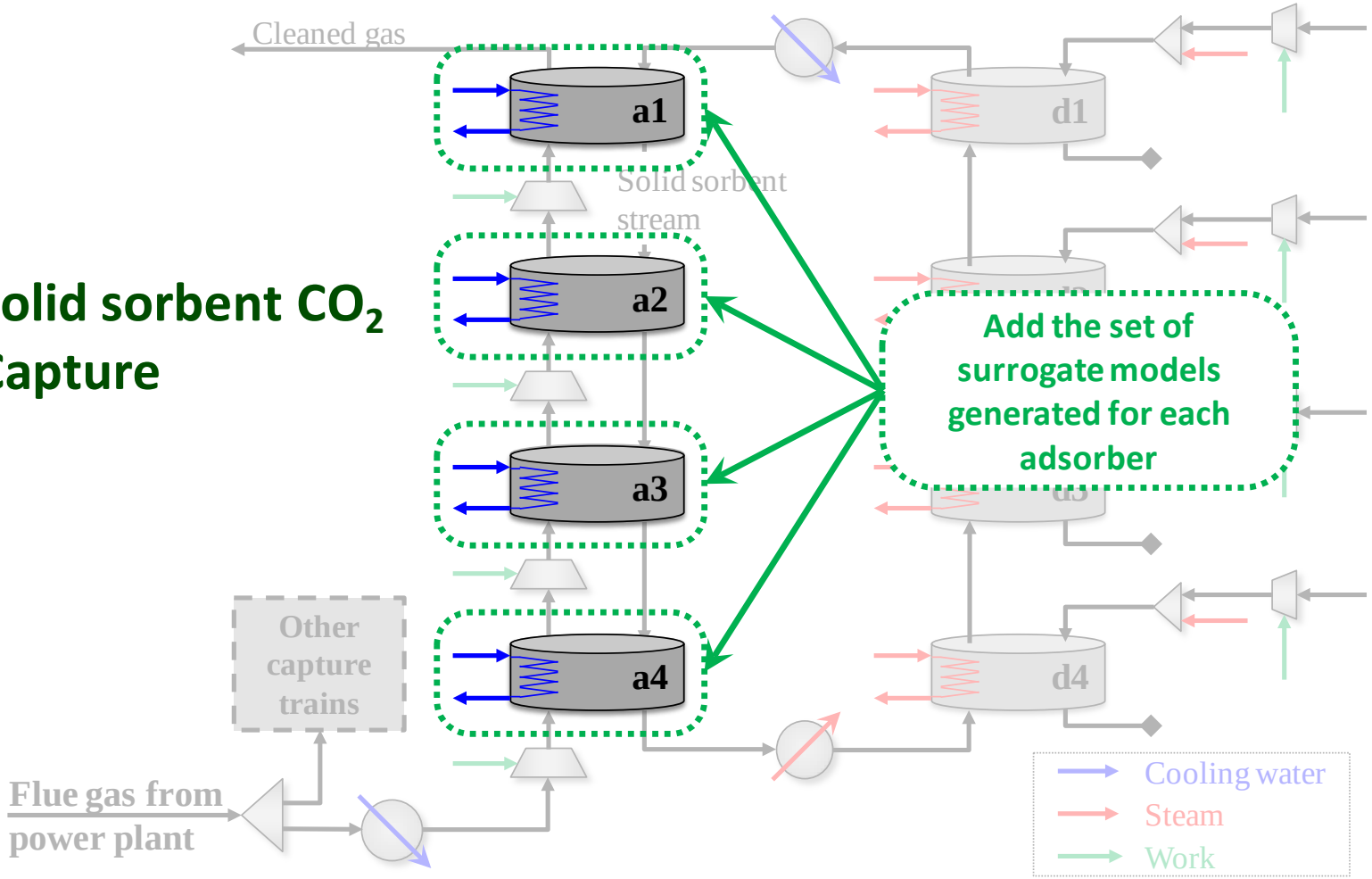
Superstructure Formulation & Optimization

Solid sorbent CO_2 Capture

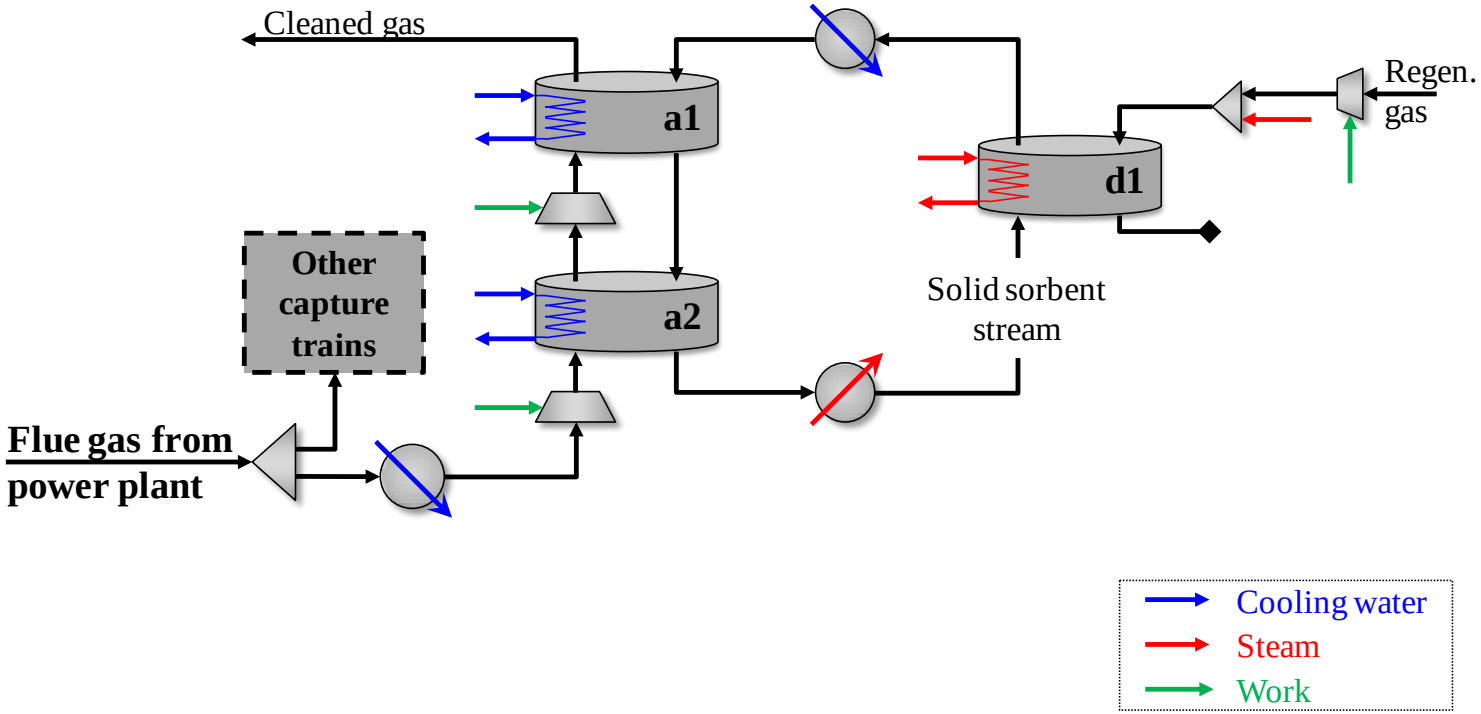


Insert Algebraic Surrogates into Superstructure

Solid sorbent CO_2 Capture

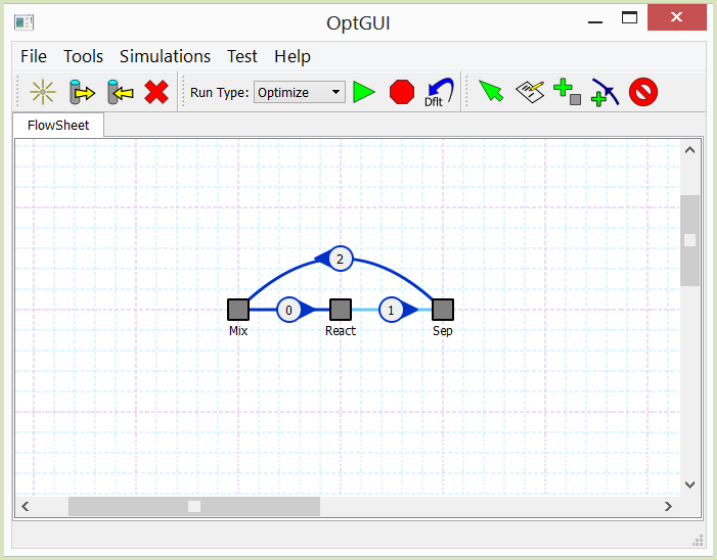


Initial Superstructure Solution



Simulation-Based Optimization Framework

Graphical Interface



Turbine Gateway

(runs simulations and stores results
can run simulations in parallel)

Optimization Engine

Derivative-free optimizer

Sample Points

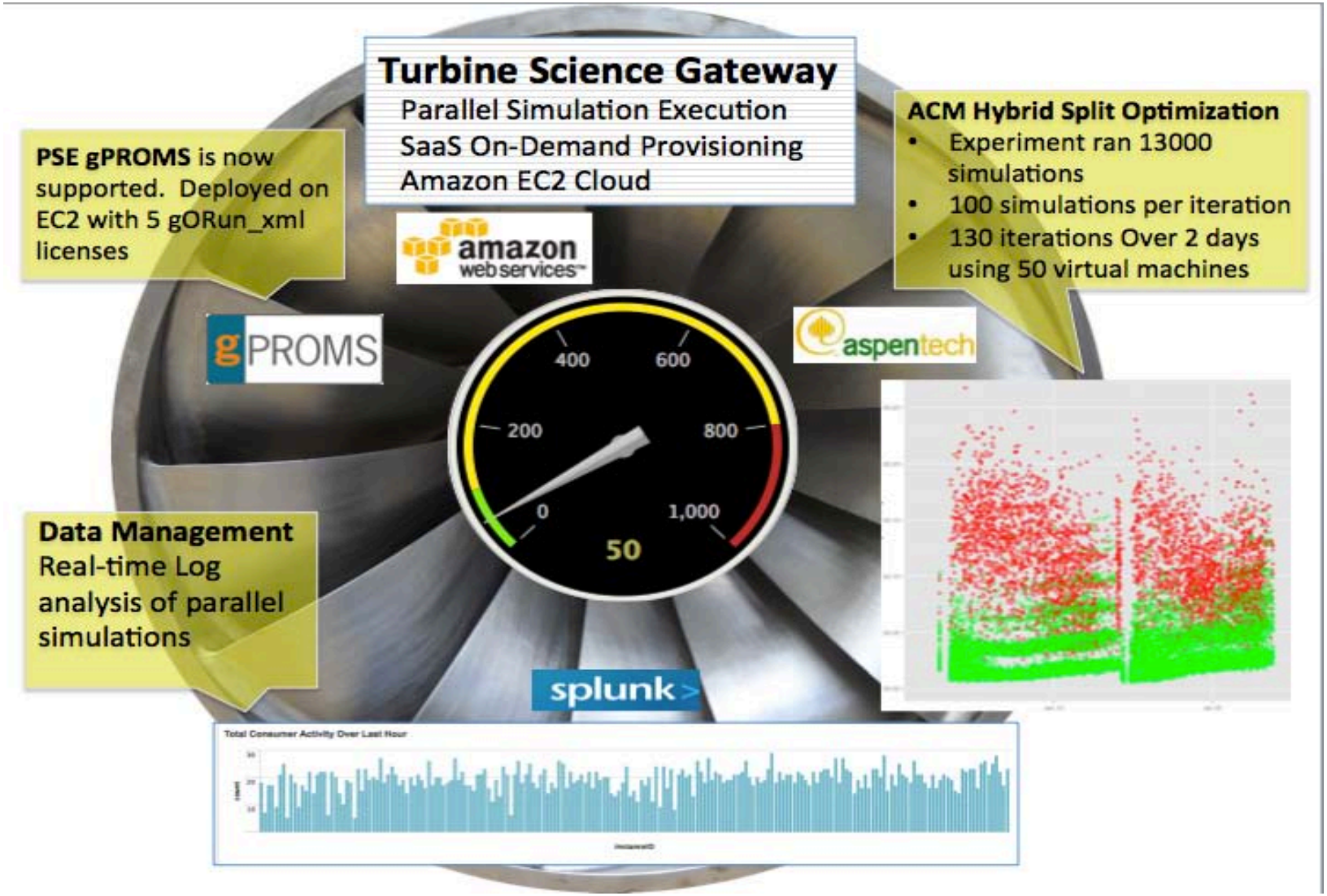
Objective Functions

Meta-flowsheet connects simulations in various software

Option for rigorous heat integration

Miller, D.C.; Sahinidis, N.V.; Cozad, A.; Lee, A.; Kim, H.; Morinelly, J.; Eslick, J.; Yuan, Z. "Computational Tools for Accelerating Carbon Capture Process Development". In Proceedings of The 38th International Technical Conference on Clean Coal & Fuel Systems, Clearwater, FL, USA. June 2 to 6, 2013.;

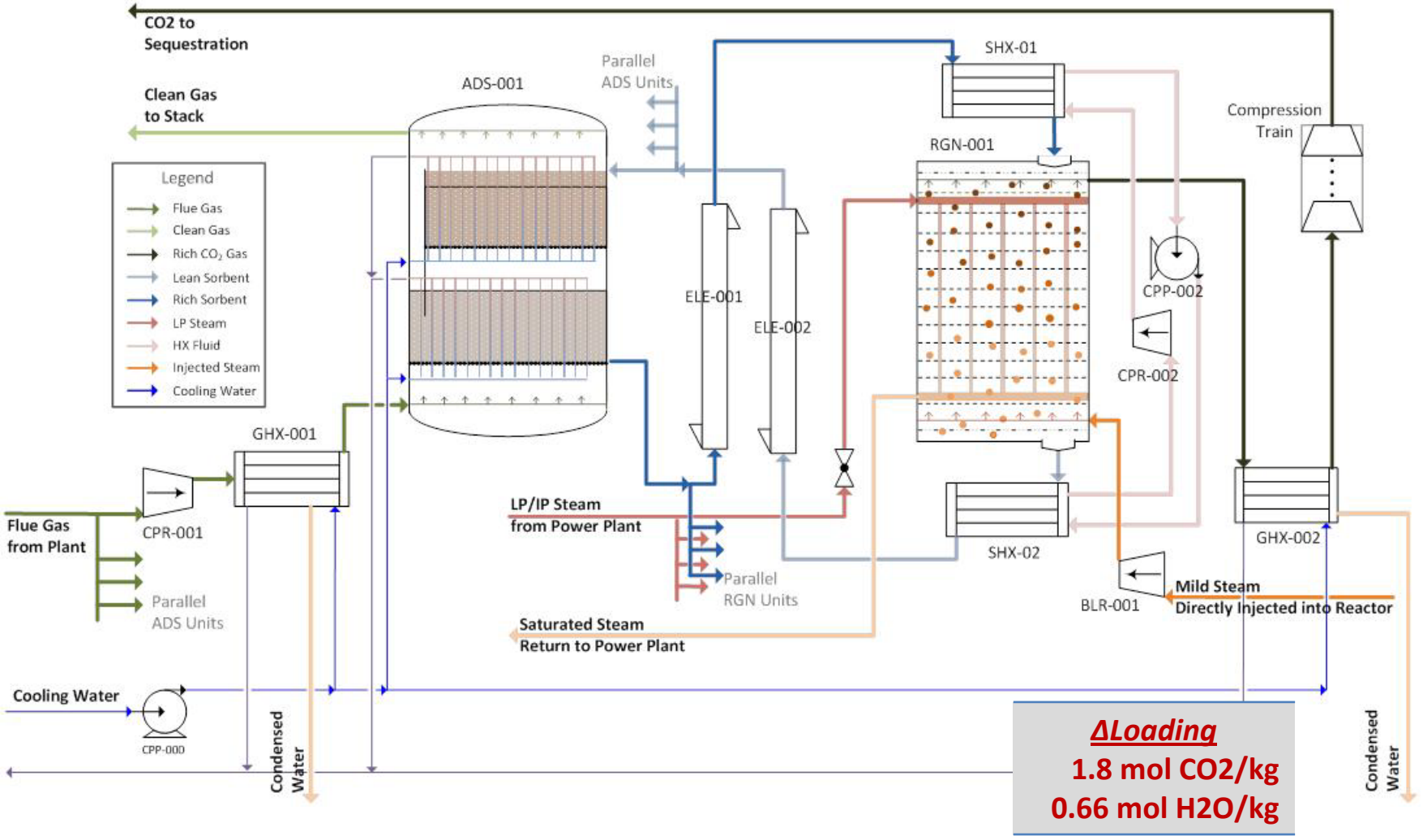
Turbine Science Gateway



Decision Variables

Input Variable	Lower Bound	Upper Bound
Adsorber Diameter (m)	7	10
Top & Bottom Adsorber Bed Depth (m)	4	10
Top & Bottom Adsorber Heat Exchanger Tube Diameter (m)	0.01	0.05
Top & Bottom Adsorber Heat Exchanger Tube Pitch (m)	0.1	0.2
Top & Bottom Adsorber Cooling Water Flowrate (kmol/hr)	30,000	60,000
Sorbent Flowrate per Adsorber (kg/hr)	350,000	600,000
Gas Pre-Cooler Temperature (°C)	40	60
Regenerator Height (m)	3	7
Regenerator Diameter (m)	6	10
Regenerator Heat Exchanger Tube Diameter (m)	0.01	0.05
Regenerator Direct Steam Injection Rate (kmol/hr)	900	1400
Regenerator Heat Exchanger Steam Flowrate (kmol/hr)	2,500	5,000

Optimized Capture Process Developed using CCSI Toolset



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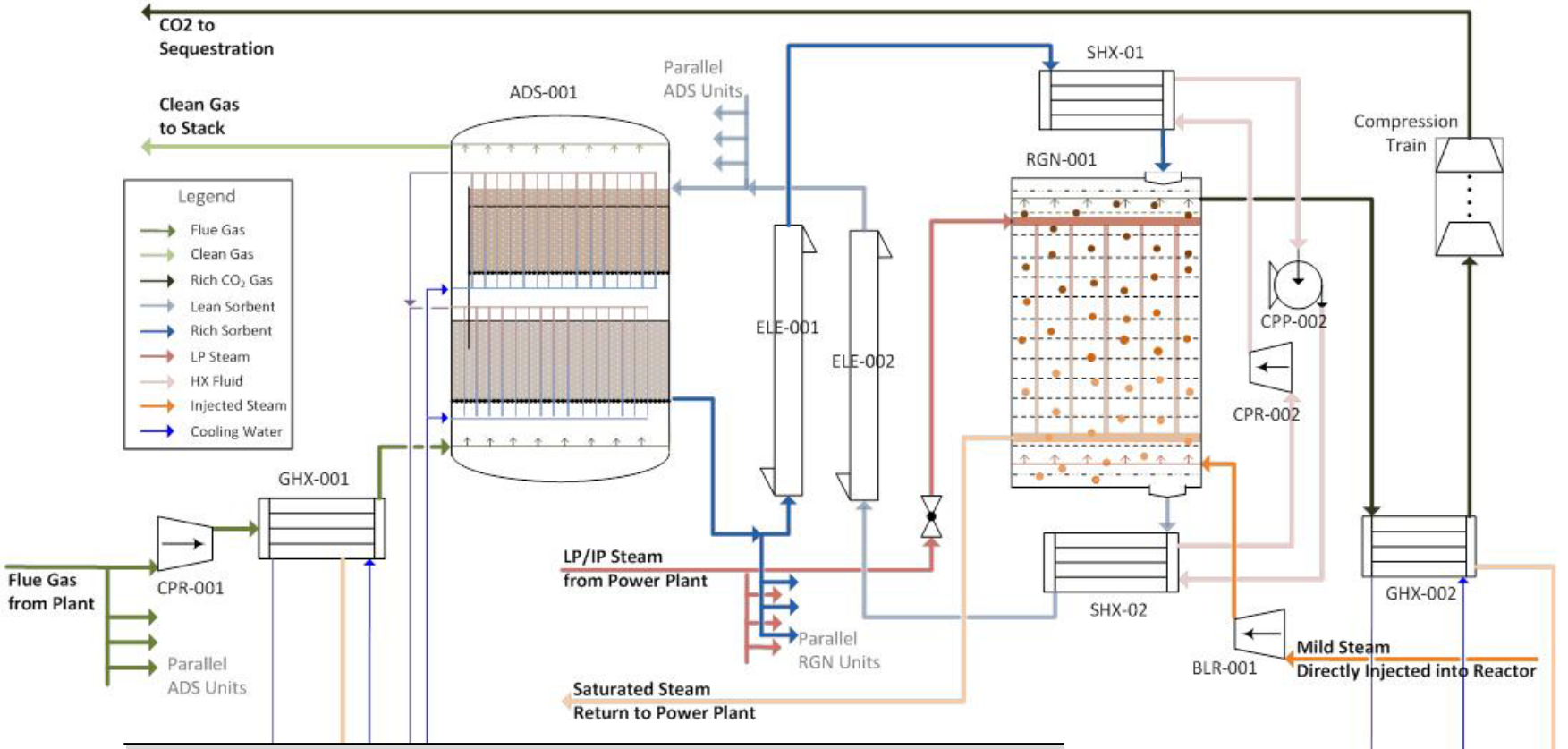
Optimized Capture Process Developed using CCSI Toolset



	Solid Sorbent	MEA (Δ10°C HX)	MEA (Δ5°C HX)
Q_Rxn (GJ/tonne CO2)	1.82	1.48	1.48
Q_Vap (GJ/tonne CO2)	0	0.61	0.74
Q_Sen (GJ/tonne CO2)	0.97	1.35	0.68
Total Q	2.79	3.44	2.90

ΔLoading
1.8 mol CO2/kg
0.66 mol H2O/kg

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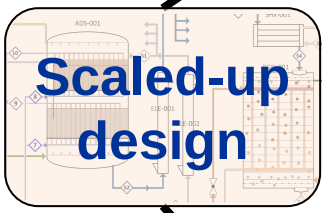
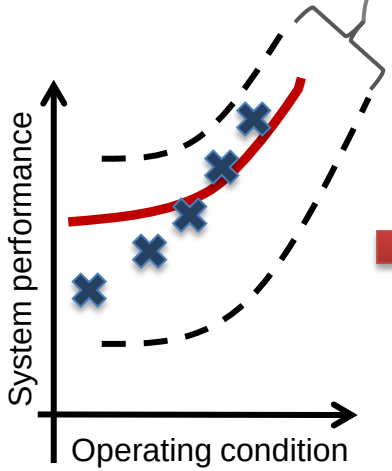
Uncertainty Quantification: How certain are we that our model can predict the system performance accurately?

- How to quantify these error bounds *a priori*?
- How to reduce these bounds?

CCSI simulation



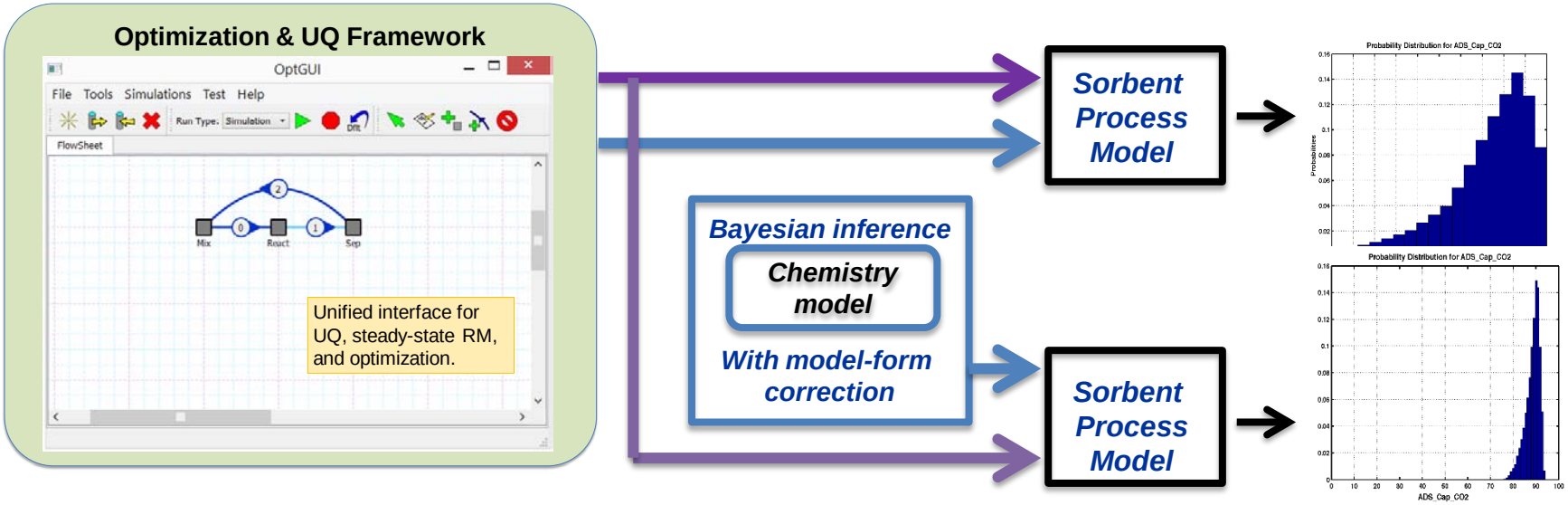
Scaled-up design



Risk analysis

How does the uncertainty in the prediction affect the risk assessment outcome?

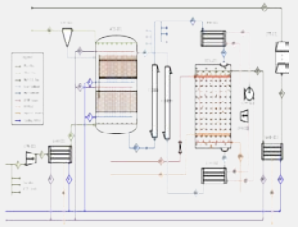
Multi-Scale Uncertainty Quantification Framework



- **UQ for basic data models**
  - Bayesian UQ methodology
  - Integration of model form discrepancy into process & CFD models
- **UQ for CFD models**
  - Adaptive sampling capability for RM/UQ
  - Bayesian calibration capability
  - UQ of discrepancy between CFD/process models
- **UQ for process models**
  - Integration with optimization platform
  - Optimization under uncertainty

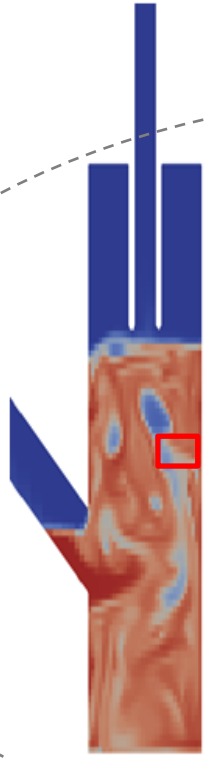
Detailed CFD Simulations of Specific Equipment

Process Models & Optimized Process

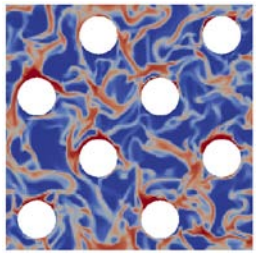


ANSYS FLUENT

Heat-transfer-tube-scale hydrodynamics

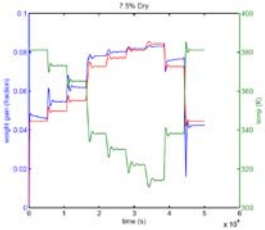


$$f^*_{drag} = \beta^* \left(-v^*_s \left| v^*_s \right| \right) + \gamma^*$$

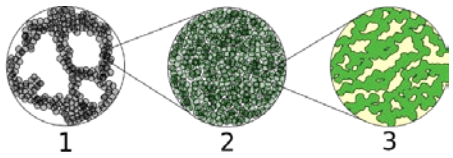


MFiX

Void Fraction along vertical center plane



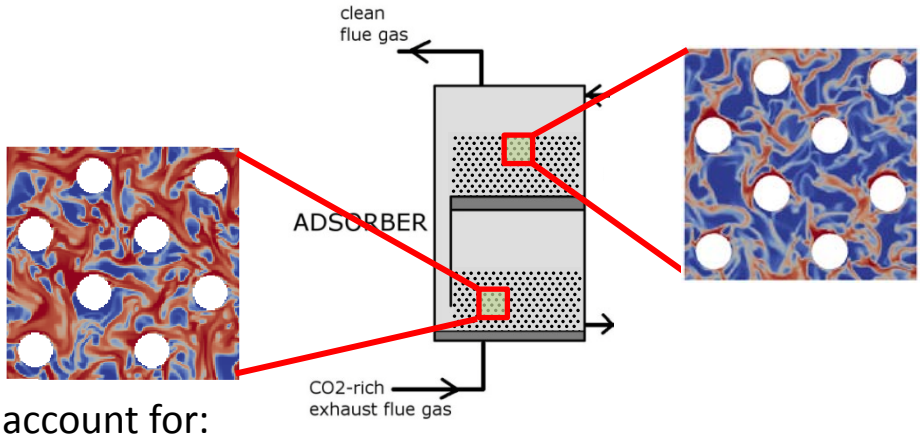
SORBENTFIT



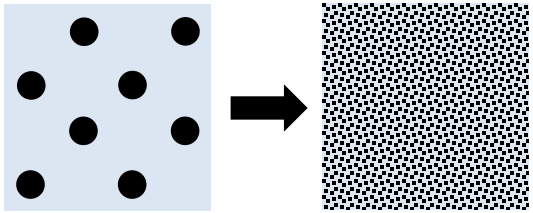
Experimental Kinetic/Mass Transfer Data

High Resolution Particle Models

- Problem: Explicit resolution of small-scale particle clusters and cooling tubes in large devices computationally infeasible!



- Solution – Develop sub-grid 'filtered' that account for:
  - Unresolved particle clusters.
  - Drag exerted by cylinders on suspension. Work well along the way for horizontal tubes

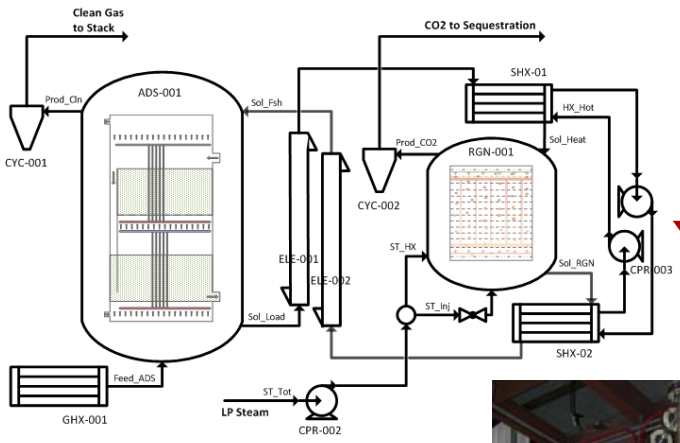


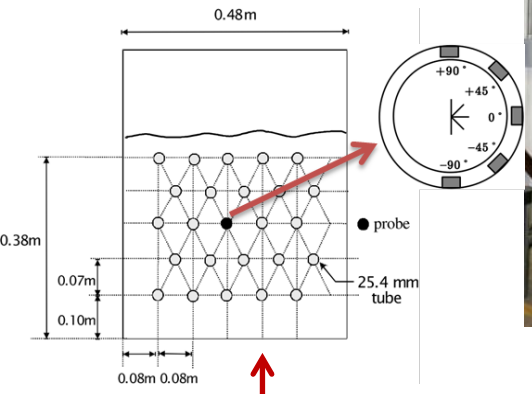
*Cylinders replaced by an **equivalent** stationary, porous medium.*

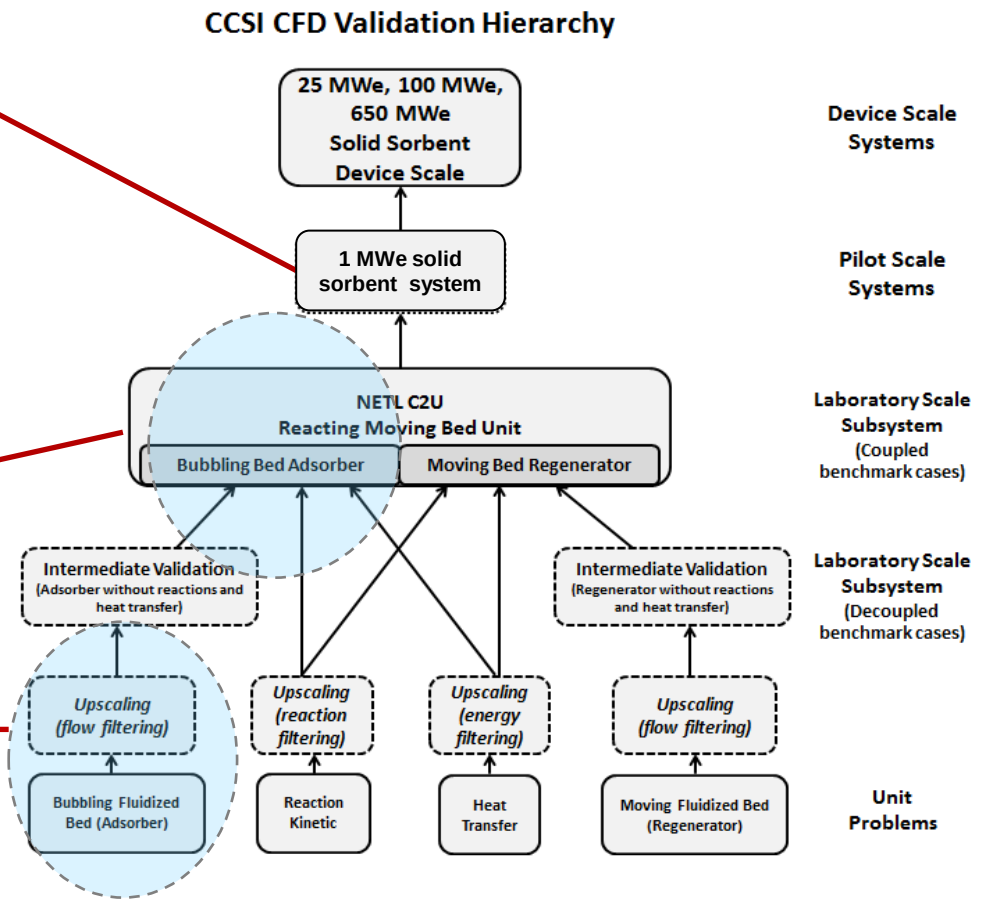
- Benefit: The sub-grid 'filtered' models can be implemented in faster, coarse-grid simulations.

Validated CFD Models at the Device Scale

Objective: To provide quantitative confidence on device-scale (CFD) model predictions for devices that are yet to be built.



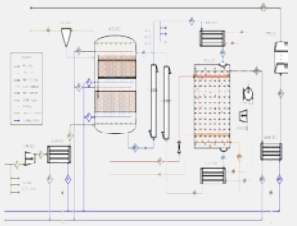




Rigorous Validation of Models

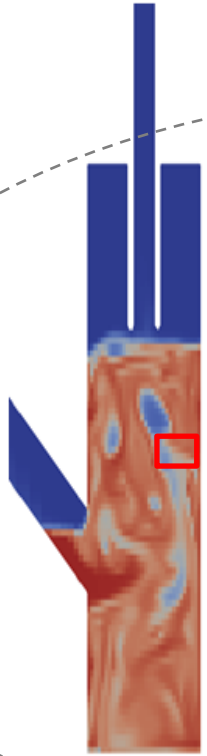
Experimental Validation

Process Models & Optimized Process



ANSYS FLUENT

Heat-transfer-tube-scale hydrodynamics



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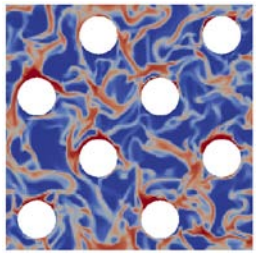

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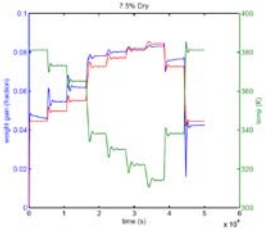
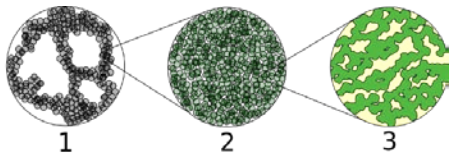
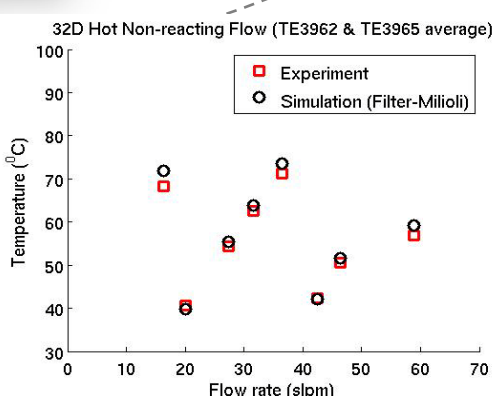


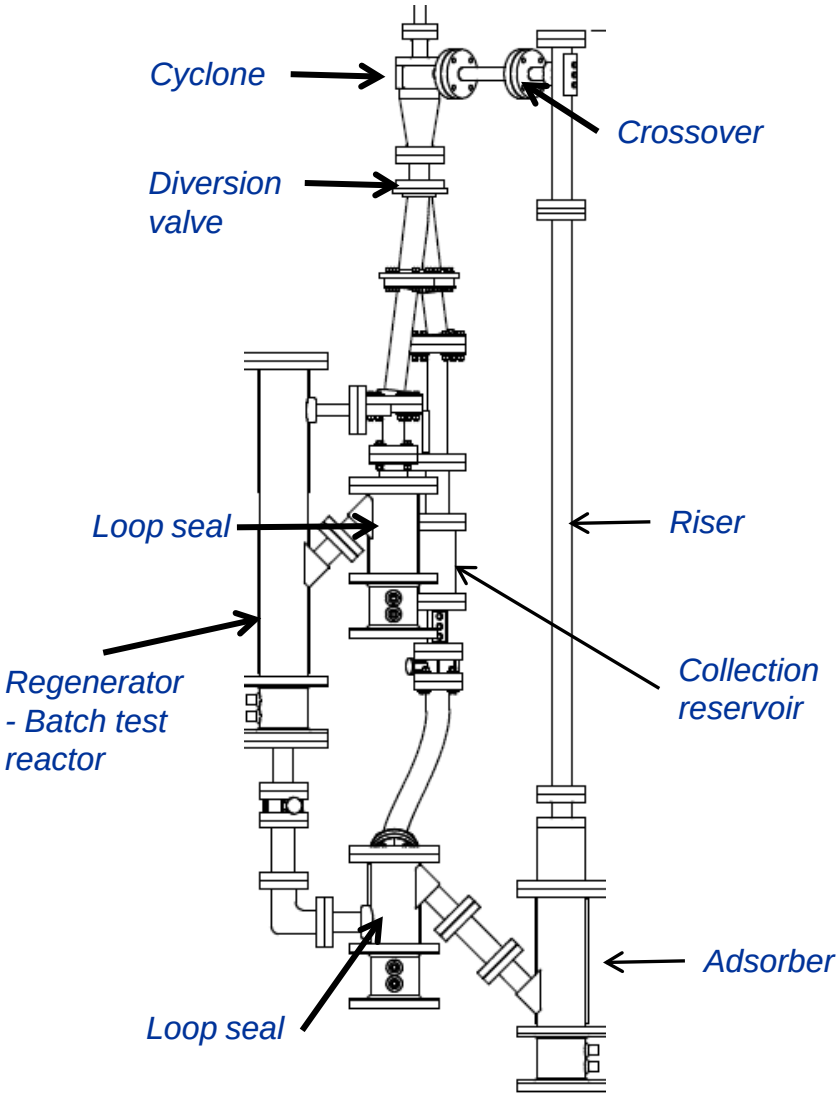
SORBENTFIT



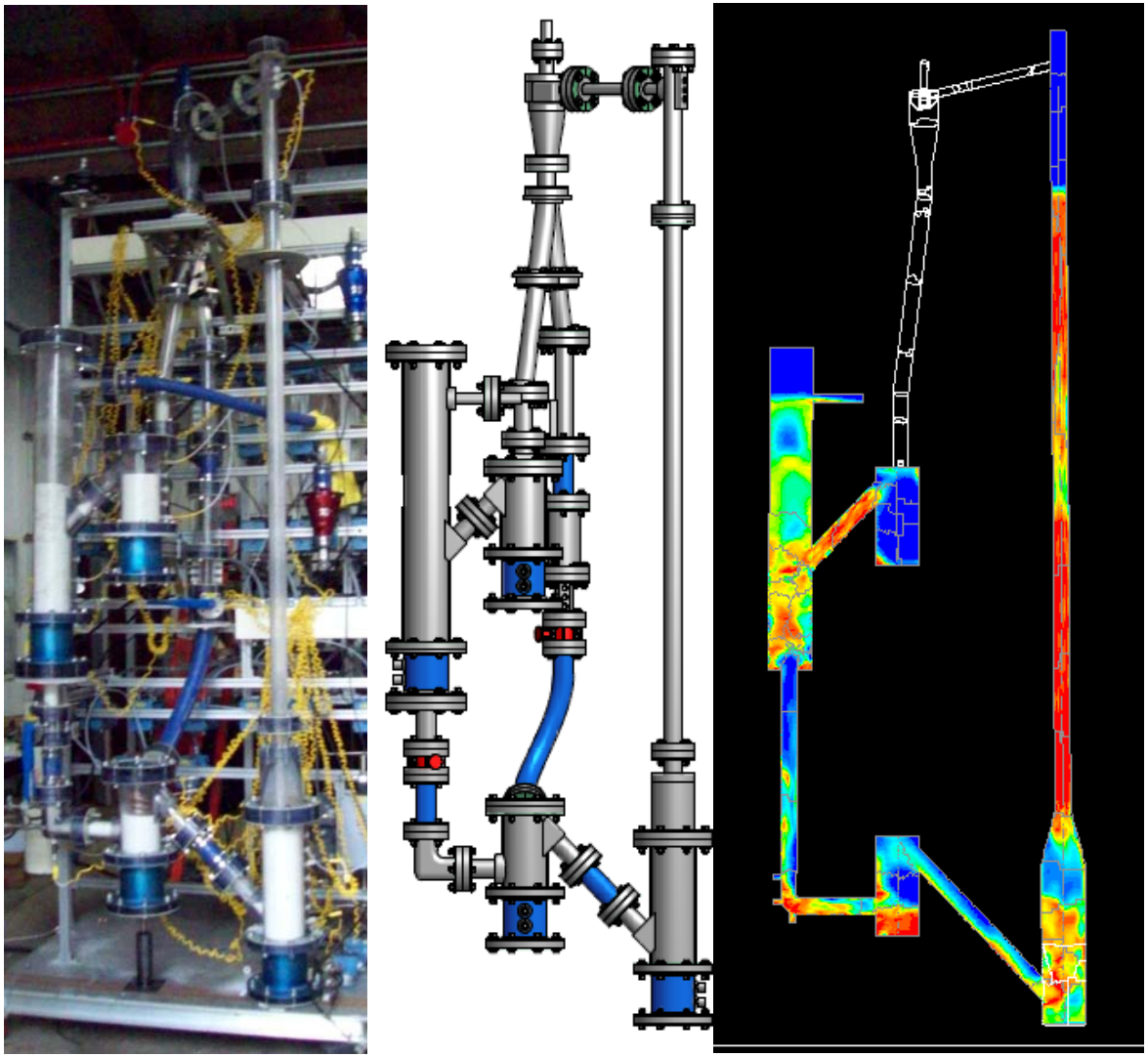
Experimental Kinetic/Mass Transfer Data



C2U and validation data



C2U and validation data



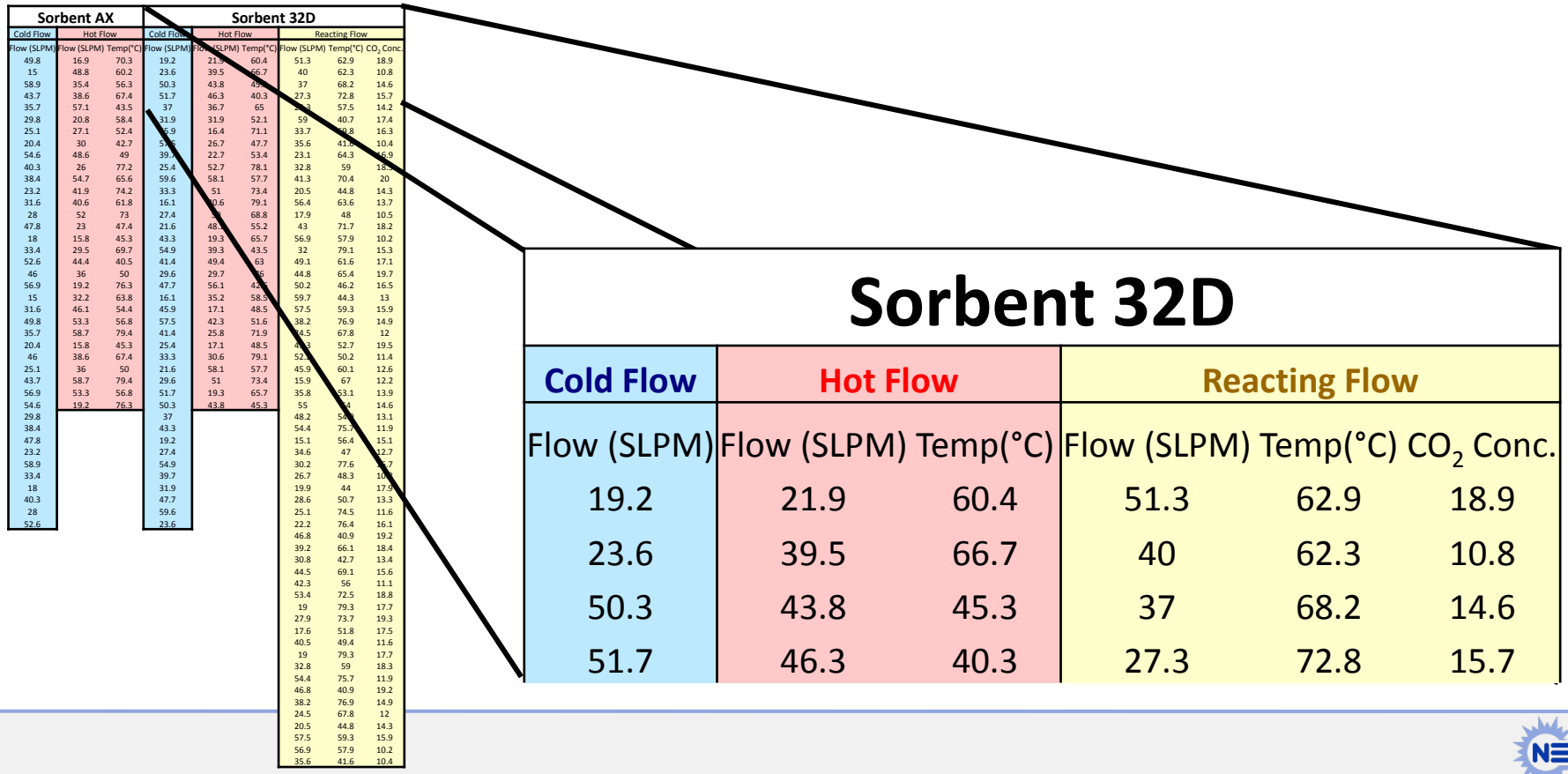
C2U Progression

1. Design and construction
2. Shakedown and modification as needed
3. Revise design drawing
4. Create system models from revised drawings

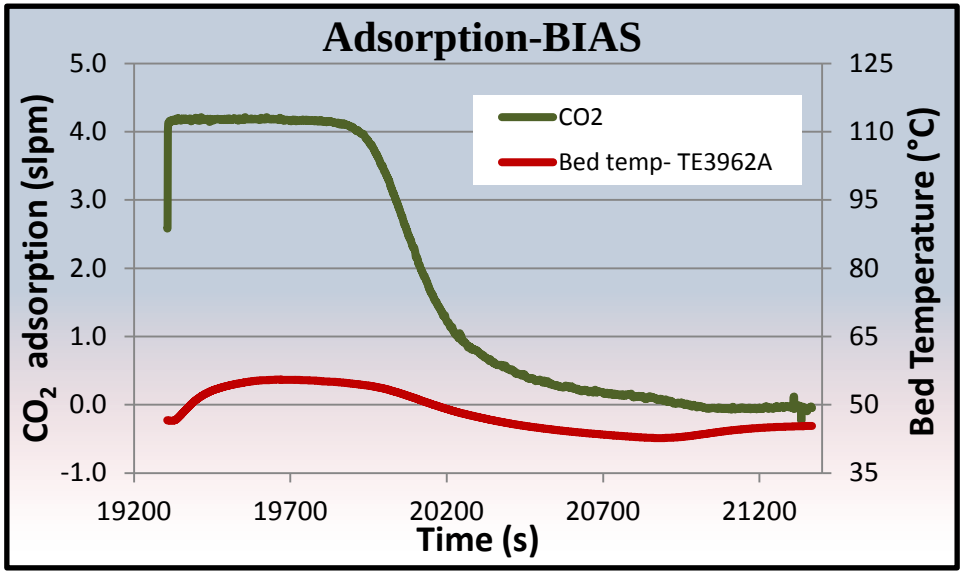
C2U and validation data

To validate individual models, three sets of tests where statistically devised and randomized

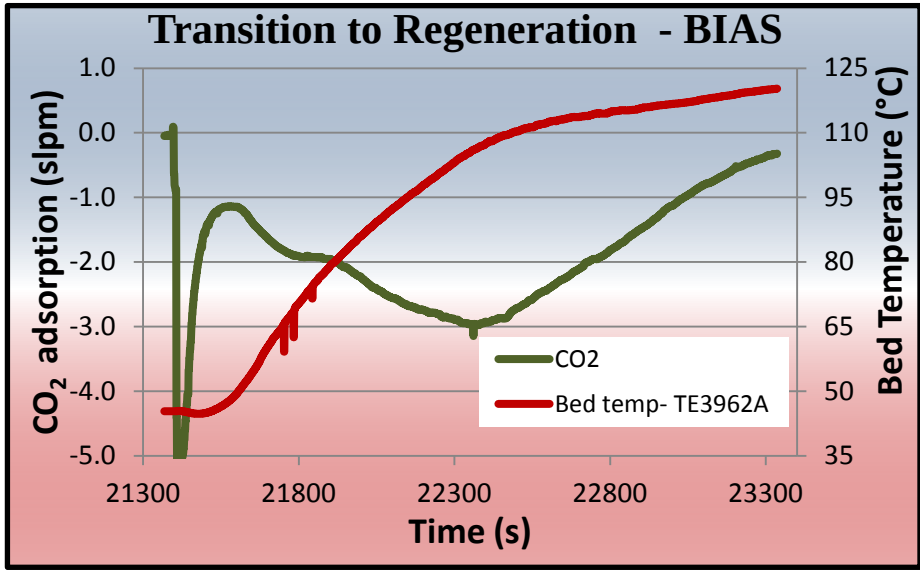
1. Cold Flow testing – hydrodynamics
2. Hot Flow testing – heat transfer, hydrodynamics
3. Reaction testing – reaction kinetics, heat transfer, hydrodynamics

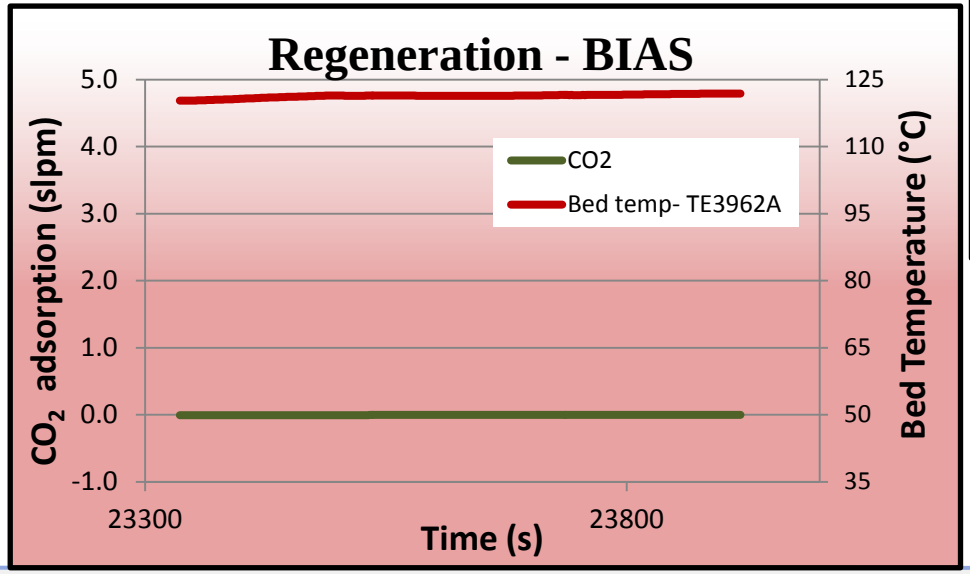


C2U Initial testing data



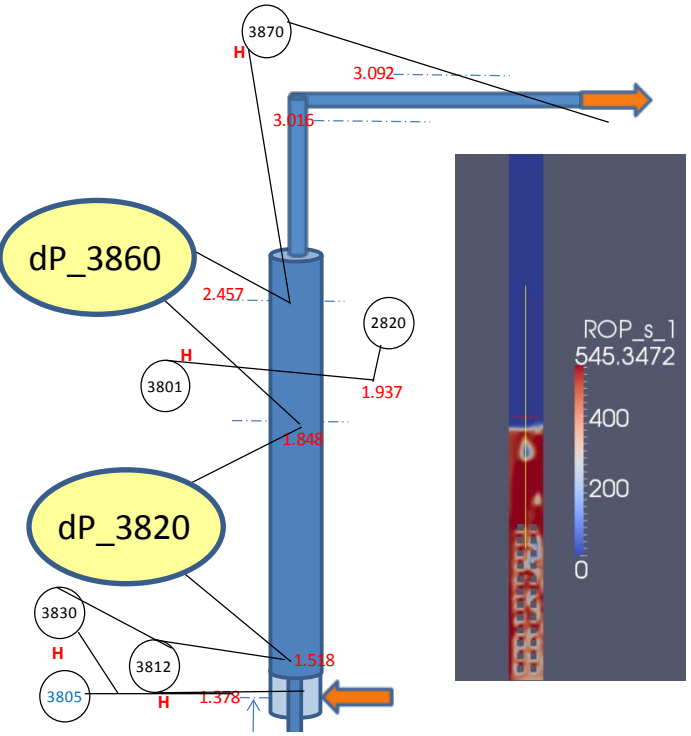
Batch test conducted in the regenerator with the BIAS sorbent



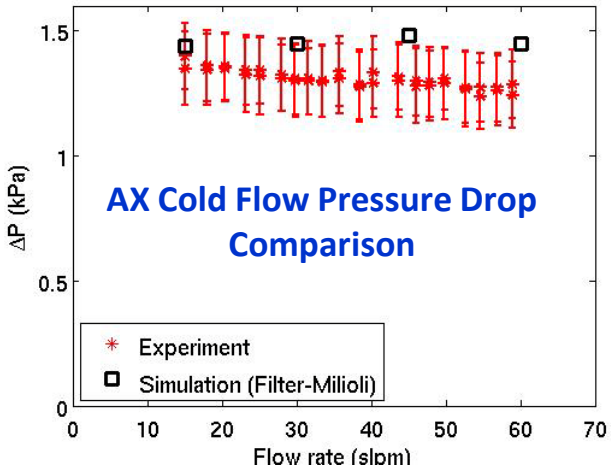


Most CO_2 is released before achieving the regeneration temperature

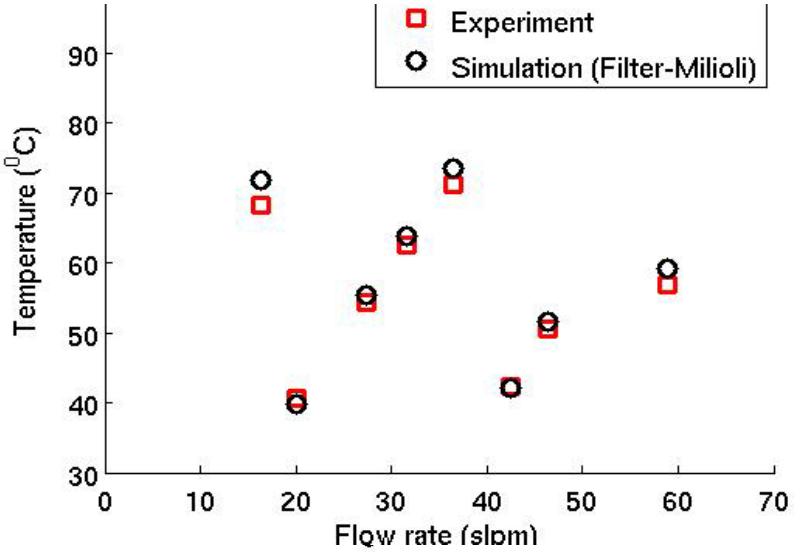
CFD Validation with C2U non-circulating Experiments

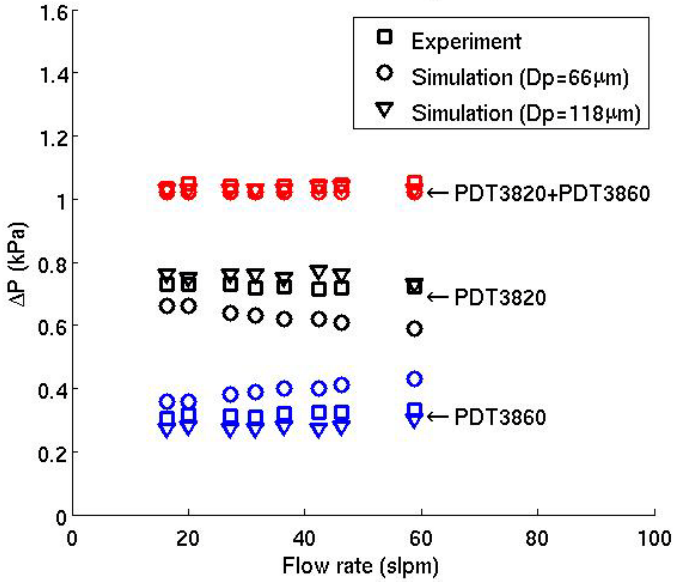


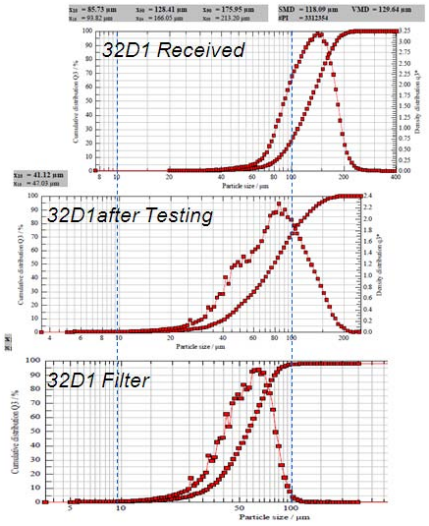
AX Cold Flow, PDT3820



32D Hot Non-reactive Flow







Conclusion

- **Coupling experimental development with simulation enables**
  - New approaches to be screened more quickly
  - Focuses development on most promising material and process conditions
- **Simulation with uncertainty quantification**
  - Focuses experimental efforts on elements with the most impact to the process/technology
- **Focused experiments for model validation enable**
  - Lower risk for scale up through quantitative confidence of model predictions

Computational Toolset Demonstration

CCSI
Carbon Capture Simulation Initiative

- **5-7 PM today in Elwood I**
  - Demonstration and detailed discussion of capabilities
- ***Sorbents, Solvents, Membranes, Oxycombustion***
- Initial toolset released Oct. 2012
  - Four (4) companies have already licensed
  - Additional releases planned for Fall 2013, 2014, 2015
  - Final release planned for Jan. 2016