

Development of SOFC Interconnects and Coatings

**J.W. Stevenson, G.G. Xia, J.P. Choi, Y.S. Chou, E.C. Thomsen,
K.J. Yoon, R.C. Scott, X. Li, and Z. Nie**

Pacific Northwest National Laboratory
Richland, WA 99352

July 26-28, 2011

12th Annual SECA Workshop

Pittsburgh, PA

Presentation Outline

- ▶ Objectives
- ▶ Background
 - AISI 441
 - Spinel coatings for steel interconnects
- ▶ Results:
 - Performance of Ce-modified MnCo spinel-coated AISI 441
 - Effect of alloy surface treatments
 - Optimization of Ce-modified MnCo spinel coatings
 - Alternative coating compositions
 - Ceramic interconnect materials
- ▶ Summary
- ▶ Future Work
- ▶ Acknowledgements

Objectives

► Global Objectives

- Develop cost-effective, optimized materials and fabrication approaches for SOFC interconnects
- Identify, understand, and mitigate degradation processes in SOFC interconnects

► Specific Objectives

- Improved understanding of performance and long-term stability of AISI 441 steel coated with Ce-modified $(\text{Mn}_{0.5}\text{Co}_{0.5})_3\text{O}_4$ spinel coating
 - ASR, oxidation behavior, scale adhesion at 800 and 850°C
 - Stack fixture testing
- Evaluation of alloy surface treatments
 - Collaborations with Allegheny Ludlum and NETL-Albany
- Optimization of Ce-modified $(\text{Mn}_{0.5}\text{Co}_{0.5})_3\text{O}_4$ spinel coatings
 - Ultrasonic spray process; effect of coating thickness
- Evaluation of cost reduction approaches
 - Reduced Co content to lower coating cost

Candidate Interconnect Alloy: AISI 441

- ▶ Ferritic stainless steel: Good CTE match to other components; Electrically conductive Cr-based oxide scale
- ▶ Inexpensive - Manufactured via conventional melt metallurgy
 - No vacuum processing required
- ▶ Similar to AISI 430, but additions of Nb and Ti improve high temperature strength and prevent formation of insulating SiO₂ layer at alloy/scale interface
- ▶ Similar to all other FSS, relatively high oxidation rate at SOFC operating temperatures (and volatility of Cr) indicates need for protective coating
- ▶ Also, relatively weak scale adherence (no RE in alloy)

Typical Analysis:

Designation	Cr	Mn	Ni	C	Al	Si	P	S	Ti	Nb	La
AISI 441	18	0.35	0.30	0.01	0.05	0.34	0.023	0.002	0.22	0.50	
AISI 430	16-18	≤1.0		≤0.12		≤1.0	≤0.04	≤0.03			
Crofer 22 APU	23.0	0.4-0.8		0.030	≤0.02	≤0.02	0.02	0.050	≤0.2		0.04-0.20

Sources: Allegheny Technologies, Inc.; Thyssen Krupp



Pacific Northwest
NATIONAL LABORATORY

Ce-modified $(\text{Mn}_{0.5}\text{Co}_{0.5})_3\text{O}_4$ Spinel Coatings

- ▶ High electrical conductivity
~60 S/cm at 800°C

$$\sigma_{\text{Mn}_{1.5}\text{Co}_{1.5}\text{O}_4} = 10^{3\sim 4} \sigma_{\text{Cr}_2\text{O}_3}$$

- ▶ Good CTE match to FSS and anode-supported cells

$$\text{CTE}_{\text{Mn}_{1.5}\text{Co}_{1.5}\text{O}_4} \cong 11 \times 10^{-6} \text{K}^{-1}, 20 - 800^\circ\text{C}$$

- ▶ Chemically compatible with contact pastes, cathodes
- ▶ Cr-free composition
- ▶ CeO_2 inclusions improve scale adhesion of alloy substrate (rare earth effect)
- ▶ Reaction-sintering process developed at PNNL increases coating density at low processing temperatures

Coating provides:

Reduced Cr volatility from steel

Improved scale adhesion

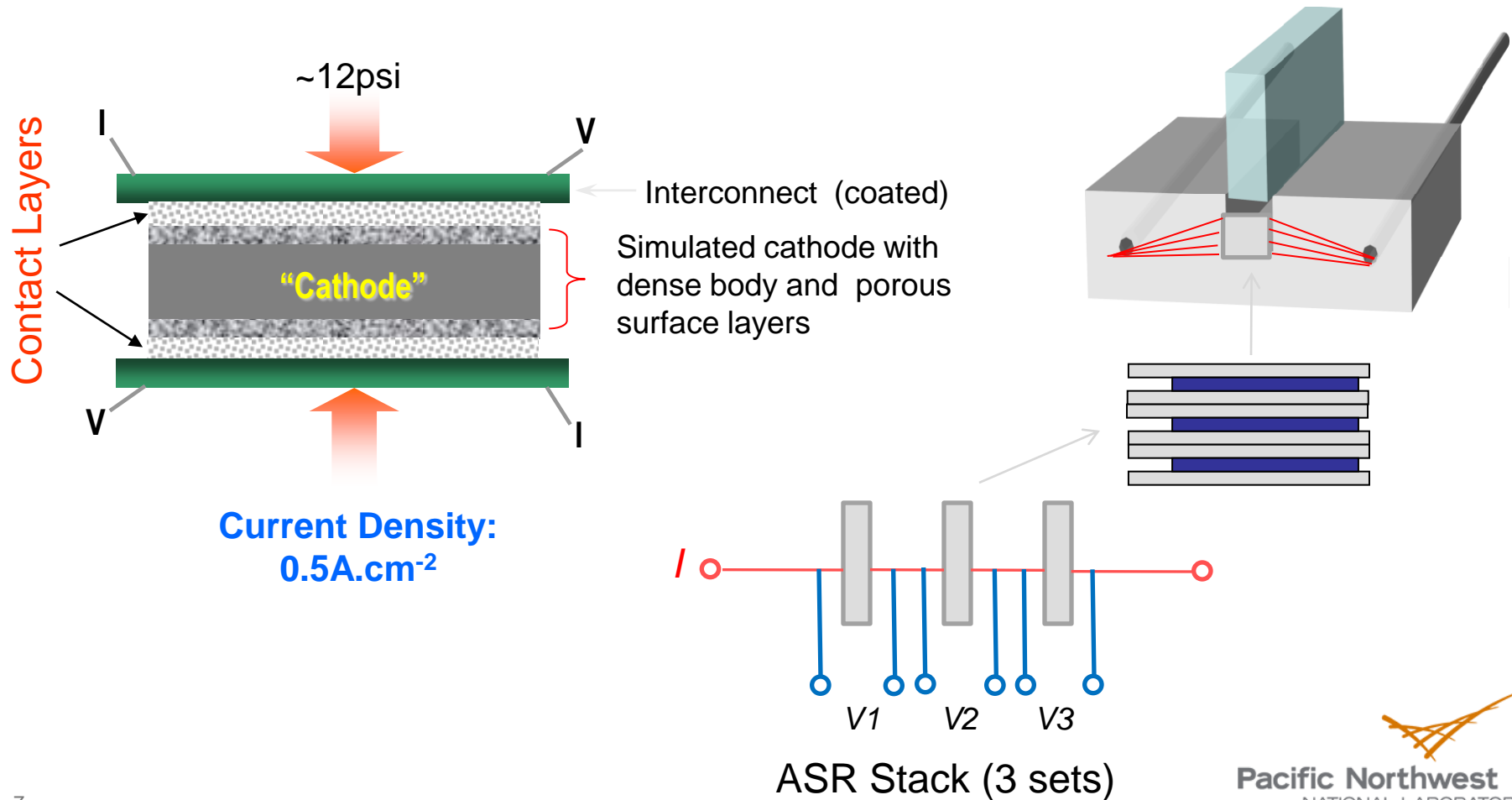
Reduced oxidation rate of alloy:

k_p ($\text{g}^2/\text{cm}^4\text{-s}$)	800°C	850°C
Ce-MC coated 441	2×10^{-14}	1×10^{-13}
Bare 441	5×10^{-14}	3×10^{-13}

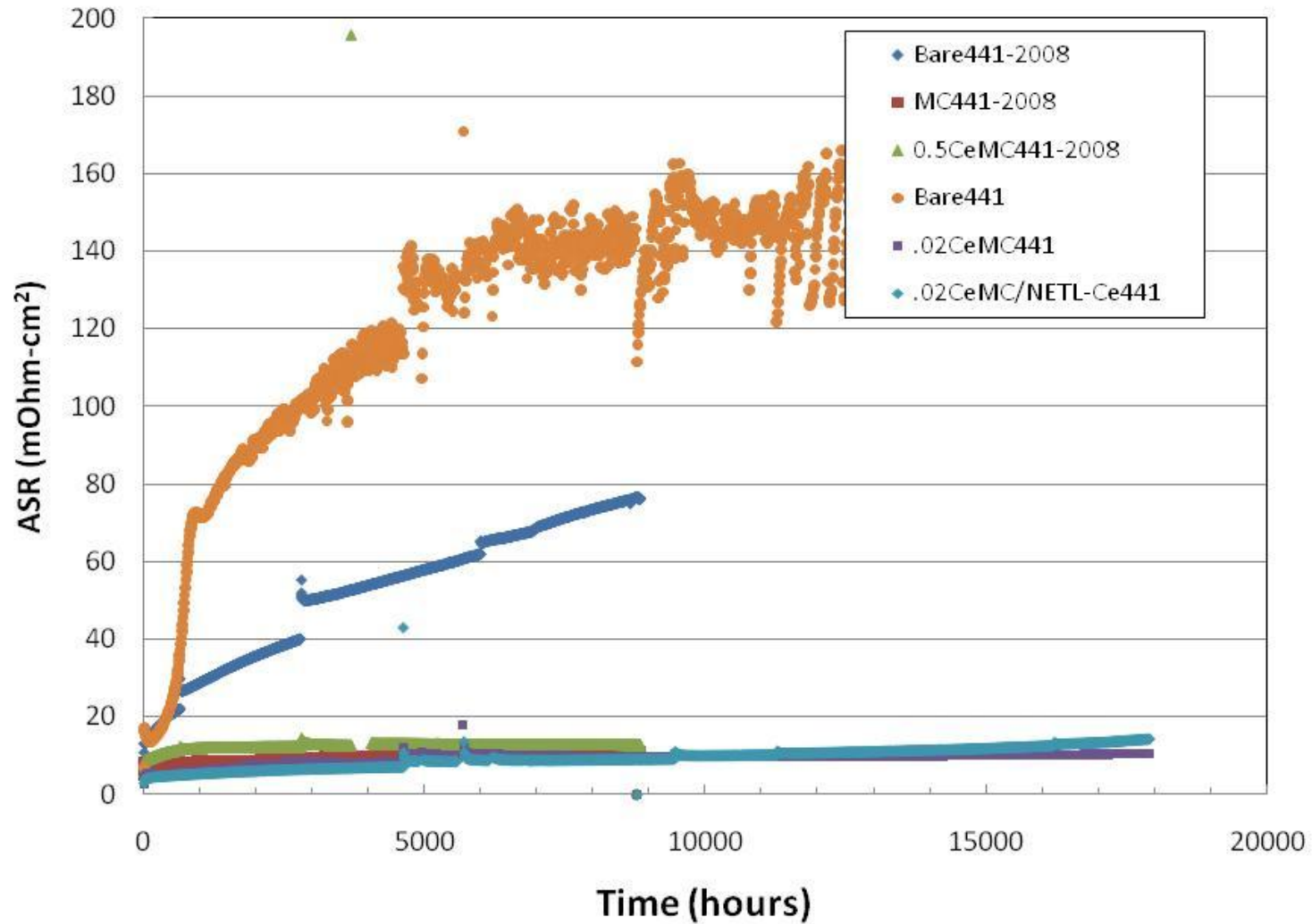
Performance of Ce-modified $(\text{Mn}_{0.5}\text{Co}_{0.5})_3\text{O}_4$ spinel coatings on AISI 441 steel

Area Specific Resistance (ASR) Measurements

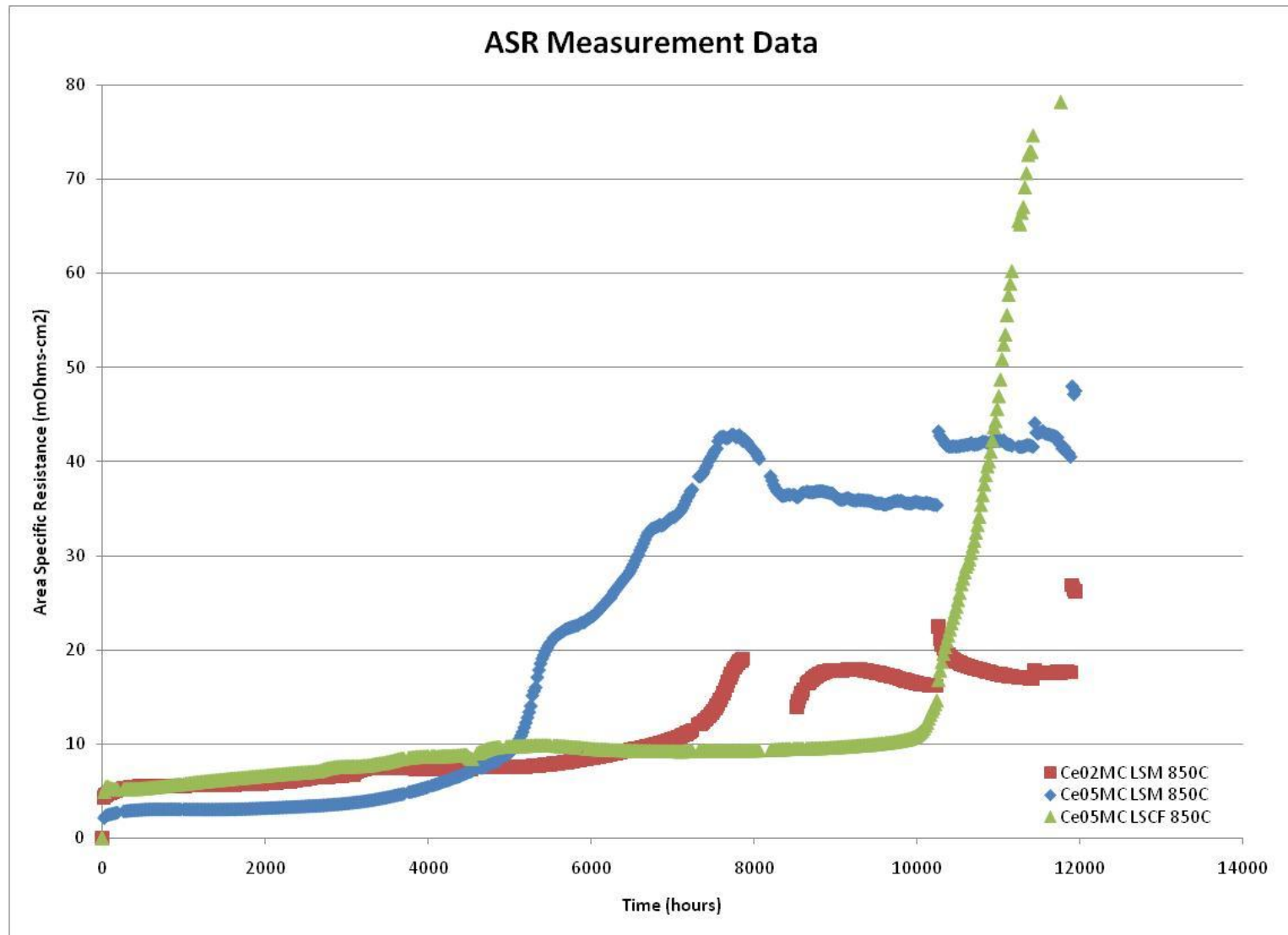
$$ASR_{cathode-interconnect} = \Phi(scale, contactmaterial, coatings)$$



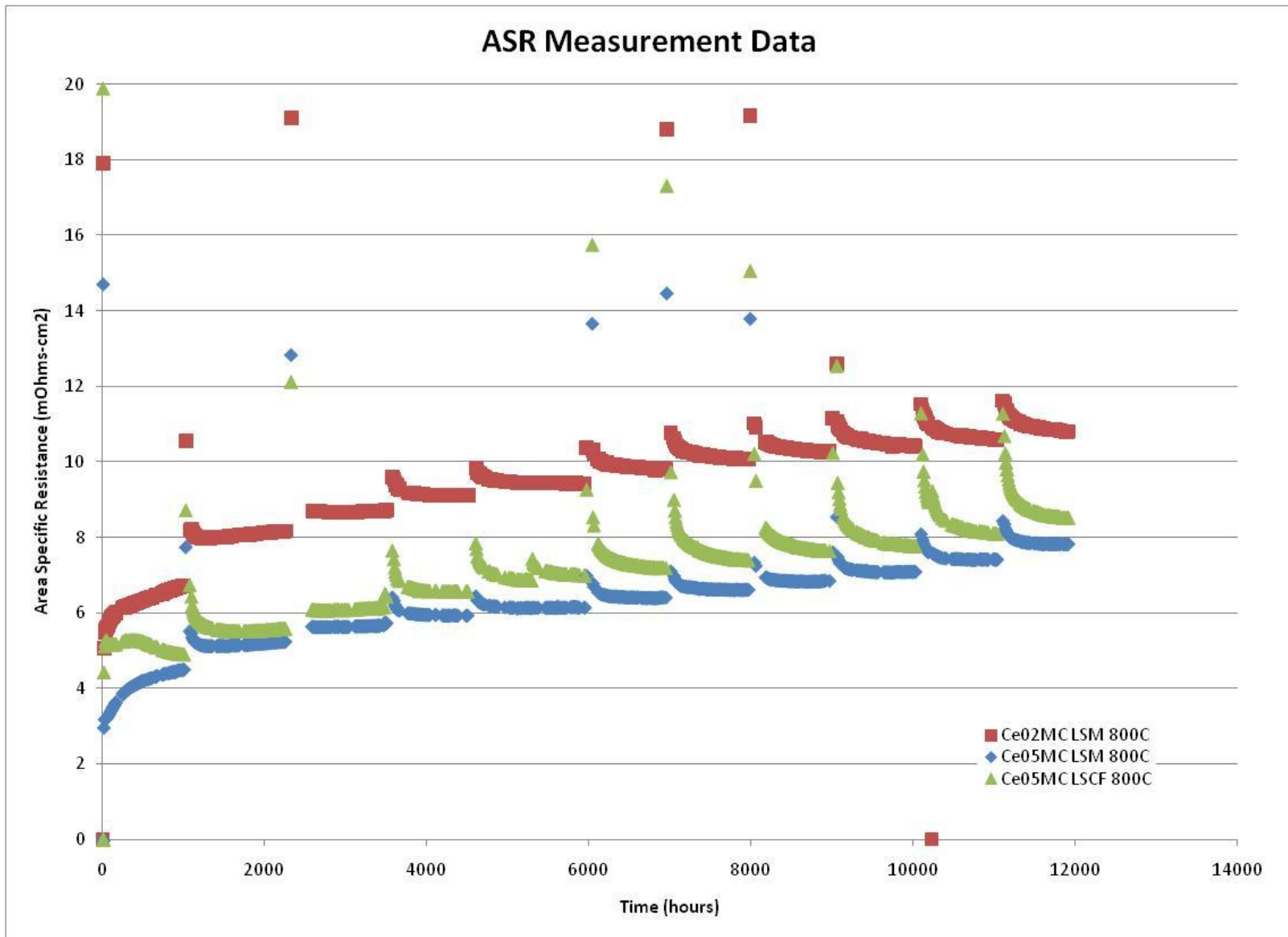
Long-Term ASR measurements: 800°C



Long-Term ASR measurements: 850°C



Long-term testing at 800°C w/ deep thermal cycle every ~1000 hours



Surface Modifications to AISI 441

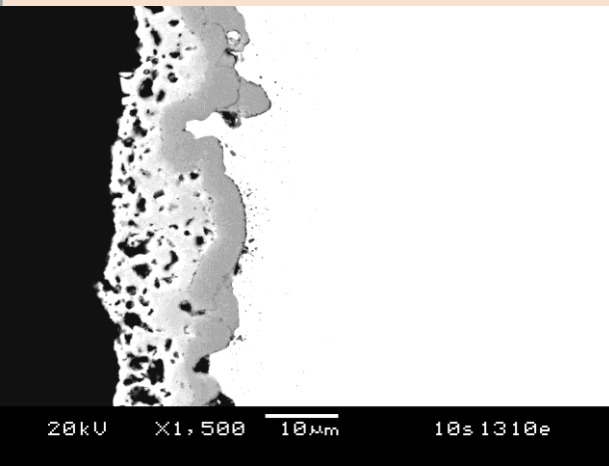
- Goal: Improve long-term scale adhesion under spinel coating
- Provided by Allegheny Ludlum:
 - 1. Mill reference (as would be provided to a customer without any additional modifications)
 - 2. Desiliconized (treatment to sequester silicon from the near surface of the sheet; an alternative to decreasing Si content of alloy)
 - 3. Surface blasted (abrasion/peening resulting in surface deformation)
 - 4. Surface ground (rough surface abrasion resulting in surface deformation)
 - 5. Temper rolled (cold rolling process resulting in through-thickness deformation)
- 0.020" thick coupons coated with Ce-MnCo spinel, heat-treated in air at 800 or 850°C; 16 coupons for each condition
- Study is in progress
 - Interim report was sent to SECA industry representatives in February, 2011

Effect of Surface Condition on Oxidation/Spallation Behavior of Spinel-coated 441 (800°C)

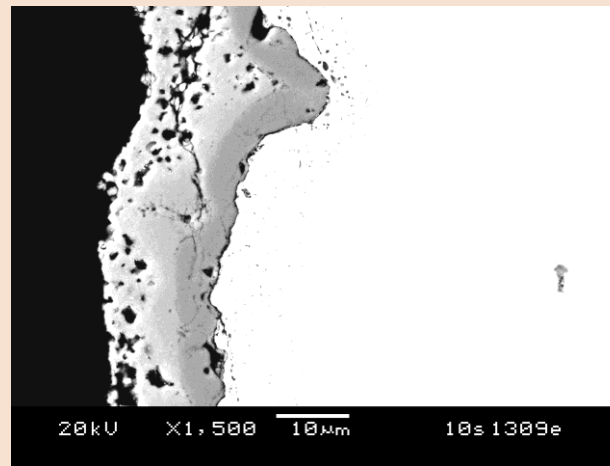
- ▶ 2000 hours
 - No spallation
- ▶ 4000 hours
 - Spallation observed on 1 mill reference coupon
- ▶ 6000 hours
 - Spallation on all except 1 one of the mill reference coupons, also 1 desiliconized coupon
 - De-bonding at scale/alloy interface observed in mounted temper-rolled coupon
- ▶ 8000 hours
 - Last of the mill reference coupons spalled, others were OK
- ▶ 10000 hours
 - No further spallation



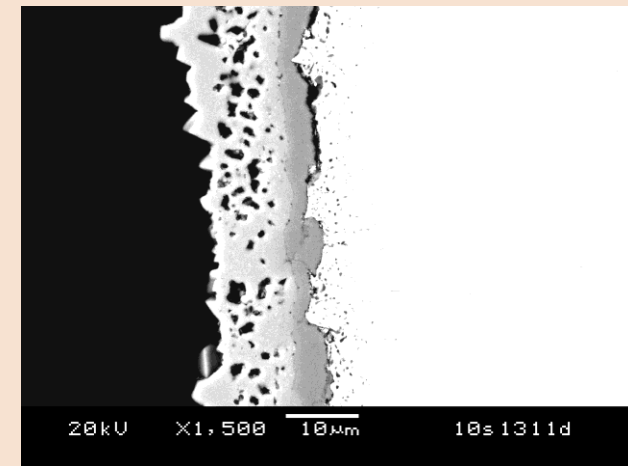
6000 h, 800°C in air



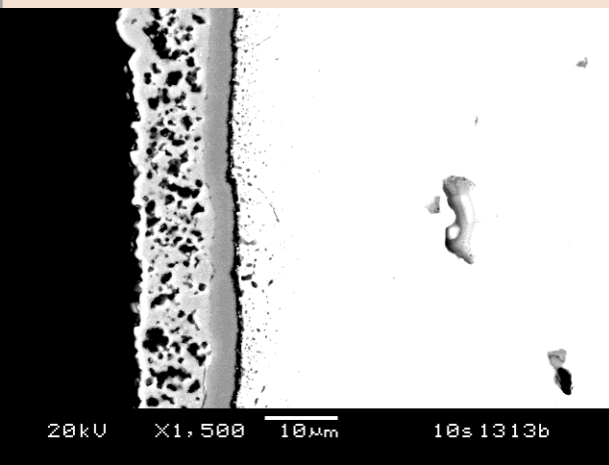
Surface Blast



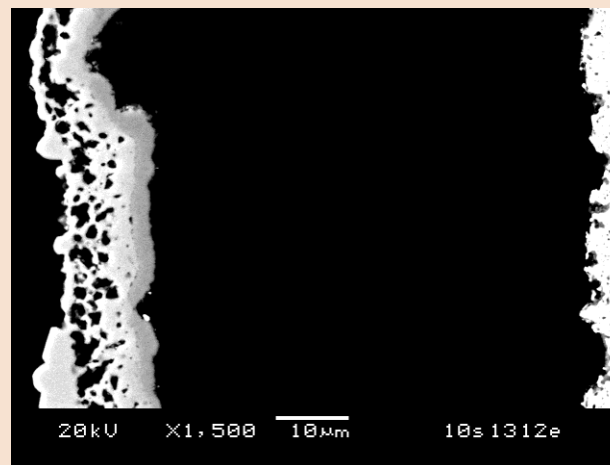
Surface Grind



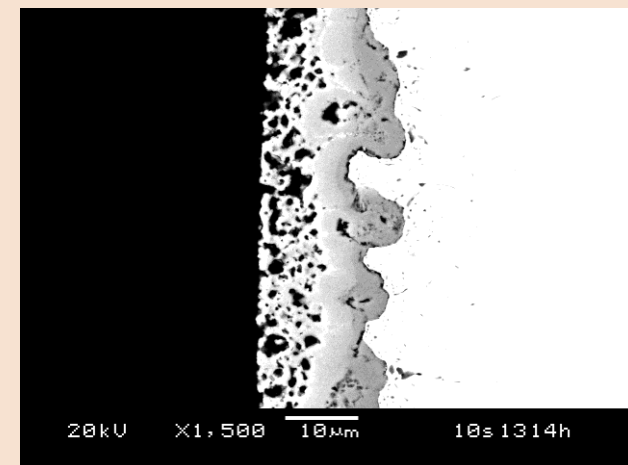
Desiliconized



Mill Reference (note: most of scale spalled after cooling)

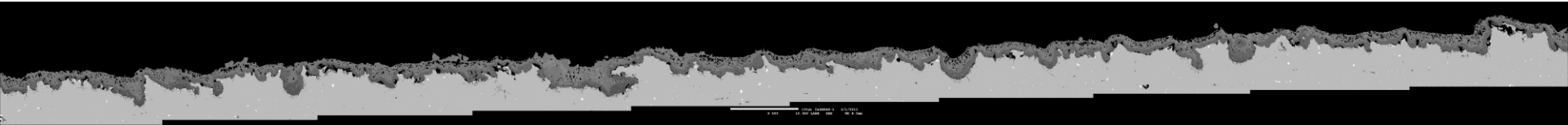


Cold Rolled (note: scale debonded during mounting)

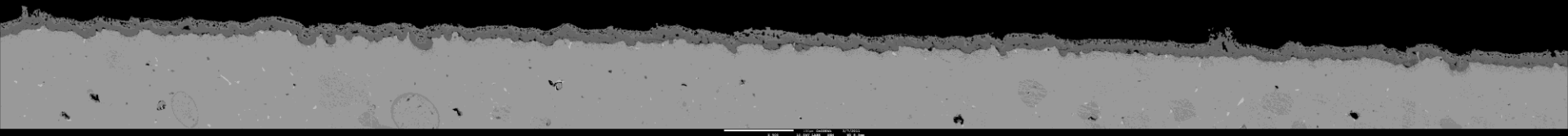


NETL-Albany Ce treatment

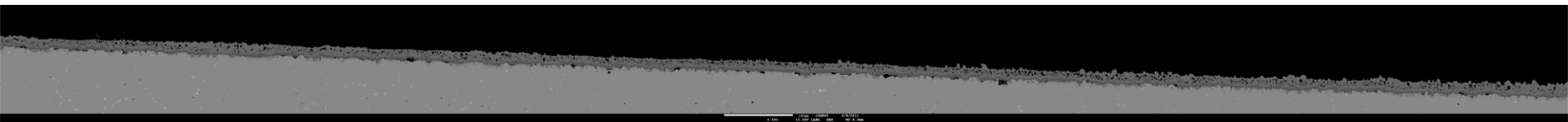
6000 h, 800°C in Air



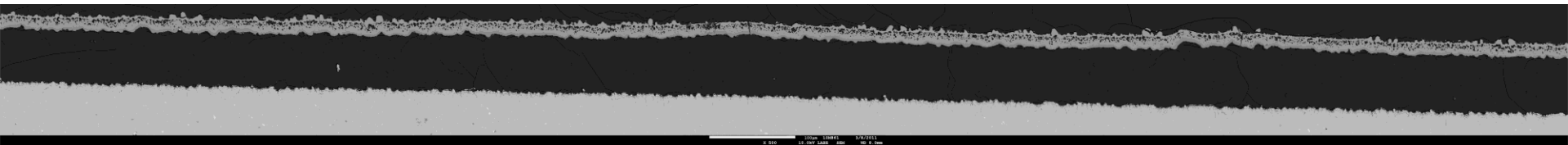
▶ Surface Blast



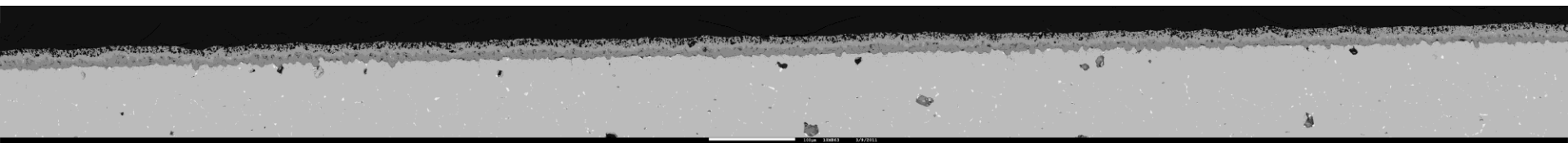
▶ Surface Ground



▶ De-siliconized

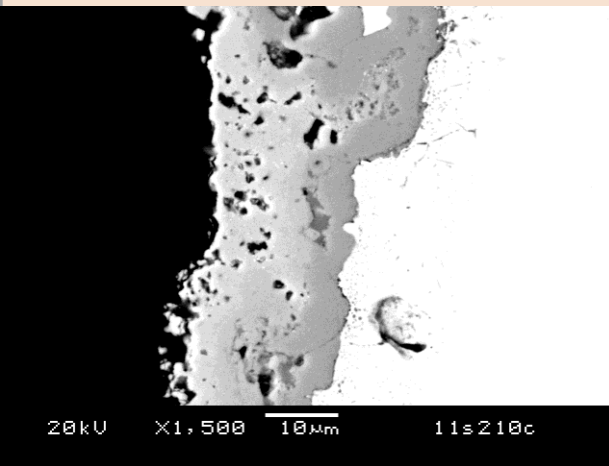


▶ 50% Cold Rolled

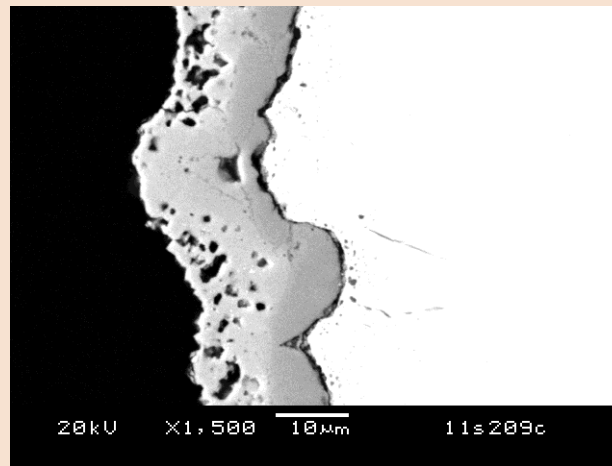


▶ NETL-Albany Ce treatment

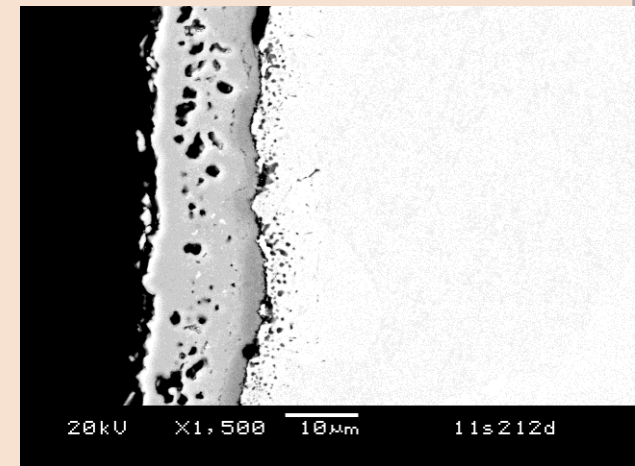
8000 h, 800°C in air



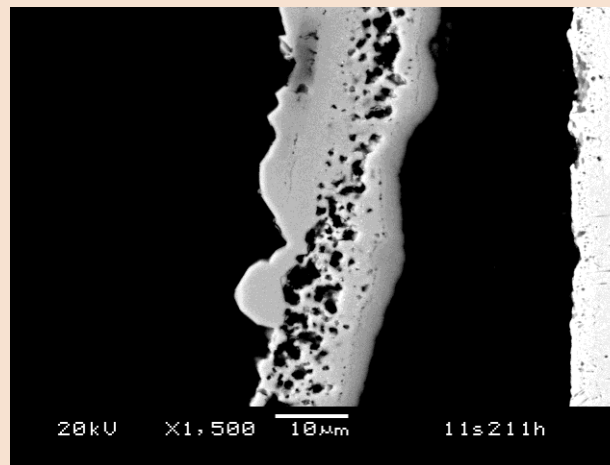
Surface Blast



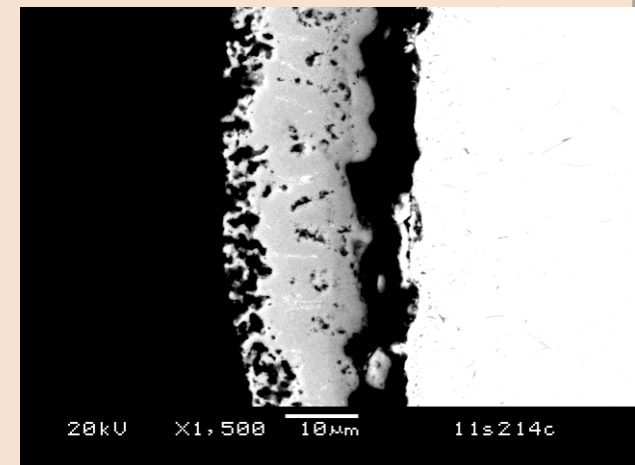
Surface Grind



Desiliconized

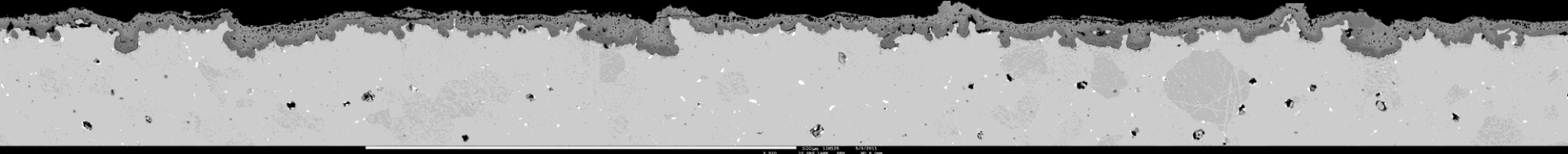


Cold Rolled (note: scale debonded during mounting)

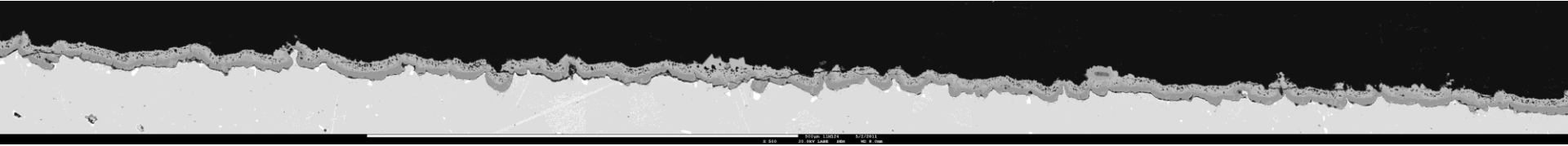


NETL-Albany Ce treatment

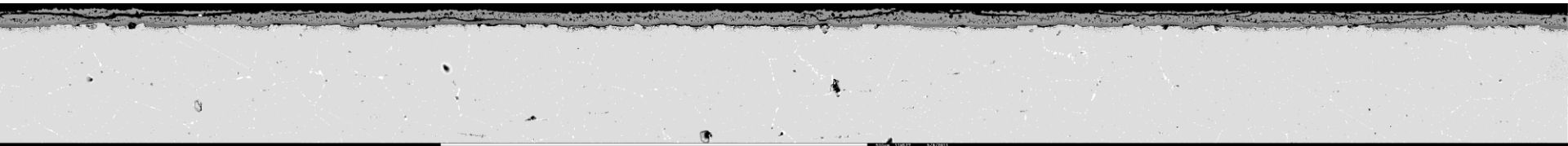
8000 h, 800°C in Air



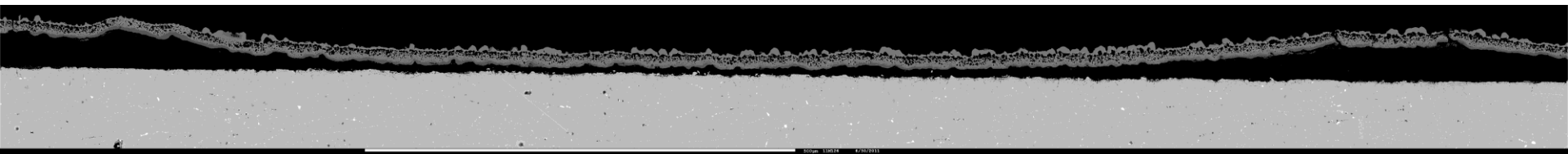
▶ Surface Blast



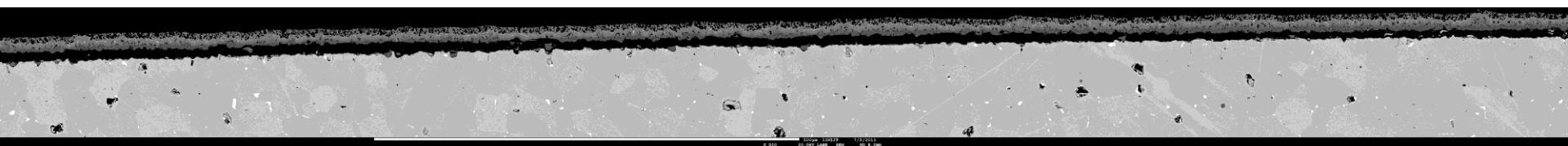
▶ Surface Ground



▶ De-siliconized

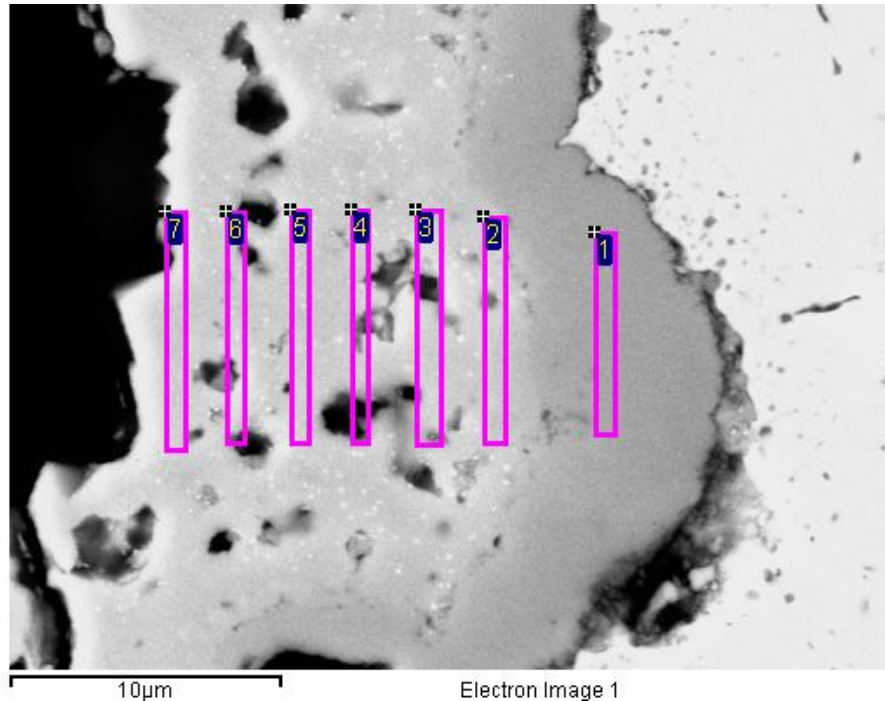


▶ 50% Cold Rolled



▶ NETL-Albany Ce treatment

Surface Blasted AISI 441 w/ Ce-modified MnCo Spinel coating: 8,000 hours, 800°C, air

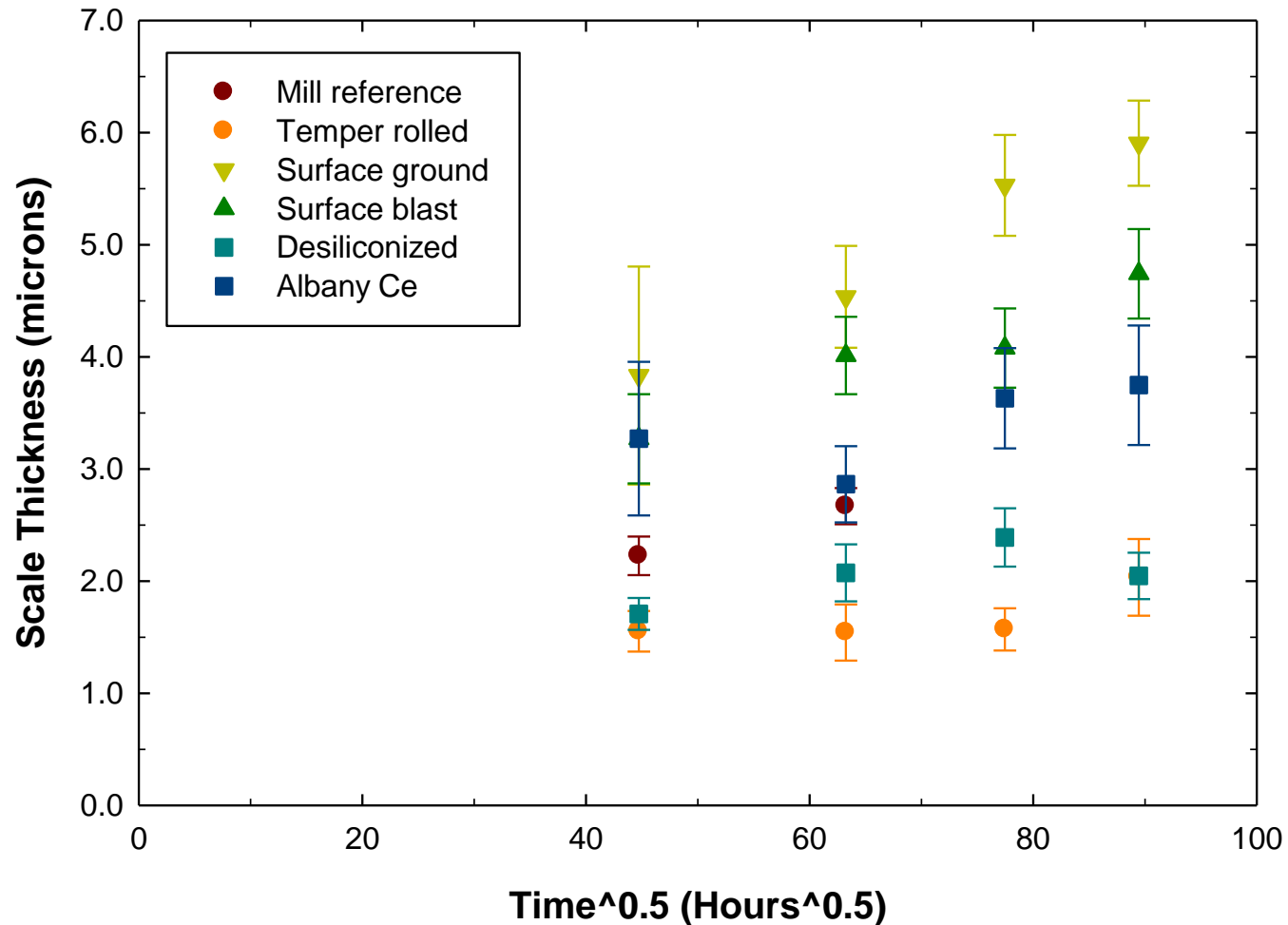


Spectrum	O	Ti	Cr	Mn	Fe	Co	Ce
1	65.53	0.97	33.21		0.28		
2	62.01	0.57	11.04	11.68	2.01	12.69	
3	60.52	0.89	1.69	18.83	2.97	15.11	
4	58.62	0.75	1.38	19.96	3.18	15.78	0.34
5	61.77	0.69	1.18	18.32	3.06	14.66	0.32
6	60.39	0.65	1.27	19.31	3.07	15.04	0.26
7	62.33	0.60	1.60	17.80	2.98	14.69	
Max.	65.53	0.97	33.21	19.96	3.18	15.78	0.34
Min.	58.62	0.57	1.18	11.68	0.28	12.69	0.26

Atomic%

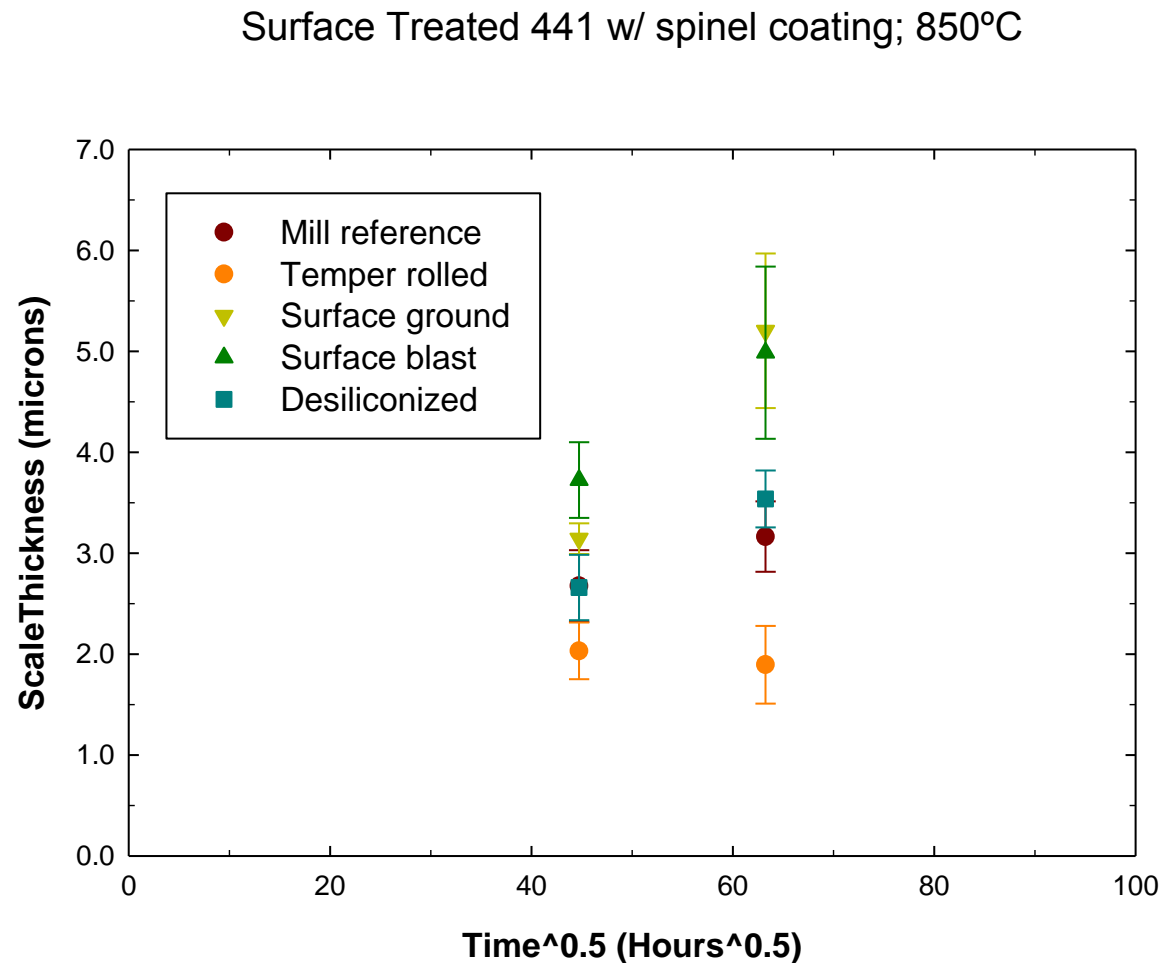
Surface Treated 441 w/coating; 800°C

Surface treated 441 w/ coating; 800°C

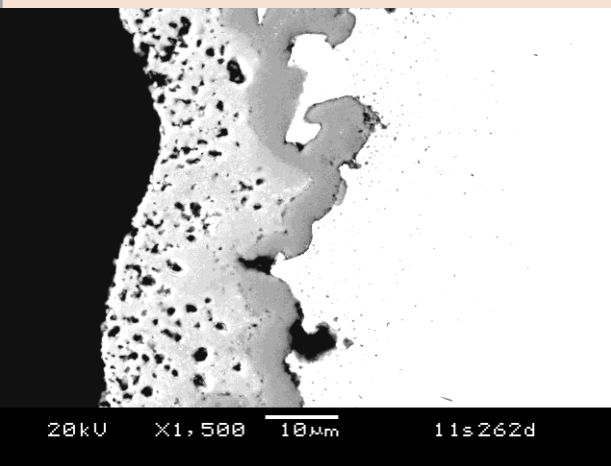


Effect of Surface Condition on Oxidation/Spallation Behavior of Spinel-coated 441 (850°C)

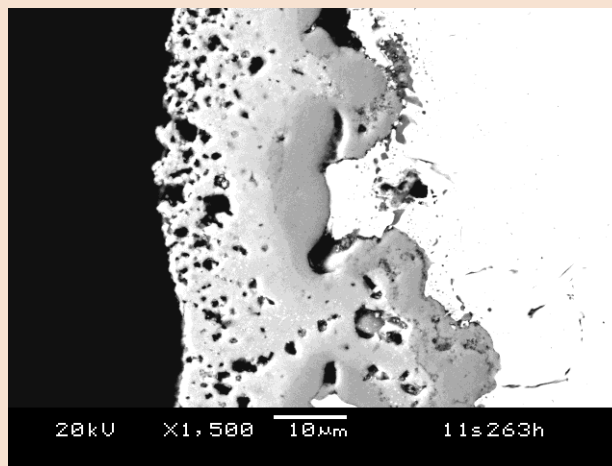
- ▶ 2000 hours
 - No spallation
- ▶ 4000 hours
 - No spallation
- ▶ Reached 6000 hours on July 20



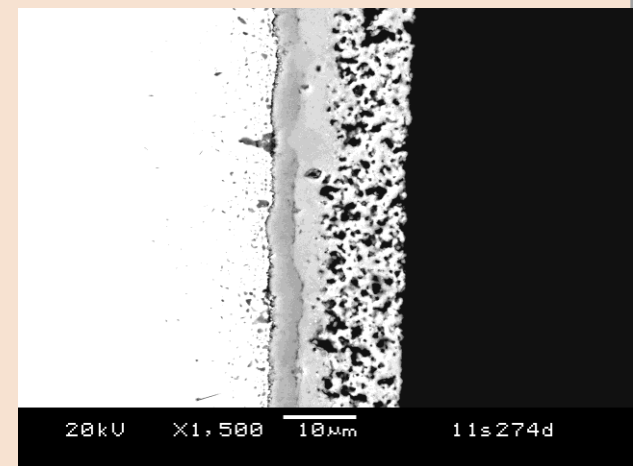
4000 h, 850°C in air



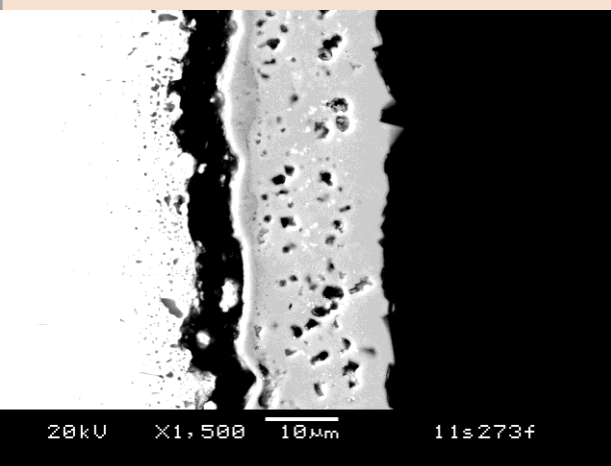
Surface Blast



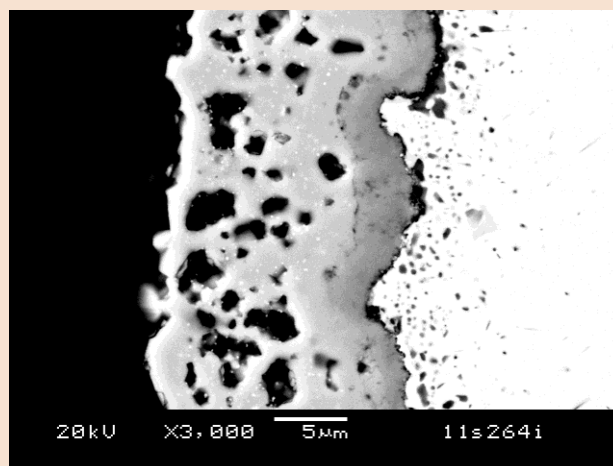
Surface Grind



Desiliconized

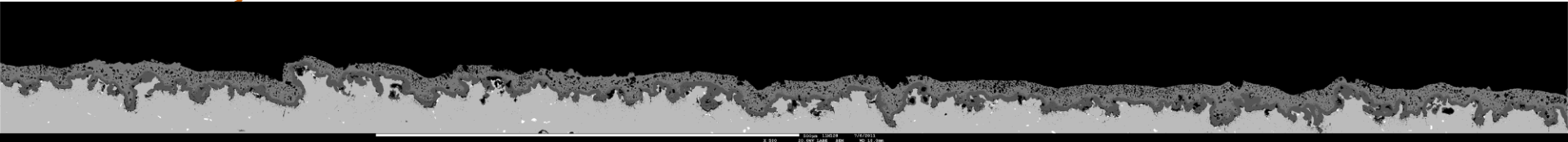


Mill Reference

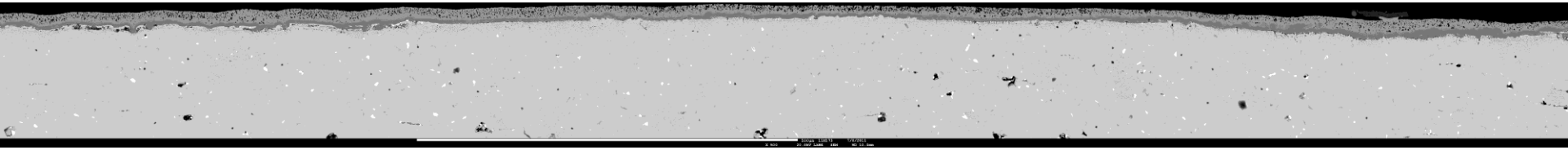


Cold Rolled – higher mag

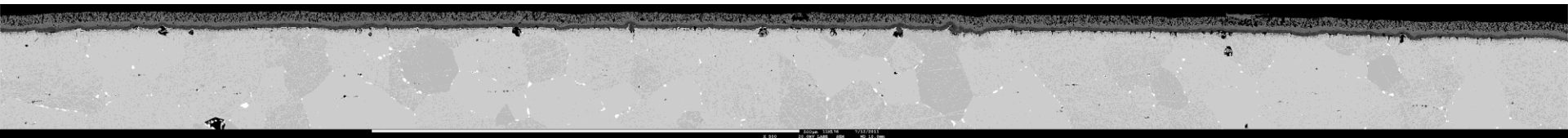
4000 h, 850°C in Air



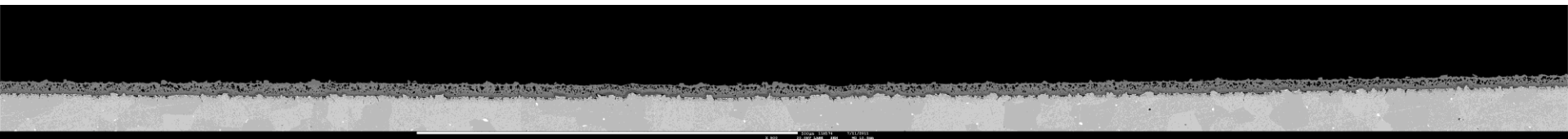
▶ Surface Blast



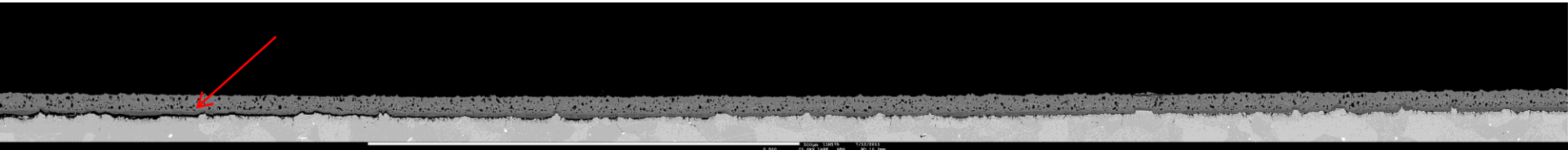
▶ Surface Ground



▶ De-siliconized

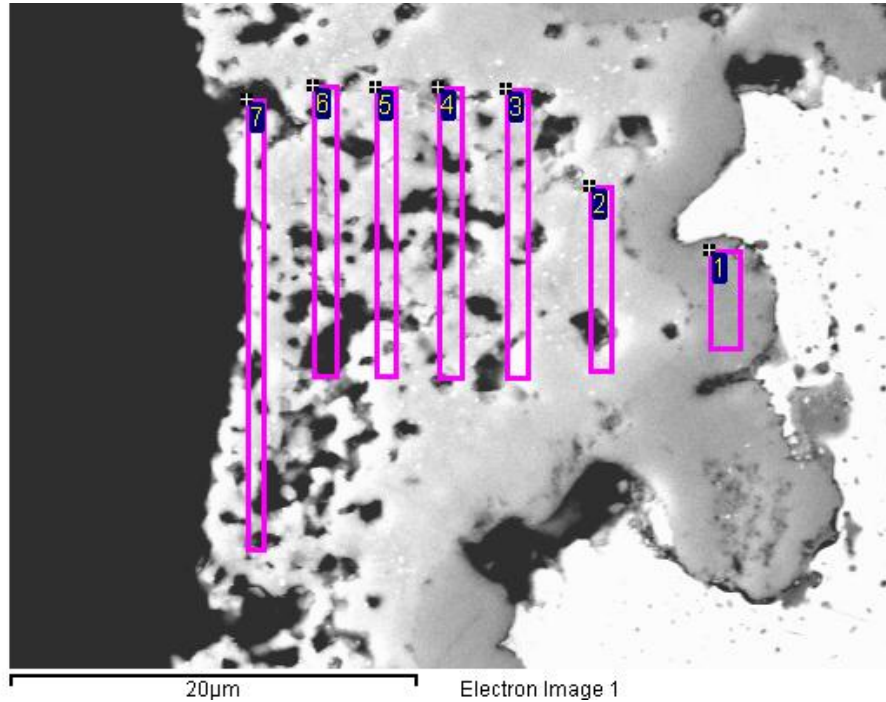


▶ 50% Cold Rolled



▶ Mill Reference

Surface Blasted AISI 441 w/ Ce-modified MnCo Spinel coating: 4,000 hours, 850°C, air



Spectrum	O	Si	Ti	Cr	Mn	Fe	Co	Ce
1	65.18	0.28	0.36	31.71	1.67	0.60	0.20	
2	60.64	0.22	0.21	4.33	17.44	1.62	15.54	
3	61.17	0.43	0.23	1.33	18.88	1.81	15.88	0.25
4	59.31	0.30	0.18	1.30	20.22	1.68	16.68	0.33
5	60.74			1.02	19.71	1.76	16.46	0.31
6	57.96			1.17	21.16	1.67	17.61	0.43
7	60.30	0.28		1.14	19.59	1.57	16.83	0.29
Max.	65.18	0.43	0.36	31.71	21.16	1.81	17.61	0.43
Min.	57.96	0.22	0.18	1.02	1.67	0.60	0.20	0.25

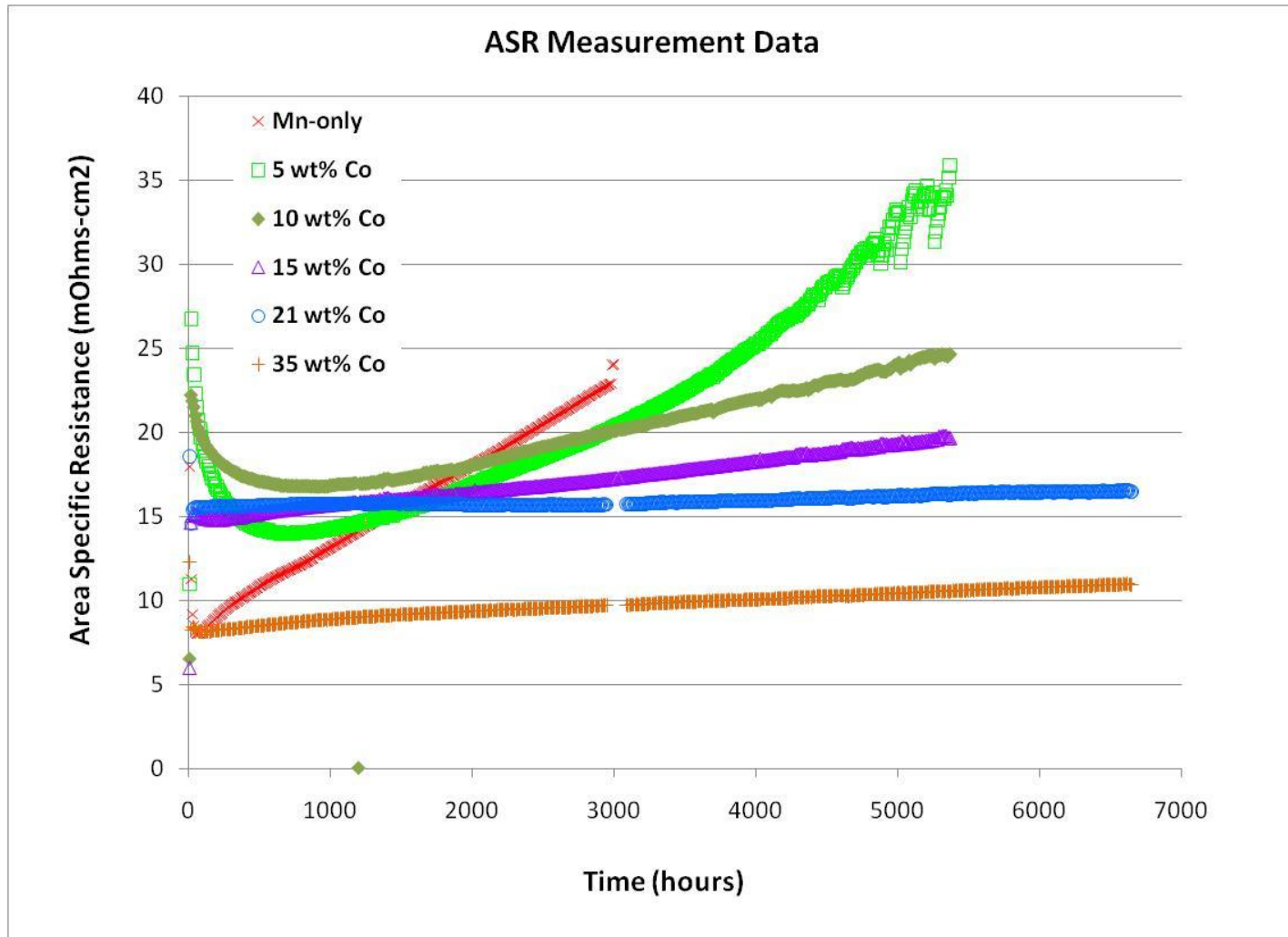
Atomic%

Optimization of Ce-MC Spinel Coatings

- ▶ Adaptation of ultrasonic spray process to Ce-modified spinel powder
 - Extension of previous optimization of fabrication process for unmodified spinel
 - Reference J.P. Choi et al., Poster Presentation, 2011 SECA Workshop

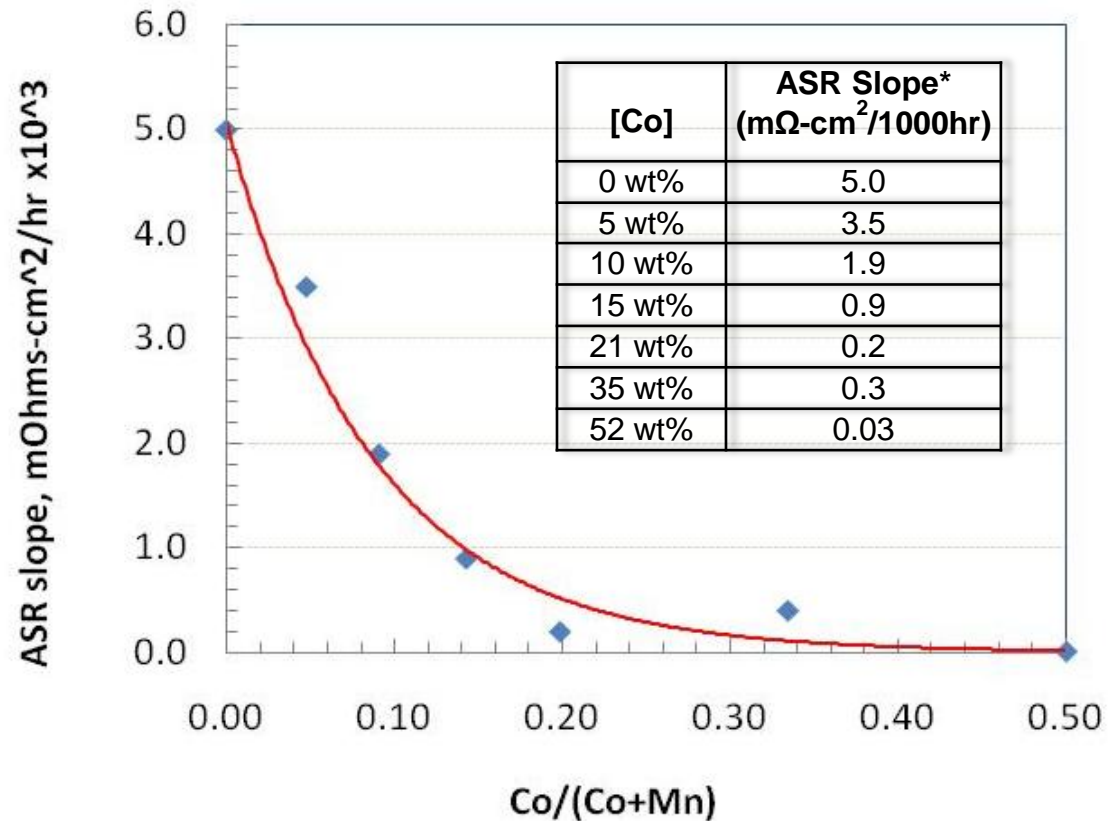
- ▶ Effect of coating thickness on oxidation resistance of AISI 441
 - Two studies in progress: Sprayed coatings, Screen-printed coatings
 - ~5, 10, 20 microns thick
 - Oxidation for 2000 hours

ASR Results for Reduced Co Content in Mn-Co Oxides on AISI441

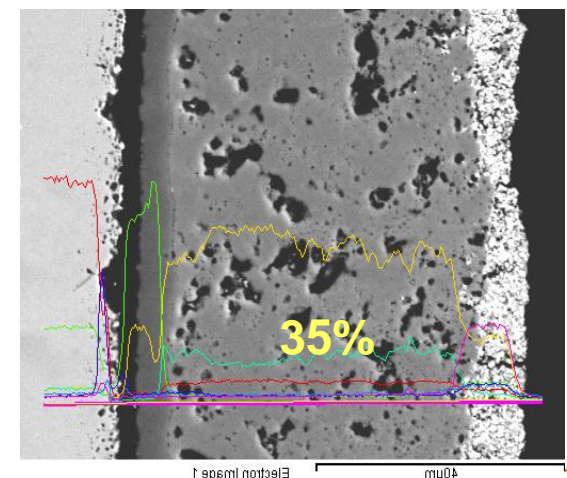
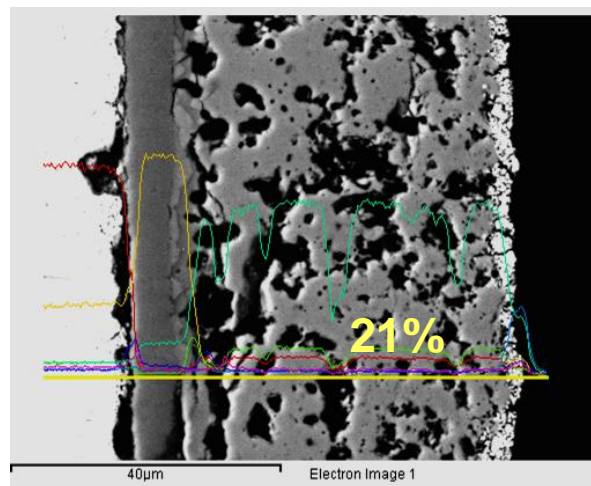
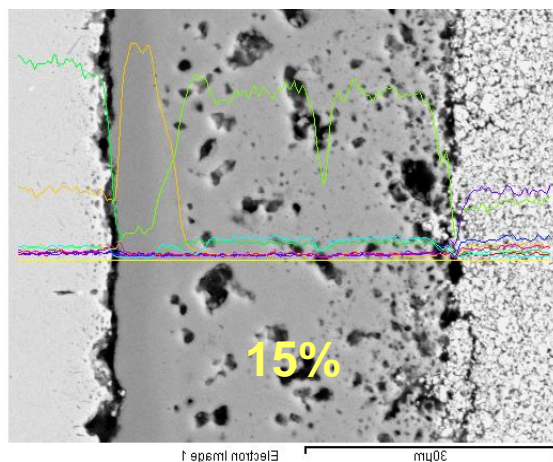
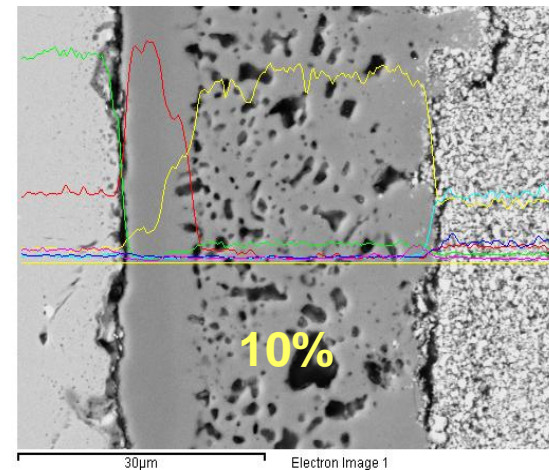
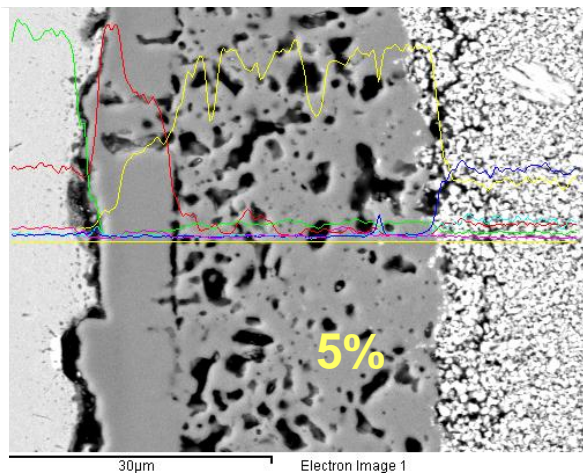
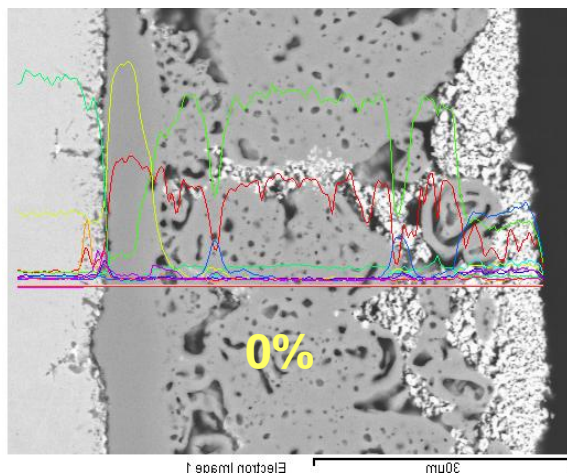


Alternative Coating Compositions

- ▶ Goal: Reduce Co content to reduce coating cost
 - Current preferred composition: $(\text{Mn}_{0.5}\text{Co}_{0.5})_3\text{O}_4$
- ▶ $(\text{Mn}_{1-x}\text{Co}_x)_3\text{O}_4$; $0.0 \leq x \leq 0.5$
 - $x = 0$ (Mn oxide)
 - Even after optimization of coating density, did not obtain stable ASR
 - $0.05 \leq x \leq 0.5$
 - Strong dependence of ASR rate of increase on Co content



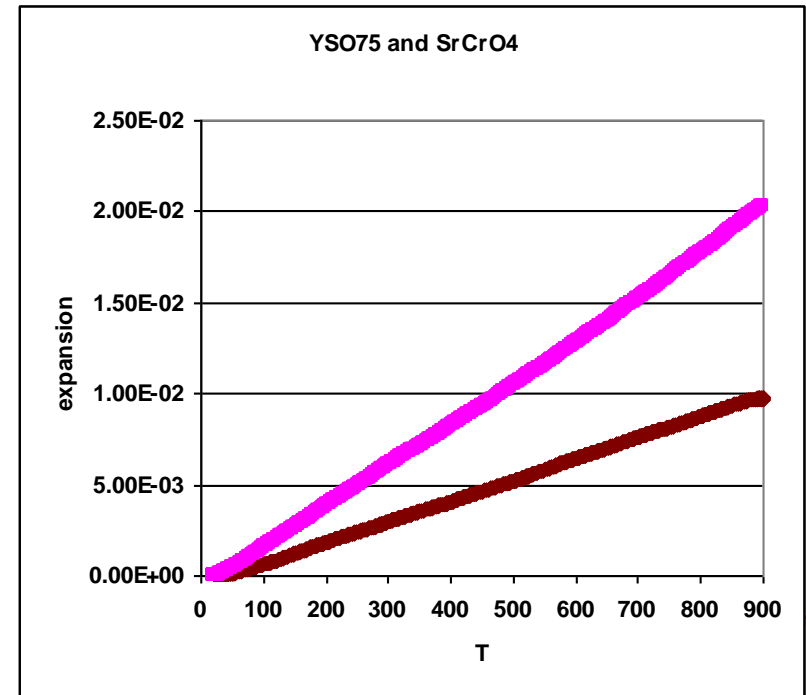
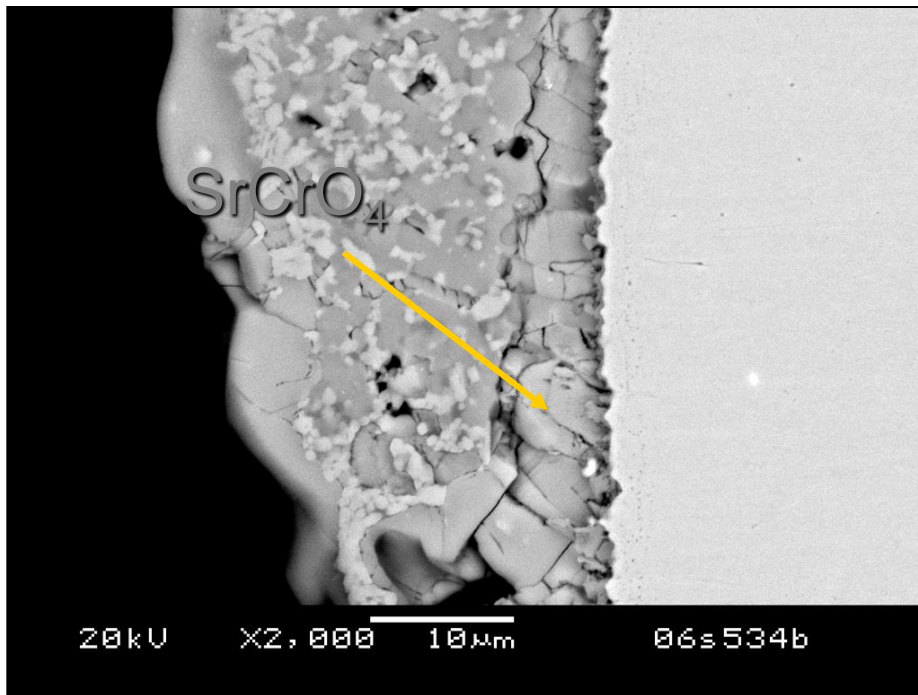
SEM Images of $\text{Mn}_{3-x}\text{Co}_x\text{O}_4$ Protection Coatings on AISI441 after ASR Tests



Pacific Northwest
NATIONAL LABORATORY

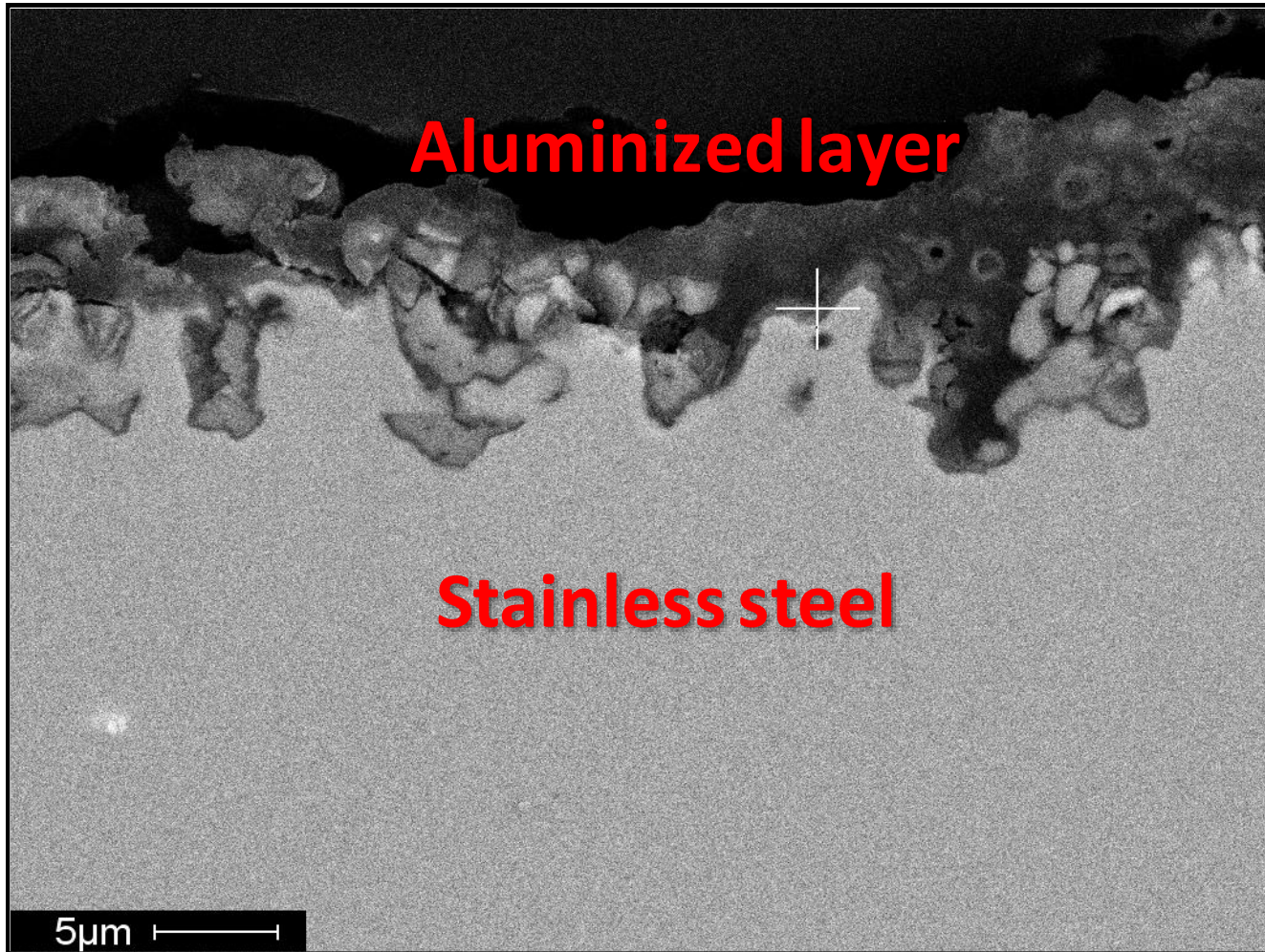
Reactive Air Aluminization

- Reaction between alkaline earths in glass seals and Cr in interconnect steel can form high CTE chromate phases (e.g., SrCrO_4), which degrade interfacial strength
- Cr volatility from alloys can poison cathodes
- Reactive Air Aluminization (RAA) offers a simple alternative to controlled atmosphere aluminization of interconnects
 - Aluminum powder slurry-based process, 1000°C heat treatment in air



Reactive Air Aluminization

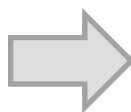
Cross sectional SEM analysis: 1000 C, 1 h oxidative heat treatment



Ceramic Interconnects for SOFC

- ▶ Doped yttrium chromite is being optimized for SOFC with operating temperature $>850^{\circ}\text{C}$
 - Ca on A-site; Co, Ni, and/or Cu on B-site
 - Electrical conductivity, CTE, ionic transference number comparable to standard material (doped lanthanum chromite)
 - Improved sinterability, reduced chemical expansion, and lower reactivity (e.g., zirconate formation) relative to lanthanum chromite

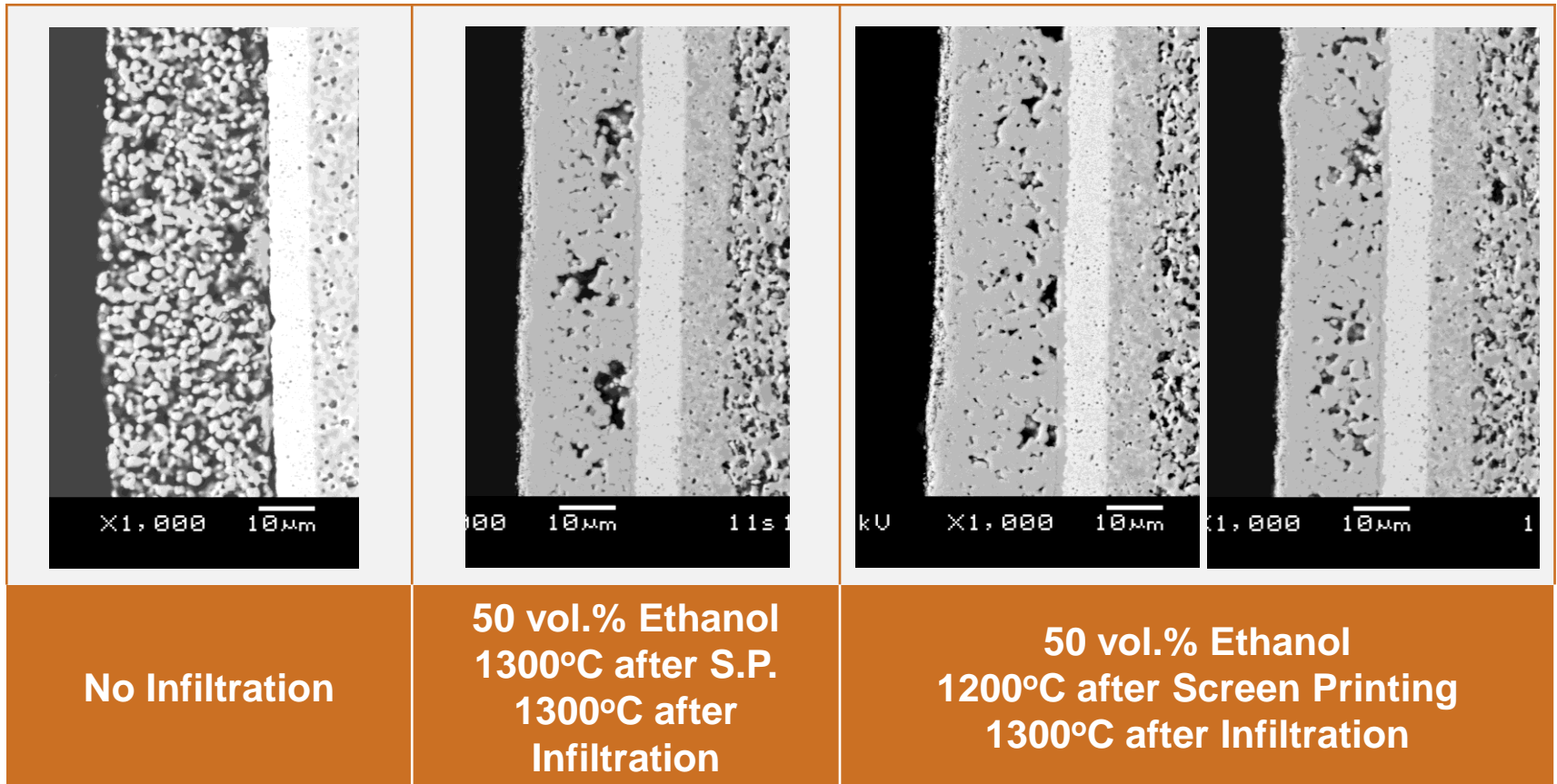
- **Electrical Conductivity**
 - Electronic, Ionic
- **Sintering Behavior**
- **Stability toward Reduction**
 - Chemical Expansion
- **Thermal Expansion**
- **Chemical Reactivity**



- **A-Site: 20% Ca**
- **B-site: 10% Co, 4% Ni, 1% Cu**

- Current emphasis on improving densification under constrained sintering and co-sintering conditions

Increased density through infiltration process



- Reference: K.J. Yoon et al., Poster Presentation, 2011 SECA Workshop

Summary

- ▶ AISI 441 w/ Ce-modified MnCo spinel coatings exhibits low, stable ASR in long-term testing
 - Less than $12 \text{ m}\Omega\text{-cm}^2$ after ~ 2 years at 800°C in air
- ▶ Surface-modified AISI 441 w/ Ce-modified MnCo spinel coatings exhibit improved long-term spallation resistance
 - 10,000 hours at 800°C (tests in progress)
 - 4,000 hours at 850°C (tests in progress)
- ▶ Based on ASR tests, effectiveness of Mn-Co spinel coatings decreases with decreasing Co content, especially for $\text{Co}/(\text{Co}+\text{Mn}) < 0.20$
- ▶ Optimization of ultrasonic spray process for application of Ce-modified MnCo spinel coatings is in progress

Future Work

- ▶ Continue to evaluate long-term stability and electrical performance of surface modified Ce-MC spinel-coated 441 steel
 - Parametric investigation of surface treatment options
 - Evaluation at 800 and 850°C
 - Long-term evaluation in stack test fixture
- ▶ Optimize thickness, and automated ultrasonic spray fabrication process, for Ce-modified spinel coatings
- ▶ Reduce cost of protective coatings through minimization or elimination of Co content
- ▶ Develop fabrication approaches for sintering of Cr-based perovskite interconnects under constrained/co-sintered conditions.

Acknowledgements

- The work summarized in this paper was funded under the U.S. Department of Energy's Solid-State Energy Conversion Alliance (SECA) Core Technology Program
- NETL: Shailesh Vora, Briggs White, Rin Burke, Travis Shultz, and Joe Stoffa
- NETL-Albany: Paul Jablonski
- ATI Allegheny Ludlum: Matt Bender
- PNNL: Jim Coleman, Shelley Carlson, Nat Saenz, Dan Edwards, Clyde Chamberlin, and Alan Schemer-Kohn